



RDECOM

Heating Rate Effect on Slow Cook-Off Response



TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.

E.L. Baker, T. Madsen, N. Al-Shehab, D. Pfau, B.E. Fuchs
U.S. Army ARDEC
Picatinny, NJ 07806-5000, USA

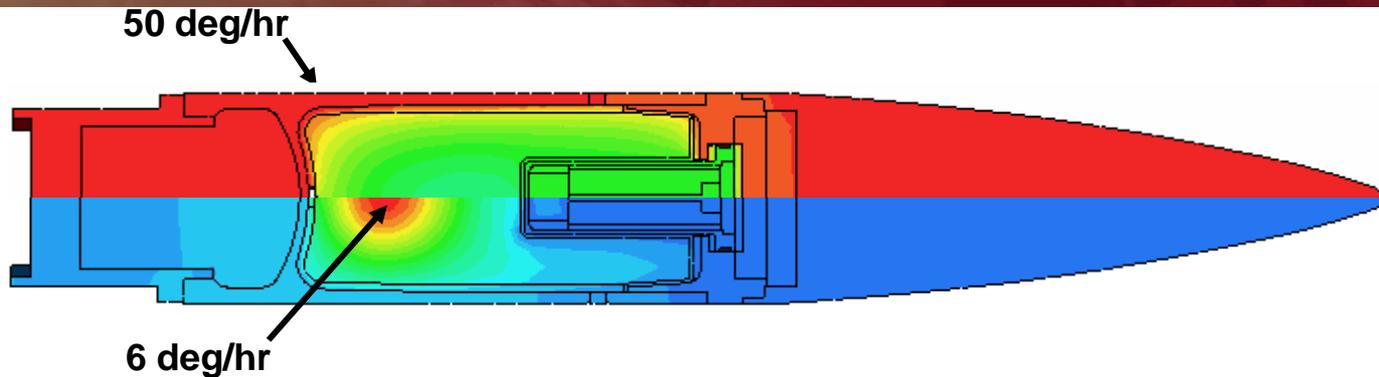
D. Hunter
GD- OTS Niceville, FL 32578

- There are many current Army IM efforts attempting to satisfy the arbitrarily difficult standard of the 6° F/hr heating rate.
- This leads to additional challenges for designers attempting to achieve system requirements, both performance and IM.

- IM solutions for 6° F/hr can produce overall system failures
 - Larger/more complicated venting schemes reduce structural integrity (e.g. gun launch/ bash-through)
- Designing to pass 6° F/hr SCO potentially means overlooking solutions for a 50° F/hr heating rate.
 - If the decomposition rate of an energetic is slower than the rate at which heat can be given off to the environment, there is a potential for a less violent reaction at 6° F/hr. Conversely utilizing the same design on 50° F/hr would result in a much more violent reaction.

- A large set of data currently exists for a variety of Army systems in development.
- This data set includes both the 6°F/hr and 50°F/hr heating rates.
- Experimental data can give direct comparisons of heating rates within a given subset of munitions to illustrate the difference in responses due to cook off.
 - While a single correlation cannot be stated (i.e. slower heating rate : more vent area), there are undeniable differences in responses of munitions when subjected to different heating rates.

XM982 Excalibur Thermal Analysis



- Hotspot = where self-heating occurs, i.e., explosive begins to burn in self sustaining reaction
- 50 deg F/hr
 - Hotspot forms on or near the surface
 - Surface burn allows gases to escape through vents
- 6 deg F/hr
 - Hot spot forms on billet centerline below the surface
 - Hot gases trapped inside the billet

Relevant IM Technologies

- Subsequent data will illustrate the use of various IM technologies.
 - Venting
 - Vent liners
 - Plastic
 - Metal
 - Meltable adapters
- Utilizing analog test setups to illustrate proof of principle of designs

XM982 50°F/hr vs. 6°F/hr

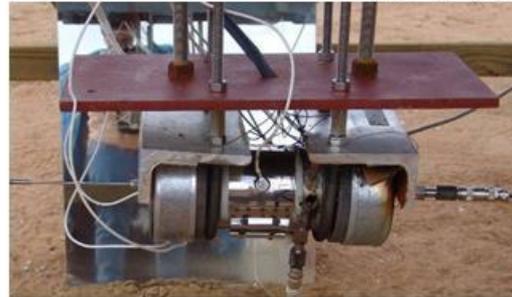
XM982 - Excalibur	6°F/hr	50°F/hr
Baseline Sub-scale		III
Subscale 2x Liner		V
Subscale Reactive Vent		III
Full Scale 2x liner	I	V/III
Full Scale 1.5x liner		III
Full Scale 1.75x liner		III

XM982 Testing (Sub-scale)

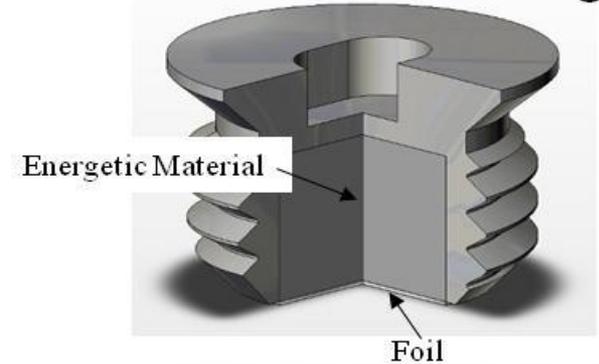
Baseline XM982



Double Thickness Liner SETUP



Reactive Vent Plug



RESULT



TYPE V



50°F/hr



TYPE III

XM982 Testing (Full-scale) Double Thickness Liner



SETUP



RESULT



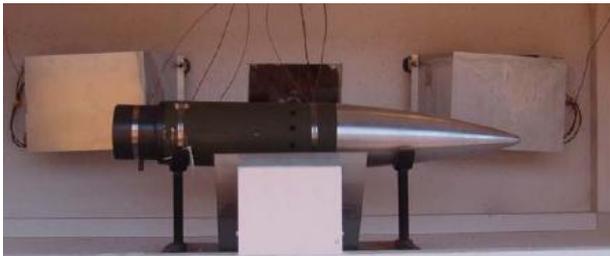
TYPE V

50°F/hr



XM982 Testing (Full-scale)

1.5X Liner



1.75X Liner



SETUP



RESULT



TYPE III

50°F/hr

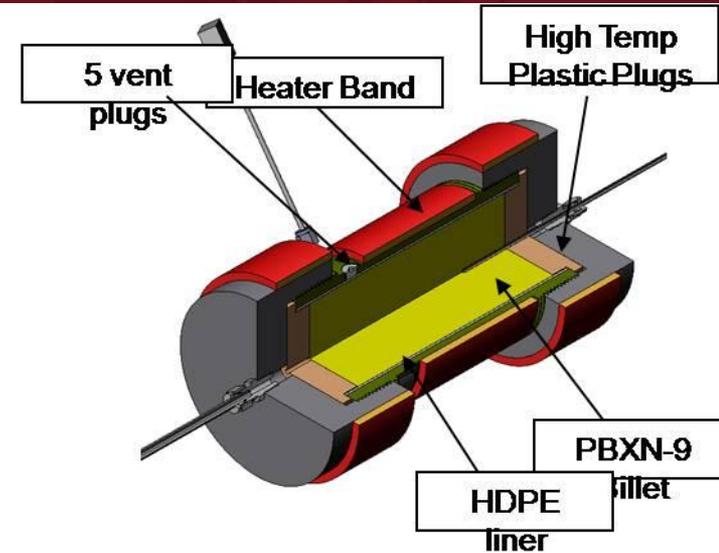
XM982 Controlled Thermal Venting Thicker Melt Liner

- Thicker melt liner venting design demonstrated on sub-scale test fixture (scaled 2/3)
- Thermal modeling conducted to design test and to determine hot spots

Double Thickness Liner
(Sub-scale)



TYPE V



50°F/hr

- Liner technology tested in full-scale hardware

Double Thickness Liner
(Full-scale)



Test 1



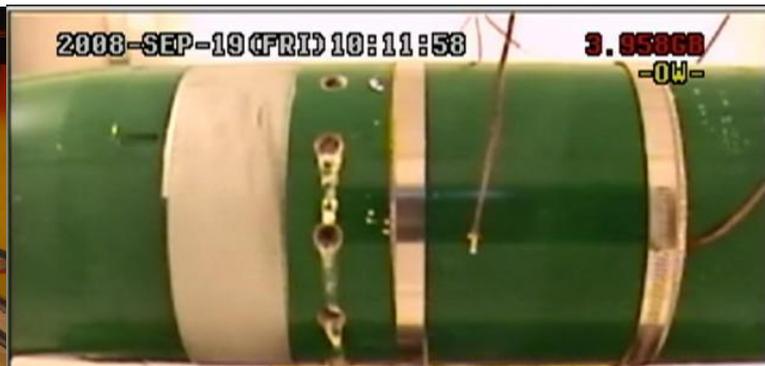
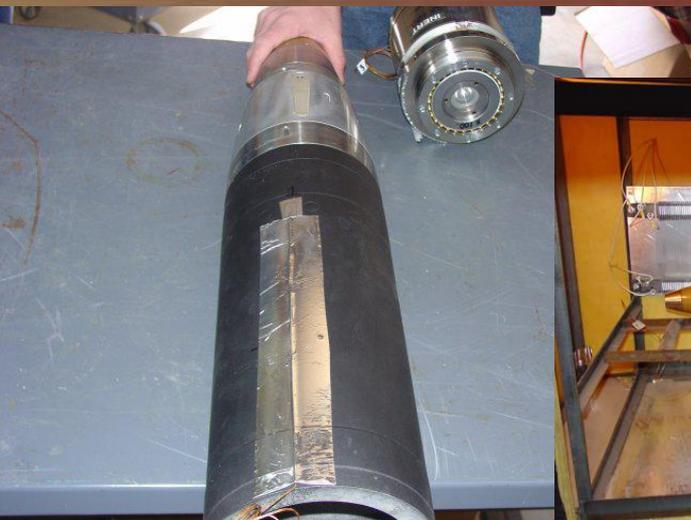
Test 2



UNCLASSIFIED

TYPE III *TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.*

XM982 Controlled Thermal Venting Thickest Melt Liner (0.225")



6°F/hr
UNCLASSIFIED

2008-SEP-18 17:39:14 FRAME PLAY



120mm IMX-104 50°F/hr vs. 6°F/hr

120mm Mortar (Venting)	6°F/hr	50°F/hr
Unfilled Adapter	V	V
Reduced Thread	III	V
Adapter V2	V/III	
Interrupted Thread (0.5)	II	
Interrupted Thread (0.75)	V*	



120mm Mortar with Unfilled Adapter Ring V2 Test Photos



6°F/hr

TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.



120mm Mortar with Reduced Thread Adapter PM-CAS Funded (IMX-104)



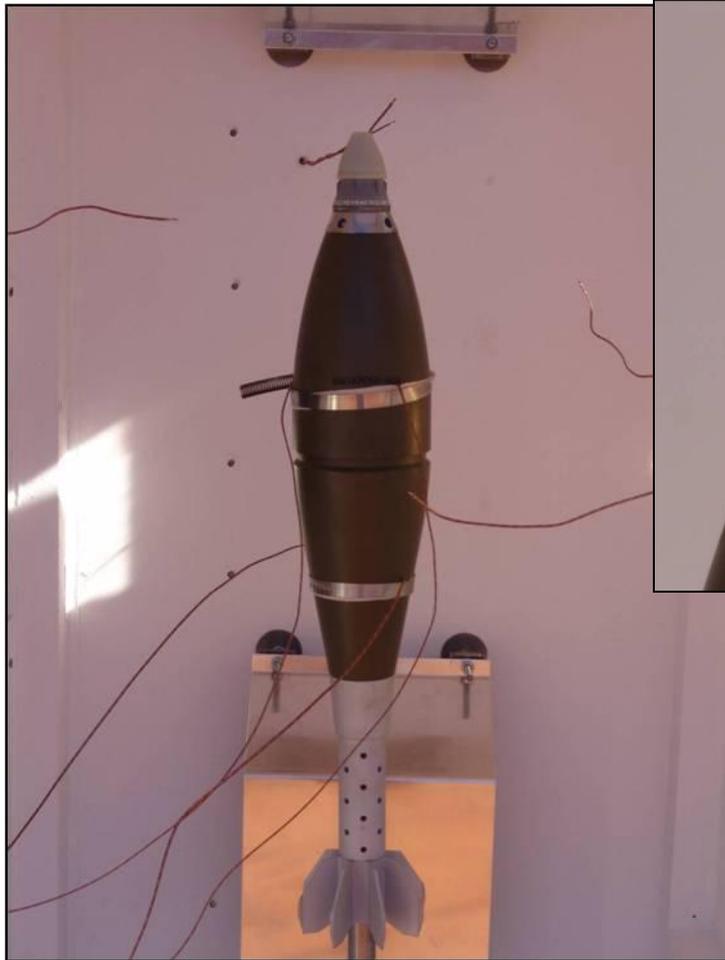
50°F/hr

TECHNOLOGY DRIVE



USED.

120mm Mortar with Filled Adapter Ring V2 Test 1 Photos



6°F/hr

120mm Mortar with Filled Adapter Ring V2 Test 2 Results



6°F/hr

UNCLASSIFIED

TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.



120mm Mortar Reduced Thread Adapter PM-CAS funded (IMX-104)



6°F/hr

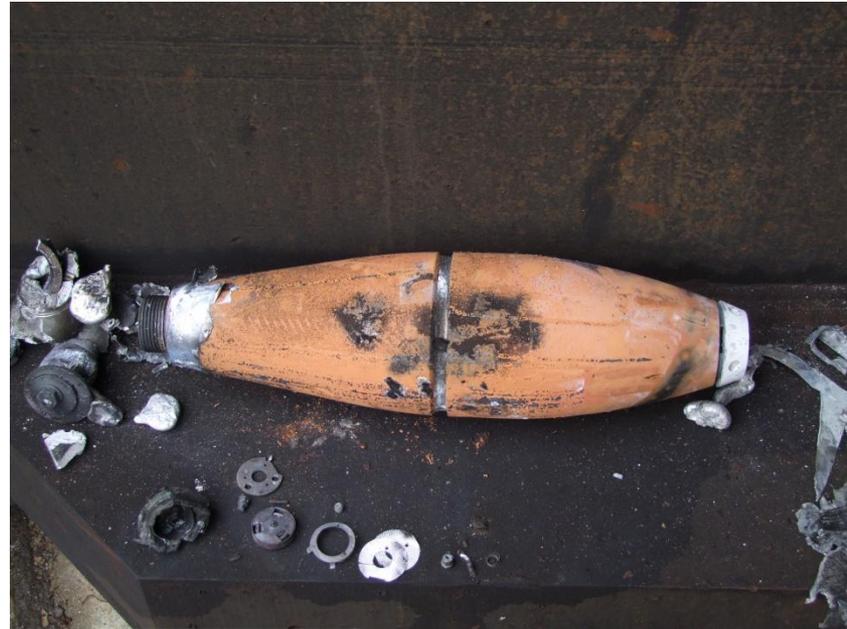
IMX-104 120mm Mortar



50°F/hr



IMX-104 120mm Mortar Interrupted Thread 0.75"



6°F/hr

TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.

TYPE V



Bangalore Torpedo 50°F/hr vs. 6°F/hr

Bangalore Torpedo	6°F/hr	50°F/hr
Baseline		V
Baseline		V
Quad Pack (1 live)		V
Quad Pack (4 live)		V
8 Pack (8 Live)	I	V

Bangalore Torpedo Baseline SCO Testing



Test Setup (Bangalore in oven)



Ignition (booster)



Burning



Pre-ignition (much HE runs out)

383°F



Post Test

50°F/hr



Type 5?



Bangalore Torpedo Baseline SCO Testing (Repeat)

160°F soak, 50°F/hr



Bulge in Endcap



HE Flows from Endcap



Test Setup (Bangalore in oven)



Booster Igniting



Item propelled toward camera

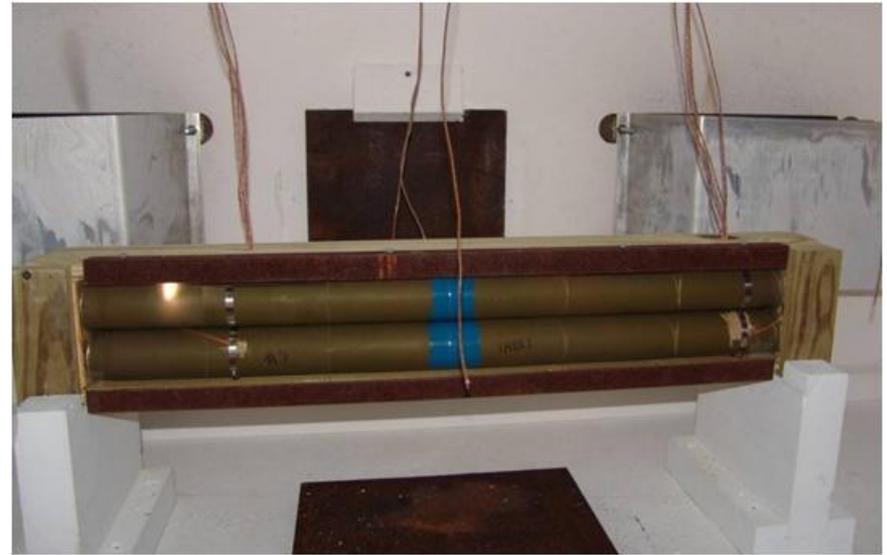


TYPE V

50°
F/hr

Bangalore Torpedo

Quad pack (1 live, 3 inert)



Test Setup (Bangalore in oven)



50°F/hr

UNCLASSIFIED

TYPE V

TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.

Bangalore Torpedo

Quad pack (4 live)



Test Setup (Bangalores in oven)



TYPE V

50°F/hr

UNCLASSIFIED



TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.

8-pack (8 live)



Test Setup

6°F/hr

TYPE I



Overall Comparison

	XM982	120mm	Bangalore
6F/hr	I	III	I
50F/hr	III/V	V	V

Difficulty of 6° F/hr Prompts Complex Solutions

- Complex solutions are generally necessary to pass the 6° F/hr requirement
 - Maximum Venting Area
 - Not always a possibility
 - Active Venting
 - Utilizes shaped charges or other techniques to provide venting
 - Thermally Initiated Venting System
 - Utilizes additional energetic that reacts at a lower temperature than main fill to cause surface ignition

We Should be Designing for Realistic Heating Rates

- As can be seen by the preceding data, there exists a real difference in energetic responses from one heating rate to the next.
- Assessments of realistic heating rates and lower bound heating rate estimates for a given munition system could provide important information in order to provide practical real improvements of Insensitive Munitions response.