Development of a Thermal and Structural Analysis Procedure for Cooled Radial Turbines

Ganesh N. Kumar  
*Sverdrup Technology, Inc.*  
*NASA Lewis Research Center Group*  
*Cleveland, Ohio*

and

Russell G. DeAnna  
*Propulsion Directorate*  
*U.S. Army Aviation Research and Technology Activity—AVSCOM*  
*Lewis Research Center*  
*Cleveland, Ohio*

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ABSTRACT

A procedure for computing the rotor temperature and stress distributions in a cooled radial turbine is considered. Existing codes for modeling the external mainstream flow and the internal cooling flow are used to compute boundary conditions for the heat transfer and stress analyses. An inviscid, quasi three-dimensional code computes the external free stream velocity. The external velocity is then used in a boundary layer analysis to compute the external heat transfer coefficients. Coolant temperatures are computed by a viscous one-dimensional internal flow code for the momentum and energy equation. These boundary conditions are input to a three-dimensional heat conduction code for calculation of rotor temperatures. The rotor stress distribution may be determined for the given thermal, pressure and centrifugal loading. The procedure is applied to a cooled radial turbine which will be tested at the NASA Lewis Research Center. Representative results from this case are included.

INTRODUCTION

Increasing the turbine-inlet temperature is the most lucrative approach to improving thermal efficiency and specific thrust of gas turbines. However, this practice is limited by the availability of materials which can withstand these high temperatures. Current materials cannot be exposed to temperatures above 1250 K without a dramatic decrease in life [1]. Blades must be cooled if significantly higher turbine inlet temperatures are desired. Mainstream air diverted from the compressor exit is used to cool the turbine. This reduces the thermal efficiency of the system. Therefore, minimizing the cooling air stream is an important task in gas turbine design. Cooled axial flow turbines have traditionally been used in these engines.

In small engines, the radial turbine has several inherent advantages over the axial turbine. Normally, the work extracted and efficiency level of two axial stages can be achieved by a single radial stage. This leads to a reduction in overall engine complexity, length, and weight. These attributes have resulted in the widespread use of uncooled radial turbines in automotive turbochargers and auxiliary power units. The radial turbine has not been used as a primary power source — where high temperatures and pressures are desired — because of the difficulties associated with fabrication of the internal cooling passages. Most of these fabrication barriers have been resolved to the point where it is feasible to design an engine with a cooled radial turbine.

Several programs have looked at the fabrication and performance of small cooled radial turbines. The first major attempt at an internally cooled radial turbine rotor was initiated under the U.S. Army in 1968 [2,3]. The turbine was designed for a 2300 F turbine inlet temperature a 2300 ft/sec tip speed, a pressure ratio of 5:1, and a corrected specific work of 40 Btu/lbm. The design required 33% of engine airflow for rotor blade cooling and achieved a total efficiency of 87.5%. Although this design clearly displayed the radial turbines advantage, the fabrication of test hardware was met with problems. In 1977 the Army sponsored a radial turbine program with the objective of providing and demonstrating the technology required to economically manufacture a cooled high temperature radial turbine [4,5]. One approach used photo etched laminates bonded together to form a complete wheel. The other approach used a cast airfoil shell diffusion bonded to a powder melt disk. Both programs showed promising results.

An important step in the design of a cooled turbine is the knowledge of the temperature and stress distribution throughout the rotor. As prototype experiments are usually extremely expensive, there is a great need for theoretical prediction methods [1]. A computational procedure has been developed by the authors to assist in the analysis and design of a cooled radial turbine. This procedure predicts the three-dimensional rotor temperature and stress distribution for a given set of operating conditions. The method
uses a quasi three-dimensional inviscid code in conjunction with a boundary layer code to compute the external blade surface heat transfer coefficients. Co coolant passage heat transfer coefficients and coolant temperatures are computed by a viscous one-dimensional internal flow code. A three-dimensional heat conduction code uses these results to compute the rotor temperature distribution. A detailed stress analysis can also be requested.

To minimize the time and effort required for complete analysis, the entire procedure is automated. Once the procedure is started, it will go through each step of the procedure in the appropriate sequence, iterating between solutions until convergence is achieved.

ANALYSIS PROCEDURE

Four main codes are linked into a procedure to compute the steady-state rotor temperature and stress distributions. The four codes are: MERID, TSONIC/STANS, CPFHA, SINDA and NASTRAN.

The three-dimensional code MERID [10] is used to compute the external heat transfer coefficients along streamlines on both the suction and pressure surfaces [6,7,8]. MERID is used to compute the one-dimensional heat transfer coefficients from hub to shroud. TSONIC uses each of these streamlines to determine the flow conditions on a surface between two blades. Stacking these surfaces from hub to shroud produces a quasi three-dimensional solution. MERID and TSONIC are steady state, inviscid, two-dimensional codes applicable to a perfect gas.

The inviscid blade surface velocities from the MERID/TSONIC combination form the input to STANS. These are used as external flow velocities in the boundary layer analysis. STANS uses these velocities to compute a two-dimensional boundary layer along each streamline. The calculated heat transfer coefficients are used as boundary conditions in the conduction analysis. The free stream velocities must be "smoothed" if STANS predicts regions of separated flow.

CPFHA (Coolant Passage Flow with Rotation and Heat Addition) is used for computing the internal coolant temperature, pressure and heat transfer coefficients along the coolant flow path [9]. It integrates the one-dimensional momentum and energy equations along a path. The equations account for area change, rotation, friction and heat addition. Flow splits cannot be determined with this code. The internal cooling passages that can be accommodated in the procedure include plain passages, finned passages, trip strips, pin fins, tip cap impingement, etc. The coolant passage wall temperature distribution and coolant inlet conditions are a required input. Thus, an iterative process between CPFHA and the heat conduction code must be used since the wall temperature distribution is not known a priori.

The heat conduction code SINDA (Systems Improved Numerical Differencing Analyzer) [10] is used in the analysis procedure to perform detailed three-dimensional heat transfer analysis of the rotor. A wedge consisting of one blade and the corresponding disk region is analyzed.

Based on the converged temperature distribution in the rotor, the MERID/TSONIC external pressure distribution, and the CPFHA internal coolant passage pressure distribution, a NASTRAN [11] structural analysis of the rotor is performed. From this analysis, nodal displacement and stress distributions and modal shapes of the rotor are obtained. The above procedure is based on the method developed by Christie, et al, [12].

MODEL GENERATION

NASTRAN Model

Based on nodal points along the streamlines of the blade suction and pressure surfaces, the disk geometry and the coolant passages geometry input data, a NASTRAN model of the blade and the associated disk is created by the code RITICN [13]. The data generated by this code can be used to:

1. Perform NASTRAN structural analysis on the blade and the disk.
2. Provide two of the six input files required by the code SMAN4 [14]. The code SMAN4 converts the NASTRAN model of RITICN to SINDA model for thermal analysis.
3. Provide plate and solid-element NASTRAN modeling, which when combined with RELACT temperature output provides input to the PATRAN 3-D color graphics plotting routines.

This preprocessing program generates the grid point and element connectivity data for a COSMIC/MSC NASTRAN finite element grid of a radial inflow turbine rotor with internally cooled blades. The grid generated by this program consists of one blade and the associated sector of the rotor disk. The NASTRAN cyclic symmetry feature is employed for structural analysis, thus requiring the above as sufficient to model the entire rotor.

The basic turbine model generated employs a hollow blade which is modeled with triangular plate elements and a disk sector which is modeled with brick elements. Blade halves are attached to the disk using rigid elements. Along the blade tip, along the leading edge, and in the scallop region, the blade halves are tied together with quadrilateral plate elements. The exhaust end of the blade halves is open. The sides of the rotor hub are "tied" together (CYJOIN) for utilization of the NASTRAN cyclic symmetry feature. All of the above is automatically generated by the program. The user has great flexibility in generating a wide range of models due to the number of user specified input variables. A typical model is depicted in Figure 1. The user may generate additional elements manually for the NASTRAN deck to model features which may be unique to a given concept/design (e.g. pins, Laffles, ribs, etc. internal to the blade halves (skins)).

SINDA Model

The SINDA model consists of nodes and conductors which provide a lumped parameter representation of the turbine rotor and its thermal boundary conditions. Nodes and conductors are generated along the streamlines, nodal lines, and in the tangential direction following an order similar to that used in RITICN. Most nodes have three conductor numbers associated with their nodal number. One conductor is oriented in the streamline direction, one in the nodal line direction, and one in the tangential direction.

The code SMAN4 creates a SINDA heat transfer model of a radial inflow turbine with internally cooled blades. The program obtains the geometric data of the model from the program RITICN.
A SINDA node is generated for each NASTRAN grid point within the blade. Adjacent to these, SINDA nodes are generated at the metal surfaces and at the points that represent the temperature boundary. Conductors are generated which represent the metal conduction along streamlines, along nodal lines, and through the thickness. Additional conductors are generated to represent the heat transfer coefficients between the metal's surface and the boundary nodes. A typical segment of the blade model is shown in Figure 2. Similar nodes and conductors are generated for the blade tips, leading edge, and root edge (Figures not shown due to space limitations).

Within the disk, a SINDA node is generated for each NASTRAN grid point. Additional nodes are generated for the temperature boundaries along the rim, back face, bore, hot gas face, and exducer end. Conductors are generated along streamlines, nodal lines, and in the tangential direction, and to represent the external heat transfer coefficients. Additional options have been incorporated which generate the thermal boundary conditions for the coolant inlet channel, exit end face (exducer) and the disk's cooling passages.

**Boundary Conditions**

The equation governing three-dimensional steady state heat conduction is of the elliptic form. Therefore, heat transfer coefficients and relative total temperature boundary conditions are required over the entire surface. The model under consideration consists of an entire blade with the corresponding disk sector. Figure 3 shows a...
typical blade/disk combination. The numbers on
the figure refer to the numbers of the following
paragraphs.

1. Suction and Pressure External Surface: The
heat transfer coefficients and free stream
total temperatures are obtained with the
MERIDIL/TSONIC/STAN5 combination.

2. Internal Cooling Passage: The heat
transfer coefficients and coolant surface
pressures are computed by CPFPA.

3. Disk Back Face: This region is connected
to a shaft. A contact resistance heat
transfer coefficient is used.

4. Blade Leading Edge: The heat transfer
coefficients are obtained by modeling the
leading edge as a cylinder in cross flow.

5. Blade Trailing Edge: The average of the
suction and pressure surface heat transfer
coefficients at the trailing edge are used.

6. Disk Exducer End Face: A contact
resistance heat transfer coefficient is
used.

7. Blade Platform: The heat transfer
coefficients are taken to be the mean of
the suction and pressure surface values at
the blade hub. Hub platform film cooling
is accounted for by adjusting the external
total temperatures.

8. Blade Scallop: Heat transfer coefficients are
taken to be the average of the external
suction and pressure values at the hub
streamline in the scallop region.

9. Disk Rim: This is the region where the
coolant comes on board the rotor. The heat
transfer coefficient is found by modeling
the flow as an enclosed rotating disk next
to a stationary wall.

10. Blade Tip: The heat transfer coefficients
are the average of the suction and pressure
values along the streamline.

Using the boundary conditions mentioned
above, SMAIN4 generates the CONDUCTOR Data and the
NODE Data required as input for analysis by SINDA.
The user is to supply the metal's thermal
conductivity as a function of temperature in the
ARRAY data as described in the SINDA user's
manual. The SIV cards required to simulate baffles, pin fins, etc. are to be hand generated
and added to the SINDA input deck created by
SMAIN4.

The output from SINDA will be a detailed
three dimensional temperature distribution in the
blade and disk.

The computer program RELACT [15] then
converts the output of a SINDA heat transfer
analysis into the thermal load input for a NASTRAN
structure analysis. RELACT has two major
functions. The first is to generate the grid
point temperature field cards: the second
is to generate plate element field cards. The first is
easily accomplished by using relation tables that
relate SINDA relative node numbers to SINDA actual
node numbers, and SINDA actual nodes numbers to
NASTRAN grid point numbers. Using these tables
the NASTRAN grid point temperature is easily
related to the SINDA relative node number which is
provided by adding a few FORTRAN statements to the
SINDA analysis output calls. The above is
performed for all grid points in the blade and
disk. Generating the plate element field cards
requires calculating the plate element's material
temperature, the bottom surface temperature, the
top surface temperature, an the thermal gradient
through the thickness of the element. In addition
to the relation tables described above, the
program requires the element connectivity and
thickness data. All the relation tables and
element data files are generated by either RITIN,
SMAIN4, or SINDA. Very little input is generated
by the user. RELACT output can be directly used
by PATRAN [16] for obtaining the three dimensional
temperature plots (in the form of temperature
tints and contour lines) on the blade and the disk.

NASTRAN Structural Analysis

The blade and disk modeling for NASTRAN
finite element analysis is created by RITIN as
explained before. The internal geometry of one
blade (Coolant passages) is modeled as follows:

- CQUAD4 quadrilateral plate elements
- CBAR rod-type elements
- CSYM2 extra mass elements

The pressure loads applied to the model
arise from two areas:
1. Internal coolant Pressure (Data
   Supplied by the Code CPFPA)
2. Working Fluid Pressure differential
   across the blade (Data Supplied by
   the MERIDIL/TSONIC/STAN5
   combination).

The thermal load applied to the model is
generated by the code RELACT using the output from
SINDA.

A static stress and deflection analysis as
well as a modal analysis can be performed on the
cooled radial turbine using NASTRAN.

ILLUSTRATIVE APPLICATION

A cooled radial turbine will be tested at
the NASA Lewis Research Center. The conditions
for the test and sample application are given in
Table 1. The turbine internal geometry is similar
to that shown in Figure 3. Cooling air entering
the rotor gets directed to the leading edge.
From there it flows down to the hub and branches
into three paths exiting at the trailing edge.
The flow splits indicated in the figure were
obtained with a flow network analysis code which
includes the momentum equation but not the energy
equation.

<table>
<thead>
<tr>
<th>Table 1: Turbine Input Conditions</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rotor Inlet Total Temperature</td>
</tr>
<tr>
<td>Rotor Inlet Total Pressure</td>
</tr>
<tr>
<td>Mass Flow Rate</td>
</tr>
<tr>
<td>Speed</td>
</tr>
<tr>
<td>Total Pressure Ratio</td>
</tr>
<tr>
<td>Work Coefficient kWh/m³</td>
</tr>
<tr>
<td>Total Enthalpy Change</td>
</tr>
<tr>
<td>Coolant Flow Rate</td>
</tr>
<tr>
<td>Coolant Onboard Total</td>
</tr>
<tr>
<td>Temperature</td>
</tr>
<tr>
<td>Coolant Onboard Total</td>
</tr>
<tr>
<td>Pressure</td>
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</tbody>
</table>
Figure 4 shows the freestream critical velocity ratio distribution along the mean streamline. These are the MERID/TSN/IC computed velocities which are used as input to STAN5. Ten streamlines between the hub and tip were chosen. The free stream velocity was "smoothed" on the suction surface of streamlines 1, 2, 5, 6, and 7 to eliminate separation. Figure 5 shows the location and amount of smoothing. Generally, STAN5 predicts separation along the suction surface in regions of high diffusion. "Smoothing" the free stream velocity, or reducing the velocity gradient, will eliminate the separation. Figures 6-8 show some of the heat transfer results predicted by STAN5 for the mean streamline. STAN5 input assumptions include turbulent flow, a recovery factor of one, and a flat inlet temperature profile. Assuming a small boundary layer thickness compared to the surface's radius of curvature allows the curved blade to be modeled as a flat surface in STAN5.

The CPFRHA predicted coolant temperature and heat transfer coefficient distribution is given in Figures 9 & 10. High heat transfer coefficients are predicted near the tip. This leads to a cool pressure side metal temperature since the external heat transfer coefficients on this side are low. The suction side temperatures are higher due to the higher external heat transfer coefficients.

Several interlinking codes were used in the procedure to generate input files required by MAIN5. For the above sample application, it took only two iterations between SINDA and CPFRHA to obtain a converged temperature distribution (where the maximum change in temperature was less than 2%).

PATRAN plot routines are used to display both SINDA and NASTRAN outputs. SINDA temperature distribution in the form of contours is displayed in Figure 11. The stress contours predicted by NASTRAN are shown in Figure 12 and the nodal displacements are shown in Figure 13. These figures are a representative sample of the typical graphical output generated by the above procedure.
Figure 8: Stanton Number Along Pressure Surface.

Figure 9: Internal Heat Transfer Coefficients (W/m²/K).

Figure 10: Coolant Temperatures (°K).

Figure 11: Temperature Contours (SINDA).
Figure 12: Stress Contours (NASTRAN).

Figure 13: Nodal Displacements (NASTRAN).

The NASTRAN model generation and the NASTRAN to SINDA conversion codes must be modified before application to axial turbines.

There are several prominent differences between axial and radial turbines. The axial turbine does not have the blade scallop found in radial machines; thus, one boundary condition is eliminated. The relative total temperature along the blade external surface is strictly a function of the radial position within the blade. A large radius change occurs in a radial turbine as the gas passes between inlet and exit. This causes the relative total temperature to drop. This temperature change does not exist in an axial turbine since the radius change is small. The process of introducing the coolant to the blade differs between axial and radial machines. This process in an axial design may be quite similar to or different from the radial machine under study. There are numerous other minor differences between the axial and radial turbine which the procedure should readily accommodate.

CONCLUDING REMARKS

An automated analysis procedure has been developed which can accomplish a rigorous thermal and structural analysis of a cooled radial turbine. This procedure after proper validation with the experimental data should result in a versatile analysis and design tool for cooled radial turbines.

REFERENCES


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