MULTIPLE PHASE-SCREEN PROPAGATION ANALYSIS FOR DEFENSE SATELLITE COMMUNICATIONS SYSTEM

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12. ABSTRACT
This report presents and analyzes simulated results for electric field propagation through a thick, extended region of high-altitude striations of electron density. The simulated results correspond to the problem of communication from a JSCS satellite to a ground station at a frequency of 7.5 GHz. Statistical results are presented for Scintillation index and intensity correlation length for a power-law and an exponential phase-screen PSD for values of phase standard deviation ranging from 1 to 100 radians and phase correlation length ranging from 1 to 10 km.

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Examples of specific realizations of the electric field amplitude and phase at the receiver are also shown. These realizations of signal structure are being used in simulations of DSCS receiver operation, reported elsewhere.
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SECTION 1

1.0 INTRODUCTION

The problem of communication from a satellite to a ground station in the presence of large, spatially extended regions of high-altitude nuclear burst produced striations of electron density can be modeled as the problem of propagation through a thick medium composed of random index-of-refraction fluctuations. Since no general analytical solution is available for this problem it must be handled numerically. In this report, a multiple phase-screen propagation simulation is developed as a method to propagate electromagnetic waves through statistically chosen realizations of the random medium.

In general, the electron density striations are represented by a number of phase screens which are chosen to possess the same statistical description as the original striations. A plane wave is then propagated from one phase screen to the next until a solution for the electric field in the receiver plane is obtained. To obtain the statistics of the received field, the problem is solved a number of times with different realizations of the phase screens (all with the same statistics) and the results are averaged.

The possibility of generating and retaining the realizations of the received electric field is an advantage of this type of simulation solution particularly when the results are to be used in conjunction with a receiver simulation of the ground station electronics. For all the work reported here several realizations of the received field were retained and are available for future analysis.
This report considers the effect of nuclear burst produced striation structure on propagation of 7.5 GHz (wavelength = 0.04 m) communication signals from a satellite to a ground station. The two different geometries relevant to the Defense Satellite Communications System (DSCS) considered are shown in Figure 1 (a) for the case of striations ranging in altitude from 300 km (F region altitude) to 15000 km and case (b) for striations ranging from 6000 km to 15000 km altitude. In both cases the striations are assumed to be elongated in the direction perpendicular to the page so that there is no variation in the y-direction. All results are given in terms of the one dimensional phase-screen power spectral density or autocorrelation function. The relationship of these quantities to the electron density power spectral density is given in Appendix B. The choice of phase-screen power spectral density is arbitrary but for this work results were obtained for two spectra:

\[
\Phi^{(1)}(K) = \frac{\sigma^2}{2} \frac{L_0}{\left(1+K^2 L_0^2\right)^{3/2}} \\
\Phi^{(2)}(K) = \frac{\sigma^2}{2} \frac{L_0}{e^{-|K| L_0}}
\]

As shown in Appendix B \(\Phi^{(1)}\) corresponds to a \(K^{-2}\) power law spectral density for one-dimensional electron density fluctuations (thought to be representative of the ambient ionosphere) and \(\Phi^{(2)}\) corresponds to a one-dimensional exponential (or Chesnut) power spectral density for integrated electron density fluctuations.

The corresponding phase screen autocorrelation functions may be analytically obtained as:

\[
B^{(1)}(\xi) = \frac{\xi}{L_0} K_1(\xi/L_0) \\
B^{(2)}(\xi) = \left(\frac{1}{1+\xi^2/L_0^2}\right)^{3/2}
\]
Figure 1. Geometry of DSCS simulation.
where $K_1(x)$ is the modified Bessel function (Abramowitz and Stegun, p. 374). (The Fourier transform relationship used here between autocorrelation function and power spectral density is given by Equations B-11 and B-14.) For this report an important parameter of interest is the autocorrelation length which is defined as the $e^{-1}$ point of the autocorrelation function. For the power law spectrum, $\phi(1)$, the correlation length is $\xi_c^{(1)} = 1.55 L_0$, and for the exponential spectrum, $\phi^{(2)}$, the correlation length is given by $\xi_c^{(2)} = 1.31 L_0$. For this report, the correlation length ranged from 1 to 10 kilometers for both choices of the phase-screen power spectral density.

The final physical parameter of interest is the total phase standard deviation of the phase-screens comprising the multiple phase-screen. Since each phase-screen is designed as an assembly of Gaussian random variables with zero mean and variance $\sigma_{\phi_1}^2$ and is independent of the other individual phase-screens, the total variance is the sum of the individual variances and thus the phase standard deviation is given by

$$\sigma_\phi = \left\{ \sum_{i=1}^{N} \sigma_{\phi_1}^2 \right\}^{1/2} \tag{1.5}$$

where $N$ is the total number of phase-screens. For this work $N$ was chosen to be 10 and $\sigma_\phi$ ranged from 1.0 to 100 radians.

The main body of this report is divided into three major sections. Sections 2 and 3 show the application of the MPS code to problems whose analytic solutions are available and allow a comparison of the code results to analytical results. Section 2 deals with the calculation of the diffraction pattern of a single Gaussian lens in the center of a phase screen. The analytic solution is obtained as a Fresnel-Kirchhoff integral which may be written as an infinite series and summed. Section 3 shows the results for a single phase-screen characterized by a Gaussian power spectral density.
and small phase variance $\sigma^{2}_\phi$. Results for the observed intensity power spectral density, and scintillation index are compared with analytic calculations in the weak-scatter approximation. Section 4 describes the results of the LSACS simulation at a frequency of 7.5 GHz. Appendix A contains a description of the multiple phase-screen code, its analytical foundation and the technique used to generate the random phase-screens. Appendix B contains a derivation of the relationship between the phase-screen standard deviation $\sigma\phi$ and the electron density fluctuations and a brief discussion of the relationship between one, two and three-dimensional power spectra. Appendix C shows one realization of all ten phase-screens and traces the signal intensity as the wave propagates through the medium for a particular geometry relevant to DSCS.
SECTION 2

2.0 DIFFRACTION BY A GAUSSIAN LENS

2.1 Gaussian Lens - Code Calculation

As a test of the multiple phase-screen propagation code, a single Gaussian phase lens given by

\[ \phi(x) = \phi_0 \exp(-x^2/r_0^2) \]  \hspace{1cm} (2-1)

was used at the first phase-screen location \((z = \eta, 0)\) with \(\phi_0\) chosen as 10 radians and \(r_0\) taken as \(\lambda\).

The intensity \(I = |E|^2\) was observed as a function of distance from the lens, \(z/\lambda\) as indicated in Figure 2(a-b). In this figure, all the phase-screens and observation screens are aligned, so that features of the diffraction pattern can be easily followed for changing \(z/\lambda\) values.

The focal length for a Gaussian lens is given by Salpeter (1967) as \(kr_0^2/2\phi_0\) where \(k\) is the wavenumber \(2\pi/\lambda\). Taking \(r_0 = \lambda\) and \(\phi_0 = 10\) radians, the focal length \(F/\lambda\) is 0.31 which corresponds reasonably well with the value of \(z/\lambda = 0.5\) where the intensity in the diffraction pattern at \(x = 0\) builds up to a maximum. At values of \(z/\lambda\) greater than the focal length, the diffraction pattern exhibits increasingly more complex patterns associated with rays coming from the edges of the lens, rather than from the center.
2.2 Gaussian Lens - Analytic Results

An analytical relationship between the electric field at \( z = z_1 \) and \( z = z_2 \) is given by the Fresnel-Kirchhoff integral (Ratcliffe, 1956)

\[
E(x, z_2) = \left( \frac{i2\pi(z_2-z_1)}{k} \right)^{-1/2} \int_{-\infty}^{\infty} \exp\left\{ -ik(z_2-z_1) \right\} \times \exp\left\{ \frac{1}{2} k(x-\xi)^2/(z_2-z_1) \right\} E(\xi, z_1)
\]

where \( E(x, z_1) \) is the electric field as a function of \( x \) in the \( z = z_1 \) plane. For an initial electric field in the \( z = 0 \) plane given by \( E(\xi) = \exp i\{\phi_0 \exp(-\xi^2/r_0^2)\} \), Equation 2-2 may be written as an infinite series by expanding \( \exp i\{\phi_0 \exp(-\xi^2/r_0^2)\} \) in a Taylor series as

\[
e^x = \sum_{n=0}^{\infty} \frac{x^n}{n!}
\]

The resulting integral over \( \xi \) may then be analytically performed using Equation 3.323(2) on page 307 of Gradshteyn and Ryzhik (1965). The result may be expressed as

\[
E(x', z') = \sqrt{\pi} \frac{e^{i2\pi x'/z'}}{\sqrt{z'}} \sum_{n=0}^{\infty} \frac{(i\phi_0)^n}{n!} \left( \frac{n/r_0^2 - i\pi/z'}{n/r_0^2 - i\pi/z'} \right)^{-1/2}
\]

\[
\exp\left[ \frac{-\pi^2 x'^2/z'^2}{(n/r_0^2 - i\pi/z')^2} \right]
\]

where the primed quantities \( x' = x/\lambda \), \( z' = z/\lambda \), and \( r_0^n = r_0/\lambda \). This series is easily summed (numerically) and the results for several values of \( z/\lambda \) are shown in Figure 2 to be identical to the code calculation for \( z/\lambda \leq 2.0 \).
Figure 2(a). Diffraction pattern of a Gaussian lens - numerical results from simulation on left-hand side versus theoretical results on right-hand side.
Figure 2(b). Diffraction pattern of a Gaussian lens - numerical results from simulation on left-hand side versus theoretical results on right-hand side.
For $z/\lambda = 10$ the multiple phase-screen calculations deviate from the theoretical results because energy which has left one side of the grid is coming back into the other side (this is the well known wrap-around or aliasing effect in fast Fourier transforms). Hendrick (1977) has determined criteria required to avoid this and other numerical problems and these criteria were used to assure proper application of the code results.
SECTION 3

3.0 DIFFRACTION BY A RANDOM THIN PHASE-SCREEN

This section contains a second application of the multiple phase-screen propagation code to a problem for which analytical results are available - scattering through a thin phase-screen characterized by a Gaussian power spectral density. For this example, only one phase-screen was used to characterize the random medium. The screen was located at \( z = 0 \) and was generated with a phase power spectral density (PSD) of

\[
\phi_\phi(K) = \sigma_\phi^2 \frac{x_0^2}{2\sqrt{\pi}} \exp(-K^2x_0^2/4) \tag{3-1}
\]

where the phase standard deviation was chosen as \( \sigma_\phi = 0.1 \) radians and \( x_0 \) was taken as \( 1\lambda \). The corresponding phase autocorrelation function is then

\[
\varphi_\phi(\xi) = \exp(-\xi^2/x_0^2) \tag{3-2}
\]

To obtain statistical results for the received signal, the simulation was exercised ten times with ten different random phase-screens (each screen chosen used a different set of random numbers; see Appendix A). Figure 3 shows a comparison of the intended phase-screen power spectral density \( \phi_\phi(K') \) where \( K' = K\lambda \) (dotted line) with the actual mean power spectral density obtained by averaging the power spectral densities of each of the ten realizations. Although no statistical study was performed to show the effect of averaging over different numbers of realizations this result indicates that ten realizations are sufficient to obtain reasonably accurate statistics.
Figure 3. Comparison of intended phase-screen power spectral density with that generated by the simulation for $\sigma_{\phi_i} = 0.1$ radians.
Figure 4 shows the average intensity \(|E|^2\) power spectral density at the locations \(z/\lambda = 0.628, 6.28, \text{ and } 37.7\), each compared to the theoretical results from Salpeter (1967)

\[
\Phi_I(K) = 4\Phi_\phi(K) \sin^2(K_0^2z/2k)).
\] (3-3)

(Strictly speaking, \(\Phi_I\) is the PSD of the normalized intensity deviation \((|E|^2 - \langle |E|^2 \rangle)/\langle |E|^2 \rangle\)). Excellent agreement between the theoretical and simulation results is shown with the simulation results for \(z/\lambda = 6.28\) even matching the location of the nulls (but not the infinite depth) of the analytical result. In all three curves the simulation deviates from the analytical results for large wavenumbers, which is likely caused by aliasing which always occurs in the application of fast Fourier transform techniques. A second possible explanation for this deviation at large wavenumbers is that the small scale sizes may produce angular scatter which causes this portion of the wave to alias to the other side of the phase screen. However, this aliasing behavior should become more pronounced as the propagation distance \(z/\lambda\) increases. Since this is not the case for Figure 4, this explanation must be discarded. For \(z/\lambda = 37.7\) the simulation accurately models the peaks of the analytical curve. However, except for the first null at \(k\lambda \approx 1\) \((K_0^2z/2k = \pi)\), the details of the nulls are lacking. This smearing of the nulls is caused by the averaging process.

The circled dots of Figure 5 show the value of scintillation index \(S_4\) obtained from the simulation for values of \(\sigma_\phi\) of 0.1, 1.0 and 10.0 radians. The solid curves are analytical estimates taken from the weak-scatter approximation of Salpeter

\[
S_4^2 = 4 \int_{-\infty}^{\infty} \Phi_\phi(K) \sin^2 \left( \frac{K_0^2z}{2k} \right) dK
\] (3-4)
Figure 4. Normalized intensity PSD as a function of distance from a thin, Gaussian phase-screen ($\sigma_\phi = 0.1$ radians, $x_0 = \lambda$).
Figure 5. Circled dots show $S_4$ scintillation index for Gaussian spectrum. The solid lines are analytic approximations valid for the weak-scatter case ($x_0 = \lambda$).
which may be exactly integrated for the Gaussian phase power spectral density given by Equation (3-1) to obtain

\[
S_4^2 = \sigma_\phi^2 \left\{ 2 - \left( \frac{1}{16} + \frac{2}{k^2 x_0^2} \right)^{-1/4} \cos \left( \frac{1}{2} \tan^{-1} \frac{4z}{kx_0^2} \right) \right\}.
\]  

It is seen from Figure 5 that excellent agreement is obtained between this analytical approximation and simulation results when the weak-scatter assumption inherent in Equation 3-5 is valid.
section 4

4.0 DSCS Simulation Results

This section describes the results of the simulation as applied to the satellite communication problem discussed in the introduction. As stated there, the simulation was applied to the two geometries shown in Figure 1, for two different phase-screen PSD's as given by Equations 1-1 and 1-2. The phase correlation lengths ranged from 1 to 10 km, and the phase standard deviation (as given by Equation 1-5) ranged from 1.0 to 100 radians. Table 4-1(a) and (b) shows the cases which were simulated for the power-law PSD and for the exponential PSD respectively. In addition to the phase correlation length, $l_c$, and phase standard deviation, $\sigma_\phi$, for each case the simulated phase-screen length $L$ is also included. In all cases, for this section of the report, the statistical results were obtained by averaging results for ten different realizations of the problem. For each realization, the striated region was represented by ten phase-screens, each composed of 2048 points.

In general, the results were not a strong function of the two geometries shown in Figure 1. For the weak scattering cases listed in Table 4, the scintillation index for the thicker striation region geometry (Figure 1(a)) was up to 25% less than that for the thinner region with the same total phase standard deviation. This is intuitively expected since for the thicker geometry, the phase-screens very close to the receiver plane will not be as effective at producing amplitude scintillation as phase-screens farther away. In the rest of this section only results for the geometry of Figure 1(a) are presented.
Table 4-1(a). Simulation parameters for power-law PSD.

<table>
<thead>
<tr>
<th>Phase Correlation Length</th>
<th>Phase Standard Deviation</th>
<th>Phase Screen Length</th>
<th>Resulting Scintillation Index</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>$\xi_c$</td>
<td>$\sigma_\phi$</td>
<td>Geometry 1*</td>
</tr>
<tr>
<td></td>
<td>$L$</td>
<td></td>
<td>Geometry 2**</td>
</tr>
<tr>
<td>1 km</td>
<td>1.0 rad</td>
<td>30 km</td>
<td>.37</td>
</tr>
<tr>
<td></td>
<td>2.5</td>
<td>30</td>
<td>.32</td>
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<td>.31</td>
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<td>10</td>
<td>31.6</td>
<td>100</td>
<td>.41</td>
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* Geometry 1 refers to Figure 1(a)
** Geometry 2 refers to Figure 1(b).

Table 4-1(b). Simulation parameters for exponential PSD.

<table>
<thead>
<tr>
<th>Phase Correlation Length</th>
<th>Phase Standard Deviation</th>
<th>Phase Screen Length</th>
<th>Resulting Scintillation Index</th>
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<tr>
<td></td>
<td>$\xi_c$</td>
<td>$\sigma_\phi$</td>
<td>Geometry 1*</td>
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<td>$L$</td>
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<td>Geometry 2**</td>
</tr>
<tr>
<td>1 km</td>
<td>1.0 rad</td>
<td>30 km</td>
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<td></td>
<td>2.5</td>
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<td>3.16</td>
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<tr>
<td>10</td>
<td>100.0</td>
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<td>.89</td>
</tr>
</tbody>
</table>

* Geometry 1 refers to Figure 1(a)
** Geometry 2 refers to Figure 1(b).
In Figure 6 the scintillation index is shown as a function of the total integrated phase standard deviation $\sigma_{\phi}$ for both spectra for values of the striation autocorrelation distance of 1, 3 and 10 kilometers. As expected, the scintillation index increases with increasing $\sigma_{\phi}$ but should ultimately saturate at a value of unity, characteristic of Rayleigh electric field strength statistics (Fante, 1977). Values greater than unity prior to saturation are not prohibited and have been observed in ionospheric measurements (Dr. E.J. Fremouw, personal communication, Stanford Research Institute, 1977). The large value of 1.6 for $S_4$ in Figure 6 is caused by strong focusing effects.

Figure 7 shows results obtained for the autocorrelation distance of the signal intensity as a function of the total phase standard deviation for the same cases as shown in Figure 6. These results were obtained by finding the distance corresponding to the $e^{-1}$ point from the circular correlation functions obtained from the average of the ten realizations. The general trend of decreasing correlation distance with increasing $\sigma_{\phi}$ is expected intuitively as is the association of large autocorrelation length with large striation autocorrelation distance. The range of these curves is limited by requirements on the phase-screen sampling distances. In order to extend the calculation of the intensity correlation distance farther into the multiple-scatter regime two techniques appear useful. The first involves a numerical solution of the differential equations for the mutual coherence function $\langle I(\rho) I(\rho+\xi) \rangle$ as discussed by Yeh, et al., (1975). A second possible method involves an approximate theory developed by Fante (1975). Both techniques require further evaluation.
Figure 6. $S_4$ scintillation index versus $\sigma_\phi$ as a function of phase-screen PSD and correlation length $\xi_c$ for $\xi_c = 1, 3, \text{ and } 10 \text{ km.}$
Figure 7. Signal intensity correlation distance versus $\sigma_\phi$ as a function of phase-screen PSD and correlation length $\lambda_c$ for $\lambda_c = 1$, 3, and 10 km.
4.1 Simulation Results - 1 kilometer Correlation Length

This section and the following two sections discuss the results obtained for realizations of the DSCS propagation simulation. In all cases the random number seed was the same for each computer run so that the set of phase-screen realizations was similar in "overall" appearance for all the runs. This also has the result that some features of the received intensity and phase are recognizable as the phase standard deviation and correlation length change.

Figure 8 shows a comparison of the actual power spectral densities of the phase-screens as generated by the MPS simulation for a one kilometer correlation length. Since the Fresnel length $\sqrt{\lambda z}$ ranges from 0.1 km ($z = 300$ km) to 0.8 km ($z = 15000$ km) which correspond to the wavenumber regime from $7.8 \text{ km}^{-1}$ to $62.8 \text{ km}^{-1}$, where the spectra are somewhat similar, the overall simulation results should be similar for these two spectra, since amplitude scintillations are caused by irregularities whose scale sizes are of the order of the Fresnel length. But since the power-law spectrum is somewhat higher at high wavenumbers (corresponding to smaller scales), the received electric field should exhibit more small-scale structure for the power-law PSD.

This behavior is evident in Figures 9 and 10 which show one realization of received intensity ($I = |E|^2$) for the two PSD's for values of the phase standard deviation of 1.0, 3.16 and 10.0 radians. Figures 11 and 12 show the phase (plotted between $\pm \pi$) corresponding to the intensities shown in Figures 9 and 10.

Figures 13 and 14 show the intensity power spectral density corresponding to the cases shown in Figures 9 and 10. (The results shown in Figures 13 and 14 result from averaging the PSD's of ten realizations, the
Figure 8. Comparison of simulation generated phase-screen PSD's for correlation length \( \kappa_c = 1 \) km, \( \lambda = 0.04 \) m. (\( \sigma_{\phi_1} = \sqrt{10} \) radians in figure).
Figure 9. Realizations of signal intensity for power-law PSD with $\xi_c = 1$ km.

- $\sigma_\phi = 1$ radian
- $\sigma_\phi = 3.16$ radians
- $\sigma_\phi = 10$ radians

Distance (km)
Figure 10. Realizations of signal intensity for exponential PSD with $\xi_c = 1$ km.
Figure 11. Realizations of signal phase for power-law PSD with $l_c = 1$ km.
Figure 12. Realizations of signal phase for exponential PSD with $\ell_c = 1$ km.
Figure 13. Normalized intensity PSD for power-law phase-screen PSD with $\chi_c = 1$ km, $\lambda = 0.04$ m.
Figure 14. Normalized intensity PSD for exponential phase-screen PSD with $L_c = 1$ km, $\lambda = 0.04$ m.
first of which is shown in Figures 9 and 10.) For the weak scattering cases ($\sigma_\phi = 1.0$) the intensity PSD closely matches the PSD of the phase-screen for wavenumbers greater than the inverse Fresnel length. This behavior is required by Equation 3-3 for weak scattering since the intensity PSD is the product of the phase-screen PSD with a sine-squared factor which averages to $1/2$ for wavenumbers much greater than the inverse Fresnel length. For the strong scattering cases ($\sigma_\phi > 1.0$), the intensity PSD gradually becomes flatter near the inverse Fresnel length but retains a high-wavenumber rolloff where the spectrum again has the same slope as the phase-screen PSD. This flat low-wavenumber spectrum with a high-wavenumber rolloff is similar to observations of intense ionospheric scintillations shown by Whitney and Basu (1977). This flattening of the intensity PSD, of course, also corresponds to a sharpening of the intensity autocorrelation function with a resulting decrease in the signal intensity correlation distance with increasing $\sigma_\phi$. This behavior is shown in Figure 7.
4.2 Simulation Results - 3 kilometer Correlation Length

Figure 15 shows a comparison of the measured (simulation) phase-screen PSD's for a phase correlation length of 3 km. For this case, the power-law PSD is much larger than the exponential PSD near wavenumbers corresponding to the Fresnel length, and therefore one would expect a much greater difference between the received signals for the \( \lambda_c = 3 \) km case than for the \( \lambda_c = 1 \) km case discussed in the previous section.

The difference is apparent in Figures 16 and 17 which show realizations of the received intensity for values of \( \sigma_\phi = 3.16 \) and 10.0 radians for the power-law PSD and \( \sigma_\phi = 3.16, \ 10.0 \) and 31.6 radians for the exponential PSD. Note the absence of small scale structure for the exponential PSD for \( \sigma_\phi = 3.16 \) and 10.0 radians.

The phases corresponding to the intensities of Figures 16 and 17 are shown in Figures 18 and 19.

For the interested reader Appendix C shows the realization of the ten phase-screens and the electric field intensity as the wave progresses through the screens to the observation plane for the case \( \sigma_\phi = 31.6 \) and the exponential PSD.

Figures 20 and 21 show the mean intensity PSD's corresponding to the intensity realizations shown in Figures 16 and 17. Again, as the phase standard deviation \( \sigma_\phi \) increases, the intensity PSD goes from a close resemblance to the phase-screen PSD for wavenumbers greater than the inverse Fresnel distance to a much flatter behavior for larger \( \sigma_\phi \).
Figure 15. Comparison of simulation generated phase-screen PSD's for correlation length $\lambda_c = 3$ km, $\lambda = 0.04$ m. ($\sigma_\phi = \sqrt{10}$ radians in figure).
Figure 16. Realizations of signal intensity for power-law PSD with $l_c = 3$ km.
Figure 17. Realizations of signal intensity for exponential PSD with $\lambda_c = 3 \text{ km}$. 

$\sigma_\phi = 3.16 \text{ radians}$

$\sigma_\phi = 10 \text{ radians}$

$\sigma_\phi = 31.6 \text{ radians}$
Figure 18. Realizations of signal phase for power-law PSD with $\ell_c = 3 \text{ km}$.
Figure 19. Realizations of signal phase for exponential PSD with $k_c = 3$ km.
Figure 20. Normalized intensity PSD for power-law phase screen PSD with \( \lambda_c = 3 \text{ km} \), \( \lambda = 0.04 \text{ m} \).
Figure 21. Normalized intensity PSD for exponential phase-screen PSD with $\lambda_C = 3$ km, $\lambda = 0.04$ m.
4.3 Simulation Results - 10 kilometer Correlation Length

For phase correlation length \( \lambda_c = 10 \text{ km} \), the two phase-screen PSD's generated by the code differ significantly in the wavenumber region near the inverse Fresnel length as shown in Figure 22. This difference is dramatically shown in Figures 23 and 24 which show realizations of intensity for \( \sigma_\phi = 10.0 \) and 31.6 radians for the power-law PSD and for \( \sigma_\phi = 10.0 \), 50.0, and 100 radians for the exponential PSD. The corresponding phase realizations are shown in Figures 25 and 26.

Figures 27 and 28 show the mean intensity PSD corresponding to intensities shown in Figures 23 and 24.
Figure 22. Comparison of simulation generated phase-screen PSD's for correlation length $\xi = 10$ km, $\lambda = 0.04$ m. ($\sigma_{\phi} = 10$ radians in figure).
Figure 23. Realizations of signal intensity for power-law PSD with $\rho_c = 10$ km.

$\sigma_\phi = 10$ radians

$\sigma_\phi = 31.6$ radians
Figure 24. Realizations of signal intensity for exponential PSD with $\xi_c = 10$ km.
Figure 25. Realizations of signal phase for power-law PSD with $\lambda_c = 10$ km.
Figure 26. Realizations of signal phase for exponential PSD with $\varphi_c = 10$ km.

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Figure 27. Normalized intensity PSD for power-law phase-screen PSD with $\varepsilon_c = 10$ km, $\lambda = 0.04$ m.
Figure 28. Normalized intensity PSD for exponential phase-screen PSD with $\xi_c = 10$ km, $\lambda = 0.04$ m.
5.0 CONCLUSIONS

This report has presented and analyzed simulated results for electric field propagation through a thick, extended region of high-altitude striations of electron density. The simulated results correspond to the problem of communication from a DSCS satellite to a ground station at a frequency of 7.5 GHz. The results are parameterized in terms of the phase-screen power spectral density (PSD) and phase standard deviation $\sigma_\phi$, which may be related to the in-situ electron density PSD and electron density fluctuation $\sigma_{N_e}$ by formulae developed in Appendix B. Statistical results are presented for $S_q$ scintillation index and intensity correlation length for a power-law and an exponential phase-screen PSD for values of phase standard deviation $\sigma_\phi$ ranging from 1 to 100 radians and phase correlation length $\xi_c$ ranging from 1 to 10 km.

Examples of specific realizations of the electric field amplitude and phase at the receiver are also shown. These realizations of signal structure are being used in simulations of DSCS receiver operation, reported elsewhere.
BIBLIOGRAPHY


This Appendix describes the multiple phase screen propagation code as used to solve the scalar wave equation. Also included is a description of the technique used to generate the random phase-screens.

A.1 Scalar Wave Equation Solution

The problem of interest is that of a plane wave, incident at \( z = 0 \) on a random medium consisting of index of refraction fluctuations. Assume that the random medium extends from \( z = 0 \) to some distance and that its autocorrelation function is not a function of \( y \). That is, the medium can be thought to consist of a number of random striations or tubes which are infinitely extended in the \( y \)-direction.

The propagating wave is then only a function of \( x \) and \( z \). Ignoring depolarization, the scalar wave equation may be written

\[
(V^2 + k^2 n^2) \psi = 0
\]  
(A-1)

where

\[
V^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial z^2}
\]

and \( n = 1 + \Delta n \) is the index of refraction with \( \Delta n \) a small perturbation. The equation

\[
\frac{\partial^2 u}{\partial z^2} + i2k \frac{\partial u}{\partial z} + \frac{\partial^2 u}{\partial x^2} + 2k^2 \Delta nu = 0
\]  
(A-2)
may be obtained from Equation A-1 using the substitution

\[ \psi = u \exp(ikz) \]  

(A-3)

and ignoring terms in \((\Delta n)^2\).

The complex amplitude \(u\) can vary markedly over distances no smaller than the inhomogeneity scale size \(\ell\); that is, the worst case variation of \(u\) in the direction of propagation can be characterized by \(u \sim \exp(-z^2/\ell_m^2)\) where \(\ell_m \geq \ell\). Thus, the second derivative \(\partial^2 u/\partial z^2\) is of the order of \(u/\ell_m^2\). On the other hand, the second term of Equation A-2 is of the order of \(u/\lambda ell_m\). Therefore, for \(\lambda \ll \ell_m\), or \(\lambda \ll \ell\), the first term of Equation A-2 may be ignored with respect to the second term to obtain the parabolic wave equation

\[ \frac{\partial^2 u}{\partial x^2} + 12k \frac{\partial u}{\partial z} + 2k^2 \Delta n u = 0 \]  

(A-4)

Now for a given initial field, the propagation simulation must generate values of the field such that Equation A-4 is satisfied. To do this, the medium is divided into screens defined by planes on which \(z\) is constant. To propagate from one screen to the next write \(u(x,z)\) in the form

\[ u = we^\phi \]  

(A-5)

where

\[ \phi(x,z) = ik \int_{z-\Delta z/2}^{z+\Delta z/2} \Delta n(x,z') \, dz' \]  

(A-6)

so that

\[ \frac{\partial \phi}{\partial z} = ik \Delta n(x,z) \]  

(A-7)
Equations A-5 and A-7 may be substituted into Equation A-4 to obtain

\[ e^{-\phi} \frac{\partial^2}{\partial x^2} (\omega e^\phi) + 2i k \frac{\partial \omega}{\partial z} = 0 \]  
(A-8)

To solve this equation, assume that the step size \( \Delta z \) is sufficiently small so that the effect of the exponential factors in Equation A-8 is small. Thus, one can solve

\[ \frac{\partial^2 \omega}{\partial x^2} + 2i k \frac{\partial \omega}{\partial z} = 0 \]  
(A-9)

A simple solution may be obtained using the Fourier transform relation

\[ w(x,z) = \int_{-\infty}^{\infty} dK \hat{w}(K,z) e^{-iKx} \]  
(A-10)

which may be substituted into Equation A-9 to obtain

\[ 2i k \frac{\partial \hat{w}}{\partial z} - k^2 \hat{w} = 0 \]  
(A-11)

whose solution is

\[ \hat{w}(K,z) = \hat{w}(K,0) \exp \left( -\frac{iK^2}{2k} z \right) \]  
(A-12)

or using Equation A-12 in Equation A-10

\[ w(x,z) = \int_{-\infty}^{\infty} dK \hat{w}(K,0) \exp \left( -\frac{iK^2 z}{2k} - iKx \right) \]  
(A-13)

Equation A-13 may be rewritten by applying Equation A-12 for \( z = z_1 \) and \( z = z_2 \) where \( z_1 \) and \( z_2 \) are two successive phase-screen locations.
\[ W(x,z_2) = \int_{-\infty}^{\infty} dK \hat{W}(K,z_1) \exp \left( -\frac{iK^2(z_2-z_1)}{2k} -iKx \right) \]  \hspace{1cm} (A-14)

Now, using Equation A-5 and Equation A-3 and replacing \( \psi \) by the electric field we obtain from Equation A-14

\[ E(x,z_2) = e^{ik(z_2-z_1)} \int_{-\infty}^{\infty} dK \hat{E}(K,z_1) \left( \exp \left( -\frac{iK^2}{2k} (z_2-z_1) -iKx \right) \right) \]  \hspace{1cm} (A-15)

where \( E(K,z_1) \) is now the Fourier transform of the product

\[ E(x,z_1) \exp \left\{ ik \int_{z_1-\Delta z/2}^{z_1+\Delta z/2} dz' \Delta n(x,z') \right\} \]  \hspace{1cm} (A-16)

At this point it is interesting to note that one can obtain the Fresnel-Kirchhoff integral by substituting the Fourier transform

\[ E(K,z_1) = \frac{1}{2\pi} \int_{-\infty}^{\infty} d\xi E(\xi,z_1)e^{iK\xi} \]

into Equation A-15 and performing the \( K \) integration (Gradshteyn and Ryzhik, p. 397) as

\[ E(x,z_2) = \left( \frac{i2\pi(z_2-z_1)}{k} \right)^{-1/2} \int_{-\infty}^{\infty} d\xi e^{ik(z_2-z_1)} \]

\[ \times \exp \left\{ i \frac{1}{2} k(x-\xi)^2/(z_2-z_1) \right\} E(\xi,z_1) \]  \hspace{1cm} (A-17)

The propagation simulation thus breaks up the random medium into a number of screens. The electric field incident on a phase-screen in then multiplied by the phase shift caused by the random medium lying between the
previous and current phase-screen (Equation A-12). The wave then propagates as if in free space to the next phase-screen (Equation A-11). Propagation from one phase-screen to the next is accomplished very efficiently by the use of the fast Fourier transform so that once the electric field is multiplied by the appropriate complex phase term (as in Equation A-12) its Fourier transform is taken, multiplied by \( \exp(-iK^2(z_2-z_1)/k) \) and then another fast Fourier transform is performed to obtain the electric field at the next screen \( E(x,z_2) \).

A.2 Generation of the Random Phase Screen

The following procedure taken from Buckley (1975) was used to generate the random phase screen with arbitrary variance and power spectral density.

Assume that \( P_i \) is a sequence of random numbers uniformly distributed between \(-1/2\) and \(1/2\). Then

\[
\langle P_i \rangle = 0
\]

\[
\langle P_i P_j \rangle = \frac{1}{12} \delta_{ij}
\]

(A-18)

where \( \delta_{ij} \) is the Kronecker delta function. Now choose the phase as a sequence given by the circular (see Enslein, et al., p. 380) correlation

\[
\phi_{\lambda} = \phi(\lambda \Delta x) = \sum_{j=0}^{N-1} w_j P_{j+\lambda}; \lambda = 0, N-1
\]

(A-19)

where the phase screen is sampled at increments \( \Delta x = L/N \) where \( L \) is the total length of the screen. The \( w_j \) are a set of weights which are to be determined.
Since each value $\phi_k$ is a sum of a large number $N$ of independent random variables, it follows from the central limit theorem that the sequence $\{\phi_k\}$ will possess a Gaussian distribution with zero mean. Now the phase autocorrelation function $\rho_k$ may be formed by noting

$$
\langle \phi_i \phi_{i+k} \rangle = \left( \sum_{j=0}^{N-1} w_j p_{j+i} \sum_{\ell=0}^{N-1} w_{\ell} p_{\ell+i+k} \right)
$$

$$
= \sum_{j=0}^{N-1} w_j \sum_{\ell=0}^{N-1} w_{\ell} \frac{1}{12} \delta_{j,\ell+k}
$$

$$
= \frac{1}{12} \sum_{\ell=0}^{N-1} w_{\ell} w_{\ell+k} \quad (A-20)
$$

Set

$$
\phi_0^2 \equiv \langle \phi_i \phi_i \rangle = \frac{1}{12} \sum_{\ell=0}^{N-1} w_{\ell}^2 \quad (A-21)
$$

to obtain the autocorrelation function

$$
\rho_k \equiv \frac{1}{\phi_0^2} \langle \phi_i \phi_{i+k} \rangle
$$

$$
\rho_k = \frac{1}{12\phi_0^2} \sum_{\ell=0}^{N-1} w_{\ell} w_{\ell+k} \quad k=0, \ldots, N-1 \quad (A-22)
$$

The $\rho_k$ sequence may be interpreted as

$$
\rho(k \Delta x), \quad k = 0, \ldots, N-1; \text{ that is, } \rho_k
$$

is a discrete representation of the continuous autocorrelation function.
Now in order to relate the still unknown weights \( \{w_k, k=0,\ldots,N-1\} \) to the power spectral density of the phase we must use the Fourier transform pair
\[
\rho(x) = \int_{-\infty}^{\infty} S(K) e^{-iKx} dK \quad (A-23)
\]
\[
S(K) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \rho(x) e^{iKx} dx \quad (A-24)
\]
and their discrete representations
\[
\rho(k\Delta x) = 2\pi\Delta Q \sum_{k=0}^{N-1} S(2\pi\Delta Q) e^{-i(k\Delta x)(2\pi\Delta Q)}, \quad k=0,\ldots,N-1 \quad (A-25)
\]
\[
S(2\pi\Delta Q) = \frac{\Delta x}{2\pi} \sum_{k=0}^{N-1} \rho(k\Delta x) e^{i(k\Delta x)(2\pi\Delta Q)}, \quad \ell=0,\ldots,N-1 \quad (A-26)
\]
where \( \Delta K = 2\pi\Delta Q \). Noting that \( \Delta x = L/N \), where \( L \) is the length of a phase screen, \( \Delta Q = 1/L \), \( \Delta x\Delta Q = 1/N \), Equation A-25 and Equation A-26 may be rewritten as
\[
\rho_k = \rho(k\Delta x) = 2\pi\Delta Q \sum_{\ell=0}^{N-1} S_{\ell} e^{-i2\pi k\ell/N}, \quad k=0,\ldots,N-1 \quad (A-27)
\]
\[
S_{\ell} = \delta(2\pi\Delta Q) = \frac{\Delta x}{2\pi} \sum_{k=0}^{N-1} \rho_k e^{i2\pi k\ell/N}, \quad \ell=0,\ldots,N-1 \quad (A-28)
\]
Now the Fourier transfer of Equation A-22 is given by
\[
S_r = \frac{\Delta x}{2\pi} \frac{1}{12\phi^2} \sum_{k=0}^{N-1} \sum_{\ell=0}^{N-1} w_{\ell+k} e^{-i2\pi k\ell/N} \quad (A-29)
\]
The Fourier transform of the weight is given by \( \hat{\mathbf{W}} \) as

\[
\hat{\mathbf{W}} = 2\pi\Delta Q \sum_{m=0}^{N-1} \hat{\mathbf{w}}_m e^{-i2\pi m\mathbf{q}/N} \tag{A-30}
\]

and similarly for \( \hat{\mathbf{W}}_{\mathbf{q}+\mathbf{k}} \)

\[
\hat{\mathbf{W}}_{\mathbf{q}+\mathbf{k}} = 2\pi\Delta Q \sum_{n=0}^{N-1} \hat{\mathbf{w}}_n e^{-i2\pi (\mathbf{q}+\mathbf{k})n/N} \tag{A-31}
\]

Now since the weights \( \{\mathbf{w}_k\} \) are real \( \mathbf{w}_k = \mathbf{w}_k^* \) and we can use the complex conjugate of Equation A-30 and Equation A-31 with Equation A-29 to obtain

\[
\hat{\mathbf{S}}_{\mathbf{r}} = \frac{4\pi^2(\Delta Q)^2}{24\pi\phi_0^2} \sum_{k} \sum_{\mathbf{q}} \sum_{m} \sum_{n} \hat{\mathbf{w}}_m^* e^{+i2\pi m\mathbf{q}/N} \hat{\mathbf{w}}_n e^{-i2\pi (\mathbf{q}+\mathbf{k})n/N} e^{i2\pi k\mathbf{r}/N} \tag{A-32}
\]

Now since

\[
\sum_{k=0}^{N-1} e^{-2\pi kn/N} e^{i2\pi m\mathbf{q}/N} = N\delta_{mn} \tag{A-33}
\]

\[
\sum_{k=0}^{N-1} e^{-i2\pi kn/N} e^{i2\pi k\mathbf{r}/N} = N\delta_{hr} \tag{A-33}
\]

Equation A-32 may be summed to yield

\[
\hat{\mathbf{S}}_{\mathbf{r}} = \pi(\Delta Q)^2 \Delta x \frac{N^2}{6\phi_0^2} |\hat{\mathbf{W}}_{\mathbf{r}}|^2 \tag{A-34}
\]

or since \( \Delta Q = 1/\Delta x \) the Fourier transform of the weights is given by:

\[
\hat{\mathbf{W}}_{\mathbf{r}} = \sqrt{\frac{6\Delta x\phi_0^2}{\pi}} \frac{1}{S_{\mathbf{r}}} \tag{A-35}
\]

where \( S_{\mathbf{r}} \) is the discrete Fourier transform representation of the phase-screen power spectral density.
Thus, to generate the phase values for a phase-screen, one may start with the power spectral density, obtain the Fourier transform of the weights via Equation A-35, and take the inverse Fourier transform to obtain the weights themselves.
APPENDIX B

RELATIONSHIP BETWEEN PHASE AND ELECTRON NUMBER DENSITY

B.1 Phase Screen PSD Related to Electron Density PSD

As discussed in Appendix A, the electric field at each phase screen is multiplied by the factor $e^{i\phi(x)}$ where

$$\phi(x) = k \int_{-\Delta z/2}^{\Delta z/2} \Delta n(x,z) \, dz$$  \hspace{1cm} (B-1)

which effectively collapses the index-of-refraction fluctuations in the region from $-\Delta z/2$ to $\Delta z/2$. In the absence of significant electron collisions, the index of refraction is given as

$$n^2 = 1 - \frac{N_e}{n^*}$$  \hspace{1cm} (B-2)

where $N_e$ is the electron number density and $n^*$ is the critical electron number density

$$n^* = \frac{\varepsilon_0 m_e \omega^2}{e^2} = 1.24 \times 10^{-8} f^2 \left[ \text{e}^2/\text{cm}^3 \right]$$  \hspace{1cm} (B-3)

where $\varepsilon_0$ is the permittivity of free space, $m_e$ is the mass of an electron, $e$ is the electron charge, and $f$ is the radio frequency in Hertz. From Equation B-2, the deviation in refractive index is, for $N_e \ll n^*$

$$\Delta n = \frac{1}{2} \frac{\Delta N_e}{n^*}$$  \hspace{1cm} (B-4)
so that Equation B-1 can be written as

$$\phi(x) = \frac{1}{2} \frac{k}{n} \int \frac{\Delta z}{2} \Delta N_e(x, z) \, dz \quad (B-5)$$

Now the autocorrelation function can be formed as

$$\sigma^2_{\phi} B_{\phi}(\xi) = \left\langle \Delta \phi(x) \Delta \phi(x+\xi) \right\rangle$$

$$= \frac{1}{4} \frac{k^2}{n^*} \int \frac{\Delta z}{2} \int \frac{\Delta z}{2} \left\langle \Delta N_e(x, z) \Delta N_e(x+\xi, z') \right\rangle \, dz \, dz' \quad (B-6)$$

The double integral here can be reduced to a single integration by a change of variables as explained by Par"alis (1965), page 325 as

$$\sigma^2_{\phi} B_{\phi}(\xi) = \frac{\sigma^2_{N_e}}{4} \frac{k^2}{n^*} \int \frac{\Delta z}{2} \int \frac{\Delta z}{2} B_{N_e}(\xi, z-z') \, dz \, dz'$$

If $\Delta z$ is greater than the correlation length of the electron density fluctuations, then the contribution of the second term in the integration will always be negligible so that
Now, by multiplying both sides of Equation B-8 by $e^{i k \xi / 2 \pi}$ and integrating with respect to $\xi$ and using the Fourier transform relationship given by Equations B-11 and B-14 and their 2-D extensions one obtains

$$\phi_\phi(K_x) = \frac{2 \pi \Delta z}{4} \frac{k^2}{n^2} \Phi_{ne}(K_x, K_z = 0)$$

Equation B-9 is a general relationship between the phase spectrum and the 2-dimensional electron density spectrum.

Setting $\xi = 0$ in Equation B-8 and noting that $B_\phi(0) = 1$ gives the relationship between the variance of phase and the variance of electron density fluctuations

$$\sigma_\phi^2 = \frac{\sigma_N^2}{4} \frac{k^2}{n^2} \Delta z \int_{-\infty}^{\infty} B_{ne} (0, n) \, dn$$

B.2 One, Two and Three Dimensional Power Spectra

Given an isotropic and homogeneous random medium with the autocorrelation functions $B_1(x)$, $B_2(o)$, and $B_3(r)$ in one, two, and three-dimensions, then the respective power spectral densities are:

$$\phi_1(K) = \frac{\sigma^2}{2\pi} \int_{-\infty}^{\infty} dx \cos Kx B_1(x)$$

$$\phi_2(K) = \frac{\sigma^2}{2\pi} \int_{0}^{\infty} \rho \, d\rho \, J_0(K\rho) \, B_2(\rho)$$
\[ \Phi_3(K) = \frac{\sigma^2}{2\pi^2 K} \int_0^\infty dr \ r \sin Kr \ B_3(r) \quad (B-13) \]

which have the inverse transforms:

\[ \sigma^2 B_1(x) = \int_{-\infty}^\infty dK \cos Kx \ \phi_1(K) \quad (B-14) \]

\[ \sigma^2 B_2(\rho) = 2\pi \int_0^\infty dK \ K J_0(K\rho) \ \phi_2(K) \quad (B-15) \]

\[ \sigma^2 B_3(r) = \frac{4\pi}{r} \int_0^\infty dK \ K \sin Kr \ \phi_3(K) \quad (B-16) \]

where the subscripts again denote the dimensionality.

These relationships above are consistent with the relationships between the spectra in various dimensions (Rufenach, 1975):

\[ \phi_2(K_x, K_y) = \int dK_z \ \phi_3(K_x, K_y, K_z) \quad (B-17) \]

\[ \phi_1(K_x) = \int dK_y \ \phi_2(K_x, K_y) \quad (B-18) \]
Under the assumption that the autocorrelation function has the same form in one, two, or three dimensions, the following relationships are easily shown for some common autocorrelation functions. Only the 3-dimensional form of the autocorrelation function is specified.

1. Exponential Autocorrelation Function

\[ B(r) = \exp \left\{ -\frac{r}{r_0} \right\} \]  

\[ \phi_1(k) = \frac{\sigma_N^2}{\pi} \frac{r_0}{1 + k^2 r_0^2} \]  

\[ \phi_2(k) = \frac{\sigma_N^2}{2\pi} \frac{r_0^2}{(1 + k^2 r_0^2)^{3/2}} \]  

\[ \phi_3(k) = \frac{\sigma_N^2}{\pi^2} \frac{r_0^3}{(1 + k^2 r_0^2)^2} \]

2. Power-Law Autocorrelation Functions

\[ B(r) = \frac{1}{\left( 1 + \frac{r^2}{r_0^2} \right)^{n-3/2}} \]
(n need not be an integer)

$$\phi_1(K) = \sigma_{Ne}^2 \frac{4-n}{2} \frac{r_o}{\pi^{1/2} \Gamma \left(\frac{n-2}{2}\right)} (Kr_0)^{n-4} \frac{K_{n-4}}{2} (Kr_0),$$  \hspace{1cm} (B-24)

$$\phi_2(K) = \sigma_{Ne}^2 \frac{3-n}{2} \frac{r_o}{\pi \Gamma \left(\frac{n-3}{2}\right)} (Kr_0)^{n-5} \frac{K_{n-5}}{2} (Kr_0),$$  \hspace{1cm} (B-25)

$$\phi_3(K) = \sigma_{Ne}^2 \frac{2-n}{2} \frac{r_o}{\pi^{3/2} \Gamma \left(\frac{n-3}{2}\right)} (Kr_0)^{n-6} \frac{K_{n-6}}{2} (Kr_0),$$  \hspace{1cm} (B-26)

where $K(x)$ is the Bessel function of the third kind.

B.3 Two Dimensional $K^{-2}$ in-situ $N_e$ Spectrum

$\phi^{(1)}_\phi(K)$, the one-dimensional power law phase power spectral density used in this report may be derived by assuming an in-situ $K^{-2}$ spectrum for electron density fluctuations as given by Equation B-20. Then, Equation B-21 and Equation B-9 yield the phase power spectral density

$$\phi_\phi(K) = \frac{2 \pi \Delta z}{4n^2} \frac{k^2}{r^2} \frac{r_o^2}{2\pi} \sigma_{Ne}^2 \frac{\Delta z}{(1+k^2r_o^2)}^{3/2}$$  \hspace{1cm} (B-27)

The integral specified by Equation B-10 may be performed using Equation B-19 as the autocorrelation function to obtain

$$\sigma_{\phi}^2 = \frac{r_o}{2n^2} \frac{k^2 \Delta z}{\sigma_{Ne}^2}$$  \hspace{1cm} (B-28)
or using Equation B-28 in Equation B-27 one comes full circle to obtain

$$\phi_\phi(K) = \sigma_\phi^2 \frac{r_0}{2} \frac{1}{(1+K^2 r_0^2)^{3/2}}$$

(B-29)

which is identical to Equation 1-1 with $r_0$ replaced by $L_0$.

B.4 Two-dimensional Exponential in-situ $N_e$ Spectrum

$\phi^{(2)}_\phi(K)$, the one-dimensional exponential phase PSD given by Equation 1-2 may be obtained from Equation B-25 with $n = 6$ so that Equation B-25 represents a two-dimensional exponential PSD for electron density fluctuations

$$\phi_{N_e}(K) = \sigma_{N_e}^2 \frac{r_0^2}{2\pi} e^{-Kr_0}$$

(B-30)

The autocorrelation function is then

$$B_{N_e}(r) = \frac{1}{(1+(r/r_0)^2)^{3/2}}$$

(B-31)

So that the phase PSD may be determined as

$$\phi_\phi(K) = \sigma_\phi^2 \frac{r_0}{2} e^{-Kr_0}$$

(B-32)

where

$$\sigma_\phi^2 = \frac{r_0}{2n} \frac{k^2 \Delta z}{\sigma_{N_e}^2}$$

(B-33)
APPENDIX C

PHASE-SCREEN REALIZATIONS

For all the 7.5 GHz DSCS simulation results presented in this report the striated region was modeled by ten phase-screens and the simulation was run ten times, each time with a different set of phase-screen realizations, to obtain statistical results. This Appendix shows all ten phase-screens used for the first realization and also the observed intensity at each screen so that the reader may "watch" as the wave propagates through the medium to the receiver plane. For this case the exponential PSD given by Equation 1-2 with a phase standard deviation $\sigma_\phi = 31.6$ radians and a correlation length $\lambda_c = 3.0$ km is used.

The 10 phase screens are shown in Figure C-1 (a-d) as a function of distance $z$ from the top of the disturbed region (see Figure 1 (a)).

Figure C-2 (a-d) shows the intensity observed at the second through tenth phase screen location (the intensity at the first phase-screen location is a constant) and at the receiver plane located 300 km from the tenth phase screen. It is interesting to try to trace the focusing effects which are occurring as the wave propagates through the screen. The Gaussian irregularity denoted by an arrow on the first phase screen ($z = 0$, Figure C-1(a)) can be seen to be the cause of the intensity diffraction pattern which is traceable for $z = 3,300$ km to $z = 15,000$ km and denoted by arrows on each observation screen.
This realization of all ten screens can be used as another visual test of the accuracy of the simulation by using the Fresnel-Kirchhoff equation to analytically compute the diffraction pattern of the Gaussian lens shown in Figure C-3. The diffraction pattern is shown as a function of $z$ on the same scale as used in Figure C-2 and shows a striking resemblance to the results generated for the random screen realization.
Figure C-1(a). Realizations of phase-screens with exponential PSD 
($\sigma_\phi = 31.6$ rad, $\lambda_c = 3$ km).
Figure C-1(b). Realizations of phase-screens with exponential PSD ($\sigma_\phi = 31.6$ rad, $\lambda_\text{c} = 3$ km).
Figure C-1(c). Realizations of phase-screens with exponential PSD ($\sigma_\phi = 31.6 \text{ rad}, \lambda_C = 3 \text{ km}$).
Figure C-1(d). Realizations of phase-screens with exponential PSD ($\sigma_\phi = 31.6 \text{ rad}, \ell_c = 3 \text{ km}$).
Figure C-2 (a). Realizations of intensity at each observation screen location.
Figure C-2 (b). Realizations of intensity at each observation screen location.
Figure C-2 (c). Realizations of intensity at each observation screen location.
Figure C-2 (d). Realizations of intensity at each observation screen location.
Figure C-3. Analytic diffraction pattern of a Gaussian lens as a function of distance $Z$ from the lens.
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