



Computerized Generation and Simulation of Meshing and Contact of New Type of Novikov-Wildhaber Helical Gears

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COMPUTERIZED GENERATION AND SIMULATION OF MESHING AND CONTACT OF NEW TYPE OF NOVIKOV-WILDHABER HELICAL GEARS

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SUMMARY

In this report, we propose a new geometry for low-noise, increased-strength helical gears of the Novikov-Wildhaber type. Contact stresses are reduced as a result of their convex-concave gear tooth surfaces. The gear tooth surfaces are crowned in the profile direction to localize bearing contact and in the longitudinal direction to obtain a parabolic function of transmission errors. Such a function results in the reduction of noise and vibrations.

Methods for the generation of the proposed gear tooth surfaces by grinding and hobbing are considered, and a tooth contact analysis (TCA) computer program to simulate meshing and contact is applied. The report also investigates the influence of misalignment on transmission errors and shift of bearing contact. Numerical examples to illustrate the developed approaches are proposed.

The proposed geometry was patented by Ford/UIC (Serial Number 09-340-824, pending) on June 28, 1999.

1.0 INTRODUCTION

In comparison with conventional involute helical gears, Novikov-Wildhaber (N-W) gears (refs. 1 and 2) have reduced contact stresses. This reduction has been achieved because at the point of contact, there is only a small difference between the curvatures of the concave and convex mating gear tooth surfaces. At every instant, the tooth surfaces are in a point contact spread under the load over an elliptical area; therefore, we say that the bearing contact is localized. There is a probability that the lubrication conditions of N-W gears are slightly improved because in the process of meshing, the instantaneous contact ellipse moves not across the tooth surface but in the longitudinal direction. This direction of the contact path is favorable because it causes a "pumping effect." However, the same direction of the contact path can also be achieved for involute helical gears if profile modification is provided.

Novikov-Wildhaber gears or the generating imaginary rack-cutters are provided with circular-arc profiles. There are two versions of Novikov gears, the first having one zone of meshing (fig. 1.1) and the other having two. The design of gears with two zones of meshing was an attempt to reduce high bending stresses caused by point contact. Novikov gears with two zones of meshing have been standardized in the former USSR and in China (refs. 3 and 4). Figure 1.2 shows imaginary rack-cutters for the generation of Novikov gears with two zones of meshing.

Unfortunately for Novikov followers, who enthusiastically thought that N-W gears would be a substitute for conventional involute helical gears, their expectations have not been realized. After more than 40 years since their invention, N-W gears have found application only in low-speed reducers manufactured in the oil and mine industries. These gears are still applied in areas where manufacturers try to avoid grinding and expect that a sufficient bearing contact will be obtained by running under the load and lapping in the gear drive housing. Only soft materials are still applied for N-W gears, and the gear tooth surfaces are not hardened and nitrified.

The major disadvantage of N-W gears is that gear misalignment (such as a change in the shaft angle or in the lead) causes an impermissible noise. Because of this high-level noise, the only example of the application of N-W gears in high-speed transmissions is that of the Westland Helicopter Company. The other disadvantage of N-W gears is the shift in the bearing contact (to the addendum or dedendum areas) that results from a change in the center distance. This shift can be reduced by increasing the difference between the curvatures of the tooth surfaces but this negates the attempt to reduce the contact stresses.

Experience with the design and application of involute helical gears shows that the resources used to employ them have almost been exhausted. Attempts to localize bearing contact had been concentrated on profile modification, but such efforts could not reduce the noise level. Even though the geometry of involute helical gears presents

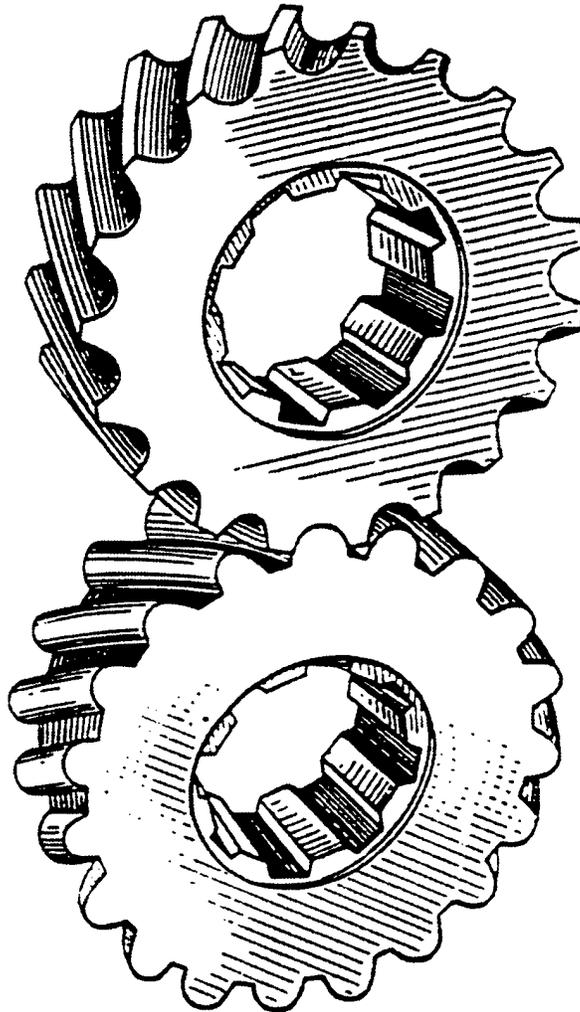


Figure 1.1.—Novikov gears of previous design.

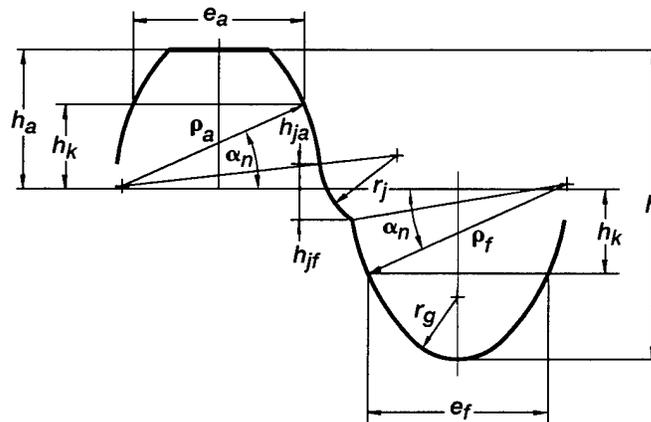


Figure 1.2.—Profiles of rack-cutter for Novikov gears with zones of meshing.

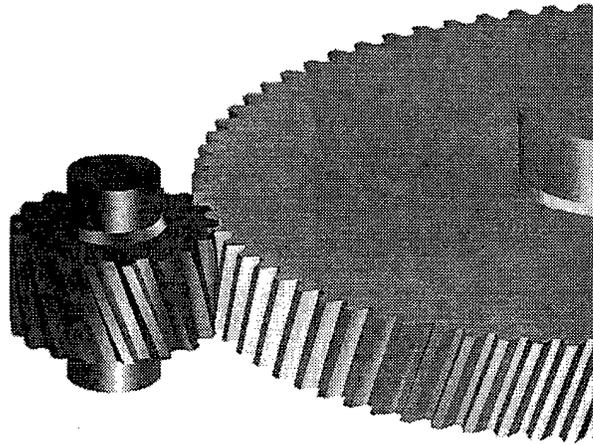


Figure 1.3.—Helical gears with new geometry.

an obstacle in the reduction of contact stresses and noise, they are still an example of high-precision gear drives because of the possibility of grinding by a worm or form grinding.

The new type of helical gears developed by the authors of this report has presented new possibilities for the design and manufacture of low-noise, increased-strength helical gear drives. Although the details of this development are covered in sections 2.0 to 5.0, a brief summary of the project follows:

1. The bearing contact is localized and the contact stresses are reduced because of the tangency of concave-convex tooth surfaces of the mating gears. Two versions of the proposed design were investigated (see secs. 2 to 4): one has a convex pinion tooth surface and the other a concave. Figure 1.3 is a three-dimensional view of the designed helical gears with convex pinion teeth.

2. The conjugation of pinion-gear teeth is based on the application of two imaginary rack-cutters with mismatched surfaces Σ_c and Σ_t (see details in subsec. 2.1). The normal section of each rack-cutter is a parabola as shown in figure 1.4. A current point of the parabola is determined in an auxiliary coordinate system S_i by the equations

$$x_i = u_i, \quad y_i = a_i u_i^2 \quad (1.1)$$

where u_i is a variable parameter that determines the location of the current point in the normal section and a_i is the parabolic coefficient.

Henceforth, we designate by an abbreviated symbol S_k an orthogonal coordinate system $S_k(x_k, y_k, z_k)$ where (x_k, y_k, z_k) indicate the coordinate axes of S_k .

3. The normal profiles of mating rack-cutters are in tangency at reference point Q , and axis y_i (fig. 1.4) is the normal to the profiles at Q . The normal profiles are mismatched (fig. 1.5) because different parabolic coefficients a_i for the mating rack-cutters have been applied. Points Q of various normal sections of the mating rack-cutters form a line of tangency of their surfaces Σ_c and Σ_t . It is imagined that rack-cutter surfaces are rigidly connected to each other and generate separately the pinion and gear tooth surfaces. The generated pinion-gear tooth surfaces are in a point contact that spreads under load over an elliptical area (ref. 5).

4. The advantages of applying rack-cutter parabolic profiles in comparison with applying circular-arc profiles in previous designs are as follows:

- a. The possibility of increasing the height of the pinion addendum that is limited by tooth pointing and the height of the pinion dedendum that is limited by the possibility of undercutting
- b. The possibility of increasing the tooth thickness at the point of tangency of the active profile with the fillet and reducing the bending stresses

These advantages are illustrated by figure 1.6, which shows parabolic profile 1 and circular-arc profile 2 with the same curvature radius ρ_1 at point Q . Point C_1 is the center of the circle of radius ρ_1 ; α is the profile angle at Q .

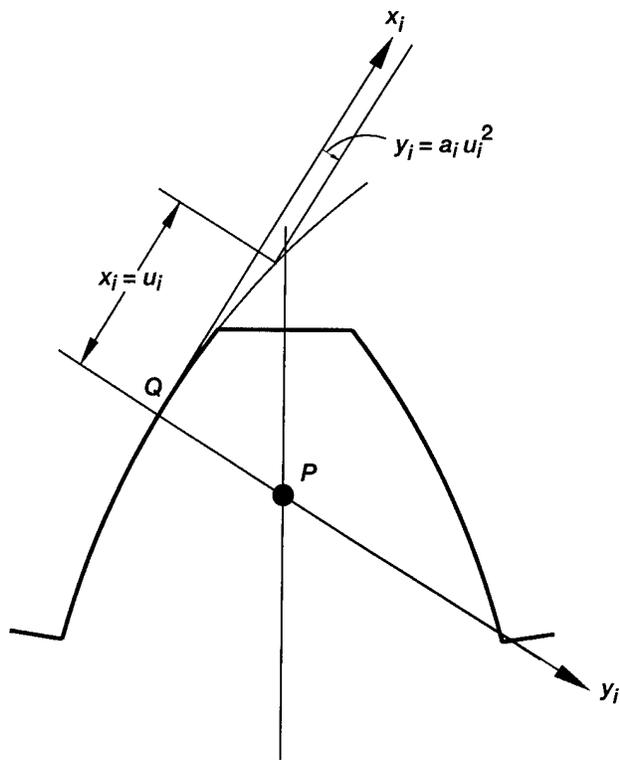


Figure 1.4.—Parabolic profile of rack-cutter in normal section.

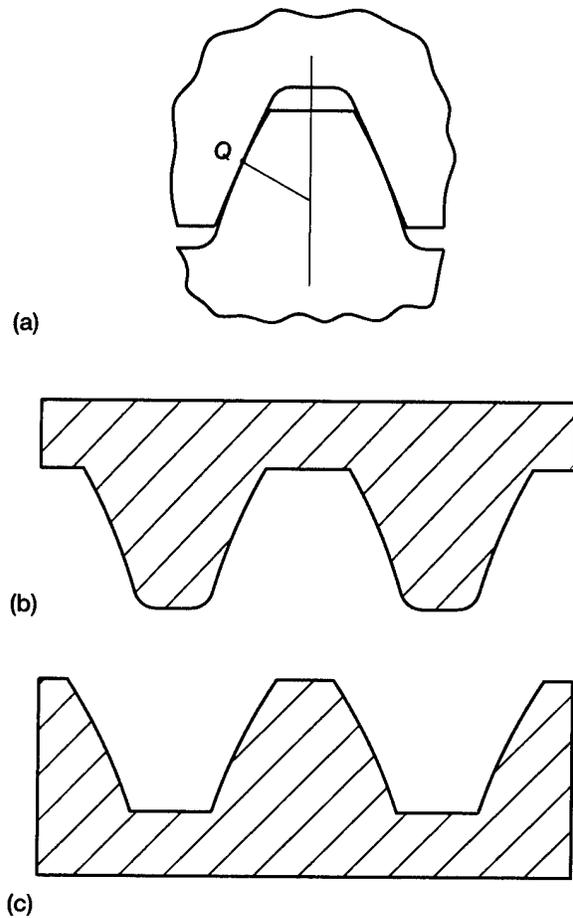


Figure 1.5.—Rack-cutter applied for generation. (a) Normal profiles of rack-cutters. (b) and (c) Normal sections of pinion and gear rack-cutters.

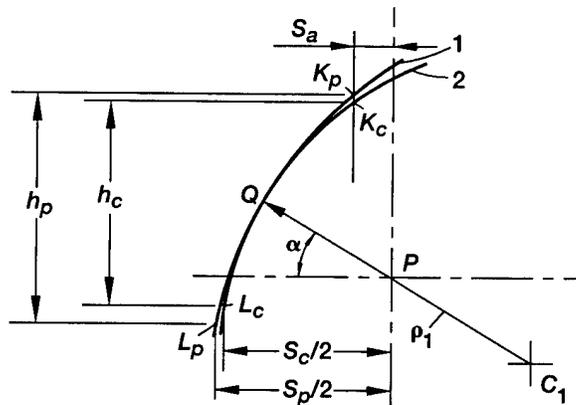


Figure 1.6.—Comparison of parabolic (1) and circular (2) profiles of rack-cutters.

Point P is the point of intersection of the normal to the tooth profile with the axis of the tooth symmetry and is located on the instantaneous axis of rotation. Points L_p and L_c indicate limiting points of tooth profiles (for the new and previous design, respectively) obtained from the condition of no undercutting. Similarly, K_p and K_c indicate limiting points of tooth profiles obtained from the condition of pointing determined for tooth profiles with the same value of S_a . Parameters h_p and h_c are the possible tooth heights for the new and previous designs, respectively. Dimensions S_p and S_c are the possible tooth thicknesses at the point of tangency of the active profile and the fillet for the new and previous designs, respectively.

5. The curvature radii of the rack-cutter profiles for the new gear design are substantially larger than those of the existing design that are based on the application of circular-arc profiles. Thus, the advantages of the new design are that they allow one to

- a. Increase the dimensions of the instantaneous contact ellipse and obtain a more favorable orientation, as shown in figure 1.7 where μ_1 is the angle between the major axis of the contact ellipse and the tangent to the path of contact on the pinion tooth surface. The center of the contact ellipse coincides with the point of contact Q . The dimensions of the contact ellipse have been determined by considering that the elastic approach of tooth surfaces is $\delta = 0.00025$ in.
- b. Reduce the sensitivity of the gear drive to a change in the gear center distance ΔE , which causes a shift of the bearing contact to the tooth addendum or dedendum (depending on the sign of ΔE).

6. The generation of gears for the new and previous designs is based on the application of two mating hobs or grinding worms that are conjugated to the rack-cutters shown in figure 1.5. Two shaped grinding disks can be applied instead of hobs or grinding worms.

In both designs, the bearing contact of tooth surfaces is localized (the tooth surfaces are in point contact at every instant).

7. The main differences in the generation methods for both designs are

- a. Only profile crowning is provided in the generation of gears for the previous design. Therefore, the function of transmission errors is almost a linear discontinuous one for a misaligned gear drive (fig. 1.8(a)). Such transmission errors cause vibration for Novikov-Wildhaber gears when the meshing of one pair of teeth is changed for another one.

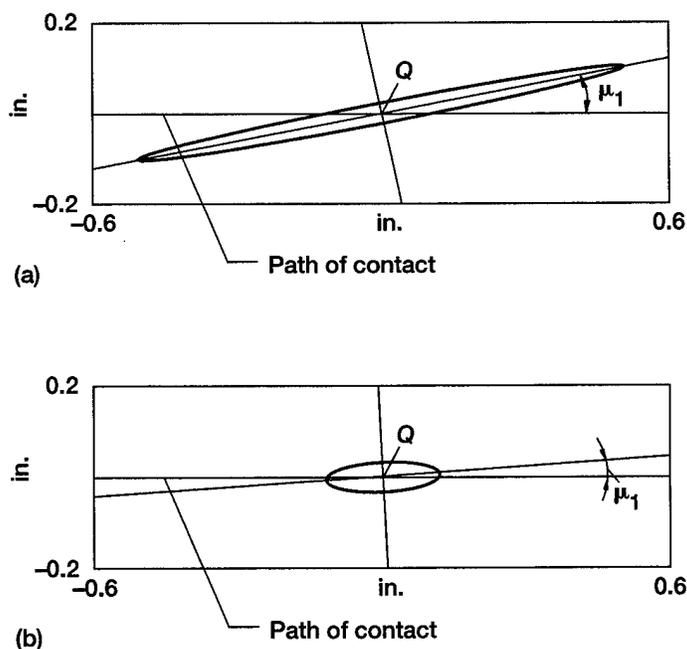


Figure 1.7.—Contact ellipse on pinion tooth surface for (a) proposed design and (b) previous design.

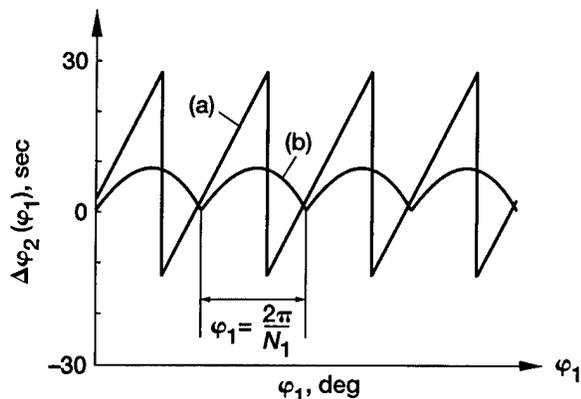


Figure 1.8.—Functions of transmission errors. (a) Linear function of transmission errors caused by error of shaft angle $\Delta\gamma = 3$ arc min. (b) Reduction and transformation of errors provided by new geometry of tooth surfaces.

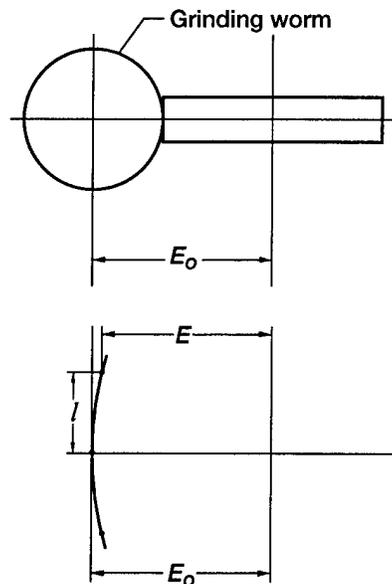


Figure 1.9.—Plunging of grinding worm.

- b. The new design provides crowning in two directions: profile and longitudinal. The longitudinal crowning is obtained by the varied plunge of the tool when a grinding worm is applied (fig. 1.9). The shortest distance E between the axes of the grinding worm and the workpiece is represented by

$$E(l) = E_0 - al^2 \quad (1.2)$$

where l is the displacement along the axis of the workpiece; E_0 is the nominal value of the shortest axis distance; and a is the parabolic coefficient. A parabolic function $E(l)$ must also be provided for generation by hobbing and form grinding.

The varied plunge makes it possible to provide a predesigned parabolic function of transmission errors (fig. 1.8(b)) that can absorb the linear functions of transmission errors caused by gear misalignment and also reduce the magnitude of transmission errors (refs. 5 and 6). The varied plunge of the tool is required only for the generation of one of the mating gears, either the pinion or the gear.

8. The absorption of the linear functions of transmission errors by a parabolic function (provided by tool plunging) is confirmed by tooth contact analysis (TCA) for gears of the new design (see sec. 2.8). The reduction of noise and vibration in the new gears means that they can be used in high-speed transmissions.

9. The misalignment of the new gears may cause a shift in the bearing contact to the edge (fig. 1.10). Drawings in figure 1.10 show the contact path for the following cases: (a) without errors of alignment; (b) a change in the gear center distance ΔE of 0.1 mm; (c) a change in the shaft angle $\Delta\gamma$ of 3 arc min; (d) a change in the lead angle $\Delta\lambda$ of 3 arc min.

The authors have developed a method to correct the contact path (and the bearing contact) by correcting the lead angle of the pinion or the gear. Because of the existence of a predesigned parabolic function of transmission errors, correcting the lead angle will allow the location of the contact path to be restored without causing transmission errors.

10. The new geometry of helical gears can be extended to conventional involute helical gears as follows: (a) one of the imaginary rack-cutter surfaces is a plane that generates a conventional screw involute surface; (b) the mating rack-cutter is provided with a parabolic profile in the normal section (fig. 1.4) but with a very small curvature; (c) the crowning in the longitudinal direction is accomplished by tool plunging (fig. 1.9), making it possible to obtain a predesigned parabolic function.

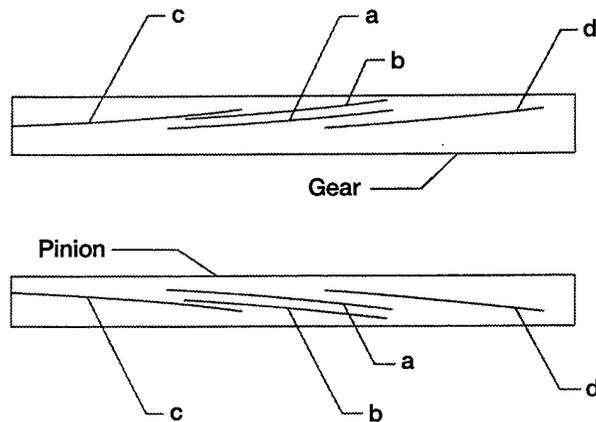


Figure 1.10.—Contact paths on pinion and gear surfaces for one cycle of meshing obtained for helical gears with new geometry. (a) Without errors of alignment. (b) Change of center distance $\Delta E = 0.1$ mm. (c) Change of shaft angle $\Delta\gamma = 3$ arc min. (d) Change of lead angle $\Delta\lambda = 3$ arc min.

The advantage of the proposed modification of conventional involute helical gears is the possibility of reducing the magnitude of transmission errors and transforming their shape (see plot (b) in fig. 1.8).

This report covers

1. The computerized design and imaginary rack-cutter generation of two versions of profile-crowned helical gears. The two versions are designed as pinion convex-gear concave (sec. 2.0) and pinion concave-gear convex (sec. 3.0). The designed gearing is a new type of Novikov-Wildhaber helical gear.
2. The avoidance of undercutting and tooth pointing (secs. 2.0 and 3.0).
3. The grinding (or cutting) of the designed helical gears crowned in the profile and longitudinal directions by the application of a disk or worm (sec. 4.0).
4. The computerized simulation of the meshing and contact of the designed helical gears crowned in (a) the profile direction only, and (b) the profile and longitudinal directions (secs. 2.0 to 4.0).

2.0 HELICAL PINION CONVEX AND GEAR CONCAVE PROFILE-CROWNED TOOTH SURFACES

2.1 Basic Considerations

This section covers the geometry, generation, design, and simulation of the meshing and contact of profile-crowned tooth surfaces. The pinion and gear tooth surfaces are convex and concave. Section 3.0 discusses another version of tooth surfaces, pinion concave and gear convex.

The generation of pinion-gear tooth surfaces is based on the following ideas:

1. Two imaginary rigidly connected rack-cutters for the separate generation of the pinion and the gear are applied (fig. 1.5).
2. The axodes of the pinion and the gear in mesh with the rack-cutters are two pitch cylinders of radii r_{p1} and r_{p2} (fig. 2.1.1(a)). The axode of the rigidly connected rack-cutters is plane Π that is tangent to the pitch cylinders. The pinion and gear perform rotational motions about their axes whereas the rack-cutters perform translational motions, all of which are related. The pitch cylinders and plane Π are in tangency at line $P-P$, which is the instantaneous axis of rotation in relative motion.
3. The rack-cutters are provided with skew teeth (fig. 2.1.1(b) and from the drawings, it is obvious that a left-hand rack-cutter generates a left-hand pinion and a right-hand gear. The helix angles on the pinion-gear pitch cylinders are equal to angle β of the skew teeth of the rack-cutters.

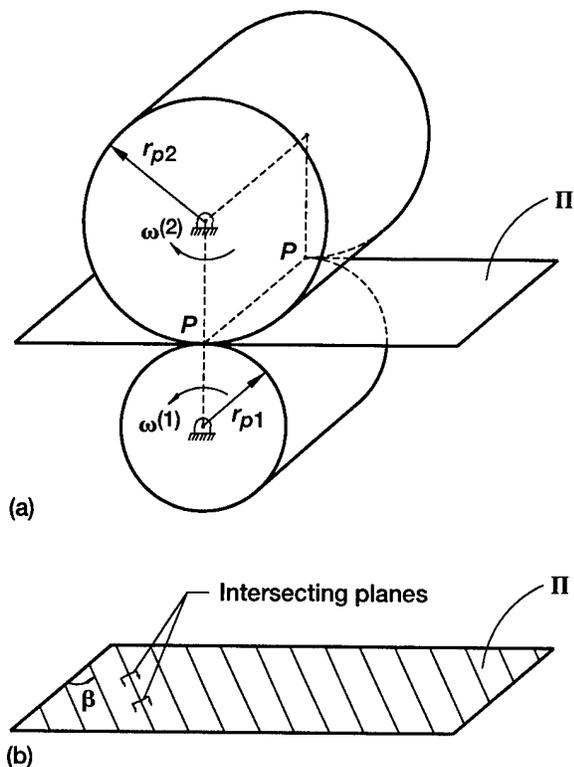


Figure 2.1.1.—Axodes of pinion, gear, and rack-cutter.
(a) Axodes. (b) Direction of rack-cutter teeth.

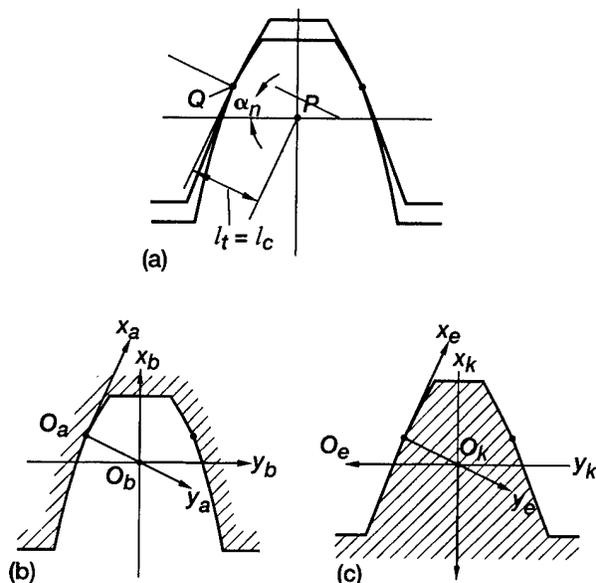


Figure 2.1.2.—Normal sections of rack-cutters
(a) Profiles of pinion and gear rack-cutters.
(b) Pinion rack-cutter. (c) Gear rack-cutter.

4. The normal profiles of rack-cutters are obtained by the intersection of rack-cutter surfaces by a vertical plane that is perpendicular to the direction of rack-cutter teeth. The normal profiles are two mismatched parabolas in tangency at point Q (fig. 2.1.2(a)), and their common normal passes through point P that belongs to the instantaneous axis of rotation $P-P$ (fig. 2.1.1(a)).

5. Using various intersecting normal planes (fig. 2.1.1(b)) results in the same rack-cutter normal profiles shown in figure 2.1.2(a). Henceforth, we will consider two rack-cutter surfaces Σ_c and Σ_l that generate the pinion and gear tooth surfaces Σ_1 and Σ_2 , respectively. Surfaces Σ_c and Σ_l are in tangency along a straight line that passes through points Q of tangency of various normal profiles. The orientation of the line of tangency of Σ_c and Σ_l is determined by angle β .

Because the rack-cutter surfaces are mismatched, the pinion-gear tooth surfaces are in point contact (but not in line contact) and therefore the bearing contact is localized.

2.2 Derivation of Pinion Tooth Surface Σ_1

Pinion rack-cutter surface Σ_c .—The derivation of rack-cutter surface Σ_c is based on the following procedure:

Step 1: The normal profile of Σ_c is a parabola and is represented in coordinate system S_a (fig. 2.1.2(b)) by equations that are similar to equations (1.1):

$$\mathbf{r}_a(u_c) = \begin{bmatrix} u_c & a_c u_c^2 & 0 & 1 \end{bmatrix}^T \quad (2.2.1)$$

where a_c is the parabolic coefficient.

Step 2: The normal profile is represented in S_b by matrix equation

$$\mathbf{r}_b(u_c) = \mathbf{M}_{ba}\mathbf{r}_a(u_c) \quad (2.2.2)$$

The distance $|\overline{O_a O_b}|$ is designated as l_c , and \mathbf{M}_{ba} indicates the 4×4 matrix used for the coordinate transformation from coordinate system S_a to S_b (ref. 7). Homogeneous coordinates of a point are considered in reference 7.

Step 3: Consider that rack-cutter surface Σ_c is formed in S_c while coordinate system S_b with the normal profile performs a translational motion in the direction $a-a$ of the skew teeth of the rack-cutter (fig. 2.2.1).

Surface Σ_c is determined in coordinate system S_c in two-parameter form by the following matrix equation:

$$\mathbf{r}_c(u_c, \theta_c) = \mathbf{M}_{cb}(\theta_c)\mathbf{M}_{ba}\mathbf{r}_a(u_c) = \mathbf{M}_{ca}(\theta_c)\mathbf{r}_a(u_c) \quad (2.2.3)$$

where $\theta_c = |\overline{O_c O_b}|$ (fig. 2.2.1) and (u_c, θ_c) are surface parameters.

Step 4: The normal \mathbf{N}_c to rack-cutter surface Σ_c is determined by matrix equation (ref. 7)

$$\mathbf{N}_c(u_c, \theta_c) = \mathbf{L}_{cb}(\theta_c)\mathbf{L}_{ba}\mathbf{N}_a(u_c) \quad (2.2.4)$$

Here

$$\mathbf{N}_a(u_c) = \mathbf{k}_a \times \frac{\partial \mathbf{r}_a}{\partial u_c} \quad (2.2.5)$$

where \mathbf{L}_{cb} indicates the 3×3 matrix that is the submatrix of \mathbf{M}_{cb} and is used for the transformation of vector components; \mathbf{k}_a is the unit vector of axis z_a .

The transverse section of rack-cutter Σ_c is shown in figs. 2.2.2(a) and (b).

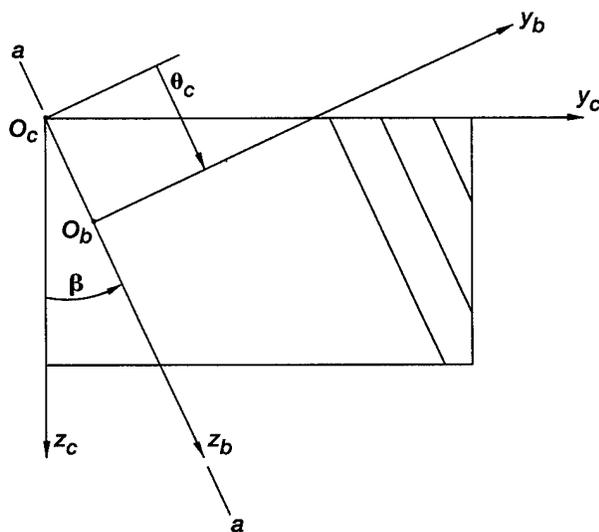


Figure 2.2.1.—For derivation of pinion rack-cutter surface Σ_c .

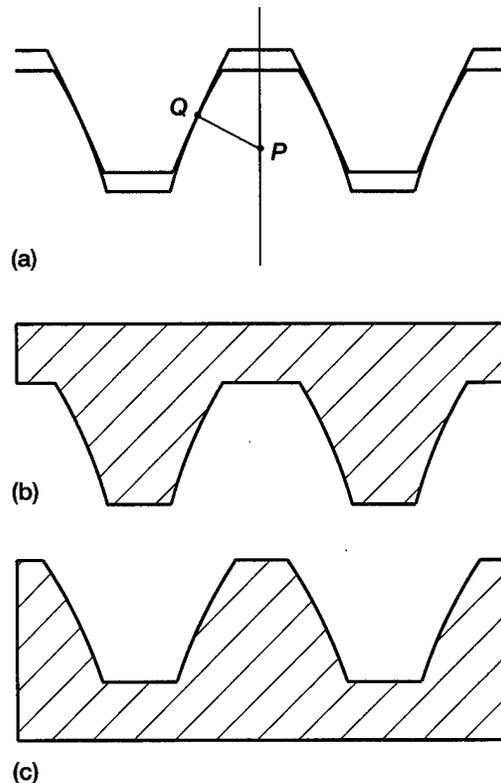


Figure 2.2.2.—Rack-cutter transverse profiles. (a) Mating profiles. (b) Pinion rack-cutter profile. (c) Gear rack-cutter profile.

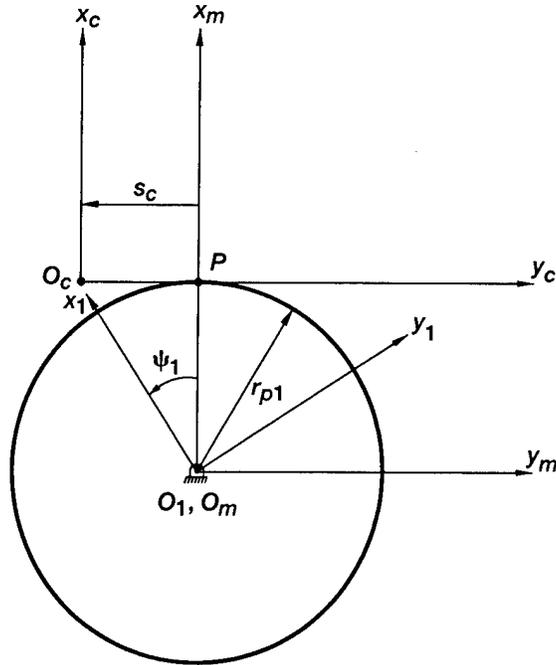


Figure 2.2.3.—Generation of pinion by rack-cutter Σ_c .

Determination of pinion tooth surface Σ_1 .—The determination of Σ_1 is based on the following considerations:

1. Movable coordinate systems S_c and S_1 (fig. 2.2.3) are rigidly connected to the pinion rack-cutter and the pinion, respectively. The fixed coordinate system S_m is rigidly connected to the cutting machine.
2. The rack-cutter and the pinion perform related motions, as shown in figure 2.2.3 where $s_c = r_{p1}\psi_1$ is the displacement of the rack-cutter in its translational motion, and ψ_1 is the angle of rotation of the pinion.
3. A family of rack-cutter surfaces is generated in coordinate system S_1 and is determined by the matrix equation

$$\mathbf{r}_1(u_c, \theta_c, \psi_1) = \mathbf{M}_{1c}(\psi_1)\mathbf{r}_c(u_c, \theta_c) \quad (2.2.6)$$

4. The pinion tooth surface Σ_1 is generated as the envelope to the family of surfaces $\mathbf{r}_1(u_c, \theta_c, \psi_1)$. Surface Σ_1 is determined by simultaneous consideration of vector function $\mathbf{r}_1(u_c, \theta_c, \psi_1)$ and the so-called equation of meshing:

$$f_{1c}(u_c, \theta_c, \psi_1) = 0 \quad (2.2.7)$$

5. To derive the equation of meshing (2.2.7), apply the following theorem (refs. 5 and 7): *The common normal to surfaces Σ_c and Σ_1 at their line of tangency must pass through the instantaneous axis of rotation P (fig. 2.2.3).* The result is

$$\frac{X_c - x_c}{N_{xc}} = \frac{Y_c - y_c}{N_{yc}} = \frac{Z_c - z_c}{N_{zc}} \quad (2.2.8)$$

where (x_c, y_c, z_c) are the coordinates of a current point of Σ_c ; (N_{xc}, N_{yc}, N_{zc}) are the components of the normal to Σ_c ; $X_c = 0, Y_c = r_{p1}\psi_1$, and Σ_c are the coordinates of the intersection point of normal N_c with the instantaneous axis of rotation P (fig. 2.2.3).

To derive the equation of meshing (2.2.7), it is sufficient to consider equation

$$-\frac{x_c(u_c, \theta_c)}{N_{xc}(u_c, \theta_c)} = \frac{r_{p1}\psi_1 - y_c(u_c, \theta_c)}{N_{yc}(u_c, \theta_c)} \quad (2.2.9)$$

The gear tooth surface is represented by equations

$$\mathbf{r}_2 = \mathbf{r}_2(u_t, \theta_t, \psi_2) \quad (2.3.3)$$

$$f_{2t}(u_t, \theta_t, \psi_2) = 0 \quad (2.3.4)$$

Equation (2.3.3) represents in S_2 the family of rack-cutter surfaces Σ_t determined as

$$\mathbf{r}_2(u_t, \theta_t, \psi_2) = \mathbf{M}_{2t}(\psi_2) \mathbf{r}_t(u_t, \theta_t) \quad (2.3.5)$$

The derivation of the equation of meshing (2.3.4) may be accomplished similarly to that of equation (2.2.10)

$$f_{2t}(u_t, \theta_t, \psi_2) = (r_{p2}\psi_2 - y_t)N_{xt} + x_tN_{yt} = 0 \quad (2.3.6)$$

Drawings of figs. 2.1.1 and 2.3.1 show that a left-hand rack-cutter generates a right-hand gear. Equations (2.3.5) and (2.3.6) represent the gear tooth surface by three related parameters. The linear parameter θ_t can be eliminated and the gear tooth surface represented in two-parameter form by vector function $\mathbf{r}_2(u_t, \psi_2)$.

2.4 Avoidance of Undercutting and Pointing

The generation of a helical tooth surface by a rack-cutter may be accompanied by undercutting of the surface being generated. The discovery of undercutting is based on the following theorem proposed in references 5 and 7: *Singular points of the generated surface Σ occur when the velocity of a contact point in its motion over Σ becomes equal to zero. Note that at a singular surface point, the surface normal is equal to zero.* Thus, the appearance of a singular point heralds the oncoming of surface undercutting.

References 5 and 8 propose an approach for determining a line L of regular points on the tool surface that generates singular points on the generated surface. The dimensions of the tool surface must be limited by line L to avoid undercutting. In the case of generation by a rack-cutter, the limiting line L of the rack-cutter surface determines the limiting height of the rack-cutter addendum.

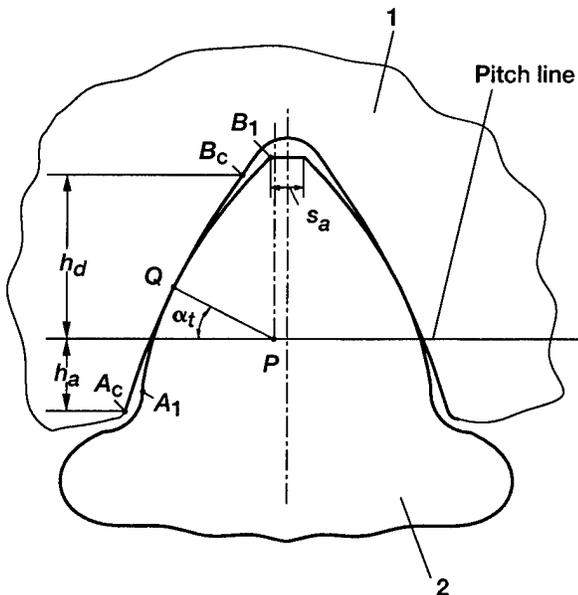


Figure 2.4.1.—For determination of conditions of undercutting and pointing by rack-cutter.

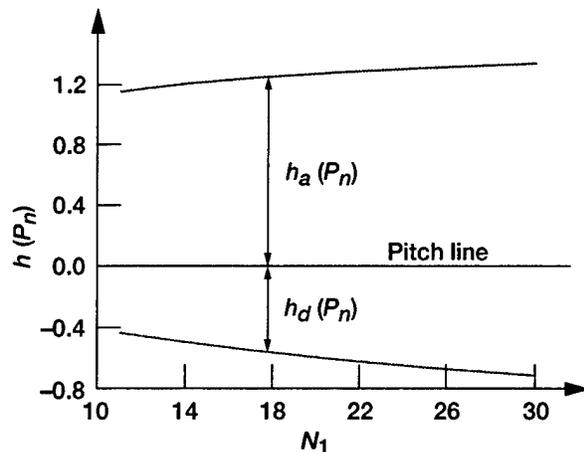


Figure 2.4.2.—Permissible dimensions of rack-cutter addendum h_a and dedendum h_d .

The pointing of generated teeth means that the top-land width of the generated teeth becomes equal to zero. In the present project, pointing was avoided because a minimal value of the top-land width was provided.

Figure 2.4.1 shows the transverse profiles of the rack-cutter space and the profiles of the generated pinion tooth. Point A_c is the limiting one of the rack-cutter left profile that generates the singular point A_1 of the left pinion transverse profile. Point B_c of the rack-cutter profile generates point B_1 of the pinion profile. The width of the pinion top-land is designated by S_a . The left transverse profiles of the rack-cutter and the pinion are shown at a position where they are in tangency at point Q . Point P belongs to the instantaneous axis of rotation. The heights h_a and h_d of the working parts of the rack-cutter addendum and dedendum are measured from the pitch line of the rack-cutter.

The results of the present investigation are illustrated by the curves of figure 2.4.2, which represent functions $h_a(N_1)$ and $h_d(N_1)$ determined for the data $\beta = 20^\circ$, $\alpha_n = 25^\circ$, $10 \leq N_1 \leq 30$, and $P_n = 1/\text{in}$. These curves were obtained by considering the meshing of the transverse profile of the rack-cutter with the transverse profile of the pinion (or the gear). Note that the normal profile of the rack-cutter is a parabola and the rack-cutter surface Σ_c is a parabolic cylinder. The transverse profile of the rack-cutter has also been proven to be a parabola. The parabolic coefficients a_c^* and a_c of the transverse and normal profiles are related as

$$a_c^* = a_c \frac{\cos^3 \alpha_t}{\cos^3 \alpha_n \cos \beta} \quad (2.4.1)$$

The surface of action between the rack-cutter surface and the generated pinion (or gear tooth surface) is a cylindrical surface. The transverse section of the surface of action is shown in figure 2.4.3.

In summarizing the results of this investigation, we may state that undercutting may occur for a pinion with a small number of teeth (see fig. 2.4.2). A sufficient working height $h = h_a + h_d$ of the teeth is in the range $(1.5/P_n) \leq h \leq (1.9/P_n)$.

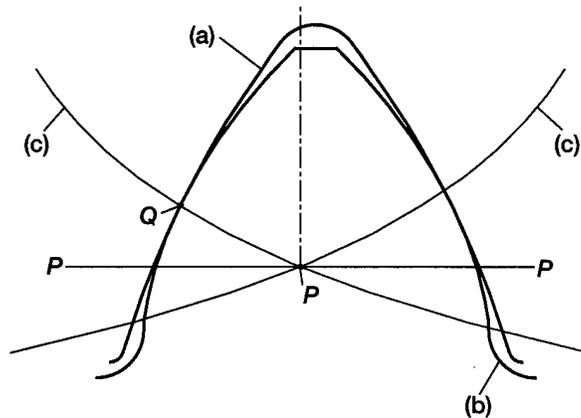


Figure 2.4.3.—Transverse profiles and lines of action.
(a) Rack-cutter profile. (b) Pinion profile. (c) Lines of action.

2.5 Principal Curvatures and Directions of Pinion-Gear Tooth Surfaces

Knowledge of principal curvatures and directions of the contacting surfaces Σ_1 and Σ_2 is required to determine the dimensions of the instantaneous contact ellipse. Determining the principal curvatures of surfaces Σ_1 and Σ_2 is based on the approach developed in references 5 and 7. The advantage of this approach is that the sought-for curvatures are expressed in terms of the principal curvatures and directions of the tool surface and the parameters of motion. In the case of the helical gears under discussion, the principal curvatures and directions of pinion-gear tooth surfaces can be expressed in terms of the principal curvatures and directions of rack-cutters and the parameters of motion.

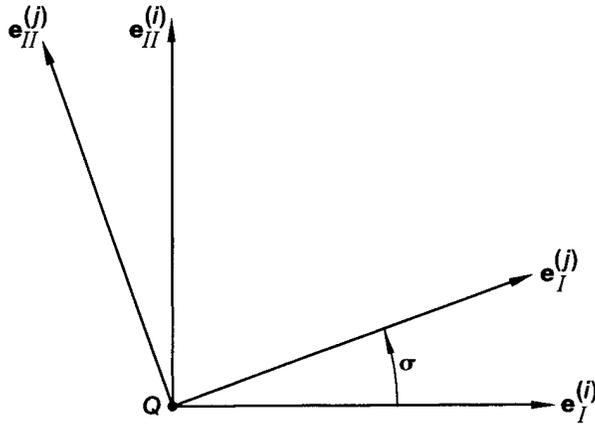


Figure 2.5.1.—Principal directions on generating and generated surfaces; $i = c, t$; $j = 1, 2$.

Let us start the derivations by determining the curvatures of the rack-cutter. The surface of rack-cutter Σ_c (or Σ_t) is a cylindrical surface whose generatrix has the direction of skew rack-cutter teeth. Such a surface is a ruled "developed" surface, which means that it is formed by straight lines (the generatrices of the cylindrical surface), and the normals along the generatrix do not change their direction. The generatrix is the surface principal direction and the principal curvature in this direction is equal to zero. This means that

$$\kappa_I^{(i)} = 0 \quad (i = c, t) \quad (2.5.1)$$

The other principal direction is the tangent to the parabola that represents the normal profile and the principal curvature is the curvature of the parabola determined at point Q as

$$\kappa_{II}^{(i)} = 2a_i \quad (i = c, t) \quad (2.5.2)$$

The principal curvatures and directions of the pinion (or gear) tooth surface generated by the rack-cutter are determined by using the approach developed in references 7 and 8, which enables us to determine the following: σ , the angle formed by principal directions $e_I^{(j)}$ and $e_{II}^{(i)}$ (fig. 2.5.1) and principal curvatures on directions $e_I^{(j)}$ and $e_{II}^{(i)}$ on surface Σ_j . Here, $j=1$ when $i=c$ (when pinion tooth surface Σ_1 generated by rack-cutter Σ_c is considered). Similarly, $j=2$ when $i=t$ (when gear tooth surface Σ_2 generated by rack-cutter Σ_t is considered).

We have limited the determination of principal curvatures and directions on surfaces Σ_1 and Σ_2 only at point Q of the tangency of the generating and generated surfaces (fig. 2.1.2). In an ideal profile-crowned gear drive, the path of contact on Σ_1 (and Σ_2) is a helix generated by point Q , and the principal curvatures and directions at any point of the helix are the same.

The approach discussed above is illustrated by an example with the following data: tooth numbers $N_1 = 17$, $N_2 = 77$; the normal profile angle $\alpha_n = 25^\circ$; the normal diametral pitch $P_n = 5$; the parabolic coefficients $a_c = 0.425$ and $a_t = 0.394$; the helix angle $\beta = 19.548^\circ$.

The results of computing the principal curvatures of Σ_1 and Σ_2 at point Q (fig. 2.1.2) are as follows: $\kappa_I^{(1)} = 0.0125$, $\kappa_{II}^{(1)} = 1.5605$, $\kappa_I^{(2)} = 0.0083$; and $\kappa_{II}^{(2)} = 0.5940$.

Therefore, for the pinion tooth surface with a convex normal profile, both principal curvatures are positive. The Gaussian curvature $K^{(1)} = \kappa_I^{(1)} \kappa_{II}^{(1)} > 0$ and all points of this surface are elliptic ones.

For the gear tooth surface with a normal profile, the principal curvatures have opposite signs. The Gaussian curvature $K^{(2)} = \kappa_I^{(2)} \kappa_{II}^{(2)} > 0$ and all points of this surface are hyperbolic.

2.6 Determination of Contact Ellipse

The determination of the instantaneous contact ellipse is based on the following considerations (refs. 5 and 7):

1. Consider as known: the principal curvatures and directions on surfaces Σ_1 and Σ_2 and angle σ formed by unit vectors $e_I^{(1)}$ and $e_I^{(2)}$ (fig. 2.6.1). The details for determining the principal curvatures of contacting surfaces are given in reference 7.

2. The elastic deformation δ of contacting surfaces is given.

Now, determine the orientation of the contact ellipse by using angle $\alpha^{(1)}$ and the dimensions a and b of the contact ellipse and by using the following equations:

$$\cos 2\alpha^{(1)} = \frac{g_1 - g_2 \cos 2\sigma}{(g_1^2 - 2g_1g_2 \cos 2\sigma + g_2^2)^{1/2}} \quad (2.6.1)$$

$$\sin 2\alpha^{(1)} = \frac{g_2 \sin 2\sigma}{(g_1^2 - 2g_1g_2 \cos 2\sigma + g_2^2)^{1/2}} \quad (2.6.2)$$

Axes of the contact ellipse are determined with equations

$$2a = 2 \left| \frac{\delta}{A} \right|^{1/2}, \quad 2b = 2 \left| \frac{\delta}{B} \right|^{1/2} \quad (2.6.3)$$

where

$$A = \frac{1}{4} \left[\kappa_{\Sigma}^{(1)} - \kappa_{\Sigma}^{(2)} - (g_1^2 - 2g_1g_2 \cos 2\sigma + g_2^2)^{1/2} \right] \quad (2.6.4)$$

$$B = \frac{1}{4} \left[\kappa_{\Sigma}^{(1)} - \kappa_{\Sigma}^{(2)} + (g_1^2 - 2g_1g_2 \cos 2\sigma + g_2^2)^{1/2} \right] \quad (2.6.5)$$

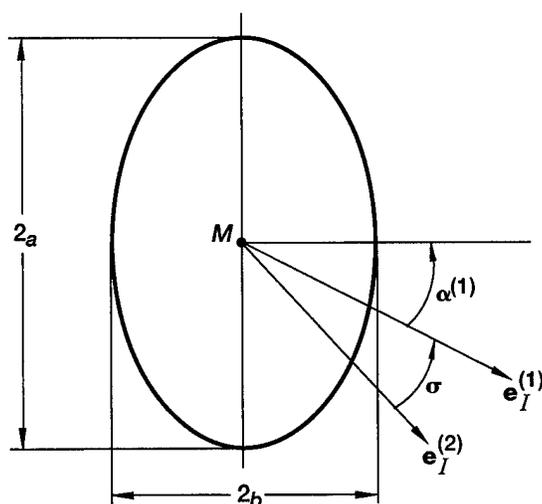


Figure 2.6.1.—Contact ellipse.

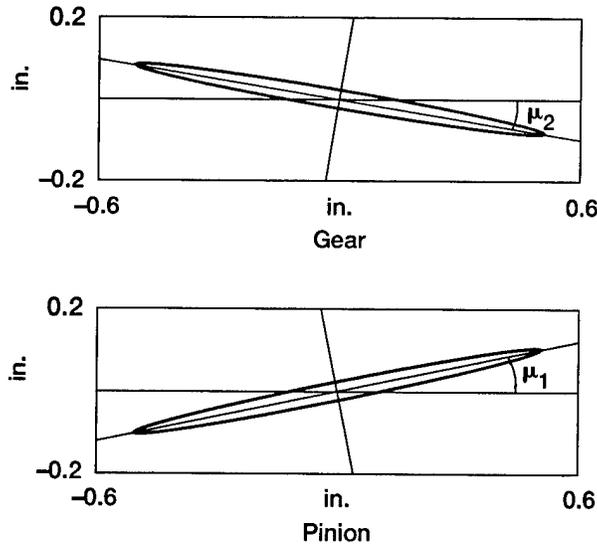


Figure 2.6.2.—Contact ellipses on pinion and gear tooth surfaces.

$$\kappa_{\Sigma}^{(i)} = \kappa_I^{(i)} + \kappa_{II}^{(i)}, \quad g_i = \kappa_I^{(i)} - \kappa_{II}^{(i)}, \quad (i = 1, 2) \quad (2.6.6)$$

Figure 2.6.2 shows the contact ellipses determined on pinion and gear tooth surfaces Σ_1 and Σ_2 . To avoid misunderstanding, we have to emphasize that the tangents to contact paths on the mating rack-cutter surfaces Σ_c and Σ_t coincide with each other (they are directed along the line of tangency of Σ_c and Σ_t). However, the tangents to the contact paths on pinion-gear tooth surfaces Σ_1 and Σ_2 at point Q of surface tangency slightly differ from each other. Therefore, the orientation of contact ellipses is determined by different angles μ_1 and μ_2 , as shown in figure 2.6.2. The dimensions and orientation of the contact ellipse have been determined for these design parameters: tooth numbers $N_1 = 17$ and $N_2 = 77$; normal profile angle $\alpha_n = 25^\circ$; normal diametral pitch $P_n = 5$; parabolic coefficients $a_c = 0.425$ and $a_t = 0.394$; helix angle $\beta = 19.548^\circ$; elastic deformation $\delta = 0.0025$ in. The other design parameters are the same as those mentioned in section 2.5.

2.7 Recommended Parameters of Rack-Cutter Normal Profiles

The normal profiles of mating rack-cutters are shown in figure 2.7.1 (see also fig. 2.1.2(a)); Q is the point of tangency of the profiles; P relates to the pitch line (the instantaneous axis of rotation); $l_i = |\overline{QP}|$ ($i = c, t$), α_n is the normal pressure angle; C_2 and C_1 are the centers of curvature at point Q of the gear and pinion profiles. The choice and determination of design parameters shown in figure 2.7.1 are based on the following considerations:

1. The normal pressure angle α_n is chosen as 25° to 30° , which is in agreement with previous experience in designing the Novikov-Wildhaber helical gears. The increase in the pressure angle causes a higher sensitivity of the gearing to the error in the center distance and a larger value of the contact force. However, using a larger value of α_n allows us to obtain more favorable relations between the curvatures of the gear tooth surfaces, thereby reducing the stresses.

2. The distance l_i ($i = c, t$) is chosen as $l_i = (\cos \alpha_n) / (P_n)$, where P_n is the normal diametral pitch.

3. The recommendation for $\rho_c = |\overline{QC_2}|$ and $\rho_c = |\overline{QC_2}|$ (fig. 2.7.1) are based on the following relations:

a. The radius of curvature of the gear rack-cutter must satisfy the inequality

$$\rho_t < \frac{N_2 \sin \alpha_n}{2P_n \cos^3 \beta} + l_t \quad (2.7.1)$$

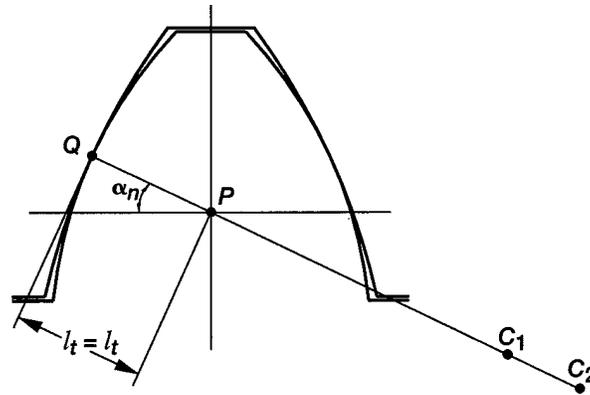


Figure 2.7.1.—Choice of design parameters for two rack-cutter normal profiles.

where N_2 is the number of gear teeth and β is the helix angle.

Inequality (2.7.1) is derived by using the Euler-Savari equation that relates the curvatures of the transverse profiles of the gear rack-cutter and the gear. Inequality (2.7.1) is the condition of the gear normal profile to be concave in the neighborhood of the designated point Q .

b. We recommend that the radii of curvature ρ_t and ρ_c be

$$\rho_t = \frac{6.35}{P_n}, \quad \rho_c = \frac{5.88}{P_n} \quad (2.7.2)$$

to yield

$$\frac{\rho_t}{\rho_c} = 1.08 \quad (2.7.3)$$

Observing equations (2.7.2) and (2.7.3) allows us to keep the bearing contact shift caused by the change in the center distance in the working dimensions of the teeth.

c. The profiles of the rack-cutters are parabolic curves (see sec. 2.2). The parabolic coefficients a_c and a_t and the curvature radii are related as follows

$$a_c = \frac{1}{2\rho_c}, \quad a_t = \frac{1}{2\rho_t} \quad (2.7.4)$$

4. The values of the addendum and dedendum of the rack-cutter profiles must guarantee that the undercutting and pointing of generated teeth be avoided. Section 2.4 gives the results of an investigation of the avoidance of undercutting and pointing.

2.8 Tooth Contact Analysis of Profile-Crowned Helical Gears

The purpose of a TCA (tooth contact analysis) of profile-crowned helical gears is to prove that the meshing of such gears is accompanied by an unfavorable shape of the function of transmission errors that causes vibration and noise. Therefore it is necessary, as shown in section 4.0, to combine profile crowning with longitudinal crowning to transform the function of transmission errors to enable a reduction in the level of vibration and noise. Generating helical gears with profile and longitudinal crowning requires that existing technology be modified (see sec. 4.0).

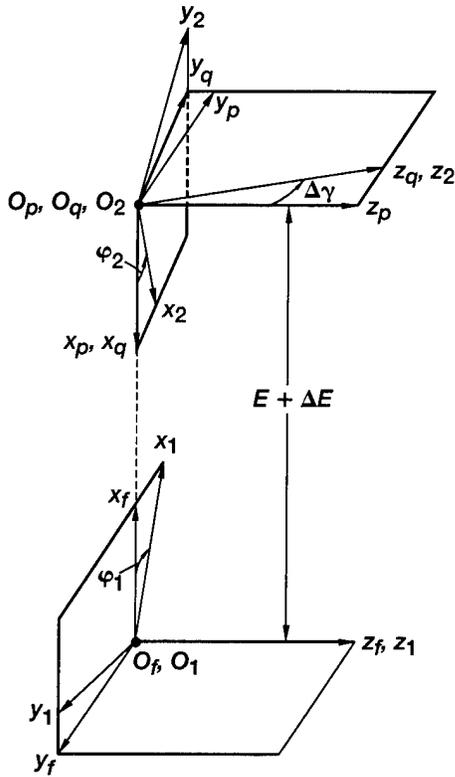


Figure 2.8.1.—Coordinate systems applied for TCA (tooth contact analysis).

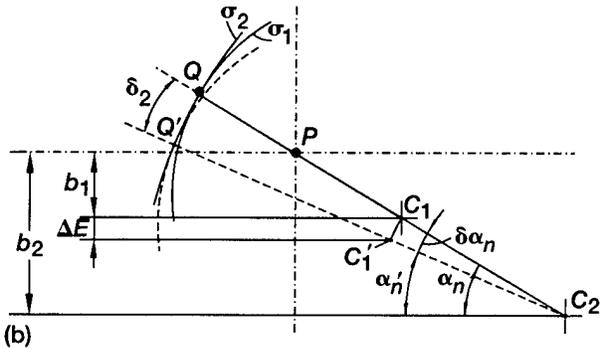
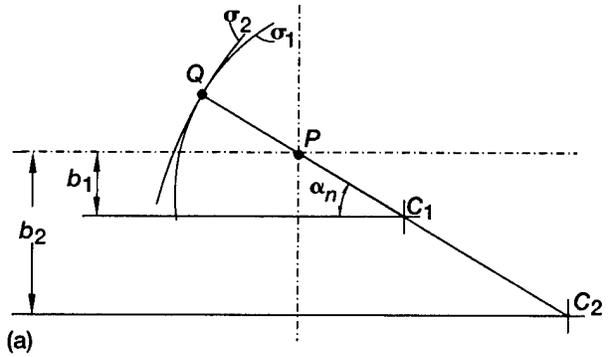


Figure 2.8.2.—Determination of change of normal pressure angle $\delta\alpha_n$ caused by change of center distance ΔE . (a) Initial tangency of profiles σ_1 and σ_2 at point Q. (b) Tangency of σ_1 and σ_2 at point Q' that corresponds to error of center distance ΔE .

Computer programs developed for TCA are based on the simulation of the continuous tangency of misaligned gear tooth surfaces. For this purpose, apply the following: (a) movable coordinate systems S_1 and S_2 rigidly connected to the pinion and the gear and (b) the basic fixed coordinate system S_f where the meshing of the gears is considered (fig. 2.8.1). Coordinate systems S_p and S_q are auxiliary coordinate systems applied to simulate errors of alignment ΔE , a change in the shortest center distance, and $\Delta\gamma$, a change in the shaft angle. In addition, the error in the lead angle $\Delta\lambda_{pi}$, ($i = 1, 2$) is also considered.

The TCA algorithm is based on the following procedure:

Step 1.—The pinion and gear tooth surfaces and their unit normals in coordinate systems S_1 and S_2 are initially represented as follows:

1. Surface Σ_1 and surface unit normal \mathbf{n}_1 are represented by vector functions $\mathbf{r}_1(u_c, \psi_1)$ and $\mathbf{n}_1(u_c, \psi_1)$.
2. Similarly, for surface Σ_2 , we have vector functions $\mathbf{r}_2(u_t, \psi_2)$ and $\mathbf{n}_2(u_t, \psi_2)$.

Step 2.—Using coordinate transformation, represent Σ_1 , \mathbf{n}_1 , Σ_2 , and \mathbf{n}_2 in S_f . The continuous tangency of Σ_1 and Σ_2 is represented by the vector equations

$$\mathbf{r}_f^{(1)}(u_c, \psi_1, \phi_1, \Delta\lambda_{p1}) = \mathbf{r}_f^{(2)}(u_t, \psi_2, \phi_2, \Delta\gamma, \Delta E) \quad (2.8.1)$$

$$\mathbf{n}_f^{(1)}(u_c, \psi_1, \phi_1, \Delta\lambda_{p1}) = \mathbf{n}_f^{(2)}(u_t, \psi_2, \phi_2, \Delta\gamma) \quad (2.8.2)$$

Errors of alignment $\Delta\gamma$ and ΔE are simulated by the proper installment of coordinate system S_g with respect to S_f (fig. 2.8.1). It is assumed that the error of the lead angle is considered for the pinion only. Angles ϕ_1 and ϕ_2 represent the rotation of pinion and gear being in mesh with each other.

Step 3.—Vector equation (2.8.1) is equivalent to three independent scalar equations, but (2.8.2) is only equivalent to two independent scalar equations since $|\mathbf{n}_f^{(1)}| = |\mathbf{n}_f^{(2)}| = 1$. The system of vector equations (2.8.1) and (2.8.2) is equivalent to five independent scalar equations in six unknowns represented as

$$f_i(u_c, \psi_1, \phi_1, u_t, \psi_2, \phi_2) = 0 \quad (2.8.3)$$

One of the unknowns, for example ϕ_1 , can be chosen as the input with the goal being to obtain the solution of the equations by functions

$$u_c(\phi_1), \psi_1(\phi_1), u_t(\phi_1), \psi_2(\phi_1), \phi_2(\phi_1) \quad (2.8.4)$$

This is an iterative process that requires at each iteration the first guess and the observation of the inequality (refs. 7 and 8).

$$\frac{D(f_1, f_2, f_3, f_4, f_5)}{D(u_c, \psi_1, \phi_1, u_t, \psi_2, \phi_2)} \neq 0 \quad (2.8.5)$$

The iterative process is computerized by using the program DNEQNF (ref. 9). The output of TCA enables us to determine the function of transmission errors $\Delta\phi_2(\phi_1)$ and the shift of the bearing contact caused by misalignment.

Investigation shows that the most dominating error for the shift of bearing contact is the error of the center distance. The approach developed in this report is based on an investigation of the meshing of the normal profiles of mating rack-cutters.

Step 1.—Figure 2.8.2(a) shows that the normal profiles σ_1 and σ_2 of the rack-cutters are initially in tangency at point Q . The curvature radii are $\rho_1 = Q C_1$ and $\rho_2 = Q C_2$, and the location of the centers of curvature C_1 and C_2 with respect to P is determined by b_1 and b_2 .

Step 2.—Simulate the tangency of σ_1 and σ_2 when the center distance of the pinion and the gear is changed, imagining that σ_2 is held at rest and normal profile σ_1 is turned about C_2 through $\delta\alpha_n$ (fig. 2.8.2(b)). Then, center C_1 will take position C'_1 and the normal profiles become in tangency at Q' . The new pressure angle is α'_n , and the shift of the tangency point over σ_2 is

$$\delta_2 = \rho_2 \delta\alpha_n, \quad \delta_1 = \rho_1 \delta\alpha_n \quad (2.8.6)$$

It is easy to verify that

$$\sin \alpha'_n = \frac{b_2 - b_1 - \Delta E}{\rho_2 - \rho_1} \quad (2.8.7)$$

To reduce the shift of the point of contact over the profiles of the rack-cutters (and over the surfaces of the pinion and gear), it is necessary to increase the magnitude of $(\rho_2 - \rho_1)$. The new design of helical gears developed in this report provides more room for such a solution without substantially affecting the contact stresses because the curvature radii ρ_2 and ρ_1 are substantially larger in comparison with the previous design of Novikov-Wildhaber gears.

Although the approach discussed for investigating the influence of ΔE_1 is an approximate one, it provides a high precision that is confirmed by applying the developed TCA computer program. The change of center distance ΔE does not cause transmission errors.

Figures 2.8.3 and 2.8.4 graphically represent the influence of errors $\Delta\gamma$ and $\Delta\lambda_{p1}$ on the transmission errors. The function of transmission errors becomes a discontinuous one and worsens the conditions for the transfer of meshing.

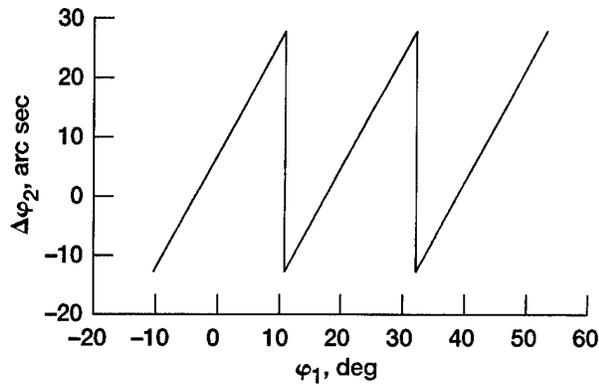


Figure 2.8.3.—Linear transmission error function when only profile crowning is applied; $\Delta\gamma = 3$ arc min.

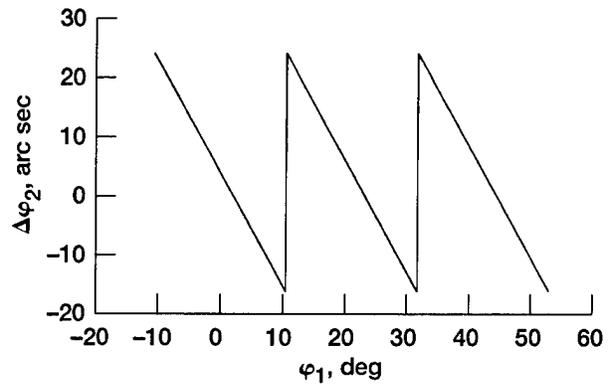


Figure 2.8.4.—Linear transmission error function when only profile crowning is applied; $\Delta\lambda = 3$ arc min.

Gear vibration and noise become inevitable if only profile crowning is provided. This is the reason why combined crowning (in the profile and longitudinal directions) has been developed by the authors (see sec. 4.0).

3.0 HELICAL PINION CONCAVE AND GEAR CONVEX PROFILE-CROWNED TOOTH SURFACES

3.1 Introduction

Section 2.0 covers the proposed design of helical gears with a pinion convex-gear concave type of surface contact. We consider in this section helical gears with pinion concave-gear convex surface contact. Our investigation shows that the first type of contact is preferable (see secs. 3.3 and 3.4). However, for the purpose of completeness of the project, the pinion concave-gear convex contact of surfaces is covered in this section, in addition to the investigation accomplished in section 2.0.

This investigation used the same design methodology as applied in section 2.0. The contents of this section cover the choice of design parameters based on the results of investigating undercutting and pointing, determining the contact ellipse, and comparing the results obtained with those obtained in section 2.0.

3.2 Preliminary Choice of Design Parameters of the Normal Section of Rack-Cutters

As mentioned in section 2.0, two imaginary rigidly connected rack-cutters Σ_c and Σ_t are applied to generate the pinion and the gear. The normal sections of the rack-cutters are shown in figure 3.2.1. The radius of curvature $|\overline{O_c C_c}|$ of the pinion rack-cutter at point Q must satisfy the inequality

$$|\overline{O_c C_c}| = \rho_c < \frac{N_1 \sin \alpha_n}{2P_n \cos^3 \beta} + l_c \quad (3.2.1)$$

The right side of the inequality represents the curvature radius of the rack-cutter that generates point Q of the pinion profile of an infinitely large curvature radius. The derivation of inequality (3.2.1) is based on the application of the Euler-Savari equation.

Inequality (3.2.1) guarantees that the pinion transverse profile is concave only at point Q but not at any point of the pinion profile. This is illustrated by the drawings of figure 3.2.2, which shows transverse profiles of the pinion and the rack-cutter. The pinion profile is concave-convex. However, choosing proper design parameters makes it possible to obtain a concave pinion profile in the whole area. An example of a set of such design parameters is

$$\alpha_n = 25^\circ, \quad l_c = \frac{0.906}{P_n}, \quad a_c = \frac{1}{2\rho_c} = 1.25P_n, \quad a_t = \frac{1}{2\rho_t} = 1.389P_n, \quad N_{p1} \geq 16$$

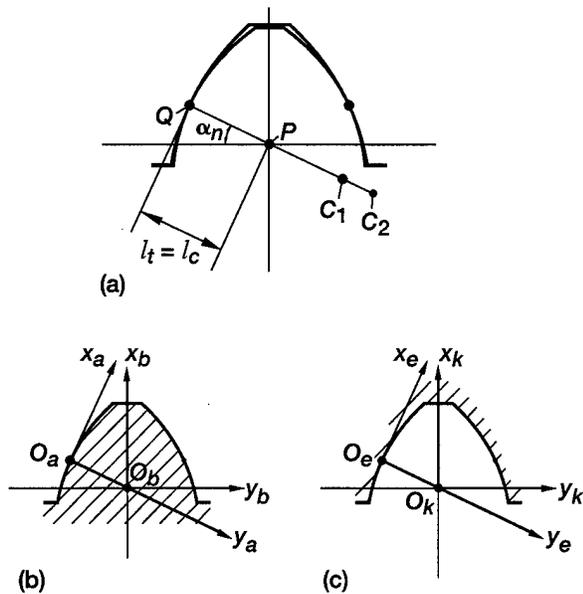


Figure 3.2.1.—Normal sections of rack-cutters. (a) Profiles of pinion concave and gear convex rack-cutters. (b) Pinion rack-cutter. (c) Gear rack-cutter.

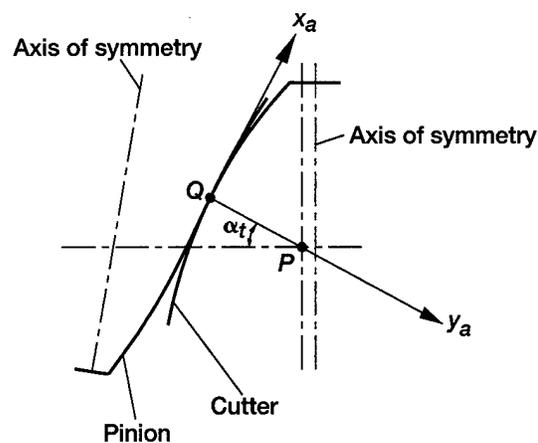


Figure 3.2.2.—Concave-convex pinion and convex rack-cutter transverse profiles.

The limitations of the rack-cutter addendum and dedendum are determined in subsection 3.3.

3.3 Avoidance of Undercutting and Pointing

The developed approach is based on the same considerations that have been represented in section 2.4. The final results of the concluded investigation are formulated as follows:

1. Undercutting by a rack-cutter may occur only for the generated convex profile gear and does not occur for the concave profile pinion. Undercutting may be avoided by limitations of the active part of the rack-cutter addendum. Function $h_a P_n(N_2)$ is represented in figure 3.3.1 by curve 1.

2. Pointing may occur for a gear with a small number of teeth. Curve 2 in figure 3.3.1 shows function $h_d P_n(N_2)$ where h_d is the active part of the rack-cutter dedendum. The curve has been determined under the condition that the tooth thickness on the gear addendum circle be chosen as $t_a = (0.3/P_n)$.

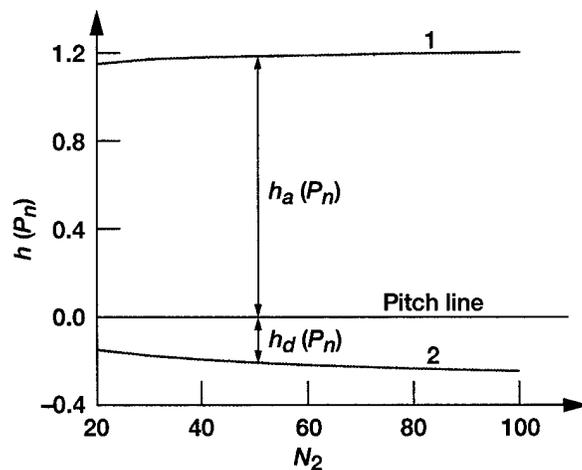


Figure 3.3.1.—Permissible dimensions of rack-cutter addendum h_a and dedendum h_d .

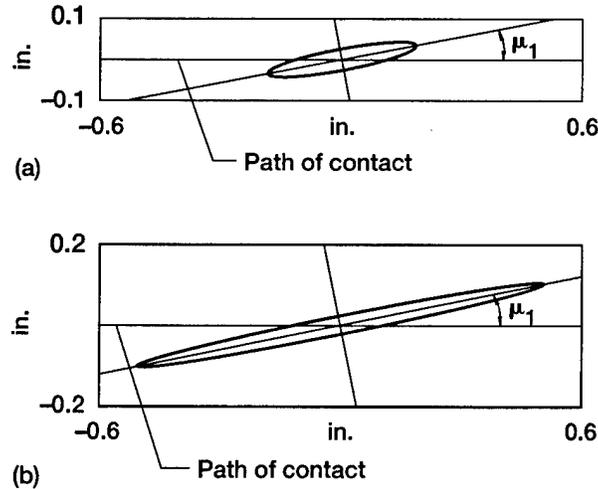


Figure 3.4.1.—Contact ellipse on pinion tooth surfaces.
 (a) Concave pinion tooth surface. (b) Convex pinion tooth surface.

The whole active tooth height for a gear with tooth number $N_2 \geq 70$ is

$$h = h_a + h_d = \frac{1.4}{P_n} \quad (3.3.1)$$

Note that we have $h = (1.8/P_n)$ in the case of the pinion convex-gear concave design that is obtained in section 2.0. The reduction of tooth height in the second version is a disadvantage of the pinion concave-gear convex design.

3.4 Contact Ellipse

Applying the approach discussed in 2.5 and 2.6, we have obtained the pinion and gear principal curvatures and directions and then have determined the dimensions and orientation of the instantaneous contact ellipse. The numerical computations have been obtained for both designed versions of helical gears and then were compared. The design parameters are the same as those applied in section 2.0. The obtained contact ellipses for both versions are shown in figure 3.4.1. It is evident that because of the decrease in the contact ellipse, the second version of the design cannot be recommended for application. The preferable design version is the pinion convex-gear concave type of surface contact.

4.0 GENERATION OF DOUBLE-CROWNED PINION TOOTH SURFACE BY GRINDING DISK

4.1 Research Goals and Developed Approaches

In sections 2.0 and 3.0, profile crowning of pinion-gear tooth surfaces Σ_1 and Σ_2 was shown to be sufficient only for the localization of bearing contact. If crowning is accomplished in the profile direction only, misalignment of the gear drive will cause almost linear discontinuous functions of transmission errors (see curve *a* in figure 1.8 and figs. 2.8.3 and 2.8.4). Then, high vibration of the gear drive becomes inevitable. To avoid such a defect, the authors have proposed the following methods for crowning:

1. Profile and longitudinal crowning is applied for pinion generation. Profile crowning is based on the mismatch of imaginary rack-cutter surfaces used to derive theoretical pinion-gear tooth surfaces. Longitudinal crowning of the pinion tooth surface is achieved by tool plunging. The tool may be (a) a grinding (or a cutting) disk or (b) a grinding worm (a hob).

2. Only profile crowning is applied for gear generation, which is achieved by the mismatch of imaginary rack-cutter surfaces as mentioned above.

This section covers the (1) generation of the pinion tooth surface by a plunging disk; (2) generation of the pinion tooth surface by a plunging worm; and (3) TCA for aligned and misaligned gear drives.

4.2 Generation of Pinion Tooth Surface by Plunging Disk

The proposed method for the generation is a modification of the existing method of form grinding and is based on the following considerations.

1. Consider initially that the pinion tooth surface Σ_1 is a helicoid determined as the envelope to the imaginary rack-cutter surface Σ_c . Surface Σ_1 is represented by vector function $\mathbf{r}_1(u_c, \psi_1)$ (see 2.2).

2. Then determine surface Σ_d of the shaped disk, considering as given the pinion tooth surface Σ_1 (refs. 5 and 7). The axes of the pinion and the disk are crossed and the installment of the disk with respect to the pinion is shown in figure A1 of appendix A. The disk surface Σ_d is determined as the envelope to the family of pinion tooth surfaces. Figure 4.2.1 shows the cross-sectional profile of the grinding disk.

3. Consider at this stage that surface Σ_d of the grinding disk is given and that the grinding disk performs a screw motion and is plunged with respect to the pinion. It is obvious that surface Σ_d will generate a modified pinion tooth surface Σ_p as the envelope to the family of surfaces Σ_d of the grinding disk.

Detailed derivations are presented in appendixes A and B.

The meshing and contact of pinion-gear tooth surfaces generated as proposed above have been tested by the TCA method, and the results are presented in section 5.5.

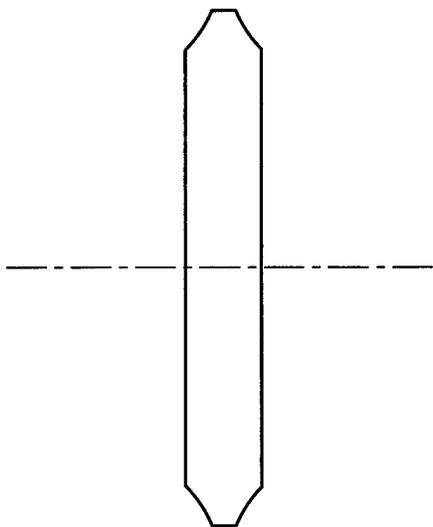


Figure 4.2.1.—Cross-sectional profile of grinding disk.

APPENDIX A
DETERMINATION OF SURFACE Σ_d OF GENERATING DISK

Introduction

Recall that the derivation of the pinion tooth surface generated by a plunging disk is divided into following stages (see 4.2):

1. Determination of disk surface $\Sigma_d(u_d, \theta_d)$ that is conjugated to the profile-crowned pinion tooth surface $\Sigma_1(u_c, \psi_1)$, which is considered a helicoid.
2. Determination of pinion tooth surface $\Sigma_1(u_d, \theta_d)$ generated by disk surface $\Sigma_d(u_d, \theta_d)$ that is plunged during the process generation.

Stages 1 and 2 of the derivations are presented in appendixes A and B.

Algorithm for Computation of Surface Σ_d

The derivation of Σ_d is based on the following procedure.

Step 1.—Apply three fixed coordinate systems S_1 , S_d , and S_F . Coordinate systems S_1 and S_d are rigidly connected to the pinion and the disk (figs. A.1 and 2). Coordinate system S_F is an auxiliary fixed coordinate system. The drawings of figures A.1 and 2 illustrate the applied coordinate systems in orthogonal projections and in three-dimensional space. The need for three coordinate systems and the reason they are considered as fixed is discussed in the following derivations.

Step 2.—The installment of the disk with respect to the pinion is defined by the shortest distance E_d and the crossing angle γ_d . The shortest distance E_d is determined by

$$E_d = R_o + r_{1d} \quad (A1)$$

where R_o is the outer radius of the grinding disk and r_{1d} is the dedendum radius of the pinion.

The crossing angle γ_d between the axes of rotation of the grinding disk and of the pinion is identical to the lead angle λ_{p1} .

Step 3.—The pinion tooth surface Σ_1 and its normal N_1 are represented in coordinate system S_1 by (sec. 2.2)

$$\mathbf{r}_1 = \mathbf{r}_1(u_c, \psi_1) \quad (A2)$$

$$\mathbf{N}_1 = \mathbf{N}_1(u_c, \psi_1) \quad (A3)$$

where (u_c, ψ_1) are the surface parameters.

Equations (A2) and (A3) are obtained for the case when axis x_1 is the tooth axis of symmetry (fig. A.3(a)). The grinding disk generates the pinion space and therefore we need the pinion tooth surface equations with axis x_1 as the axis of symmetry of space (fig. A.3(b)). This can be achieved by turning the pinion through angle

$$\theta_1 = \frac{\pi}{N_1} \quad (A4)$$

where $2\pi/N_1$ is the pinion pitch angle. Using coordinate transformation, the pinion tooth surface and its normal may be represented now by vector equations

$$\mathbf{r}_1 = \mathbf{r}_1(u_c, \psi_1 + \theta_1) \quad (A5)$$

$$\mathbf{N}_1 = \mathbf{N}_1(u_c, \psi_1 + \theta_1) \quad (A6)$$

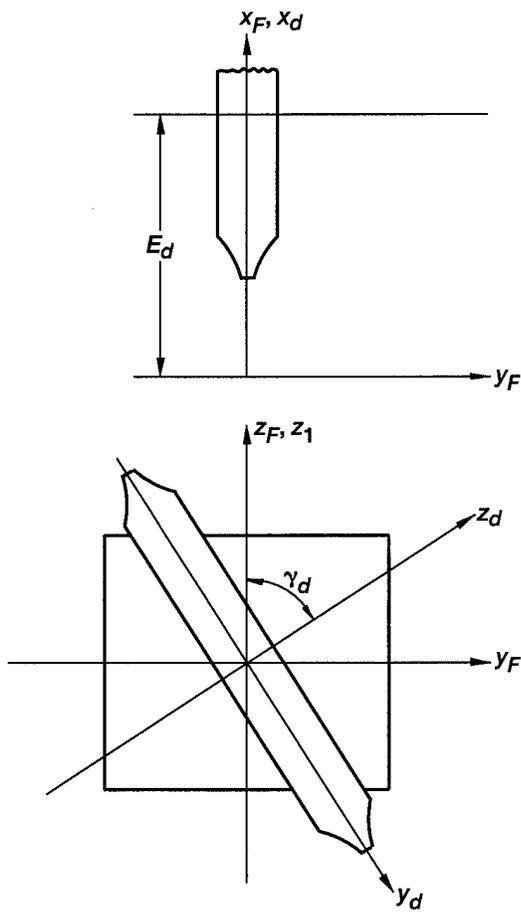


Figure A.1.—Installment of grinding disk.

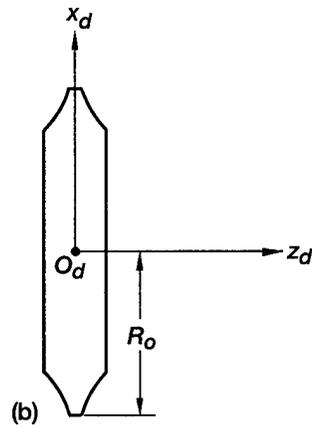
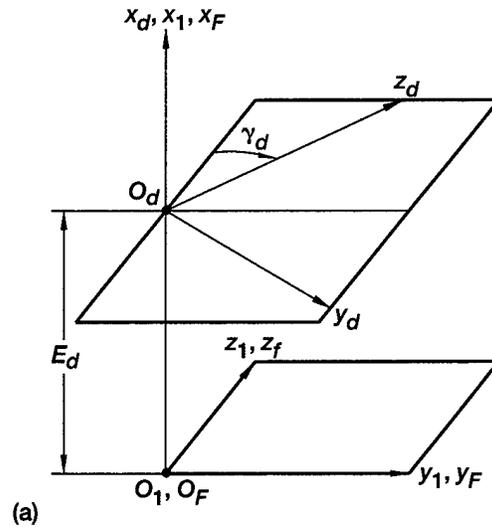


Figure A.2.—Coordinate systems applied for derivation of Σ_d . (a) Coordinate systems. (b) Disk axial section.

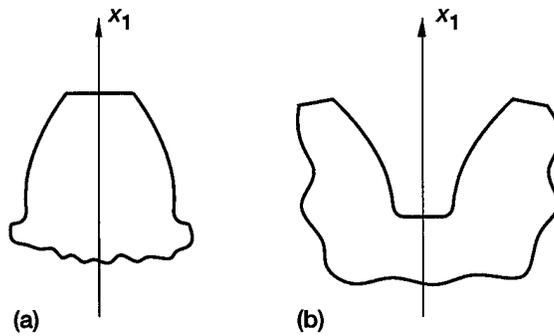


Figure A.3.—Orientation of axis of symmetry of (a) tooth and (b) space.

Step 4.—Our next goal is to determine on surface Σ_1 the instantaneous line of tangency of surfaces Σ_1 and Σ_d . This can be accomplished considering that the normal \mathbf{N}_1 to Σ_1 at any point of tangency of Σ_1 and Σ_d must pass through the grinding disk axis (refs. 5 and 7). This requirement, which follows from the condition that the disk surface be a surface of revolution, is represented by equations (refs. 5 and 7)

$$\frac{X_1 - x_1(u_c, \psi_1)}{N_{x_1}(u_c, \psi_1)} = \frac{Y_1 - y_1(u_c, \psi_1)}{N_{y_1}(u_c, \psi_1)} = \frac{Z_1 - z_1(u_c, \psi_1)}{N_{z_1}(u_c, \psi_1)} \quad (\text{A } 7)$$

where (x_1, y_1, z_1) and $(N_{x_1}, N_{y_1}, N_{z_1})$ are the point coordinates and the components of \mathbf{N}_1 at a current point on Σ_1 ; X_1, Y_1, Z_1 are the coordinates of the point of intersection of normal \mathbf{N}_1 to surface Σ_1 with the disk axis. Here, for the case when a left-hand pinion is generated (figs. A.4, 1, and 2), we have

$$X_1 = E_d, \quad \frac{Y_1}{Z_1} = \tan \gamma_d \quad (\text{A } 8)$$

In the case of a left-hand helicoid, we have (refs. 5 and 7)

$$y_1 N_{x_1} - x_1 N_{y_1} = -p N_{z_1} \quad (\text{A } 9)$$

Equations (A7) to (A9) yield the relation

$$f_{d_1}(u_c, \psi_1) = (E_d - x_1 + p_1 \cot \gamma_d) N_{z_1} - E_d \cot \gamma_d N_{y_1} + z_1 N_{x_1} = 0 \quad (\text{A } 10)$$

Equation $f_{d_1} = 0$ may be called the equation of meshing of surfaces Σ_1 and Σ_d .

The line of tangency of Σ_1 and Σ_d is determined by applying simultaneously equations (A5), (A6), and (A10). The same equations determine the line of tangency of Σ_1 and Σ_d in coordinate system S_F because coordinate systems S_1 and S_F coincide with each other (figs. A.1 and 2).

Step 5.—The line of tangency between surfaces Σ_1 and Σ_d is determined in coordinate system S_d by

$$\mathbf{r}_d(u_c, \psi_1) = \mathbf{M}_{dF} \mathbf{r}_F(u_c, \psi_1), \quad \mathbf{N}_d(u_c, \psi_1) = \mathbf{L}_{dF} \mathbf{N}_F(u_c, \psi_1), \quad f_{dF}(u_c, \psi_1) = 0 \quad (\text{A } 11)$$

where $\mathbf{r}_F(u_c, \psi_1) \equiv \mathbf{r}_1(u_c, \psi_1 + \theta_1)$, $\mathbf{N}_F(u_c, \psi_1) \equiv \mathbf{N}_1(u_c, \psi_1 + \theta_1)$, $f_{dF}(u_c, \psi_1) \equiv f_{d1}(u_c, \psi_1) = 0$.

Step 6.—The next goal is to determine the axial profile of the grinding surface Σ_d . Equations (A11) enable us to determine the coordinates of the current point M of the line of tangency of Σ_d and Σ_1 by equations

$$x_d = x_d(u_c, \psi_1), \quad y_d = y_d(u_c, \psi_1), \quad z_d = z_d(u_c, \psi_1), \quad f_{dF}(u_c, \psi_1) = 0 \quad (\text{A } 12)$$

The axial profile of the grinding disk (fig. A.5) is determined by

$$x_d^{(M)} = -\rho = -(x_d^2, y_d^2)^{0.5}, \quad z_d^{(M)}(u_c, \psi_1), \quad f_{dF}(u_c, \psi_1) = 0 \quad (\text{A } 13)$$

The disk surface $\Sigma_d(u_d, \theta_d)$ may be formed by rotating the axial profile about the disk axis; parameter θ_d is the current angle of rotation of the axial profile.

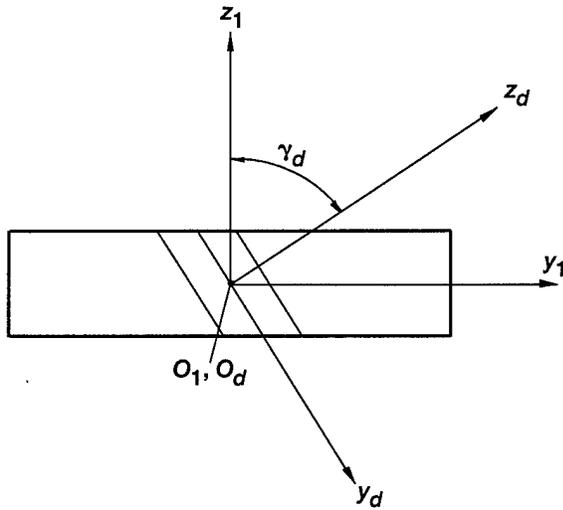


Figure A.4.—Orientation of coordinate system S_d with respect to S_1 or a left-hand pinion.

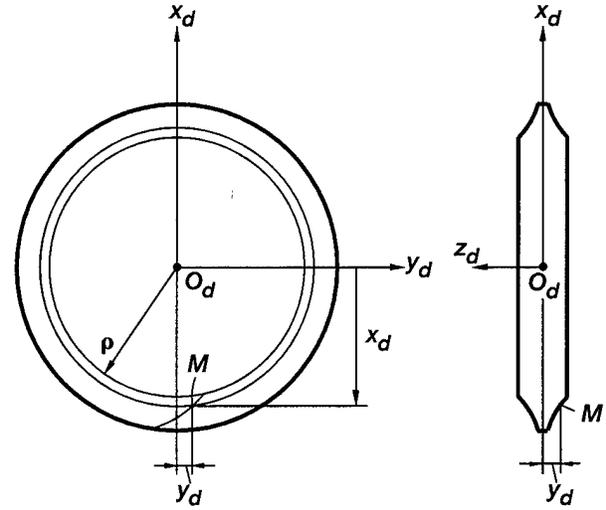


Figure A.5.—Derivation of axial profile of grinding disk.

Determination of Crossing Angle γ_d

The determination of crossing angle γ_d must satisfy the following requirements:

1. The line of tangency between Σ_d and Σ_1 has to contain point Q of the tangency of the pinion rack-cutter and the pinion tooth surface in their common normal section (fig. 4.1.1). Recall that point Q is simultaneously the point of tangency of pinion-gear tooth surfaces for an aligned gear drive. This requirement is satisfied with pinion surface parameter $u_c = 0$.

2. The normal to the pinion tooth surface should not only intersect the axis of the grinding disk but pass through a point of the pinion tooth surface Σ_1 that belongs to plane $z_F = 0$.

These two requirements yield the following equations in two unknowns, ψ_1 and γ_d :

$$z_F^{(1)}(u_c, \psi_1) \equiv z_F^{(1)}(0, \psi_1) = 0 \quad (\text{A14})$$

$$f_{d1}(u_c, \psi_1) \equiv f_{d1}(0, \psi_1) = [E_d - x_F^{(1)}(0, \psi_1) + p_1 \cot \gamma_d] N_{zF}^{(1)}(0, \psi_1) - E_d \cot \gamma_d N_{yF}^{(1)}(0, \psi_1) = 0 \quad (\text{A15})$$

where (A15) is the transformed equation of meshing.

The final equation for the determination of γ_d is

$$\cot \gamma_d = \frac{[E_d - x_F^{(1)}(0, \psi_1^*)] N_{zF}^{(1)}(0, \psi_1^*)}{E_d N_{yF}^{(1)}(0, \psi_1^*) - p_1 N_{zF}^{(1)}(0, \psi_1^*)} \quad (\text{A16})$$

where ψ_1^* is determined from

$$z_F^{(1)}(0, \psi_1^*) = 0 \quad (\text{A17})$$

APPENDIX B
COMPUTERIZED GENERATION OF PINION TOOTH SURFACE BY PLUNGING DISK

We designate the pinion tooth surface generated by the plunging disk as $\Sigma_1(\psi_1, \psi_p)$ to differentiate it from surface $\Sigma_1(u_c, \psi_1)$. Recall that $\Sigma_1(u_c, \psi_1)$ is a profile-crowned pinion surface whereas $\Sigma_1(\psi_1, \psi_p)$ is the pinion surface crowned in the profile and longitudinal directions. The longitudinal crowning is provided by the plunge of the grinding disk.

For the derivation of $\Sigma_1(\psi_1, \psi_p)$, we apply two coordinate systems: S_n , the fixed, and S_p , the movable, which is rigidly connected to the pinion (fig. B.1). The derivation of pinion surface $\Sigma_1(\psi_1, \psi_p)$ is based on the following considerations:

1. In appendix A, the line of tangency of profile-crowned pinion tooth surface $\Sigma_1(u_c, \psi_1)$ and the grinding disk surface Σ_d has been determined. This line of tangency is represented in S_n by

$$\mathbf{r}_n^{(1)} = \mathbf{r}_n^{(1)}(u_c, \psi_1), \quad f_{d1}(u_c, \psi_1) = 0 \quad (\text{B1})$$

where $\mathbf{r}_n^{(1)}(u_c, \psi_1) \equiv \mathbf{r}_1(u_c, \psi_1 + \theta_1)$ (see eq. (A5)), and $f_{d1} = 0$ is the equation of meshing represented by (A10).

2. Coordinate system S_n and the grinding disk are held at rest while coordinate system S_p performs a screw motion with the pinion and in addition is plunged with respect to S_n . The plunge is provided to the pinion instead of the disk. Figure B.1 shows the screw motion of a left-hand pinion and the components of this motion are (a) displacement $l = p_1\psi_p$, where p_1 is the pinion screw parameter, and (b) rotation through angle ψ_p . Additionally provided is the plunge displacement $\Delta E_d(\psi_p)$ of the pinion in the direction of the shortest distance where

$$\Delta E_d(\psi_p) = a_{pd} [l(\psi_p)]^2 = a_{pd} (p_1\psi_p)^2 \quad (\text{B2})$$

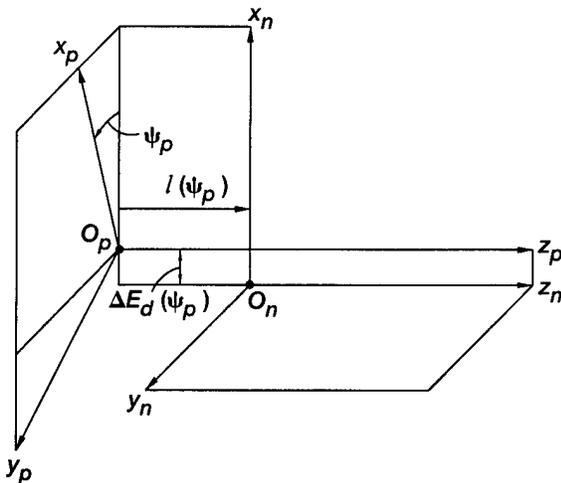


Figure B.1.—Coordinate systems applied for derivation of pinion surface Σ_1 .

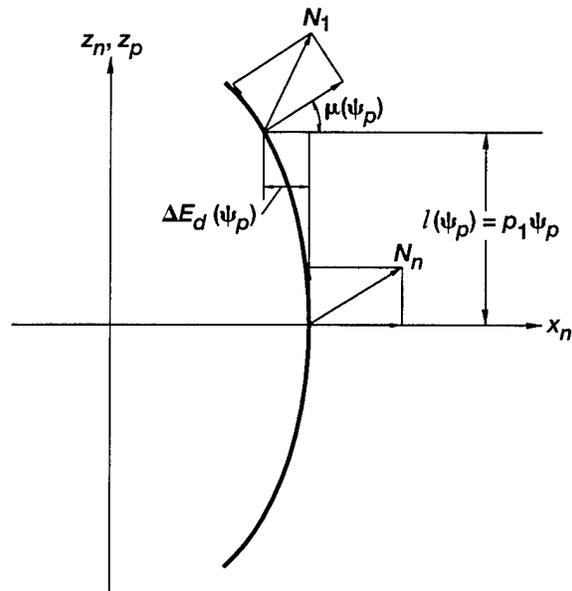


Figure B.2.—Determination of normal to generated pinion tooth surface Σ_1 .

The pinion-generated surface is determined as the family of spatial lines generated in the S_p coordinate system while the pinion performs the motions described above. Surface Σ_1 is represented by

$$\mathbf{r}_1(u_c, \psi_1, \psi_p) = \mathbf{M}_{pn}(\psi_p) \mathbf{r}_n(u_c, \psi_1), \quad f_{dn}(u_c, \psi_1) = 0 \quad (\text{B3})$$

where $f_{dn}(u_c, \psi_1) \equiv f_{dF}(u_c, \psi_1) \equiv f_{d1}(u_c, \psi_1) = 0$.

Here (fig. B.1)

$$\mathbf{M}_{pn}(\psi_p) = \begin{bmatrix} \cos \psi_p & \sin \psi_p & 0 & -\Delta E_d(\psi_p) \cos \psi_p \\ -\sin \psi_p & \cos \psi_p & 0 & \Delta E_d(\psi_p) \sin \psi_p \\ 0 & 0 & 1 & l(\psi_p) \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (\text{B4})$$

Consider that surface Σ_1 is represented by vector function

$$\mathbf{r}_1[u_c(\psi_1), \psi_1, \psi_p] \equiv \mathbf{r}_1(\psi_1, \psi_p) \quad (\text{B5})$$

Function $u_c(\psi_1)$ can be determined using the equation of meshing $f_{d1} = 0$ (see eq. (A10)).

Then, determine the normal to $\Sigma_1(\psi_1, \psi_p)$

$$\mathbf{N}_1(\psi_1, \psi_p) = \frac{\partial \mathbf{r}_1}{\partial \psi_1} \times \frac{\partial \mathbf{r}_1}{\partial \psi_p} \quad (\text{B6})$$

where

$$\frac{\partial \mathbf{r}_1}{\partial \psi_1} = \frac{\partial \mathbf{r}_1}{\partial u_c} \frac{d u_c}{d \psi_1} + \frac{\partial \mathbf{r}_1}{\partial \psi_1} \quad (\text{B7})$$

A simplified approach to the derivation of normal \mathbf{N}_1 to surface $\Sigma_1(\psi_1, \psi_p)$ is based on the following considerations:

1. The initial position of the common normal \mathbf{N}_n (fig. B2) to surface Σ_1 and the grinding disk surface Σ_d is determined in coordinate system S_n by equation (A3) as

$$\mathbf{N}_n(u_c, \psi_1) \equiv \mathbf{N}_1(u_c, \psi_1), \quad f_{dn}(u_c, \psi_1) = 0 \quad (\text{B8})$$

2. In the grinding process, the normal performs in coordinate system S_p two motions simultaneously: (a) rotation about the pinion axis of angle ψ_p (fig. B1) and (b) rotation about the y_n -axis of angle $\mu(\psi_p)$ (fig. B2) determined by

$$\tan[\mu(\psi_p)] = \frac{d[\Delta E_d(\psi_p)]}{d[l(\psi_p)]} = 2a_{pd} P_1 \psi_p \quad (\text{B9})$$

Then normal \mathbf{N}_1 can be determined as

$$\mathbf{N}_1(u_c, \psi_1, \psi_p) = \mathbf{L}_{pn}(\psi_p) \mathbf{L}_n[\mu(\psi_p)] \mathbf{N}_n(u_c, \psi_1) \quad (\text{B10})$$

where $\mathbf{L}_{pn}(\psi_p)$ is the 3×3 submatrix of matrix $\mathbf{M}_{pn}(\psi_p)$ (see eq. (B4)) and \mathbf{L}_n can be determined as

$$\mathbf{L}_n[\mu(\psi_p)] = \begin{bmatrix} \cos \mu & 0 & -\sin \mu \\ 0 & 1 & 0 \\ \sin \mu & 0 & \cos \mu \end{bmatrix} \quad (\text{B11})$$

Parameters u_c and ψ_1 are related by the equation of meshing (A10).

5.0 GENERATION OF PINION TOOTH SURFACE BY PLUNGING OF GRINDING WORM

5.1 Introduction

The generation of a pinion (gear) by a grinding worm (hob) must be considered as a two-parameter enveloping process in which the related motions of the worm and the workpiece are represented by two independent groups. One of these two groups includes the related rotations of the worm and the workpiece. The other group is referred to as the feed motion provided in the direction of the workpiece.

In our case, the workpiece is the pinion and the longitudinal crowning is provided by the plunging of the worm with respect to the pinion in the direction of the shortest distance.

5.2 Installment, Related Motions, and Applied Coordinate Systems

Derivation of crossing angle.—Consider that a left-hand pinion is generated by a left-hand hob (grinding worm). It is more favorable for cutting conditions if the pinion and hob helices are in the same direction. The drawings of figure 5.2.1 show a left-hand hob (fig. 5.2.1(a)) and its installment with respect to a left-hand pinion (fig. 5.2.1(b)). It can be easily verified from the drawings that the crossing angle γ_w is determined as

$$\gamma_w = 90^\circ - \beta_p - \lambda_w \quad (5.2.1)$$

where β_p is the pinion helix angle and λ_w is the worm lead angle.

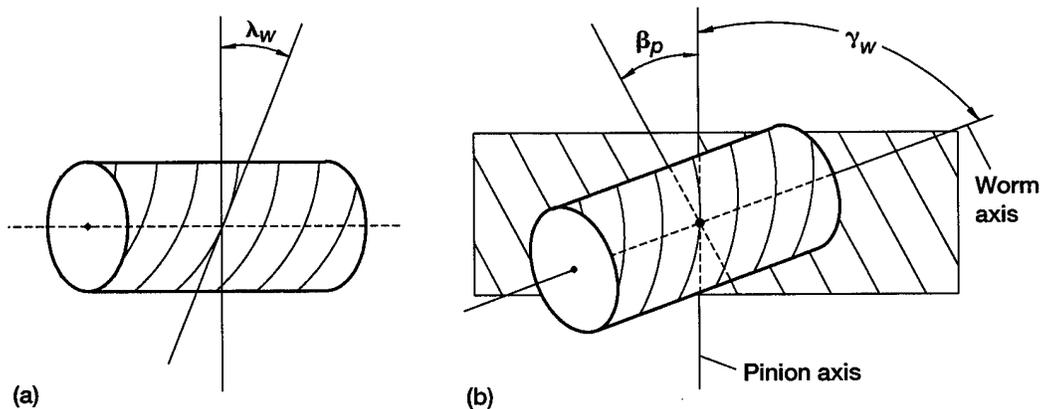


Figure 5.2.1.—Derivation of crossing angle γ_w between pinion and worm axes. (a) Left-hand worm with lead angle λ_w . (b) Installment of worm with respect to pinion.

Related motions performed during feed motion.—Figure 5.2.2 shows two positions of the worm axis when the feed motion along the pinion axis is provided. The relative motion of the worm surface with respect to the pinion surface during the feed motion must be provided along the pinion screw surface, and therefore an additional translational motion of the worm (perpendicular to the pinion axis) determined as $l_w \tan \beta_p$ must be provided.

Axial worm translational motion.—A conventional method for generating spur and helical gears by a worm is based on the requirement that the piecework and the worm perform related rotations about their axes. However, for the purpose of simplifying the derivations, the rotation of the worm can be substituted by its translational motion in the axial direction. The following derivations are based on the consideration that the worm and the pinion being generated are simultaneously in mesh with the same rack that generated the pinion.

Figure 5.2.3 shows the velocity polygon during the meshing process of the worm and the rack. The axial displacement of the worm may be represented in two components: $s_w \cos \lambda_w$ and $s_w \sin \lambda_w$ that are directed perpendicular to the tangent $t-t$ to the helix and along the helix. Similarly, the displacement of the rack may be represented

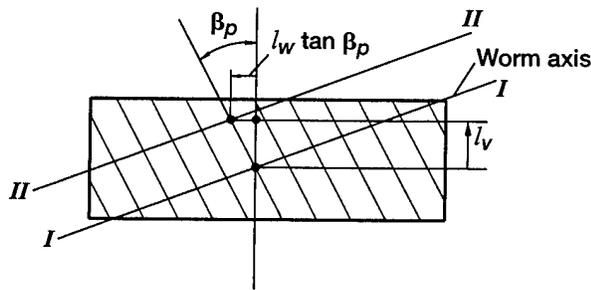


Figure 5.2.2.—Components of translational motion of worm performed during feed motion.

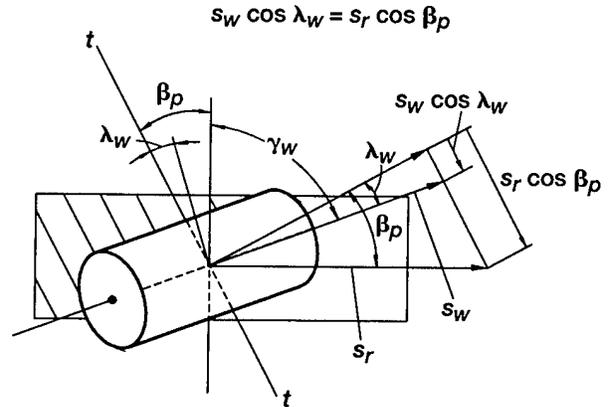


Figure 5.2.3.—Derivation of relations between axial displacement of worm and angle of rotation of pinion.

in normal and tangential components $s_r \cos \beta_p$ and $s_r \sin \beta_p$. The normal components of the worm and rack displacements must be equal. Therefore, we have

$$s_w \cos \lambda_w = s_r \cos \beta_p \quad (5.2.2)$$

The tangential components $s_w \sin \lambda_w$ and $s_r \sin \beta_p$ are not equal, which indicates sliding of the worm and rack surfaces. The displacement s_r of the rack and the angle of pinion rotation are related by

$$s_r = r_p \Psi_p \quad (5.2.3)$$

Finally, we obtain the following relations between the axial displacement s_w of the worm and the angle of gear rotation

$$s_w = \frac{r_p \cos \beta_p}{\cos \lambda_w} \Psi_p = m \Psi_p \quad (5.2.4)$$

Applied coordinate systems.—Movable coordinate systems S_w and S_p are rigidly connected to the worm and the pinion; S_m is the fixed coordinate system (fig. 5.2.4). Pinion axis z_p coincides with the z_m -axis. The pinion and worm axes form the crossing angle γ_w . Planes Π and $x_m = 0$ are parallel to the plane that is tangent to the pitch cylinders of the pinion, and the gear worm axis z_w lies in plane Π . The shortest distance between planes Π and $x_m = 0$ is varied in the generation process because of the plunging of the worm with respect to the pinion. The location of origin O_w of coordinate system S_w is represented in plane Π by vectors \overline{AB} and $\overline{BO_w}$, where

$$\overline{AB} = -l_w \tan \beta_p \mathbf{j}_m + l_w \mathbf{k}_m \quad (5.2.5)$$

$$\overline{BO_w} = s_w (\sin \gamma_w \mathbf{j}_m + \cos \gamma_w \mathbf{k}_m) \quad (5.2.6)$$

5.3 Generation of Pinion Surface Σ_p

Worm surface.—The worm surface is determined as the envelope to the family of rack-cutter surfaces as discussed in section 2.0. The worm design parameters are

1. The normal diametral pitch, the same as the pinion normal diametral pitch

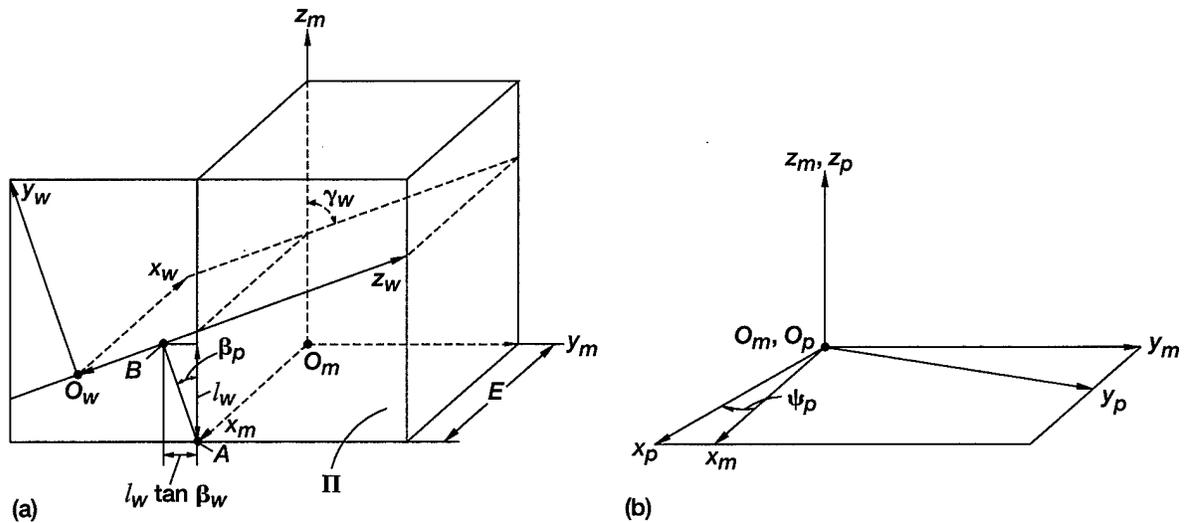


Figure 5.2.4.—Coordinate systems applied for generation of pinion by worm. (a) S_m and S_w . (b) S_m and S_p .

2. The worm thread number N_w (usually, $N_w = 1$)
3. The worm pitch radius r_{pw}

The worm lead angle is determined as

$$\lambda_w = \arcsin \left(\frac{N_w}{2P_n r_{pw}} \right) \quad (5.3.1)$$

The worm surface is represented by vector function $\mathbf{r}_w(u_w, \psi_w)$, which is similar to vector function $\mathbf{r}_1(u_c, \psi_1)$ (see eq. (2.2.6)).

Parameters of two-enveloping generation of pinion.—Surface Σ_p is the envelope to the two-parameter family of worm surfaces Σ_w , which is (the family) represented in S_p . The independent parameters of motion are (1) the angle of pinion rotation ψ_p and (2) the worm displacement l_w in feed motion. The worm axial displacement s_w depends on parameter ψ_p and other worm displacements depend on parameter l_w .

The tangential displacement of the worm determined as $(AB)\mathbf{j}_m$ substitutes an additional angle of pinion rotation $\Delta\psi_p^*$ that occurs in the real machine process and is determined as

$$\Delta\psi_p^* = \frac{l_w \tan \beta}{r_p} \quad (5.3.2)$$

The shortest distance E between the worm and pinion axis is

$$E(l_w) = E_o - a_l l_w^2 \quad (5.3.3)$$

The axial worm displacement s_w is a function of parameter ψ_p (see eq. (5.2.4)).

Generation of worm family surfaces.—The family of worm thread surfaces is represented in S_p by matrix equation

$$\mathbf{R}_p(u_w, \psi_w, l_w, \psi_p) + \mathbf{M}_{pm}\mathbf{M}_{mw}\mathbf{r}_w(u_w, \psi_w) \quad (5.3.4)$$

Here (fig. 5.2.4)

$$\mathbf{M}_{pm} = \begin{bmatrix} \cos \psi_p & -\sin \psi_p & 0 & 0 \\ \sin \psi_p & \cos \psi_p & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (5.3.5)$$

$$\mathbf{M}_{mw} = \begin{bmatrix} -1 & 0 & 0 & (\overline{O_w O_m}) \cdot \mathbf{i}_w \\ 0 & -\cos \gamma_w & \sin \gamma_w & (\overline{O_w O_m}) \cdot \mathbf{j}_w \\ 0 & \sin \gamma_w & \cos \gamma_w & (\overline{O_w O_m}) \cdot \mathbf{k}_w \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (5.3.6)$$

$$\left. \begin{aligned} (\overline{O_w O_m}) \cdot \mathbf{i}_w &= E_o - a_l l_w^2 = E_{xm} \\ (\overline{O_w O_m}) \cdot \mathbf{j}_w &= -l_w \tan \beta - m \psi_p \sin \gamma_w = E_{ym} \\ (\overline{O_w O_m}) \cdot \mathbf{k}_w &= l_w - m \psi_p \cos \gamma_w = E_{zm} \end{aligned} \right\} \quad (5.3.7)$$

Equations of meshing of worm and pinion tooth surfaces.—In the two-parameter enveloping process, apply two equations of meshing (refs. 5 and 7):

$$\mathbf{N}_m^{(w)} \cdot \mathbf{v}_m^{(wp, \psi_p)} = F_1(u_w, \psi_w, \psi_p, l_w) \quad (5.3.8)$$

$$\mathbf{N}_m^{(w)} \cdot \mathbf{v}_m^{(wp, l_w)} = F_2(u_w, \psi_w, \psi_p, l_w) \quad (5.3.9)$$

where subscript m indicates that vectors in equations (5.3.8) and (5.3.9) are represented in coordinate system S_m ; vector $\mathbf{N}_m^{(w)}$ represents the normal to the worm surface; vector $\mathbf{v}_m^{(wp, \psi_p)}$ represents the relative velocity in the motion when parameter ψ_p is varied and parameter l_w is fixed. Similarly, $\mathbf{v}_m^{(wp, l_w)}$ is the relative velocity determined for the conditions when l_w is the variable parameter and ψ_p is fixed.

Equations (5.3.4), (5.3.8), and (5.3.9) represent the pinion tooth surface by four related parameters. The derivation of relative velocities $\mathbf{v}_m^{(wp, \psi_p)}$ and $\mathbf{v}_m^{(wp, l_w)}$ represented in equations (5.3.7) and (5.3.8) is based on the following procedure:

Step 1: Represent the velocity $\mathbf{v}_m^{(wp, \psi_p)}$ as

$$\mathbf{v}_m^{(wp, \psi_p)} = \mathbf{v}_m^{(wp, \psi_p)} - \mathbf{v}_m^{(p, \psi_p)} \quad (5.3.10)$$

and then determine $\mathbf{v}_m^{(w, \psi_p)}$ and $\mathbf{v}_m^{(p, \psi_p)}$.

Step 2: Represent $\mathbf{v}_m^{(p, \psi_p)}$ by

$$\mathbf{v}_m^{(p, \psi_p)} = \omega_m^{(p)} \times \mathbf{r}_m \quad (5.3.11)$$

where

$$\omega_m^{(p)} = [0 \quad 0 \quad 1]^T \quad (5.3.12)$$

taking $|\omega_m^{(p)}| = 1 \text{ rad/sec}$ and \mathbf{r}_m is the 3×1 vector. The 4×1 vector \mathbf{r}_w is determined by matrix equation (see eqs. (5.3.6) and (5.3.7))

$$\mathbf{r}_w = \mathbf{M}_{mw} \mathbf{r}_m = \begin{bmatrix} -x_w + E_{xm} \\ -y_w \cos \gamma_w + z_w \sin \gamma_w + E_{ym} \\ y_w \sin \gamma_w + z_w \cos \gamma_w + E_{zm} \\ 1 \end{bmatrix} \quad (5.3.13)$$

Step 3: Vector $\mathbf{v}_m^{(w, \psi_p)}$ is represented as (see eqs. (5.3.6))

$$\mathbf{v}_m^{(w, \psi_p)} = \begin{bmatrix} 0 \\ \frac{\partial E_{ym}}{\partial \psi_p} \\ \frac{\partial E_{zm}}{\partial \psi_p} \end{bmatrix}^T = [0 \quad m \sin \gamma_w \quad m \cos \gamma_w]^T \quad (5.3.14)$$

Step 4: Equations (5.3.10) to (5.3.14) yield the following expression for $\mathbf{v}_m^{(wp, \psi_p)}$:

$$\mathbf{v}_m^{(wp, \psi_p)} = \begin{bmatrix} E_{ym} - y_w \cos \gamma_w + z_w \sin \gamma_w \\ m \sin \gamma_w - E_{xm} + x_w \\ m \cos \gamma_w \end{bmatrix} \quad (5.3.15)$$

Step 5: The determination of velocity $\mathbf{v}_m^{(wp, l)}$ is based on the following considerations:

a.

$$\mathbf{v}_m^{(wp, l)} = \mathbf{v}_m^{(w, l)} - \mathbf{v}_m^{(p, l)} = \mathbf{v}_m^{(w)} \quad (5.3.16)$$

since $\mathbf{v}_m^{(p, l)} = 0$ (the pinion is considered as being at rest when the feed motion is provided).

b.

$$\mathbf{v}_m^{(w, l)} = \frac{\partial}{\partial l_w} (\overline{O_w O_m}) = [-2a_l l_w - \tan \beta \quad 1]^T \quad (5.3.17)$$

Thus we found both of the relative velocities using the equations of meshing (5.3.8) and (5.3.9). The normal to the worm surface is determined by expression

$$\mathbf{N}_m^{(w)} = \mathbf{L}_{mw} \cdot \mathbf{N}_w(u_w, \psi_w) \quad (5.3.18)$$

where \mathbf{L}_{mw} is the 3×3 submatrix of matrix \mathbf{M}_{mw} (see eq. (5.3.6)). The normal to the worm surface does not depend on the relative motion parameters ψ_p and l_w because the worm performs only translative motion in the fixed coordinate system S_m .

5.4 Relations Between Tool Plunging and Parabolic Function of Transmission Errors

Recall that tool plunging Δs_{pl} and transmission errors $\Delta\phi_2$ are represented by the following parabolic functions:

$$\Delta s_{pl} = a_{pl}l^2 \quad (5.4.1)$$

$$\Delta\phi_2(\phi_1) = a_\phi\phi_1^2 \quad (5.4.2)$$

where a_{pl} (1/in.) and a_ϕ (1/rad) are the parabolic coefficients.

Our investigation resulted in the following approximate equation that relates the parabolic coefficients:

$$a_\phi = \frac{a_{pl}a_{pr} \tan \alpha_n \sin \alpha_n}{a_{pl}m_t^2 \cos^2 \beta + a_{pr}m_w \sin \alpha_n \tan^2 \beta} \frac{N_1^2}{2P_n N_2} \quad (5.4.3)$$

Here

$$a_{pr} = a_c - a_t \quad (5.4.4)$$

where a_c and a_t are the parabolic coefficients for the normal profiles of the rack-cutters (see sec. 2.0) and

$$m_t = 1 - 2a_t l_t \quad (5.4.5)$$

$$m_w = 1 - 2a_{pl}r_{pw} \quad (5.4.6)$$

where r_{pw} is the radius of the worm pitch cylinder.

Errors of alignment cause a shift Δl of the bearing contact as shown in figure 5.4.1. The relation between the error of alignment ($\Delta\lambda$ or $\Delta\gamma$) and the shift (Δl) is represented by

$$\Delta l = \frac{\Delta\lambda m_w}{2a_{pl} \tan \alpha_n \cos \beta} \quad (5.4.7)$$

An effective way to restore the central location of the bearing contact by the correction of the lead (or the lead angle) is by using equation (5.4.7). The advantage of this approach is that the correction of the lead angle will not cause additional transmission errors because a parabolic type of transmission error is predesigned. The reader should recall that a predesigned parabolic function of transmission errors absorbs the almost linear functions of the transmission errors caused by misalignment.

The accuracy of equation (5.4.3) was tested by a computerized simulation of meshing. Curves a and b in figure 5.4.1 represent the parabolic functions of transmissions obtained by TCA and by equation (5.4.3). The simulation of meshing was accomplished for a helical gear drive with a pinion crowned in the profile and longitudinal directions. The following input data were used for the computation: $N_1 = 17$, $N_2 = 77$, $P_n = 5 \text{ in.}^{-1}$, $\beta = 19.95^\circ$, $\alpha_n = 25^\circ$, $a_c = 0.425 \text{ in.}^{-1}$, $a_t = 0.394 \text{ in.}^{-1}$, $a_{pl} = 0.00139 \text{ in.}^{-1}$, $r_{pw} = 3.82 \text{ in.}$ The small difference between curves a and b confirms that equation (5.4.3) may provide sufficient accuracy for the magnitude of a_{pl} when the magnitude of a_ϕ is a given.

A simpler but less accurate equation may be applied as a substitute for equation (5.4.3). The derivation of the proposed equation is based on the following considerations:

Step 1.—We consider initially that the gear teeth are profile crowned, the path of contact is a helix, and the line of action is a straight line that is parallel to the gear axes. Figure 5.4.2(a) shows the transverse profiles in mesh after rotation from the initial position through angle $\phi_1 = \pi/N_1$ and displacements of the point of contact along the line of action on the distance $l = B/2$, where B is the working width of the gear (not shown in this figure).

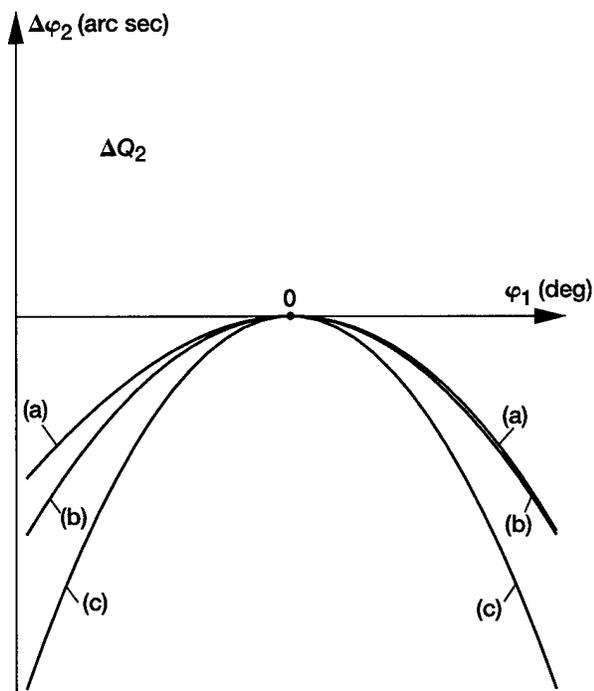


Figure 5.4.1.—Parabolic functions of transmission errors. (a) Obtained by simulation of meshing by TCA. (b) Obtained by approximate equation (5.4.3). (c) Obtained by approximate equation (5.4.12).

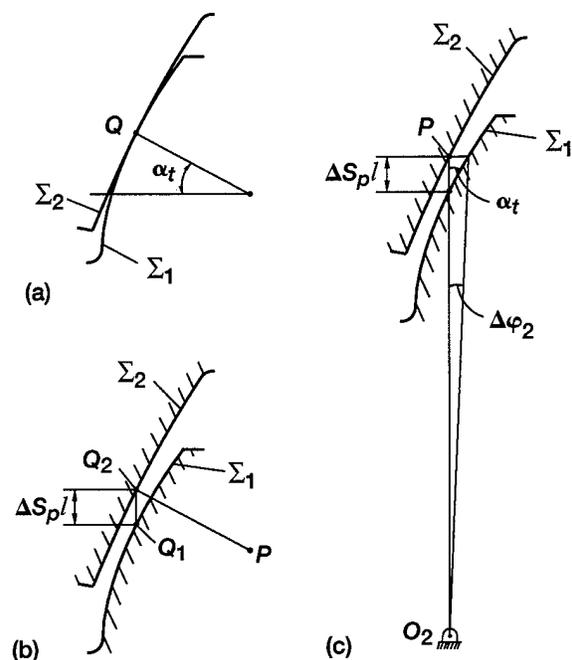


Figure 5.4.2.—Derivation of relation between coefficients of parabolae of transmission and plunging functions. (a) Transverse profiles Σ_1 and Σ_2 in initial meshing. (b) Transverse profiles after plunge of Σ_1 . (c) Representation of Σ_1 and Σ_2 as equidistant profiles.

Step 2.—Figure 5.4.2(b) shows that due to the plunge of transverse profile Σ_1 , there is a backlash between points Q_1 and Q_2 of the transverse profiles determined as

$$\Delta s_{pl} = a_{pl} \left(\frac{B}{2} \right)^2 \quad (5.4.8)$$

Step 3.—For simplification, consider the equidistant transverse profiles (fig. 5.4.2(c)). The backlash Δs_{pl} may be compensated after the turning of profile Σ_2 through angle

$$\Delta \phi_2 = \frac{\Delta s_{pl} \tan \alpha_t}{r_{p2}} \quad (5.4.9)$$

where $\Delta \phi_2$ is the transmission error.

The goal of plunging is to provide a parabolic function of transmission errors:

$$\Delta \phi_2(\phi_1) = a_\phi \phi_1^2 \quad (5.4.10)$$

Step 4.—Figure 5.4.3 shows the development of the helix on the pinion pitch cylinder, where H is the lead. Drawings of the figure yield

$$B = \frac{r_2 2\pi}{N_1 \tan \beta} = \frac{\pi}{P_t \tan \beta} \quad (5.4.11)$$

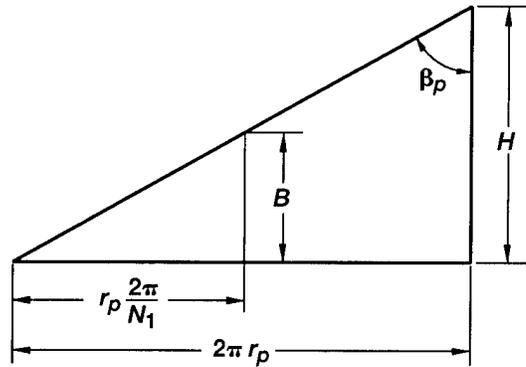


Figure 5.4.3.—Development of helix.

Step 5.—Equations (5.4.8) to (5.4.11), taking $\varphi_1 = \pi/N_1$ in equation (5.4.1), yield the following relation between the coefficients of the parabolic functions of transmission and plunging:

$$a_\varphi = \frac{N_1^2 \tan \alpha_t}{2P_t N_2 \tan^2 \beta_p} a_{pl} = \frac{N_1^2 \tan \alpha_n}{2P_n N_2 \sin^2 \beta_p} a_{pl} \quad (5.4.12)$$

Function $\Delta\varphi_2(\varphi_1)$ determined by equation (5.4.12) is illustrated by curve c in figure 5.4.1.

For the case of a modified pinion ground by a shaped disk, the relations between the coefficients of the parabolic functions of transmission errors and plunging are similar to the relations represented by expressions (5.4.3) or (5.4.12). We have to accept only equivalent coefficients of plunging parabolas for grinding disk a_d and for grinding worm a_{pl} that are related by the following approximate equation:

$$a_d \approx \frac{a_{pl} \sin \alpha_t}{\sin(\alpha_t + \varphi_{10})} \quad (5.4.13)$$

where $\varphi_{10} = \pi/N_1$.

5.5 Tooth Contact Analysis

The conditions of meshing and the contact of gears with the proposed geometry are investigated for an ideal and misaligned gear drive. The results of TCA are presented in the following two cases.

Case 1: pinion generated by grinding disk.—Figures 5.5.1 and 5.5.2 show the almost linear functions of transmission errors caused by errors $\Delta\gamma = 3$ arc min and $\Delta\lambda = 3$ arc min. The magnitude of maximal transmission errors is 40.48 arc sec in both cases. Figure 5.5.3 shows the predesigned parabolic function for an aligned gear drive with the pinion generated by a grinding disk. The magnitude of the maximal transmission error is 11.54 arc sec. Figure 5.5.4 shows the resulting parabolic function of transmission errors when $\Delta\gamma = 3$ arc min; the magnitude of the maximal transmission error is 11.66 arc sec. Figure 5.5.5 shows the resulting parabolic function of transmission errors when $\Delta\lambda = 3$ arc min; the magnitude of the maximal transmission error is 10.11 arc sec.

Case 2: pinion generated by worm.—Figures 5.5.6 and 5.5.7 show the almost linear functions of transmission errors caused by errors $\Delta\gamma = 3$ arc min and $\Delta\lambda = 3$ arc min. The magnitude of maximal transmission errors is 40.48 arc sec in both cases. Figure 5.5.8 shows the predesigned parabolic function for an aligned gear drive with the pinion generated by a worm. The magnitude of the maximal transmission error is 7.21 arc sec. Figure 5.5.9 shows the resulting parabolic function of transmission errors when $\Delta\gamma = 3$ arc min; the magnitude of the maximal transmission error is 8.33 arc sec. Figure 5.5.10 shows the resulting parabolic function of transmission errors when $\Delta\lambda = 3$ arc min; the magnitude of the maximal transmission error is 5.41 arc sec.

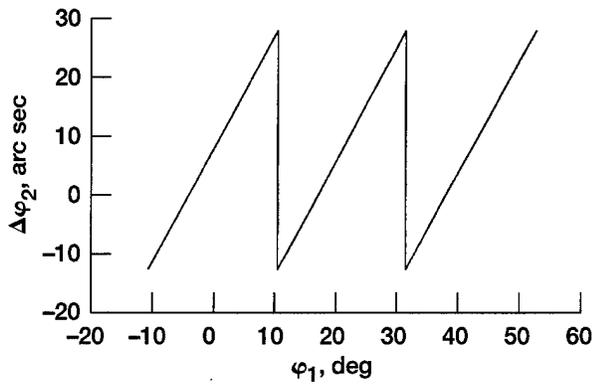


Figure 5.5.1.—Function of transmission errors of gear drive with pinion generated by grinding disk. Change in shaft angle $\Delta\gamma = 3$ arc min.

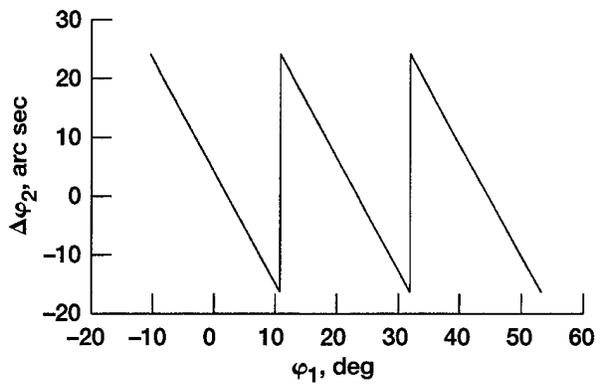


Figure 5.5.2.—Function of transmission errors of gear drive with pinion generated by grinding disk. Change in lead angle $\Delta\lambda = 3$ arc min.

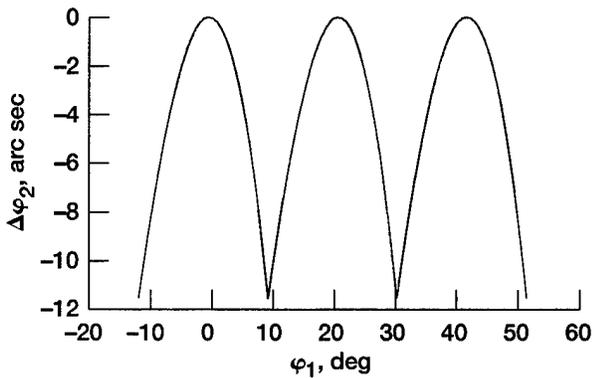


Figure 5.5.3.—Predesigned parabolic function for gear drive with pinion generated by grinding disk.

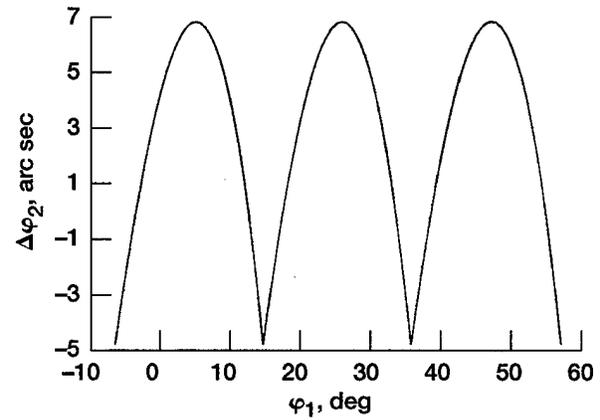


Figure 5.5.4.—Resulting function of transmission errors obtained for following conditions: pinion generated by a grinding disk; change in shaft angle $\Delta\gamma =$ arc min.

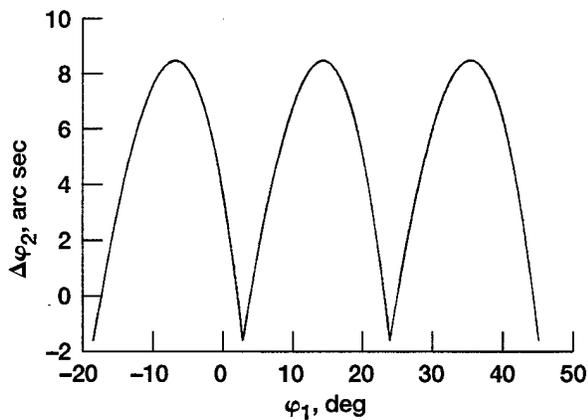


Figure 5.5.5.—Resulting function of transmission errors obtained for following conditions: pinion generated by a grinding disk; change in lead angle $\Delta\lambda =$ arc min.

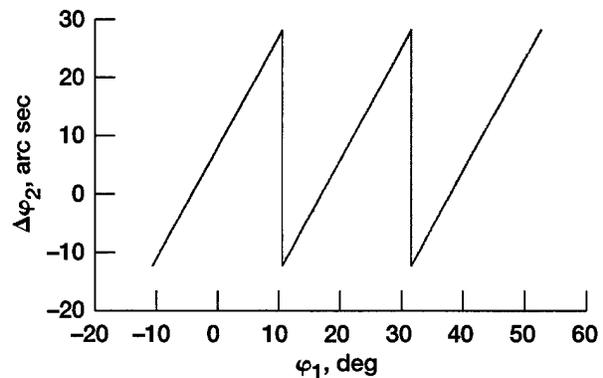


Figure 5.5.6.—Function of transmission errors of gear drive with pinion generated by worm; change in shaft angle $\Delta\gamma = 3$ arc min.

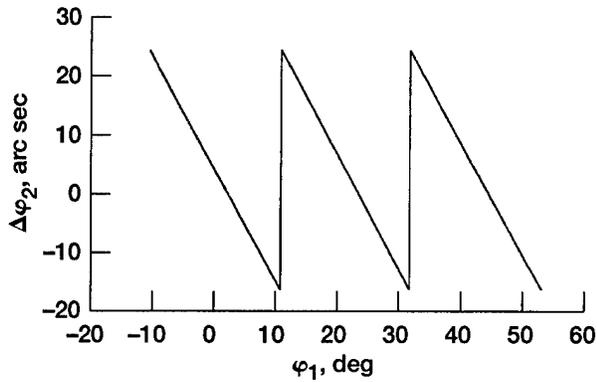


Figure 5.5.7.—Function of transmission errors of gear drive with pinion generated by worm; change in lead angle $\Delta\gamma = 3$ arc min.

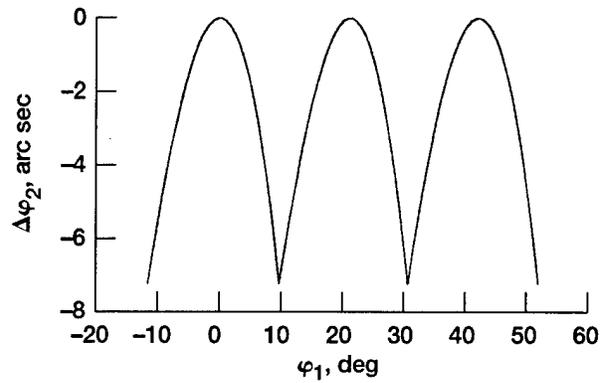


Figure 5.5.8.—Predesigned parabolic function for gear drive with pinion generated by worm.

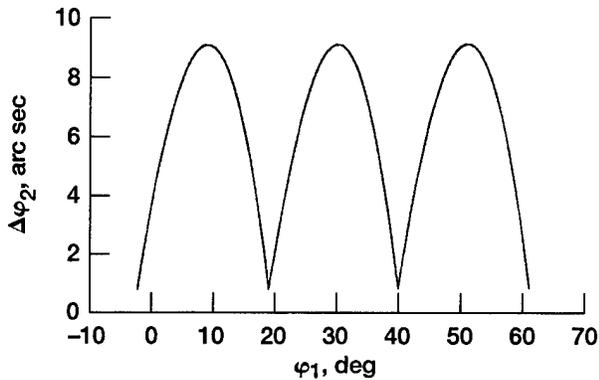


Figure 5.5.9.—Resulting function of transmission errors obtained for following conditions: pinion generated by worm; change in shaft angle $\Delta\gamma =$ arc min.

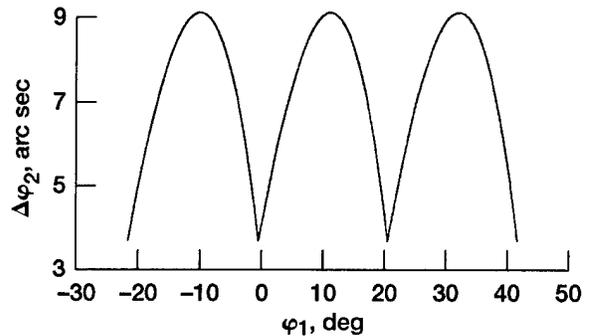


Figure 5.5.10.—Resulting function of transmission errors obtained for following conditions: pinion generated by worm; change in lead angle $\Delta\lambda = 3$ arc min.

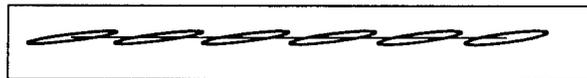


Figure 5.5.11.—Contact ellipses on pinion tooth surface.

The completed computations have confirmed in both cases that the plunging of the tool provides a parabolic function of transmission errors and such a function absorbs transmission errors caused by misalignment. Figure 5.5.11 shows the contact ellipses on the pinion tooth surface.

APPENDIX C
DERIVATION OF GRINDING WORM THREAD SURFACE

The generation of the worm thread surface Σ_w is based on the following idea: The worm is a helicoid and is generated by an imaginary rack-cutter Σ_r having the same normal section as the rack-cutter Σ_c that is applied for the generation of the pinion.

The derivation of Σ_w is based on this procedure:

Step 1.—Apply movable coordinate systems S_r and S_w that are rigidly connected to the imaginary rack-cutter and the worm. The fixed coordinate system S_n is rigidly connected to the housing of the generating machine.

Step 2.—The rack-cutter Σ_r has skew teeth determined by angle β_r (fig. C.1), which is correlated with the worm lead angle λ_w . The rack-cutter surface is generated in S_r while the coordinate system S_b with the normal profile of the rack-cutter performs a translational motion along the direction of the skew rack-cutter teeth (along the y_b -axis).

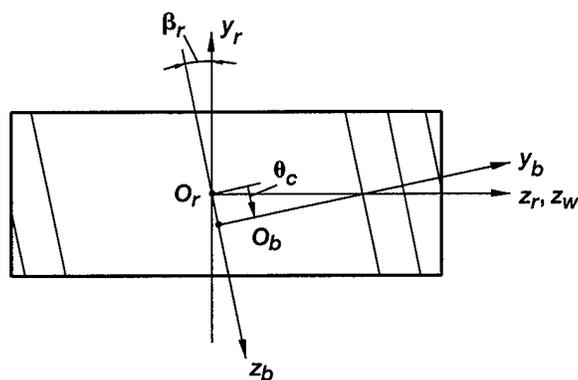


Figure C.1.—Skew rack-cutter Σ_r used for worm generation.

Step 3.—Figure C.2 shows the installment of the left-hand worm with respect to rack-cutter Σ_r . It is obvious that axes z_b and z_w form the angle $90^\circ - \lambda_w$ and $\beta_r = \lambda_w$.

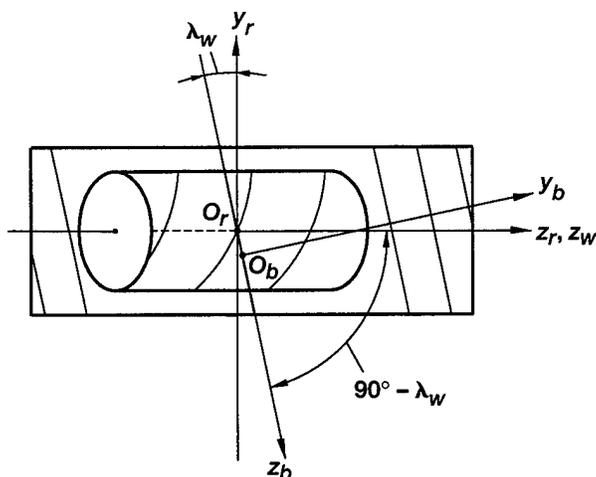


Figure C.2.—Installment of worm with respect to rack-cutter.

Step 4.—During the worm generation process, the rack-cutter performs translation S_r while the worm rotates through angle ψ_w , (fig. C.3), where

$$s_r = r_{pw} \psi_w \quad (C1)$$

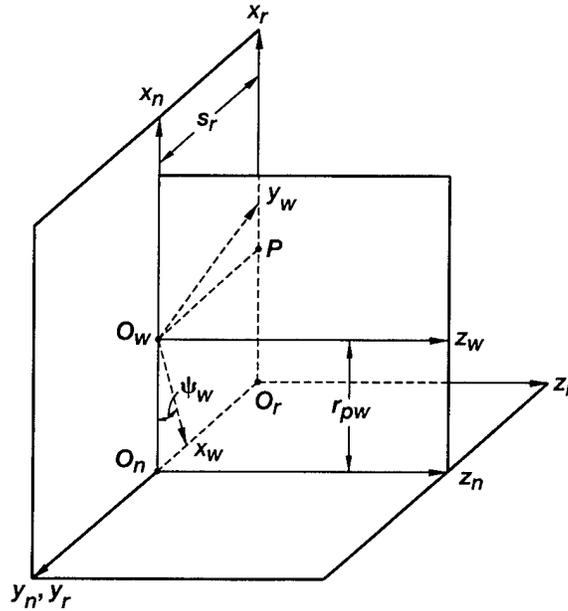


Figure C.3.—Applied coordinate systems for grinding worm and pinion.

Step 5.—The family of rack-cutter surfaces generated in S_w is represented by the matrix equation (fig. C.3)

$$\mathbf{r}_w(u_c, \theta_c, \psi_w) = \mathbf{M}_{wn} \mathbf{M}_{nr} \mathbf{M}_{rb} \mathbf{r}_b(u_c) \quad (C2)$$

where (see eq. (2.2.2))

$$\mathbf{r}_b(u_c) = \mathbf{M}_{ba} \mathbf{r}_a(u_c) \quad (C3)$$

Here

$$\mathbf{M}_{wn}(\psi_w) = \begin{bmatrix} -\cos \psi_w & -\sin \psi_w & 0 & r_{pw} \cos \psi_w \\ \sin \psi_w & -\cos \psi_w & 0 & -r_{pw} \sin \psi_w \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (C4)$$

$$\mathbf{M}_{nr}(\psi_w) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & -r_{pw} \psi_w \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (C5)$$

$$\mathbf{M}_{rb}(\theta_c) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \sin \lambda_w & -\cos \lambda_w & -\theta_c \cos \lambda_w \\ 0 & \cos \lambda_w & \sin \lambda_w & \theta_c \sin \lambda_w \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (\text{C6})$$

Step 6.—The worm thread surface is the envelope to the family of surfaces $\mathbf{r}_w(u_c, \theta_c, \psi_w)$. To determine the envelope, apply the theorem (refs. 5 and 7) that the common normal to surfaces Σ_w and Σ_r passes through the instantaneous axis of rotation that coincides with the z_n -axis.

Then we obtain

$$\frac{X_r - x_r}{N_{xr}} = \frac{Y_r - y_r}{N_{yr}} = \frac{Z_r - z_r}{N_{zr}} \quad (\text{C7})$$

where (fig. C4) $X_r = 0$, $Y_r = -s_r = -r_{pw}\psi_w$, Z_r are the coordinates of a current point of the instantaneous axis of rotation; \mathbf{N}_r is the normal to rack-cutter surface Σ_r determined as

$$\mathbf{N}_r = \mathbf{L}_{rb}\mathbf{L}_{ba}\mathbf{N}_a \quad (\text{C8})$$

where (see fig. 2.1.2(b))

$$\mathbf{N}_a = [-2a_c u_c \quad 1 \quad 0]^T \quad (\text{C9})$$

The first equation of the system of equations (C7) yields

$$x_r - \frac{(r_{pw}\psi_w + y_r)N_{xr}}{N_{yr}} = f(u_c, \theta_c, \psi_w) = 0 \quad (\text{C10})$$

Equations (C2) and (C10) represent the worm surface in three-parameter form. Equation (C10) is linear with respect to ψ_w and θ_c . Therefore θ_c can be represented by $\theta_c(u_c, \psi_w)$. Using this relation in equation (C2), the worm surface may be determined in two-parameter form as

$$\mathbf{r}_w(u_c, \psi_w) = \mathbf{M}_{wn}(\psi_w)\mathbf{M}_{nr}(\psi_w)\mathbf{M}_{rb}(\psi_w)\mathbf{r}_b(u_c) \quad (\text{C11})$$

6.0 COMPARISON OF THREE TYPES OF NOVIKOV-WILDHABER HELICAL GEARS

6.1 Introduction

The purpose of this section is to summarize the advantages and disadvantages of three types of Novikov-Wildhaber helical gears that will serve as directions for designers and manufacturers. For this purpose, section 6.2 will cover the following items:

1. Comparison of normal sections of rack-cutters used for generation
2. Description of existing and proposed methods for generation
3. Evaluation of the influence of errors of alignment on transmission errors and the shift of the bearing contact
4. Comparison of the dimensions of contact ellipses
5. Perspectives for the substitution of conventional involute helical gears by Novikov-Wildhaber helical gears

6.2 Description and Comparison of Three Types of Novikov-Wildhaber Gears

Three versions of Novikov-Wildhaber gears are compared with (a) circular-arc profiles of rack-cutters, one zone of meshing, and a very small (0.5 percent) difference between the curvature radii of the rack-cutters (refs. 1 and 2); (b) circular-arc profiles of rack-cutters and two zones of meshing in accordance with Russian and Chinese standards (refs. 3 and 4); and (c) parabolic profiles of rack-cutters (proposed by the authors of this completed project).

Input data.—The results of a numerical computation performed for the three versions are based on the following input data:

Normal diametral pitch, P_n , in. ⁻¹	5
Pinion-gear teeth numbers	
N_1	17
N_2	77
Shortest center distance, E , in.	10
Pitch helix angle, β , deg	19.548
Normal pressure angle, α_n , deg	
Versions 1 and 2	27
Version 3	25

Profiles of rack-cutters.—The normal profiles of rack-cutters for three versions of the design are presented in figure 6.2.1.

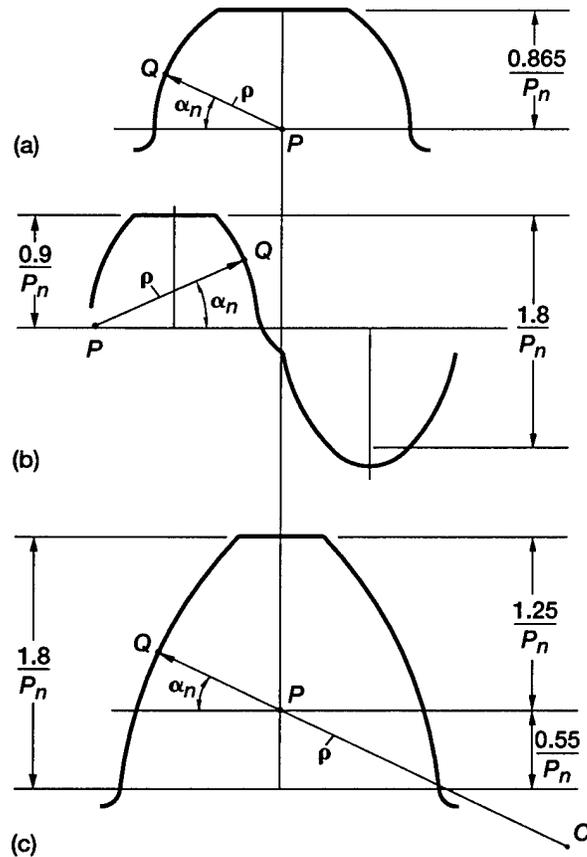


Figure 6.2.1.—Profiles of rack-cutters for generating pinion tooth. (a) Version 1. (b) Version 2. (c) Version 3.

Versions 1 and 2 have circular-arc profiles. The centers of circular arcs that generate convex tooth addendums of the pinion (in both versions) and the gear (in version 2) are located on pitch straight lines of the rack-cutters.

In version 3, the normal profiles are mismatched parabolic curves instead of circular arcs. In addition, the curvature radii of the parabolic curves are much larger than the distance QP between the designed point of tangency Q and the pitch point P .

The normal curvature radii of the rack-cutters that generate the pinion and gear teeth are presented in table 6.2.1.

TABLE 6.2.1—NORMAL CURVATURE RADI OF RACK-CUTTERS

Version	Pinion, in.	Gear, in.
1	0.200	0.201
2	.230 (.258)	.258 (.230)
3	1.176	1.270

*For design 2, the upper (lower) values correspond to pinion addendum (dedendum) and gear dedendum (addendum).

Table 6.2.1 shows that design version 3 provides much larger curvature radii and therefore the tooth shape is more favorable.

The reader is reminded that the application of parabolic profiles of rack-cutters and the enlargement of the curvature radii allow one to increase the height of the pinion addendum, which is limited by tooth pointing, and the height of the pinion dedendum, which is limited by the possibility of undercutting.

The dimensionless heights of the active parts of the addendum $h_a P_n$ and the dedendum $h_d P_n$ of rack-cutters that generate the pinion teeth are shown in table 6.2.2, which gives data for three versions of the design.

TABLE 6.2.2.—RACK-CUTTER TOOTH ELEMENT PROPORTIONS

Version	Dimensionless heights of		
	Addendum, $h_a P_n$	Dedendum, $h_d P_n$	Total height, $h P_n$
1	0.00	0.87	0.87
2	.90	.90	1.80
3	.55	1.25	1.80

Table 6.2.2 shows that the parabolic rack-cutter (design version 3 with one zone of meshing) has the same tooth height as that of the circular-arc rack-cutter (design version 2 with two zones of meshing):

$$h = h_a + h_d = \frac{1.8}{P_n} \quad (6.2.1)$$

Another important advantage of the developed gearing is the possibility of increasing the tooth thickness at the point of tangency of the active profile with the fillet. We may expect that this will allow designers to reduce the bending stresses, but this is a subject of further investigation.

Another advantage of the developed gearing (design version 3) is the possibility of reducing the sensitivity of the gear drive to the change ΔE of the center distance. Table 6.2.3 presents for all three versions the influence of ΔE on the following parameters:

1. δ_α : the normal pressure angle variation caused by the increase of $\Delta E = 0.0001$ mm of center distance E
2. δ_1 : the ratio of the contact point shift over the pinion tooth profile to the tooth active height

Values δ_α and δ_1 have been determined twice by approximate formulas presented in section 2.0 and by the application of TCA in section 3.0.

The data of table 6.2.3 show that

1. The original version 1 of Novikov-Wildhaber gears is not applicable in a real design because of a high sensitivity to the change of center distance.
2. Version 3 is less sensitive to error ΔE in comparison with version 2 and therefore is preferable.

TABLE 6.2.3—SENSITIVITY TO CHANGE OF THE CENTER DISTANCE ΔE

Version	δ_α , deg	δ_1
1	19.50	0.383
2	2.28	0.051
3	0.68	0.038

Contact ellipses and their orientation.—The contact ellipses and their orientation with respect to the tangent of the contact path (determined by angle μ_1) are shown in figure 6.2.2. The parameters of the contact ellipse axes for three versions of the design are presented in table 6.2.4.

TABLE 6.2.4.—PARAMETERS OF CONTACT ELLIPSE
[All values are determined for elastic approach,
 $\delta = 0.00025$ in.]

Version	Major axis, $2a$, in.	Minor axis, $2b$, in.	Area, F_1 , in. ²
1	0.285	0.237	0.053
2	.237	.065	.012
3	1.034	.045	.037

Figure 6.2.2. and table 6.2.4 show that “ideal” version 1 has the most favorable contact ellipse parameters. However, as mentioned in the previous paragraphs, this version cannot be applied in practice because of the high sensitivity to the change ΔE of the center distance. This defect requires that the difference of curvature radii be increased as was foreseen in version 2. Therefore, the area of the contact ellipse in version 1 is decreased by more than four times.

The proposed design version 3 has a contact ellipse area three times larger than the standard version 2. We may expect that this will substantially decrease the contact stresses. Therefore, we consider that version 3 has a great advantage in comparison with the existing Novikov-Wildhaber gear designs.

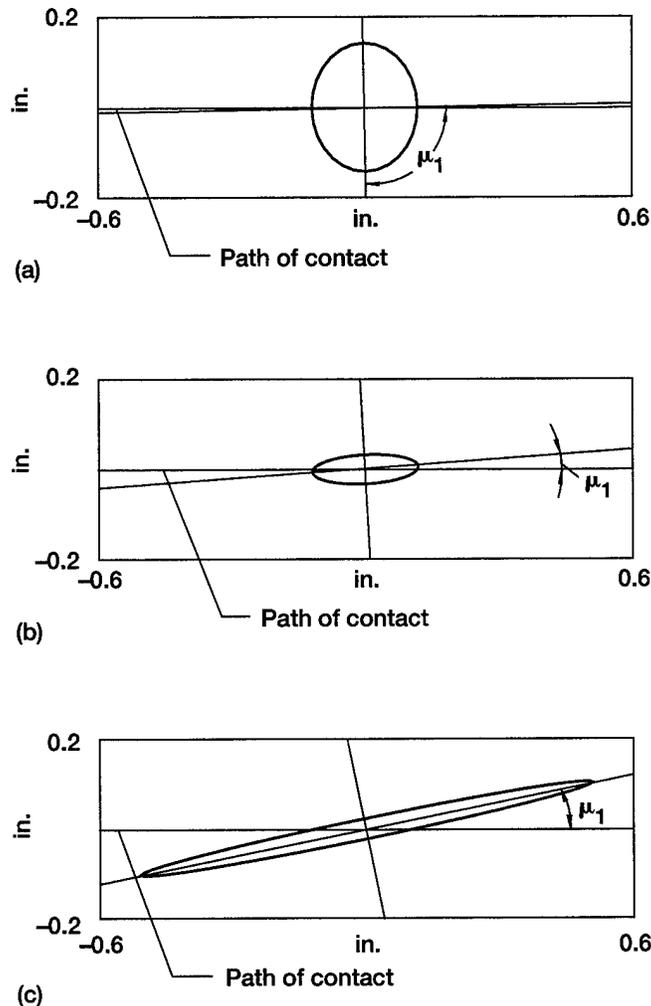


Figure 6.2.2.—Contact ellipses on pinion tooth surface.
 (a) Version 1. (b) Version 2. (c) Version 3.

6.3 Methods of Generation in Industrial Application

Gears of designs 1 and 2 can be manufactured only by hobbing. Helical gears of the new design (version 3) can be ground as proposed by a shaped grinding disk or by a grinding worm.

Presently, gears of designs 1 and 2 are applied to avoid the surface hardening that follows grinding. A good bearing contact for such versions of the design is achieved by running the gear drives in the housing. Therefore, helical gear designs 1 and 2 cannot compete with widely used conventional involute helical gears for which surface hardening is achieved by carbonizing and nitriding after grinding. Thus, Novikov-Wildhaber gears are not applied yet in high-power and high-speed reducers. The new type of helical gears (design 3) developed in this project is free of the disadvantages of existing Novikov-Wildhaber gears since the gear tooth surfaces can be hardened and ground.

The greatest disadvantage of design versions 1 and 2 is that only profile crowning of tooth surfaces is provided. This means that in these two cases only localization of bearing contact can be achieved, but the gear drives are very sensitive to misalignment and noise. The gear drive vibration is inevitable.

The newly developed gearing (design 3) is free of the disadvantages mentioned in the previous paragraph because the design and manufacture of the gear drives are based on a combination of profile and longitudinal crowning. It was shown in sections 4.0 and 5.0 that such crowning makes it possible to obtain a favorable shape of transmission error function, reduce the level of transmission errors, and as a result, reduce the noise and vibration.

7.0 CONCLUSION

A new geometry for Novikov-Wildhaber helical gears was developed, and contact stresses were reduced as a result of the contact of convex-concave gear tooth surfaces.

The conjugation of gear tooth surfaces with profile crowning was achieved by applying two rack-cutters with parabolic profiles in the normal section. In addition, crowning in the longitudinal direction provides a predesigned parabolic function of transmission errors. This type of transmission error enables the design to absorb linear function errors caused by misalignment and to reduce the noise and vibration.

Methods of generating tooth surfaces by worm grinding, form grinding, and hobbing were developed.

Computerized simulation of meshing and contact was performed and a respective computer program for the investigation of transmission errors and the shift of the bearing contact was also developed. The output of the computer program confirmed the accuracy of the proposed approaches reported herein.

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REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE October 2000	3. REPORT TYPE AND DATES COVERED Final Contractor Report	
4. TITLE AND SUBTITLE Computerized Generation and Simulation of Meshing and Contact of New Type of Novikov-Wildhaber Helical Gears			5. FUNDING NUMBERS WU-581-30-13-00 NAG3-1992 IL162211A47A	
6. AUTHOR(S) Faydor L. Litvin, Pin-Hao Feng, and Sergei A. Lagutin				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) The University of Illinois at Chicago Chicago, Illinois 60607			8. PERFORMING ORGANIZATION REPORT NUMBER E-12039	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration Washington, DC 20546-0001 and U.S. Army Research Laboratory Adelphi, Maryland 20783-1145			10. SPONSORING/MONITORING AGENCY REPORT NUMBER NASA CR-2000-209415 ARL-CR-428	
11. SUPPLEMENTARY NOTES Project Manager, Robert Handschuh, U.S. Army Research Laboratory, Structures and Acoustics Division, NASA Glenn Research Center, organization code 5950 (0300), 216-433-3969.				
12a. DISTRIBUTION/AVAILABILITY STATEMENT Unclassified - Unlimited Subject Category: 37 Available electronically at http://gltrs.grc.nasa.gov/GLTRS This publication is available from the NASA Center for AeroSpace Information, (301) 621-0390.			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) In this report, we propose a new geometry for low-noise, increased-strength helical gears of the Novikov-Wildhaber type. Contact stresses are reduced as a result of their convex-concave gear tooth surfaces. The gear tooth surfaces are crowned in the profile direction to localize bearing contact and in the longitudinal direction to obtain a parabolic function of transmission errors. Such a function results in the reduction of noise and vibrations. Methods for the generation of the proposed gear tooth surfaces by grinding and hobbing are considered, and a tooth contact analysis (TCA) computer program to simulate meshing and contact is applied. The report also investigates the influence of misalignment on transmission errors and shift of bearing contact. Numerical examples to illustrate the developed approaches are proposed. The proposed geometry was patented by Ford/UIC (Serial Number 09-340-824, pending) on June 28, 1999.				
14. SUBJECT TERMS Geometry; Gears; Helical; Novikov; Wildhaber			15. NUMBER OF PAGES 55	
			16. PRICE CODE A04	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT	