



22nd International Symposium on Ballistics
November 14-18, 2005
Vancouver, BC, Canada



NDIA
NATIONAL DEFENSE INDUSTRIAL ASSOCIATION
STRONGER THROUGH INTEGRITY & PROFESSIONALISM

Theoretical Design for a Guided Supersonic Projectile

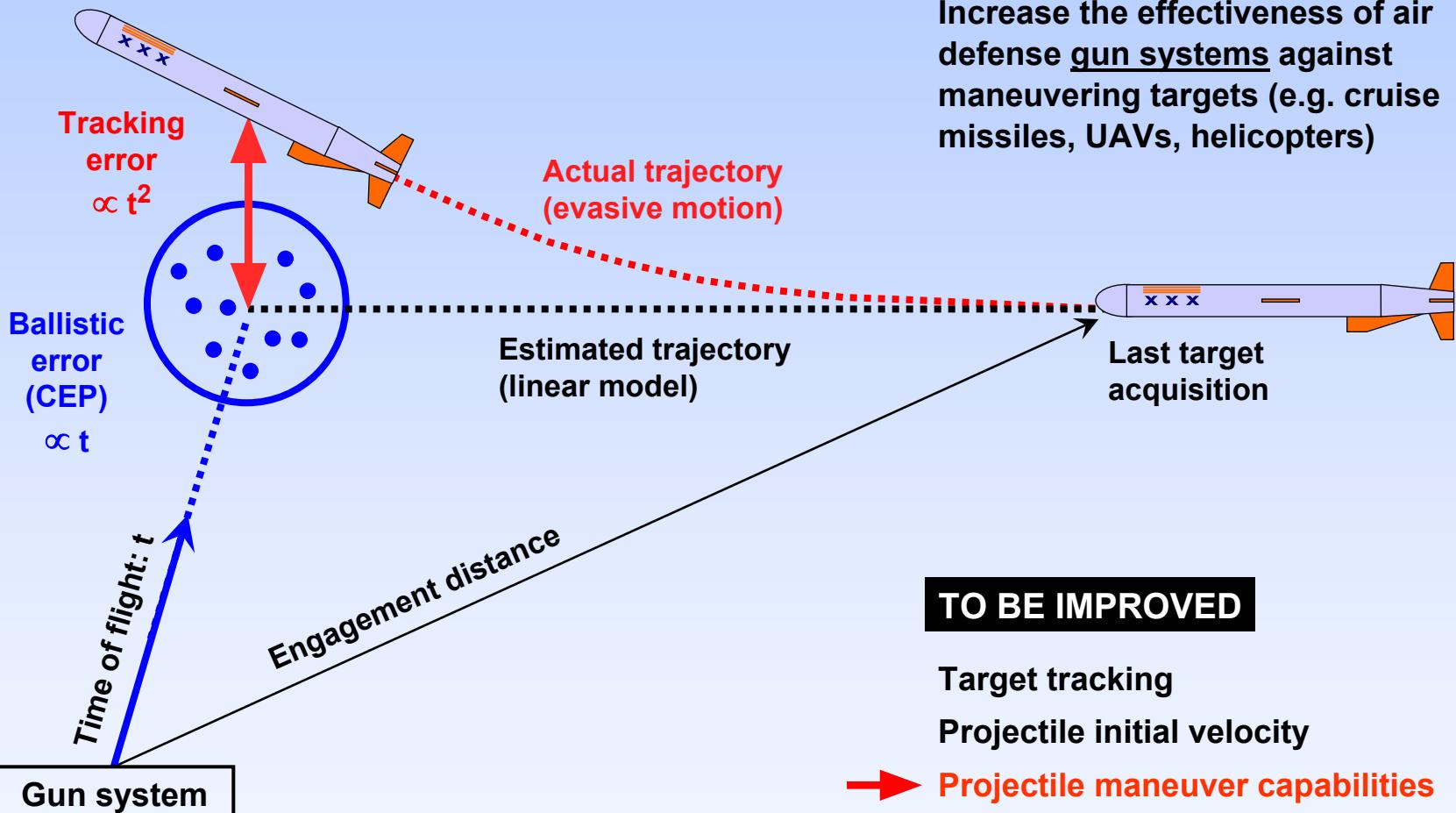
Pierre WEY, Claude BERNER, Eckhart SOMMER
Volker FLECK, Henry MOULARD

French-German Research Institute (ISL)
Saint-Louis, France

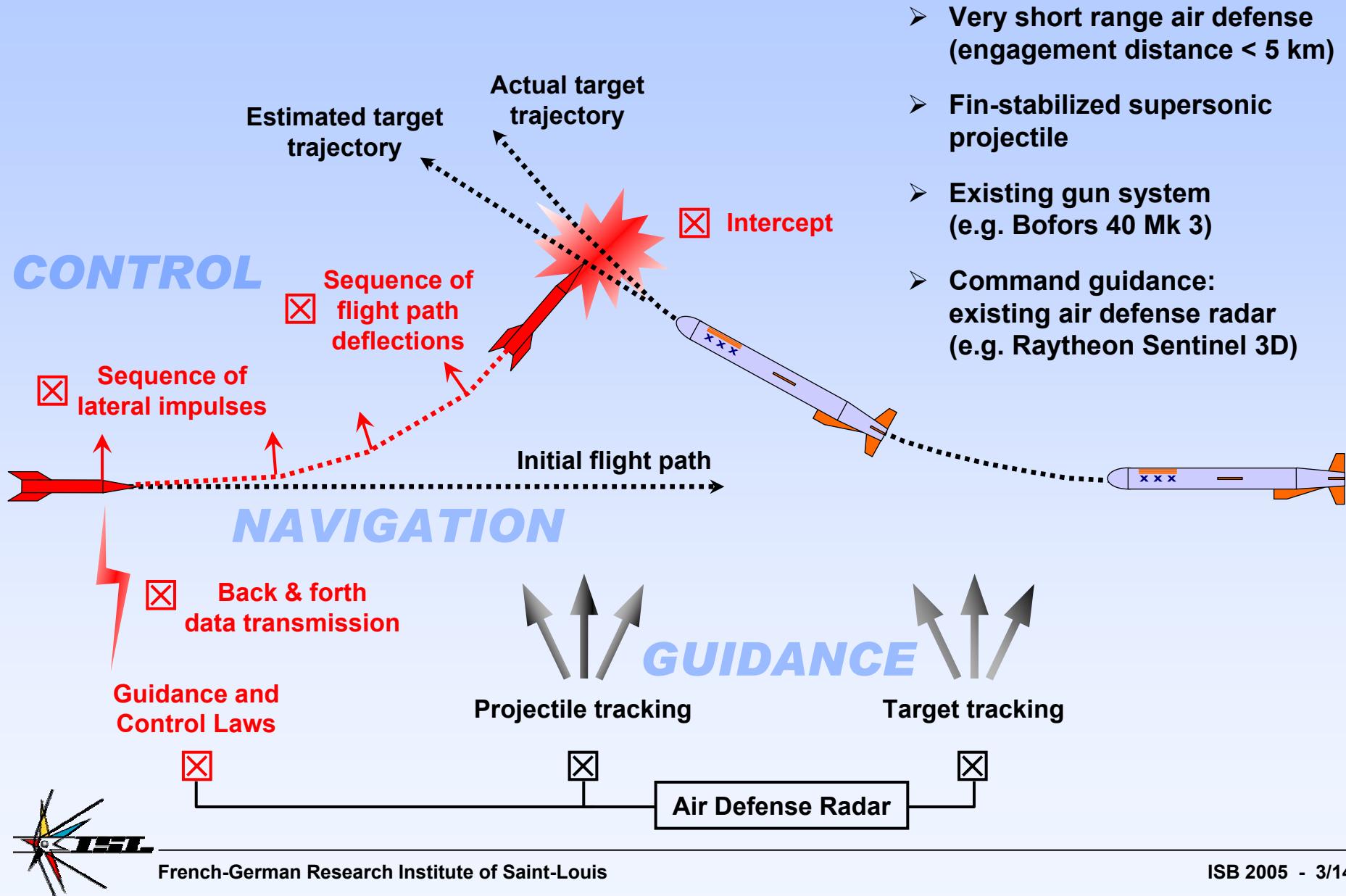


French-German Research Institute of Saint-Louis

Context: Air Defense vs. Maneuvering Targets



GSP: System Concept

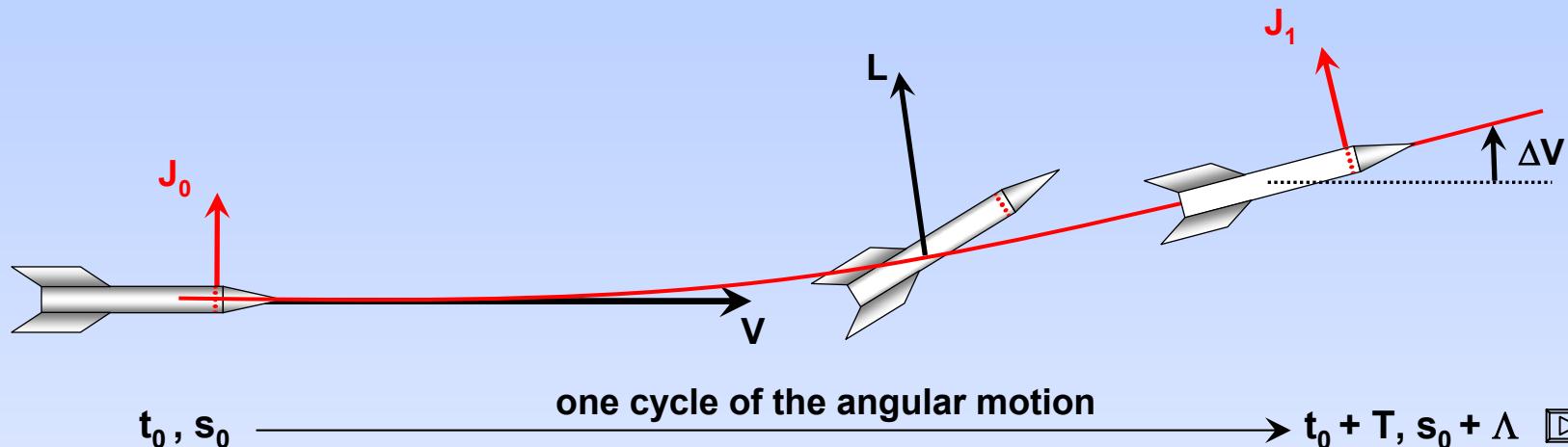


Control Sequence

1 Singular impulse J_0 yields deviation speed and triggers the yaw motion

2 Deviation speed due to the action of the lift force L

3 Singular impulse J_1 yields deviation speed and stops the yaw motion



HYPOTHESES

- Small deviation speed : $\Delta V \ll V$
- Lift force = prevalent force
- Overturning moment = prevalent moment
- Undamped angular motion
- Quasi-planar angular motion



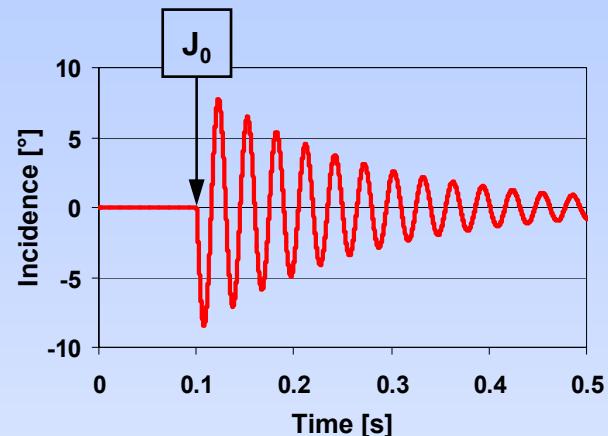
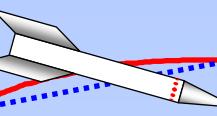
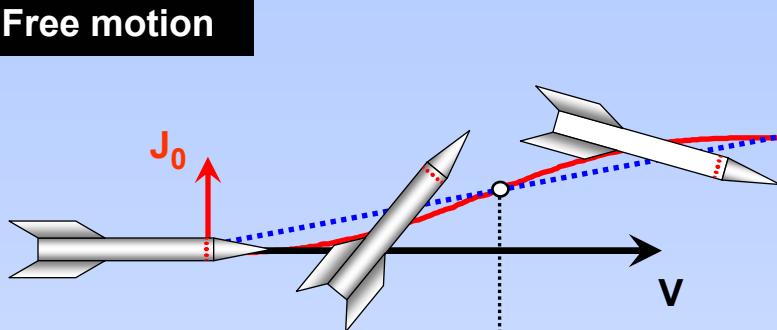
EQUATION OF THE DEVIATION SPEED

$$m\Delta V = 2J + \int_{t_0}^{t_0+T} L(t) dt = 2J + \int_{s_0}^{s_0+\Delta} L(s) \frac{d}{V} ds$$

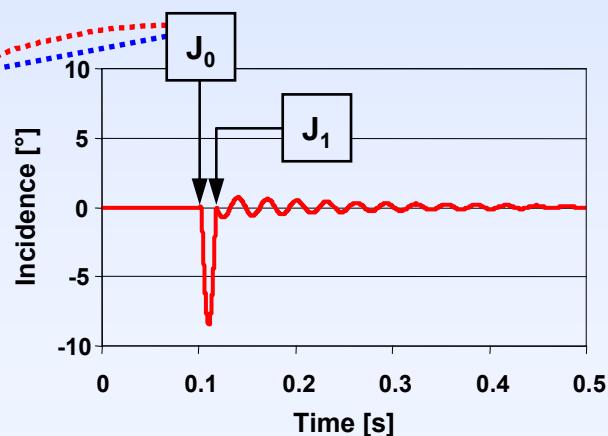
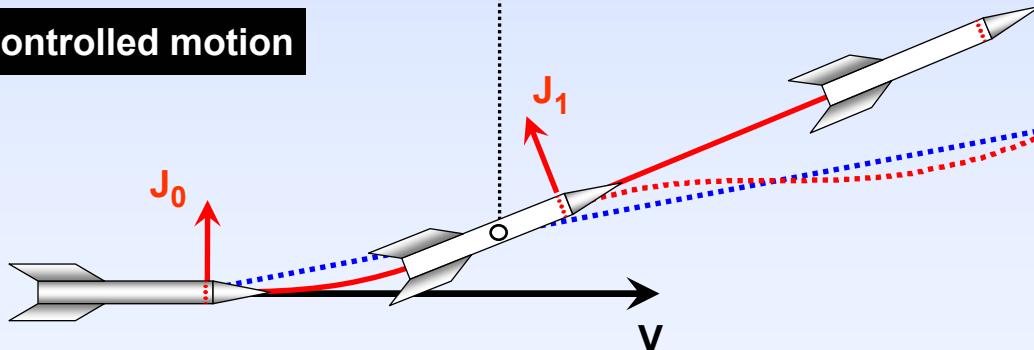


Control of the Yaw Motion

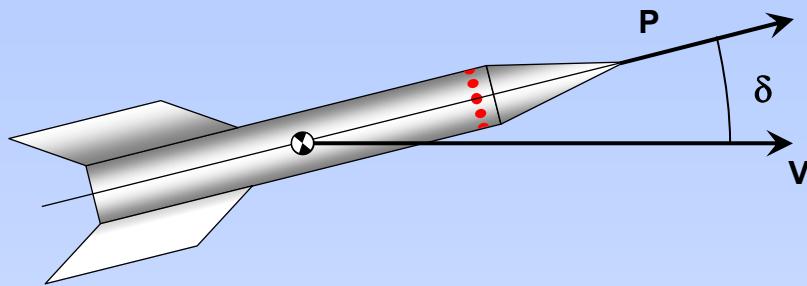
Free motion



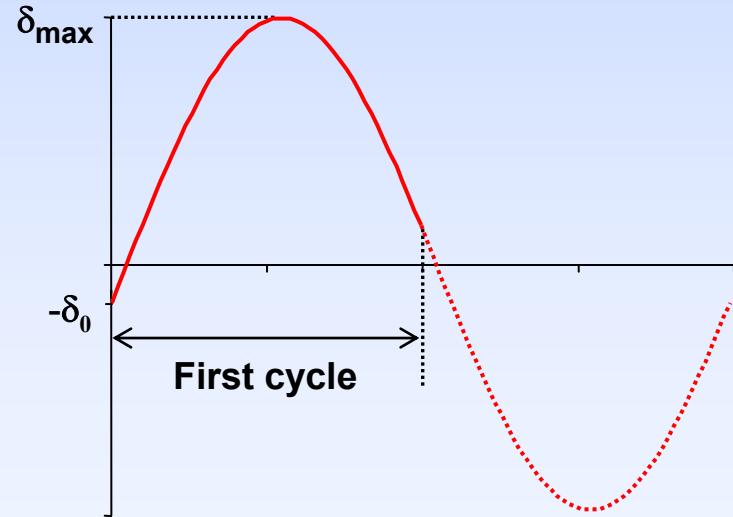
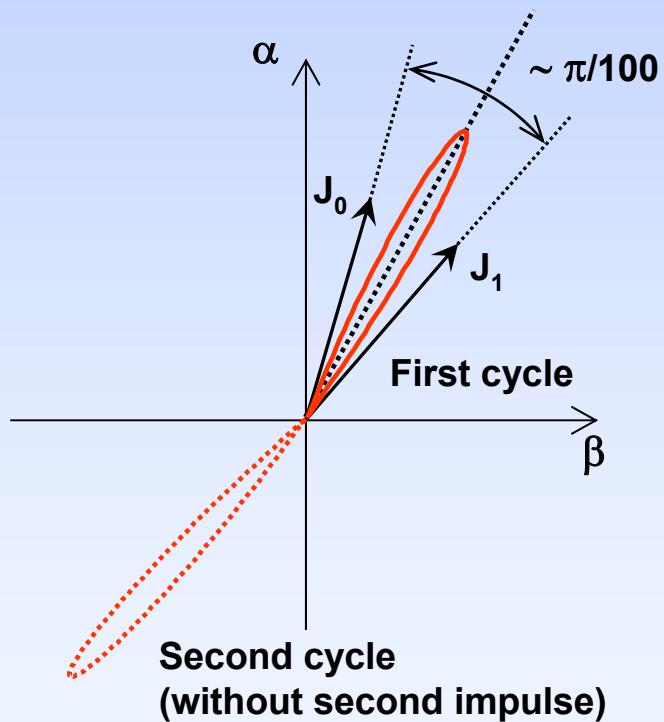
Controlled motion



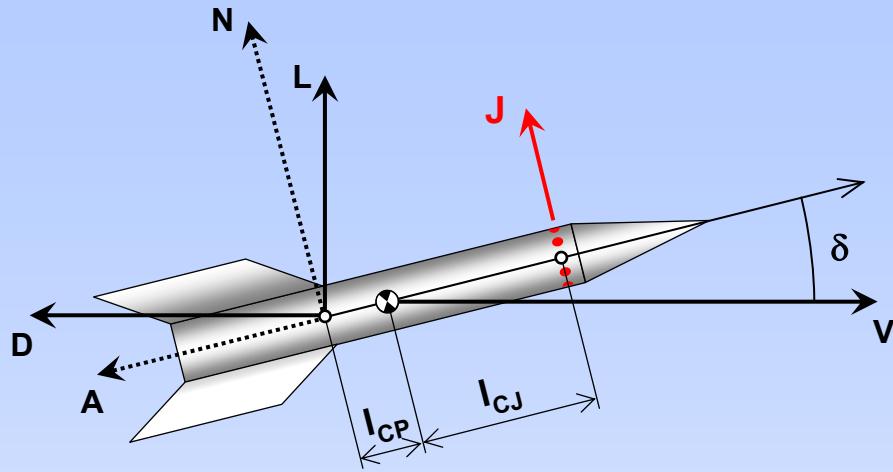
Linearized Yaw Motion



Roll rate: one half revolution during one cycle of the angular motion



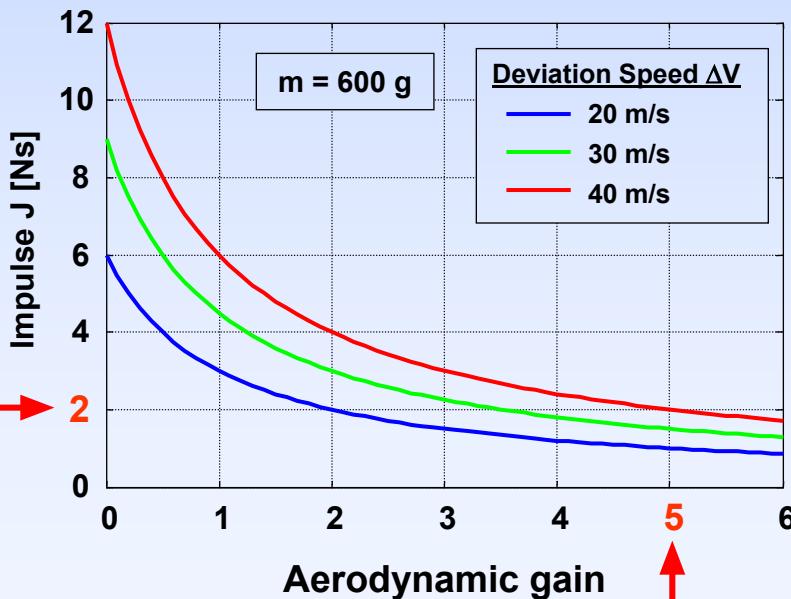
Control Law



$$\Delta V = 2 \frac{J}{m} \left(1 + I_{CJ} \frac{CL_\alpha}{|CM_\alpha|} \right)$$

$$= 2 \frac{J}{m} \left(1 + \frac{I_{CJ}}{I_{CP}} \left(1 - \frac{CX_0}{CN_\alpha} \right) \right)$$

$I_{CJ} \frac{CL_\alpha}{|CM_\alpha|}$ = Aerodynamic gain



Expected
impulse

OPTIMIZATION

- ➔ CX / CN_α ➔ I_{CJ}
- ➔ I_{CP} ➔ J
- ➔ m

CONSTRAINTS

- Stability
- Maximum yaw angle

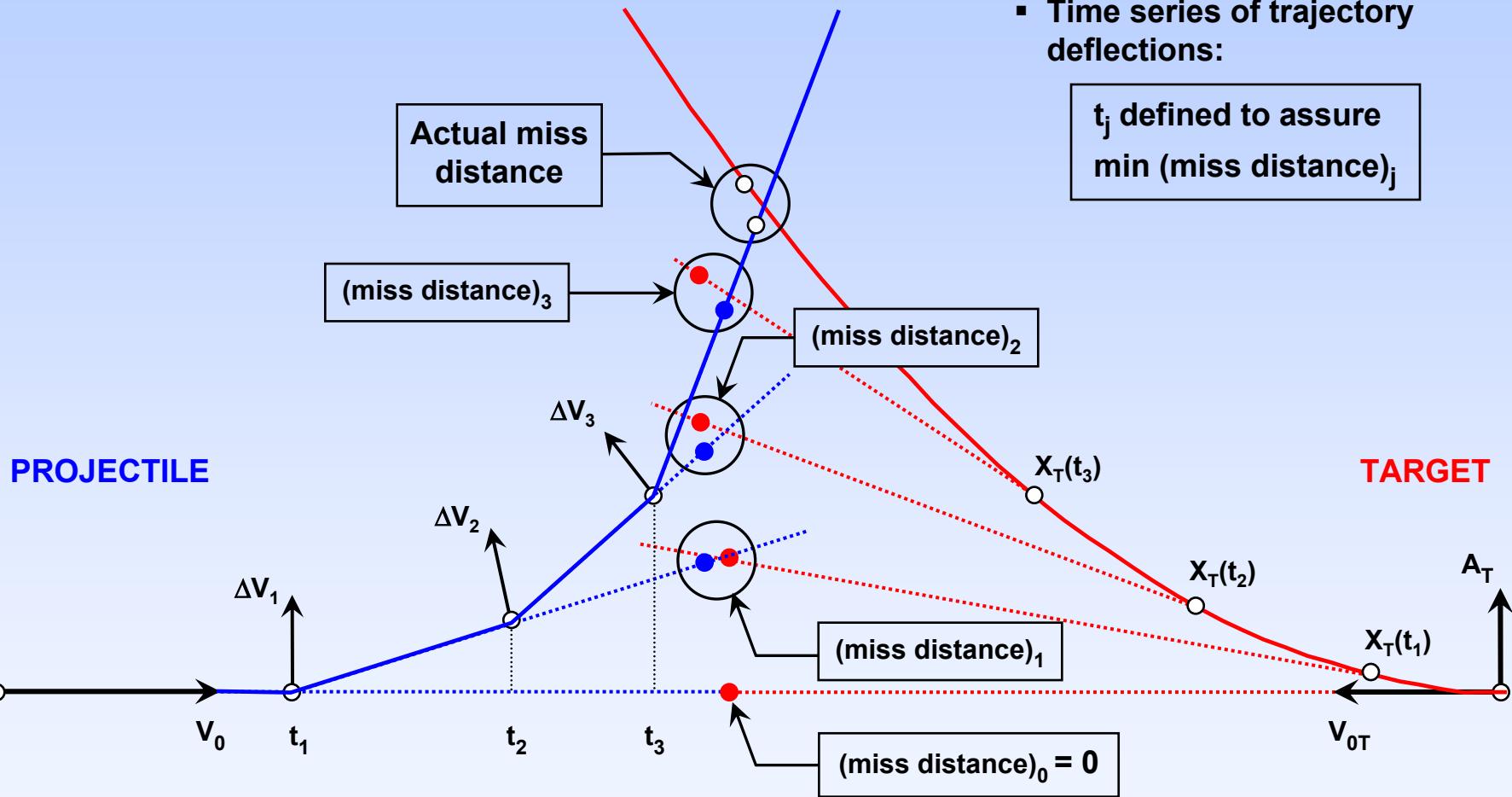


Guidance Scheme

- Estimated target positions updated using linear model

- Time series of trajectory deflections:

t_j defined to assure
 $\min (\text{miss distance})_j$



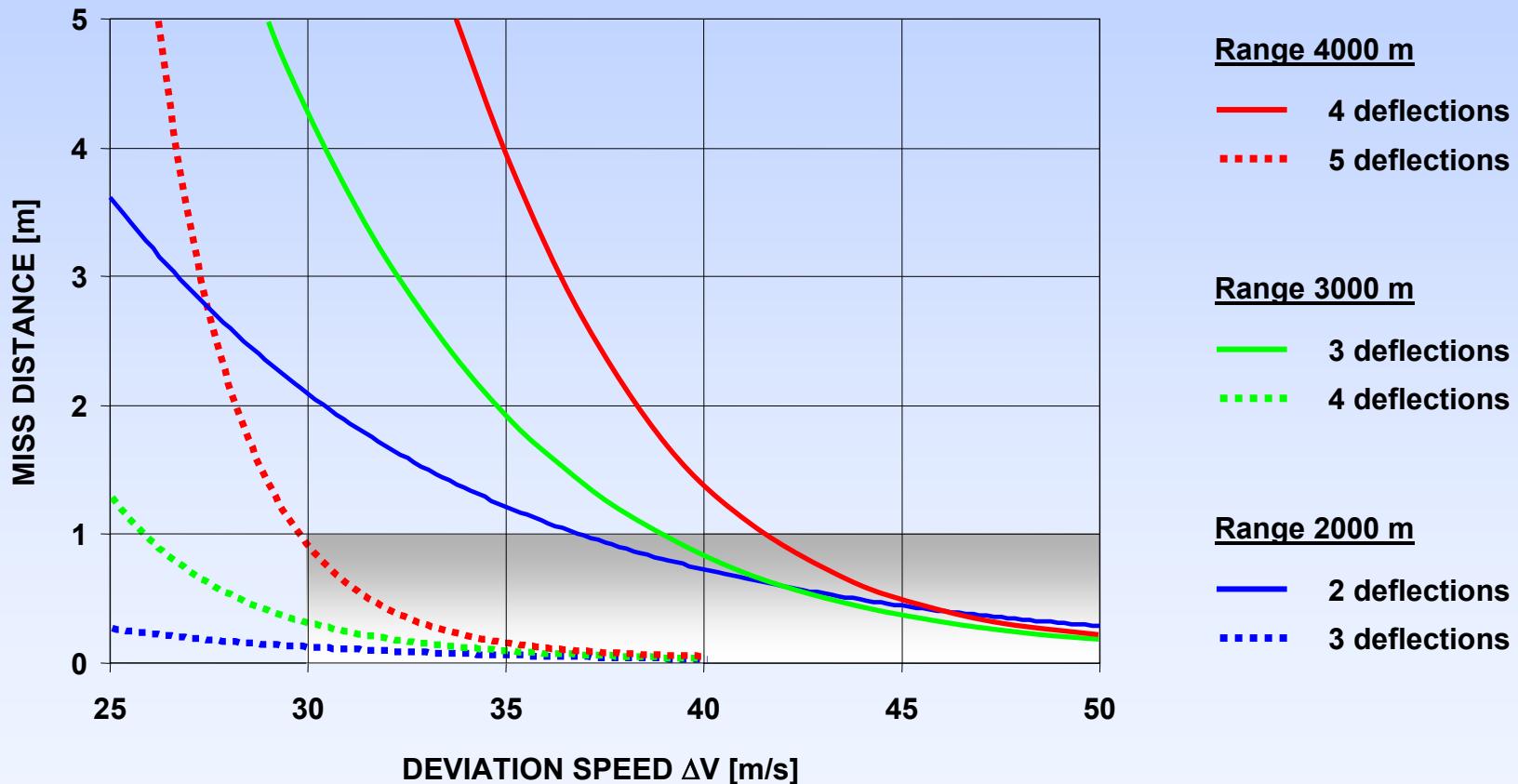
Guidance Performance

Projectile

$D = 30 \text{ mm}$ $V_0 = 1100 \text{ m/s}$
 $m = 600 \text{ g}$ $CX_0 = 0.25$

Target

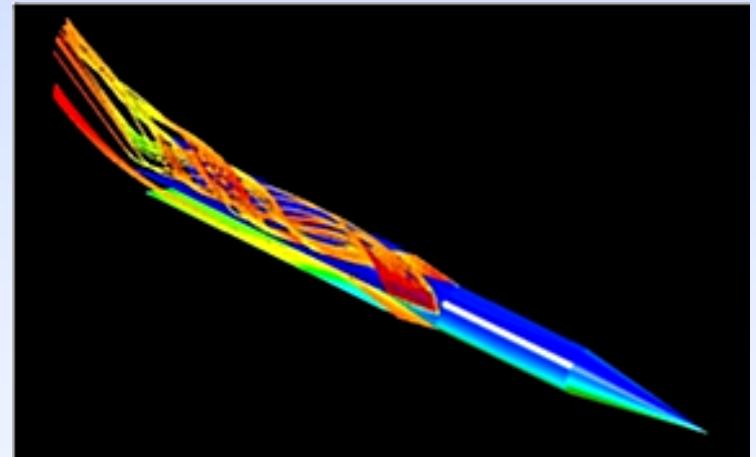
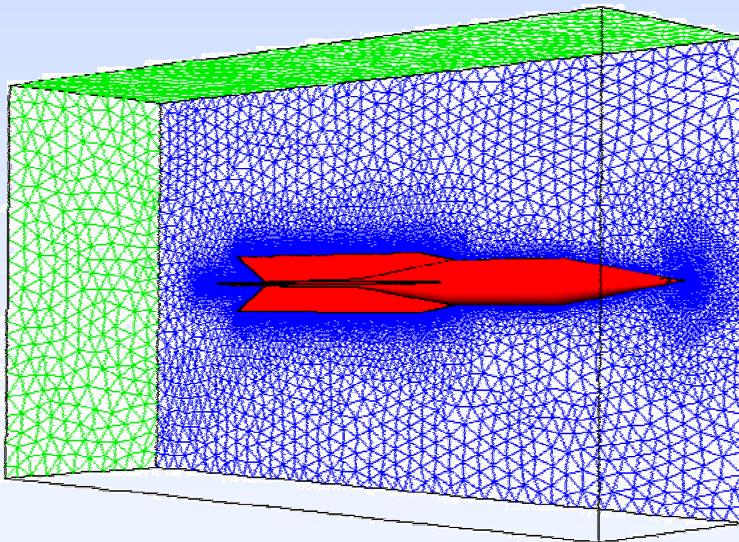
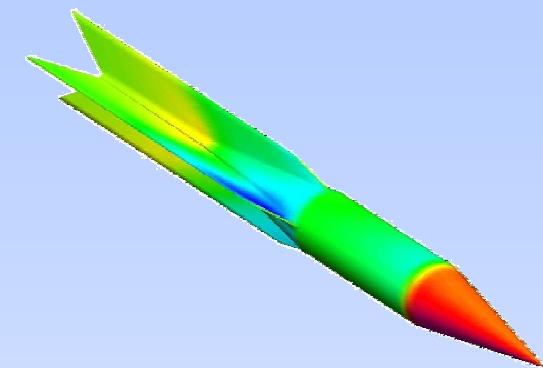
$V_0 = 300 \text{ m/s}$
 $A_T = 30 \text{ m/s}^2$



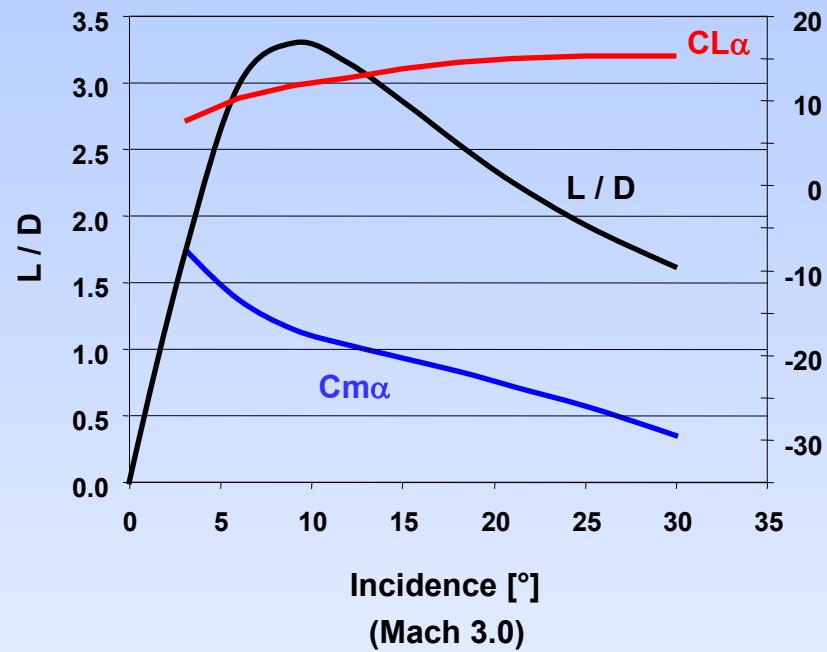
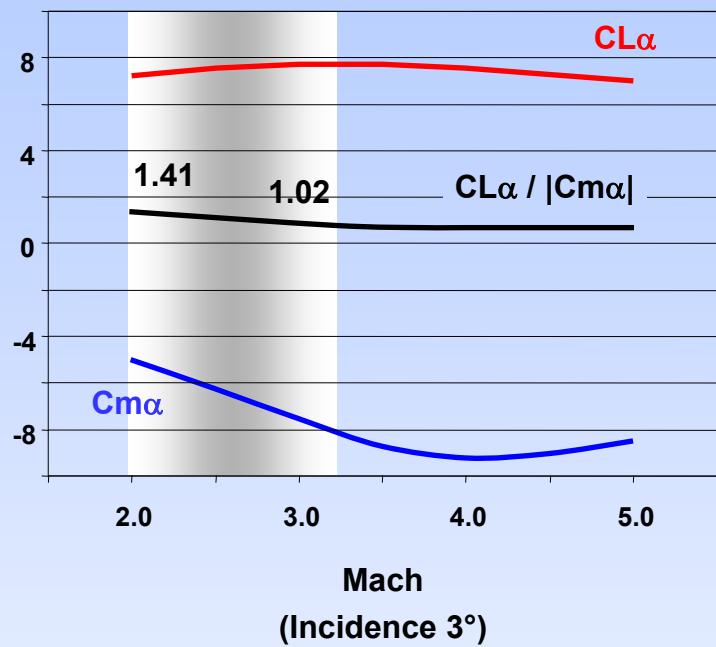
Aerodynamic Optimization (CFD)

GOALS

- Fin span limited to 40 mm
- Body caliber limited to 30 mm
- Minimize drag force D
- Maximize lift force L
- Assure projectile stability (static margin)



Aerodynamic Performance



Variation of ΔV
to be included in the
guidance law

Control law to be
validated by
6-DOF computation

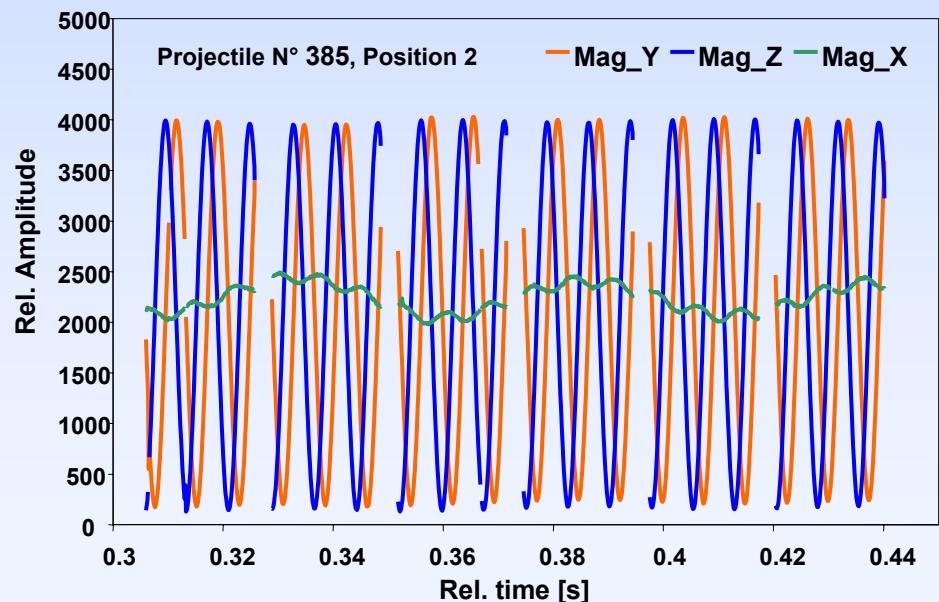


Navigation: On-board Sensors

3-D Magnetic Sensors + 6-DOF Model

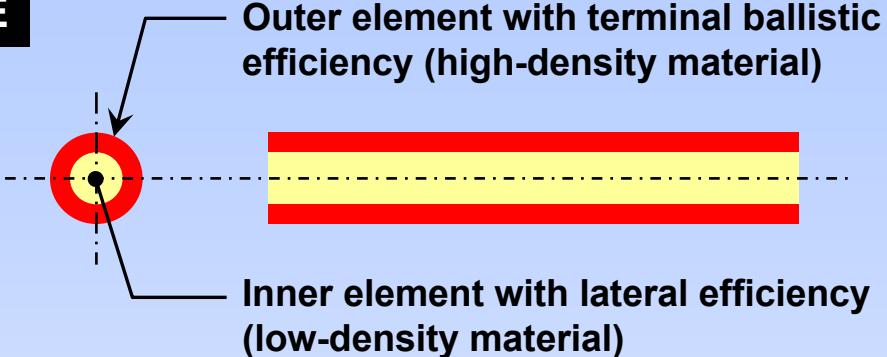
- Successful results from
 - 155mm artillery shell
 - 90mm tank ammunition
 - 30mm Air Force Finner
 - 30mm spinning finned projectile
- Latest experiment
 - 120mm Flying Rod
 - $V_0 = 1800 \text{ m/s}$
 - Acceleration: 55 000 g
 - 12-bit sampling at 8 KHz

Required data:
roll angle only



Terminal Ballistics: PELE / ALP Projectiles

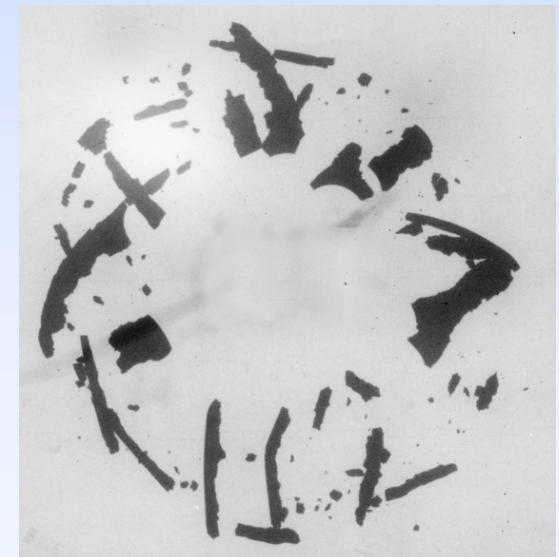
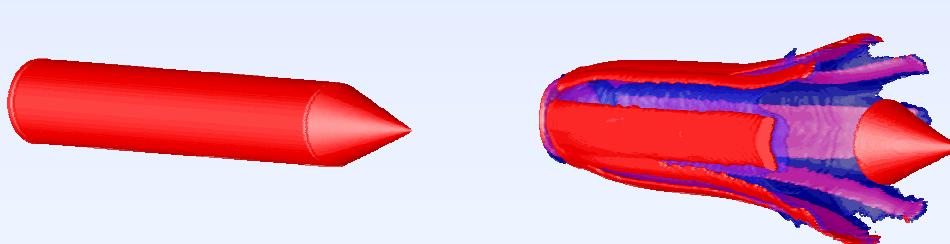
PELE



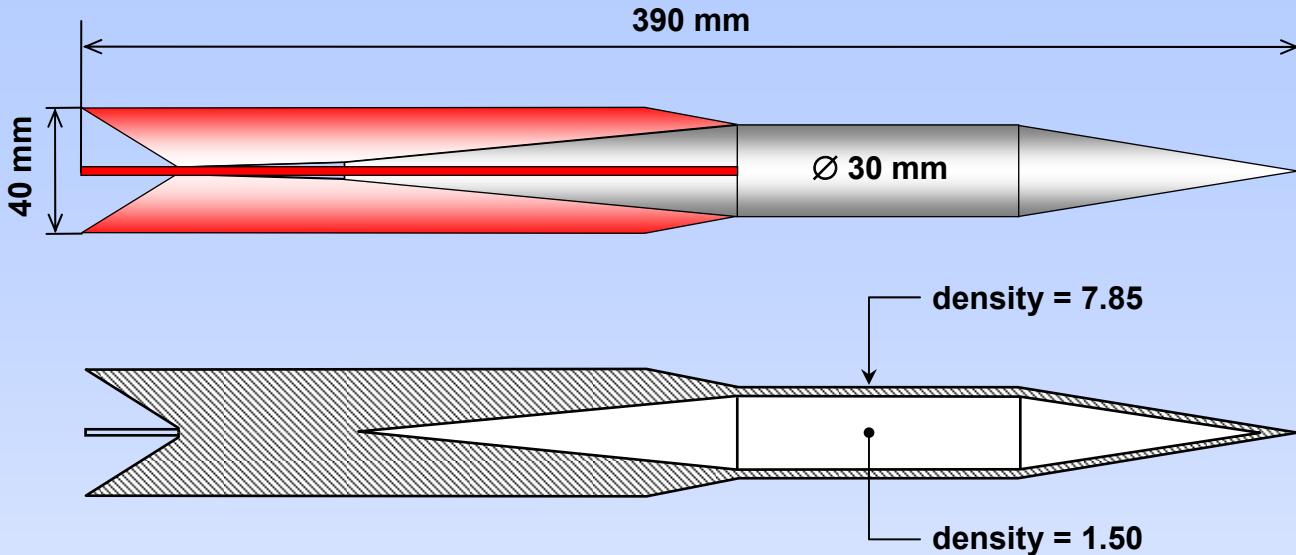
Reduction of the projectile mass
Direct hit required

ALP

PELE structure + explosive trigger before impact
Spreading of fragments with low lateral velocity



Summary



Aerodynamic data

Mechanical data

m	634 g
I_x/I_y	$1.7 \cdot 10^{-2}$
I_{CJ}	up to 3 cal

+

CX_0	0.21
CN_α	7.86
I_{CP}	0.427 cal
Λ	1094 cal
T	30 ms

Command data

I_{CJ}	2.35 cal
J	2 Ns
p	16.7 Hz

Control data

Gain	5.36
δ_{\max}	16 °
ΔV	40 m/s

