



**AFRL-RX-WP-TP-2010-4144**

**SIMULATION-BASED EXTREME VALUE MARKED  
CORRELATIONS IN FATIGUE OF ADVANCED  
ENGINEERING ALLOYS (PREPRINT)**

**Craig P. Przybyla**

**Georgia Tech  
School of Materials Science and Engineering**

**David L. McDowell**

**Georgia Tech  
GWW School of Mechanical Engineering**

**APRIL 2010**

**Approved for public release; distribution unlimited.**

*See additional restrictions described on inside pages*

**STINFO COPY**

**AIR FORCE RESEARCH LABORATORY  
MATERIALS AND MANUFACTURING DIRECTORATE  
WRIGHT-PATTERSON AIR FORCE BASE, OH 45433-7750  
AIR FORCE MATERIEL COMMAND  
UNITED STATES AIR FORCE**

<b>REPORT DOCUMENTATION PAGE</b>				<i>Form Approved</i> OMB No. 0704-0188	
<p>The public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number. <b>PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.</b></p>					
<b>1. REPORT DATE (DD-MM-YY)</b> April 2010		<b>2. REPORT TYPE</b> Journal Article Preprint		<b>3. DATES COVERED (From - To)</b> 01 April 2010 – 01 April 2010	
<b>4. TITLE AND SUBTITLE</b> SIMULATION-BASED EXTREME VALUE MARKED CORRELATIONS IN FATIGUE OF ADVANCED ENGINEERING ALLOYS (PREPRINT)				<b>5a. CONTRACT NUMBER</b> In-house	
				<b>5b. GRANT NUMBER</b>	
				<b>5c. PROGRAM ELEMENT NUMBER</b> 62102F	
<b>6. AUTHOR(S)</b> Craig P. Przybyla (Georgia Tech, School of Materials Science and Engineering) David L. McDowell (Georgia Tech, GWW School of Mechanical Engineering)				<b>5d. PROJECT NUMBER</b> 4347	
				<b>5e. TASK NUMBER</b> RG	
				<b>5f. WORK UNIT NUMBER</b> M02R3000	
<b>7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)</b> Georgia Tech School of Materials Science and Engineering GWW School of Mechanical Engineering Atlanta, GA 30332				<b>8. PERFORMING ORGANIZATION REPORT NUMBER</b> AFRL-RX-WP-TP-2010-4144	
<b>9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)</b> Air Force Research Laboratory Materials and Manufacturing Directorate Wright-Patterson Air Force Base, OH 45433-7750 Air Force Materiel Command United States Air Force				<b>10. SPONSORING/MONITORING AGENCY ACRONYM(S)</b> AFRL/RXLMN	
				<b>11. SPONSORING/MONITORING AGENCY REPORT NUMBER(S)</b> AFRL-RX-WP-TP-2010-4144	
<b>12. DISTRIBUTION/AVAILABILITY STATEMENT</b> Approved for public release; distribution unlimited.					
<b>13. SUPPLEMENTARY NOTES</b> Journal article submitted to <i>Procedia Engineering</i> . PAO Case Number: 88ABW-2010-0526; Clearance Date: 08 Feb 2010. This work was funded in whole or in part by Department of the Air Force. The U.S. Government has for itself and others acting on its behalf an unlimited, paid-up, nonexclusive, irrevocable worldwide license to use, modify, reproduce, release, perform, display, or disclose the work by or on behalf of the U.S. Government.					
<b>14. ABSTRACT</b> The objective of this research is to estimate the microstructure dependence of the extreme value probabilities of fatigue crack formation at the scale of the grains in polycrystalline and polyphase microstructures to facilitate preliminary parametric design exploration and property assessment. A simulation-based methodology is introduced for computing correlation functions of microstructure attributes marked by the extreme value microstructure-scale fatigue indicator parameters. Multiple statistically representative microstructure volumes simulated using a crystal plasticity constitutive model coupled with the FEM are used to characterize these extreme value marked correlation functions. By comparing these marked correlation functions to traditional correlation functions sampled from the bulk material, the interacting microstructure attributes important to the extreme value response are identified. This methodology is applied to identify important crystallographic relationships relative to fatigue crack formation in the polycrystalline P/M Ni-base superalloy IN100 and duplex Ti-6Al-4V.					
<b>15. SUBJECT TERMS</b> metal fatigue; extreme value statistics; marked correlation functions; microstructure-sensitive design; Ni-base superalloys; Ti-6Al-4V					
<b>16. SECURITY CLASSIFICATION OF:</b>			<b>17. LIMITATION OF ABSTRACT:</b> SAR	<b>18. NUMBER OF PAGES</b> 18	<b>19a. NAME OF RESPONSIBLE PERSON (Monitor)</b> Reji John <b>19b. TELEPHONE NUMBER (Include Area Code)</b> N/A
<b>a. REPORT</b> Unclassified	<b>b. ABSTRACT</b> Unclassified	<b>c. THIS PAGE</b> Unclassified			

Fatigue 2010

# Simulation-based extreme value marked correlations in fatigue of advanced engineering alloys

Craig P. Przybyla<sup>\*,a,b</sup>, David L. McDowell<sup>b,c</sup>

<sup>a</sup>Materials and Manufacturing Directorate, AFRL, Wright-Patterson AFB, OH, 45433, USA

<sup>b</sup>School of Materials Science and Engineering, Georgia Tech, Atlanta, GA, 30332, USA

<sup>c</sup>GWW School of Mechanical Engineering, Georgia Tech, Atlanta, GA, 30332, USA.

**Elsevier use only:** Received date here; revised date here; accepted date here

---

## Abstract

The objective of this research is to estimate the microstructure dependence of the extreme value probabilities of fatigue crack formation at the scale of the grains in polycrystalline and polyphase microstructures to facilitate preliminary parametric design exploration and property assessment. A simulation-based methodology is introduced for computing correlation functions of microstructure attributes marked by the extreme value microstructure-scale fatigue indicator parameters. Multiple statistically representative microstructure volumes simulated using a crystal plasticity constitutive model coupled with the FEM are used to characterize these extreme value marked correlation functions. By comparing these marked correlation functions to traditional correlation functions sampled from the bulk material, the interacting microstructure attributes important to the extreme value response are identified. This methodology is applied to identify important crystallographic relationships relative to fatigue crack formation in the polycrystalline P/M Ni-base superalloy IN100 and duplex Ti-6Al-4V. It was demonstrated that certain high contrast orientation relationships in both IN100 and Ti-6Al-4V (where grains oriented for hard slip are near grains oriented for easier slip) can significantly increase the driving forces for fatigue crack formation.

*Keywords:* metal fatigue; extreme value statistics; marked correlation functions; microstructure-sensitive design; Ni-base superalloys; Ti-6Al-4V.

---

## 1. Introduction

Component service life under cyclic loads (i.e. fatigue) is primarily a function of the extreme value probabilities of life limiting microstructure attributes or combinations of microstructure attributes. The life limiting microstructure attributes are those that increase the driving forces for fatigue crack formation the most within a given volume of material. Moreover, multiple interacting microstructure attributes that exist together with varying probabilities can further enhance local driving forces for fatigue crack formation. Traditionally, the extreme value microstructure dependence of components subjected to cyclic loads has only been captured empirically through extensive experimentation. In the last few decades, much work has been done to better understand the microstructure dependent mechanisms of fatigue crack formation in metals [1, 2]. However, to predict variability in

---

\* Corresponding author. *E-mail address:* [craig.przybyla@wpafb.af.mil](mailto:craig.przybyla@wpafb.af.mil)

the response of damage dependent processes like fatigue crack formation, a framework is needed that accounts for the extreme value life limiting attributes most important to the processes of fatigue crack formation.

Current probabilistic approaches that account for the extreme value statistics of life limiting microstructure attributes relative to fatigue crack formation consider only distributions of a single microstructure attribute and do not account for the effect that multiple interacting microstructure attributes has on the extreme value response distributions. For example, Murakami *et al.* [3, 4] use classical extreme value Gumbel statistics to estimate the size of the largest inclusion based on specimen volume. In this case, the authors use extreme value statistics of inclusion size to estimate the fatigue strength in clean steels based on the assumption that the life limiting fatigue crack tends to form at the largest inclusion within a given volume. Similarly, Atkinson and Shi [5] use a generalized Pereto distribution to estimate the size of the largest inclusion for a given volume. The difference being that the generalized Pereto distribution incorporates a limit on the maximum inclusion size; whereas, the extreme value Gumbel distribution predicts an ever increasing inclusion size for increasing volumes. These types of models based on a single microstructure attribute like inclusion size do not account for the interactions between the inclusion and surrounding matrix, for example. Although first order approaches based on single microstructure attributes may be sufficient for some material systems or applications, the process of fatigue crack formation in many advanced engineering alloys can be very complex. As such, to understand the processes of fatigue crack formation in complex material systems, a better probabilistic description of the interactions between multiple microstructure attributes is required.

The objective of this research is to apply a newly developed extreme value microstructure sensitive probabilistic framework to quantify the influence of polycrystalline microstructure on fatigue crack formation in the polycrystalline P/M Ni-base superalloy IN100 and in duplex Ti-6Al-4V under HCF conditions. Specifically, this new probabilistic framework uses extreme value marked correlation functions for microstructure attributes to quantify the interacting microstructure attributes that are most statistically significant relative to the measured or simulated extreme value distributions of response [6, 7]. Correlation functions for the microstructure attributes important to the operant mechanisms of fatigue crack formation are selectively sampled in regions marked by certain extreme value response parameters (*e.g.* cyclic plastic strain range). These extreme value marked correlations can then be compared to the same correlation functions sampled over the entire microstructure ensemble (*i.e.*, without regard to response) to determine the particular correlated microstructure attributes that are most significant. In general, this methodology can be applied to quantify important correlated microstructure attributes relative to their influence on the extreme value distributions of response for many different damage processes (*e.g.* fatigue, creep, fracture). In this work, multiple material volumes for both IN100 and Ti-6Al-4V are simulated via the FEM with crystal plasticity constitutive relations to explore how local crystallography influences the distributions of the estimated driving forces for fatigue crack formation as estimated by certain cyclic plasticity based fatigue indicator parameters (FIP).

### 1.1. Fatigue crack formation in polycrystalline P/M Ni-base superalloy IN100

Typically, fatigue damage formation in polycrystalline superalloys has been linked to the existence of large pores or nonmetallic inclusions introduced during processing. Fatigue cracks form at inclusions/pores under cyclic loading because of local stress concentrations [8-10]. In some cases, however, cleaner polycrystalline Ni-base superalloys are being developed that exhibit fatigue crack formation along crystallographic planes in samples or components absent of inclusions/pores. For example, Jha *et al.* [11] noted that subsurface fatigue crack formation occurs in individual grains absent of any voids/inclusions in René 88DT in the HCF regime at 593°C. Here the crystallographic facets associated with fatigue crack formation were observed to be much larger than the average grain size, suggesting that cracks tend to form in larger grains. Similar results were reported by Miao *et al.* [12] in the same superalloy in the VHCF regime. In particular, Miao *et al.* noted that the faceted grains near the fatigue crack formation site were associated with large grains, higher Schmid factors for  $\{1\ 1\ 1\} \langle 1\ 1\ 0 \rangle$  slip and twin boundaries of a particular character.

Different slip modes appear to be more important depending on the service temperature. The  $\gamma$  austenitic phase in Ni-base superalloys has a fcc crystalline lattice, which has 12 octahedral  $\{1\ 1\ 1\} \langle 1\ 1\ 0 \rangle$  slip systems. Moreover at certain elevated temperatures an additional 6 cube  $\{1\ 0\ 0\} \langle 1\ 1\ 0 \rangle$  slip systems have been observed in the  $\gamma$  phase in many Ni-base superalloys in the form of macroscopic slip traces [13]. Although limited cube slip is possible in the

L1<sub>2</sub> ordered  $\gamma'$  phase, it is not commonly considered as likely to occur in the austenitic  $\gamma$  phase. Based on observations via transmission electron microscopy (TEM), Bettge and Österle [13], postulated that cube slip observed along  $\{1\ 0\ 0\}$  planes is actually due to the “zig-zag” cross slip of screw dislocations on  $\{1\ 1\ 1\}$  planes when blocked at the  $\gamma/\gamma'$  interfaces. As these dislocation migrate within the channels between  $\gamma'$  precipitates, they create macroscopic  $\{1\ 0\ 0\}$  slip traces. In the polycrystalline P/M Ni-base superalloy IN100, fatigue cracking has been observed to propagate along  $\{1\ 1\ 1\}$  planes at lower homologous temperatures and along  $\{1\ 0\ 0\}$  planes at moderate temperatures (i.e., between 500°C to 800°C) [14].

### 1.2. Fatigue crack formation in $\alpha+\beta$ Ti alloys

Fatigue crack formation in  $\alpha+\beta$  Ti alloys is primarily associated with the development of crystallographic facets at the grain scale. Bridier *et al.* [15, 16] investigated fatigue crack formation in Ti-6Al-4V in both LCF and HCF, respectively, and found that cracks primarily form on basal slip planes and less frequently on prismatic slip planes favorably oriented for slip. Gilbert and Piehler [17] observed internal fatigue crack formation on pyramidal planes in the primary  $\alpha$  grains in Ti-6Al-4V oriented for hard basal slip (i.e., with c axis nearly parallel to the loading direction). Clusters of grains oriented for slip on pyramidal  $\langle a+c \rangle$  planes and grains oriented for basal slip were observed by the authors to enhance fatigue crack formation. Szczepanski *et al.* [18] observed fatigue facet formation in the VHCF regime of Ti-6246 on or near basal or prismatic slip planes favorably oriented for slip. In the same material, Jha and Larsen [19] noted that at moderate stress amplitudes (i.e., close to the macroscopic yield stress) that facets near the location of initial fatigue crack formation were all inclined  $\sim 35\text{--}45^\circ$  relative to the loading axis. In one sample, the facet near the location of initial fatigue crack formation appeared to be  $\sim 35^\circ$  relative to the loading direction in a grain oriented unfavorably for basal slip, suggesting the facet was formed by a  $\langle c+a \rangle$  hard slip mechanism (i.e., pyramidal slip). In another sample, the facet near the location of initial fatigue crack formation developed on an apparent basal slip plane favorably oriented for slip. The grain unfavorably oriented for basal slip that developed the facet was surrounded by other grains more favorably oriented for easy slip (i.e., prismatic or basal slip). Additionally, the sample with the facet that formed in the grain oriented for hard basal slip failed at  $\sim 60,000$  cycles; whereas, in the other sample with the facet that formed in the grain oriented for easy basal slip failed at  $\sim 2,000,000$  cycles.

### 1.3. Fatigue indicator parameters

Simulation-based strategies for investigating the microstructure-dependence of the driving forces for fatigue crack formation have greatly expanded in recent years. McDowell [20] outlined the use of plastic shear strain- based FIPs to estimate the driving forces for fatigue crack formation in metals due to plastic ratcheting and reversed cyclic plasticity. For example, the maximum plastic shear strain range (MPSS) and Fatemi-Socie (FS) [21] damage parameter, i.e.,

$$P_{MRSS} = \frac{\langle \Delta\gamma_{\max}^p \rangle_V}{2} \quad (1)$$

and

$$P_{FS} = \frac{\langle \Delta\gamma_{\max}^p \rangle_V}{2} \left( 1 + K \frac{\sigma_{\max}^n}{\sigma_y} \right) \quad (2)$$

are functions of the maximum plastic shear strain range  $\langle \Delta\gamma_{\max}^p \rangle_V$ . The stress normal to the plane of maximum plastic shear is given by  $\sigma_{\max}^n$ ,  $\sigma_y$  is macroscopic cyclic yield stress, and  $K$  controls the effect of the normal stress on fatigue crack formation. Calculations of the FS FIP for both IN100 and Ti-6Al-4V are carried out with a value of  $K=1$  based on previous studies (e.g. [7]).

Averaged over scales pertinent to the microstructure attributes relevant the processes of fatigue crack formation (i.e, specified by  $V$ ), these types of FIPs have been used to investigate the influence of several different microstructure attributes relative to their potency for fatigue crack formation. In martensitic gear steels, Prasannavenkatesan *et al.* [22] used these two parameters to characterize the relative potency of different kinds of inclusions to form grain/inclusion scale HCF cracks. Similar FIPs have also been used to characterize the influence

of microstructure on fatigue crack formation in structural steel [23, 24] and Ni-base superalloys [6, 7, 25-27]. These efforts have demonstrated the utility in using these types of parameters coupled with crystal plasticity simulations to correlate microstructure scale slip with fatigue crack formation and early stages of microstructurally small crack growth.

## 2. Methodology

### 2.1. Extreme value marked correlation functions

A new microstructure-sensitive extreme value probabilistic framework has been proposed that links correlated microstructure attributes to extreme value response via extreme value marked correlation functions [6, 7]. To construct the extreme value marked correlation functions, one must first construct the extreme value distributions of the response parameter of interest (*e.g.*, stress, strain, plastic strain). Based on classical extreme value probability theory (*cf.* [28]), the probability distribution of the extreme valued response parameter  $\alpha$  (*e.g.*,  $\alpha \equiv \text{FIP}$ ) is defined as  $F^{ex}(\alpha|\Omega)$  given a window  $\Omega$ . Thus,  $F^{ex}(\alpha|\Omega)$  describes the probability that the response parameter of value  $\alpha$  is the extreme value for a sampled volume of microstructure  $\Omega$ . The extreme value marked radial correlation function as  $R^{\max(\alpha)}(\beta, \beta'|r, \Omega)dr$ , is defined as the probability that a microstructure attribute  $\beta$  located coincident with the extreme value response parameter  $\alpha$  in  $\Omega$  is located within a distance of  $r$  to  $r + dr$  of a second microstructure attribute  $\beta'$  in any direction. We can similarly define an extreme value marked  $n$ -point correlation function, extreme value marked lineal path correlation function, extreme value marked nearest neighbor correlation function, etc. [29]. The extreme value response distribution functions describe the extreme value response of the microstructure as represented by the response parameter  $\alpha$ . Coupled with extreme value response distribution, the extreme value marked correlation functions then describes the probabilities of existing correlated microstructure attributes,  $\beta$  and  $\beta'$ , relative to the observed extreme values of  $\alpha$  in a microstructure window  $\Omega$ . Comparing  $R^{\max(\alpha)}(\beta, \beta'|r, \Omega)dr$  to the correlation function for the same microstructure attributes sampled from the complete material ensemble (*e.g.*, bulk) or  $R(\beta, \beta'|r)dr$ , the correlated microstructure attributes most unique to the locations of extreme value response can be identified.

### 2.2. Simulated statistical volume elements

To characterize the microstructure attributes most important to the slip-dominated processes of fatigue crack formation in HCF in IN100 and Ti-6Al-4V, here we consider the crystallographic attributes of the microstructure (*e.g.*, phase, grain orientation, grain disorientation, grain size, and grain shape distributions). In IN100, we recognize that fatigue crack formation is most influence by the presence of non-metallic inclusions and/or pores. However, Ni-base superalloys have been developed with much smaller populations of these types of inclusions/voids that fail crystallographically (*e.g.*, [30]). Thus, here we consider how this variant of IN100 would fail crystallographically in the absence of non-metallic inclusions or voids. In the case of Ti-6Al-4V, fatigue crack formation is predominantly crystallographic and is very much influenced by the microstructure attributes being considered here. The driving forces for fatigue damage formation on the scale of the grains is estimated by the MPSS and the FS FIP as introduce previously. In each microstructure, these parameters are calculated over grain sized averaging volumes.

To construct the extreme value marked correlation functions, multiple simulated statistical volume elements (SVE) or microstructure instantiations (*i.e.*, microstructure window  $\Omega$ ) were constructed for both IN100 and Ti-6Al-4V in the form of meshed polycrystalline microstructures with explicit grains and phases. Using the FEM, variations in local crystallographic response can be simulated using crystal plasticity constitutive relations. Each SVE is constructed based on predefined distributions of grain size, grain orientation, and grain misorientation. Here we define a SVE based on the local plastic response. In other words, each SVE is constructed to be large enough such that the local plastic strain (on the scale of the grains) is unaffected by statistical variations in the microstructure at distances on the order of the size of the SVE [7].

The SVEs for IN100 were constructed based on a Voronoi tessellation algorithm that optimized the microstructure to fit a predefine grain size distribution via a simulated annealing algorithm [7]. The duplex Ti-6Al-4V SVEs were generated using an ellipsoidal based microstructure generator. This method uses known distributions of the aspect ratios of grain equivalent ellipsoids fit to grains of experimentally characterized microstructures. Using

grain equivalent ellipsoids instead of other space filling methods like Voronoi tessellation allows construction of more complex grain morphologies such as elongated grains common in rolled ductile metals. For example, Brahme *et al.* [31] used ellipsoids fit to actual grain distributions to reconstruct Al microstructures with elongated grains. Groeber *et al.* has used similar methods to reconstruct polycrystalline representations of IN100 characterized from three-dimensional serial sections [32, 33]. The ellipsoid packing based digital microstructure generation algorithm was implemented in MATLAB [34], with logic as follows:

1. An ellipsoid is generated by randomly selecting the ellipsoid aspect ratios from a predefined distribution (*e.g.*, beta distribution).
2. The orientation of the ellipse is randomly selected based on a predefined distribution (*i.e.*, orientation distribution function for orientation of major axes of grain equivalent ellipsoids relative to the specimen axis).
3. The ellipsoid is randomly placed in the volume. If the ellipsoid overlaps with any previously placed ellipsoid, a new random location is selected repeatedly until no overlap exists.
4. Steps 1 through 4 are repeated until the jamming limit is reached and no more non-overlapping ellipsoids can be placed in the volume.
5. The ellipsoids are then allowed to grow uniformly until all the space in the microstructure volume is filled.

A two-dimensional section of a generated microstructure using this method with a bi-modal grain size distribution is given in Figure 1. The target and generated bimodal grain size distribution of a SVE for Ti-6Al-4V is given in Figure 2.



Figure 1 2-D section of a microstructure generated using the ellipsoid packing algorithm with a bi-modal grain size distribution.

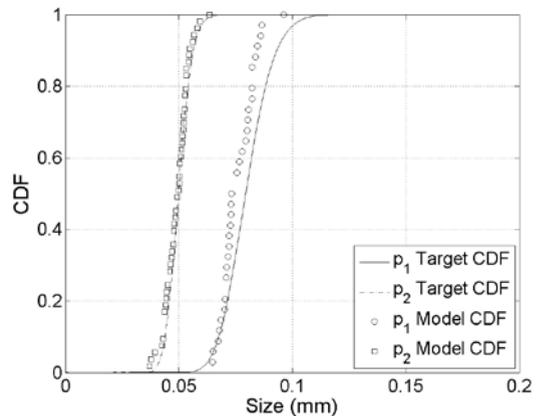


Figure 2 Target log-normal and fit model distributions of the grain size for the primary  $\alpha$  grains and the  $\alpha+\beta$ .

The crystal plasticity constitutive model for IN100 was developed by Shenoy *et al.* [35, 36]. This model does not explicitly model the  $\gamma'$  precipitates, but accounts for the influence of the primary, secondary and tertiary  $\gamma'$  precipitates via certain internal state variables incorporated into certain hardening laws. This model also accounts for the average effect of the grain size on the constitutive response and the dependence of the flow stress on crystallographic orientation. Shenoy *et al.* [35, 36] considers both the standard 12 octahedral  $\langle 110 \rangle \{111\}$  slip systems and 6 cube slip systems  $\{100\} \langle 110 \rangle$ . This crystal plasticity model for IN100 was calibrated at 650°C and incorporated into a User MATerial Subroutine (UMAT) for use in the commercially available FE package ABAQUS [37].

The crystal plasticity model for Ti-6Al-4V was developed by Bridier *et al.* [38] for application to the HCF loading regime for peak stresses at or below the macroscopic yield strength. The model accounts for four different families of slip systems in the primary  $\alpha$  phase: three  $\langle 11\bar{2}0 \rangle \{0001\}$  basal, three  $\langle 11\bar{2}0 \rangle \{10\bar{1}0\}$  prismatic, six  $\langle 11\bar{2}0 \rangle \{10\bar{1}1\}$  first order pyramidal  $\langle a \rangle$  and twelve  $\langle 11\bar{2}3 \rangle \{10\bar{1}1\}$  first order pyramidal  $\langle a+c \rangle$  slip systems or a total of 24 possible modes of slip. However, slip is dominant in the basal and prismatic slip systems due to a relatively low critical resolved shear stress when compared to the other slip systems. The lamellar  $\alpha+\beta$  colonies are homogenized in this model. A crystallographic burgers orientation relation (BOR) is maintained between the

secondary  $\alpha$  and  $\beta$  laths defined such that  $(0001)_\alpha // \{101\}_\beta$  and  $\langle 0001 \rangle_\alpha // \langle 111 \rangle_\beta$ . The 24 possible slip systems in the lamellar region include three  $\langle 11\bar{2}0 \rangle (0001)$  basal, three  $\langle 11\bar{2}0 \rangle \{10\bar{1}0\}$  prismatic, six  $\langle 11\bar{2}0 \rangle \{10\bar{1}1\}$  first-order pyramidal and twelve  $\langle 111 \rangle \{110\}$  bcc slip systems. The bcc slip systems are transformed into the hexagonal coordinate system via the BOR. Hard systems in these colonies are those that intersect the  $\alpha/\beta$  interface. Soft deformation modes are those on which dislocations glide parallel to the  $\alpha/\beta$  interface or have parallel slip planes in both the secondary  $\alpha$  and  $\beta$  phases. This crystal plasticity model was also incorporated as a UMAT in ABAQUS [37].

In all cases, the SVEs were loaded in uniaxial tension at a quasistatic strain rate of  $0.002\text{s}^{-1}$ . Periodic boundary conditions are applied in all directions to simulate subsurface conditions. The voxelated meshes of these generated microstructures consist of quadrilateral elements with reduced integration (type C3D8R in ABAQUS).

In IN100, the number of grains in each simulated SVE ranged between 325–375 grains when each SVE was dimensioned to 0.150 mm along each edge. The distribution of grain volumes normalized by the target average grain volume of  $8.0 \times 10^{-6} \text{mm}^3$  was fit to a log normal distribution with a mean of -12 and standard deviation of 0.4. This corresponds to a target average cube root grain size of  $\sim 0.020 \text{mm}$ . There are 24 elements along each edge of the SVE or 13824 elements in all. For IN100, a total of 100 SVEs were generated. The grain averaged FIPs were calculated after the third simulated cycle to allow for shakedown.

In Ti-6Al-4V, the number of grains in each generated SVE varied between 325–375. The target volume fraction of the primary  $\alpha$  phase was 30%. The standard deviation of the target log-normal grain size distribution for the primary  $\alpha$  phase was 0.025mm and 0.010mm, respectively. For the  $\alpha+\beta$  colonies the mean and standard deviation of the target log-normal grain size distribution was 0.050mm and 0.005mm, respectively. These SVEs were all dimensioned 0.400 mm along each edge. There are 26 elements along each edge of the SVE or 17576 elements in all. For Ti-6Al-4V, a total of 100 SVEs were generated. The grain averaged FIPs were calculated after the tenth cycle.

### 3. Results

#### 3.1. Extreme value marked correlations in IN100

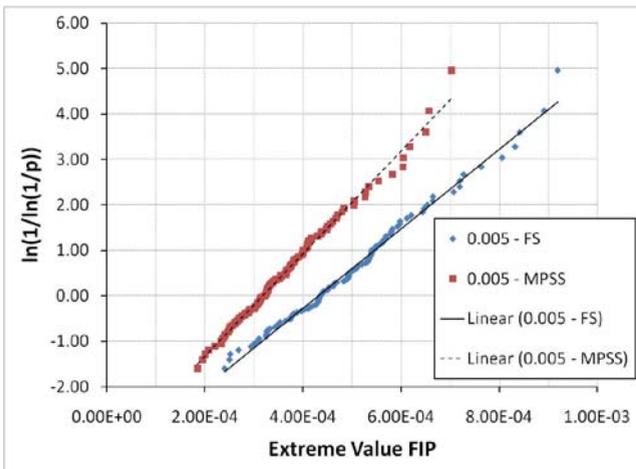


Figure 3 The extreme value grain averaged Fatemi-Socie (FS) and maximum plastic shear strain (MPSS) FIPs calculated over 100 simulated SVEs for IN100 plotted on a Gumbel probability scale.

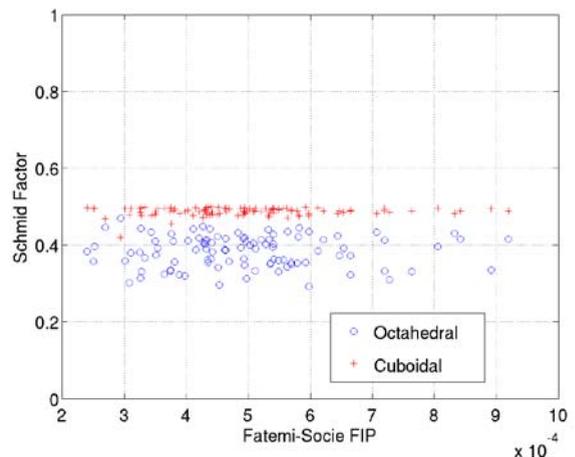


Figure 4 The cross correlations between the Schmid factors for both the octahedral and cube slip systems coincident with the grain average extreme value Fatemi-Socie FIPs in each simulated SVE for IN100.

In Figure 3 we plot the distributions of the extreme value FS and MPSS FIPs calculated from 100 simulated SVEs of IN100, each cycled three times at 0.5% maximum applied strain under completely reversed loading (i.e.  $R=-1$ ). This plot is linearized for the Gumbel distribution as outlined in [7]. The parameters of the Gumbel distributions fit via least squares regression to the observed extreme value FIPs are given in

Table 1 where the Gumbel distribution is given as

$$F_{Y_n}(y_n) = \exp\left[-e^{-\alpha_n(y_n - u_n)}\right] \quad (3)$$

The characteristic largest value of the initial variable  $X$  is given as  $u_n$ , and  $\alpha_n$  is an inverse measure of dispersion of the largest value of  $X$ . The number of samples of the initial variable  $X$  in the set of distributions of  $X$  from which  $Y_n$  is sampled is  $n$ , which for the asymptotic forms listed above is assumed to be very large [39]. The cross correlations between the Schmid factors for both the octahedral and cube slip systems coincident with the grain average extreme value FS FIPs are plotted in Figure 4.

Table 1 Fit Gumbel distribution parameters for the extreme value FIP distributions for IN100.

FIP	$\alpha_n$	$u_n$	$R^2$
FS	$8.73 \times 10^3$	$4.31 \times 10^{-4}$	0.991
MPSS	$1.13 \times 10^4$	$3.18 \times 10^{-4}$	0.993

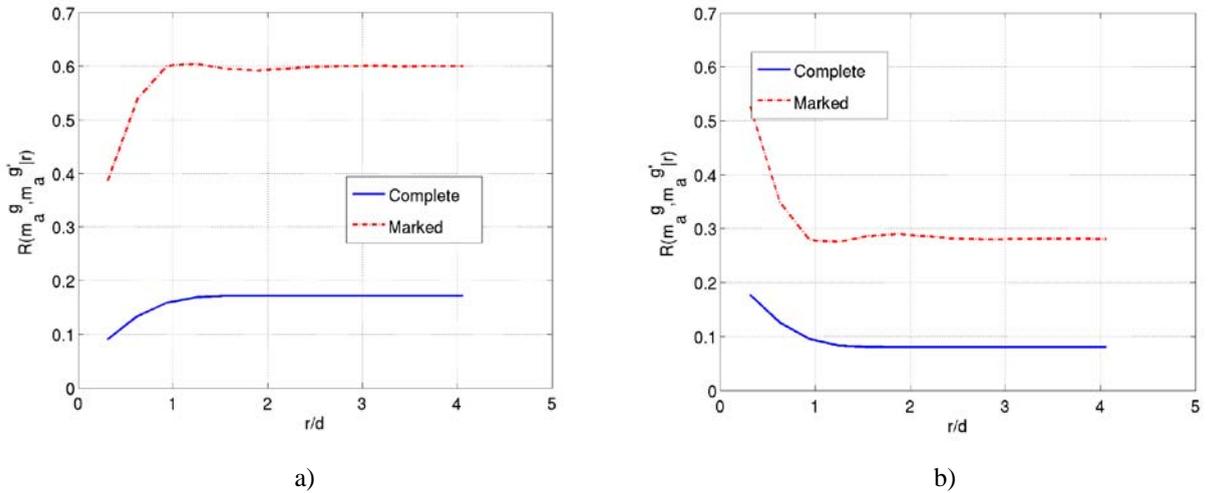


Figure 5 Radial correlation functions for the complete microstructure compared with extreme value marked radial correlation functions describing the correlation between the Schmid factors  $m$  for a) cube slip between 0.45 and 0.5 and octahedral slip between 0.45 and 0.5 and b) cube slip between 0.45 and 0.5 and cube slip between 0.45 and 0.5.

The extreme value marked correlation functions associated with the extreme value distributions of the FIPs are constructed with the microstructure attribute of the Schmid factor (computed based on the geometry of the slip systems relative to the loading direction). By using the Schmid factor, the probabilities of correlated orientations and misorientations of slip systems are indirectly considered. To construct the extreme value marked correlation functions for the Schmid factor the range of considered Schmid factors (0.3 to 0.5) a tessellated scale in 0.05 increments is used. In Figure 5, we plot the complete radial distribution estimated over the entire ensemble of simulated SVEs and the extreme value marked distribution functions sampled only at the location of the extreme value FIPs for the 100 SVEs cycled at 0.5% strain. The particular correlations plotted in Figure 5 are for the Schmid factors for a) cube slip between 0.45 and 0.5 and octahedral slip between 0.45 and 0.5 and b) cube slip between 0.45 and 0.5 and cube slip between 0.45 and 0.5.

### 3.2. Extreme value marked correlations in Ti-6Al-4V

The extreme value distributions of the FS and MPSS FIPs are given in Figure 6 for the 100 SVEs simulated for Ti-6Al-4V and cycled with a positive mean stress ( $R=0$ ) to 0.6% maximum strain. The distributions of the extreme value FIPs are plotted on a Gumbel probability scale as describe previously. The estimated distribution parameters

for the extreme value Gumbel distribution estimated via linear least squares regression are given in Table 2. The cross correlations between the Schmid factors for basal, prismatic, pyramidal  $\langle a \rangle$ , and pyramidal  $\langle a+c \rangle$  slip and the grain average extreme value Fatemi-Socie FIP estimated from each of the 100 simulated SVEs of Ti-6Al-4V are plotted in Figure 7.

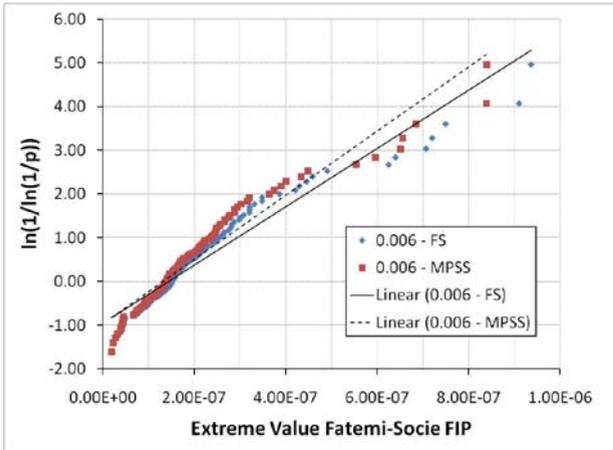


Figure 6 The extreme value grain averaged Fatemi-Socie (FS) and maximum plastic shear strain (MPSS) FIPs calculated over 100 simulated SVEs for Ti-6Al-4V plotted on a Gumbel probability scale.

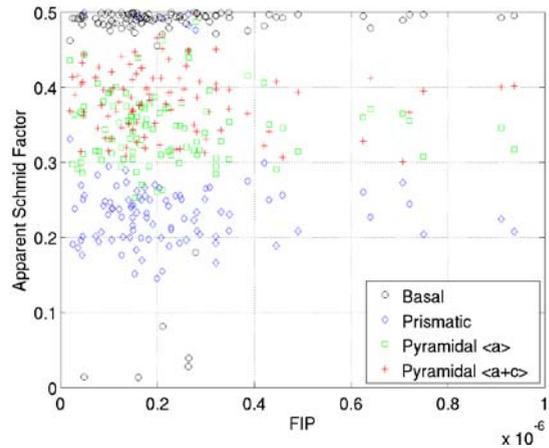


Figure 7 The cross correlations between the Schmid factors for basal, prismatic, pyramidal  $\langle a \rangle$ , and pyramidal  $\langle a+c \rangle$  slip and the grain average extreme value Fatemi-Socie FIP estimated from each of the 100 simulated SVEs of Ti-6Al-4V.

Table 2 Fit Gumbel distribution parameters for the extreme value FIP distributions for Ti-6Al-4V.

FIP	$\alpha_n$	$u_n$	$R^2$
FS	$6.68 \times 10^6$	$1.44 \times 10^{-7}$	0.934
MPSS	$7.33 \times 10^6$	$1.32 \times 10^{-7}$	0.934

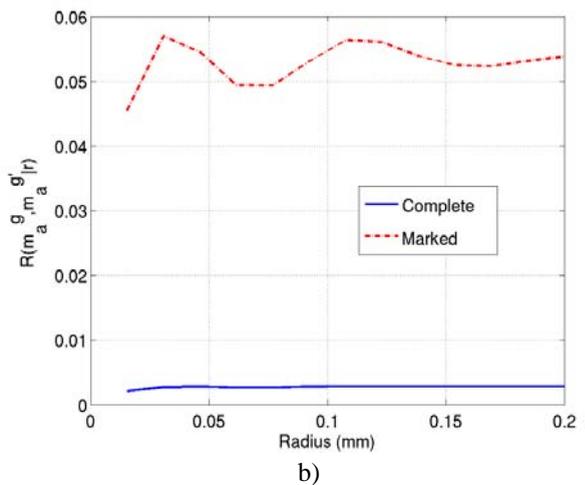
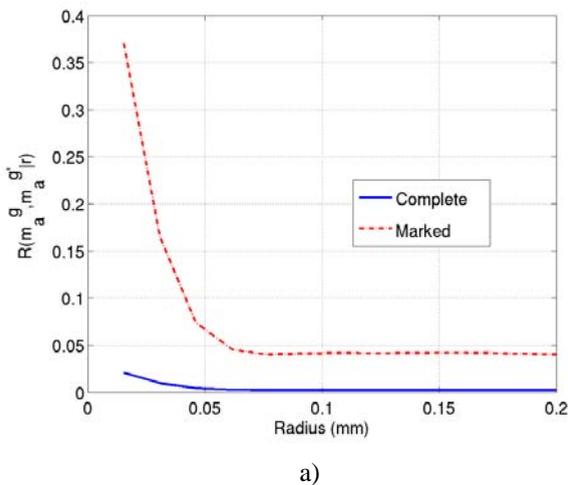


Figure 8 Radial correlation functions for the complete microstructure compared with extreme value marked radial correlation functions describing the correlation between Schmid factors for a) basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and b) basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and prismatic slip between 0.45 and 0.5 for the primary  $\alpha$  phase.

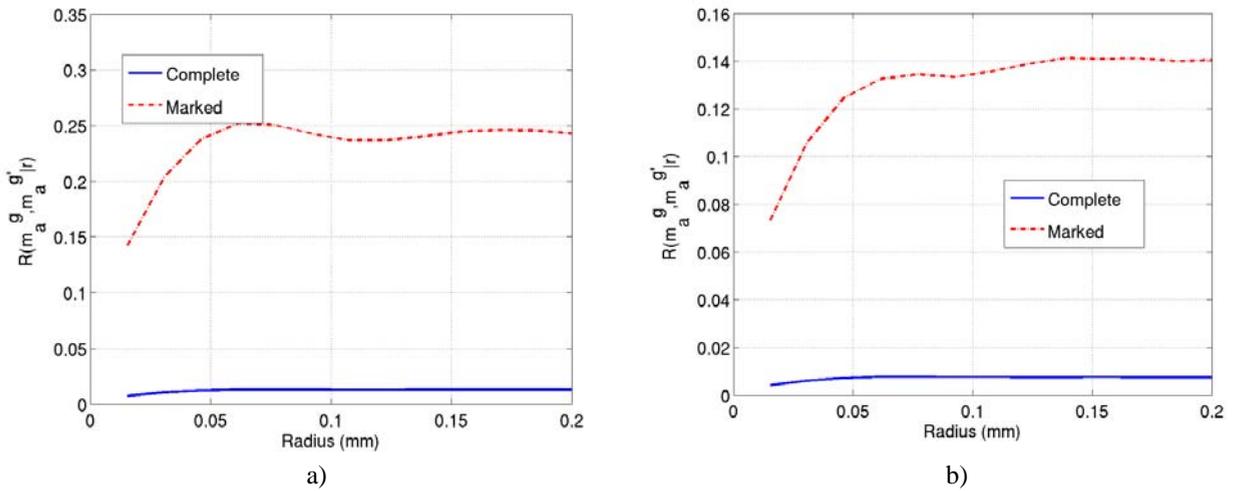


Figure 9 Radial correlation functions for the complete microstructure compared with extreme value marked radial correlation functions describing the correlation between Schmid factors for a) basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and  $\langle 111 \rangle \{110\}$  slip (transformed into the hexagonal coordinate system via the BOR) between 0.45 and 0.5 for the  $\alpha+\beta$  colony phase and, b) basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and pyramidal  $\langle a \rangle$  slip between 0.45 and 0.5 for the  $\alpha+\beta$  colony phase.

As demonstrated previously with IN100, the extreme value marked correlation functions for Ti-6Al-4V are constructed using the microstructure attribute of the Schmid factor. As shown in Figure 7, grains oriented for easy basal slip were observed to be predominate at locations of the estimated extreme value FIPs. In Figure 8, the radial correlation functions for the complete microstructure compared with extreme value marked radial correlation functions are given describing the correlation between Schmid factors for a) basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and b) basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and prismatic slip between 0.45 and 0.5 for the primary  $\alpha$  phase. In Figure 9, the complete and extreme value marked radial distribution functions are given for Schmid factors for a) basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and  $\langle 111 \rangle \{110\}$  bcc slip (transformed into the hexagonal coordinate system via the BOR) between 0.45 and 0.5 for the  $\alpha+\beta$  colony phase and b) basal slip between 0.45 and 0.5 for the primary  $\alpha$  phase and pyramidal  $\langle a \rangle$  slip between 0.45 and 0.5 for the  $\alpha+\beta$  colony phase.

#### 4. Discussion

The extreme value FIP distributions for the FS and MPSS parameters are similar in character for both IN100 and Ti-6Al-4V. In both material systems, there appears to be less scatter in the extreme value MPSS FIP distribution than then FS FIP distribution. This can be quantified by comparing the values of  $\alpha_n$  listed in Tables 1 and 2, recalling that for the Gumbel distribution,  $\alpha_n$  is an inverse measure of the dispersion of the largest values of the initial population. In IN100, the grains predicted to exhibit the extreme value response were different between the MPSS and FS FIPs in as many as 10% of the SVEs simulated. There were no grains with the predicted extreme value response in Ti-6Al-4V with the MPSS FIP that were not identically identified by the FS FIP. Although the distributions are similar between the different FIPs, the FS FIP best captures the actual mechanisms of fatigue crack formation based on the previous experimental observations of the local damage processes acting in this class of materials. As shown by McDowell and Berard [40], the FS parameter reflects mixed mode growth of small fatigue cracks. For IN100 and Ti-6Al-4V it is expected to be effective in reflecting combined effects of slip with elevated normal stress due to intergranular interactions.

In IN100, cube slip is predominate in the locations of predicted extreme value FIPs as evident from Figure 4. In Figure 5, it is evident that there is a much higher probability of finding grains with high Schmid factors (i.e. between 0.45 and 0.5) for cube slip near other grains similarly oriented or octahedral grains with similar high Schmid factors

at the locations of the extreme value FS FIPs than in the overall microstructure. These observations support the results of previous experiments of fatigue in this material system [41]. It is likely that these types of orientation relationships with a high contrast induce additional localized plasticity as the softer phases shed load onto the harder phases during cyclic deformation. Similar high contrast orientation relationships were observed to be important in Ti-6Al-4V.

In Ti-6Al-4V, all of the grains in which the extreme value FIPs are identified were primary  $\alpha$  grains. This is expected because slip is much more difficult in the colony grains, particularly at lower strain amplitudes. To consider the orientation of the grains predicted to exhibit the estimated extreme value response, Schmid factors were identified for the primary  $\alpha$  HCP slip systems including the basal, prismatic, pyramidal  $\langle a \rangle$ , and pyramidal  $\langle a+c \rangle$  slip systems. In Figure 7, the Schmid factor for each type of slip is compared to the extreme value volume averaged FS FIP for each simulation. In most cases, the grains with the maximum grain averaged FIP are oriented for easy basal slip. Additionally, prismatic slip is also observed but much less often. When the magnitude of the Schmid factor for prismatic slip is high (i.e., close to 0.5), the magnitude of the Schmid factor for pyramidal  $\langle a \rangle$  and pyramidal  $\langle a+c \rangle$  also tend to be fairly high.

The extreme value marked correlation functions constructed from the simulated SVEs of Ti-6Al-4V, also indicate that primary  $\alpha$  grains oriented with a Schmid factor for basal slip between 0.45 and 0.5 (easy slip) are much more likely to be found at the location of extreme value response than in the overall microstructure (see Figure 8). This agrees with what was found by Bridier *et al.* [15, 16], who investigated fatigue crack formation in Ti-6Al-4V. When considering multiple correlated microstructure attributes, it was much more probable to find a primary  $\alpha$  grain oriented for easy basal slip or prismatic slip near hard oriented  $\alpha+\beta$  colonies with high Schmid factors for BOR modified bcc slip or primary  $\alpha$  grains with high Schmid factors for pyramidal  $\langle a+c \rangle$  slip at the locations of the extreme value FS FIP than in the overall microstructure (see Figure 9). The latter previously mentioned correlated orientation relationships were also identified by Gilbert and Piehler [17] and Bantounas *et al.* [42] in Ti-6Al-4V. Various work in  $\alpha+\beta$  Ti alloys have demonstrated that these types of hard-soft grain combinations can dramatically increase the local stress state which in turn promotes increased plasticity in these regions [26, 43–47]. Thus, similar to that of IN100, these high contrast orientation relationships between softer basal or prismatic grains oriented for easy slip near harder grains oriented for pyramidal or bcc BOR modified slip are predicted to significantly increase the local driving forces for fatigue damage formation.

## 5. Conclusions

This work has demonstrated the use of a new microstructure-sensitive extreme value probabilistic framework that links the extreme value driving forces for fatigue crack formation in a P/M IN100 and Ti-6Al-4V to the important correlated microstructure attributes that most influence that extreme value response. Specifically, we conclude that:

- Multiple statistical volume elements (SVEs) can be constructed and simulated using appropriate constitutive models to estimate extreme value distributions of key response parameters.
- Cyclic plastic strain based fatigue indicator parameters calculated over nonlocal averaging volumes on the scale of the microstructure attributes important to the mechanisms of fatigue crack formation can be used to identify key microstructure attributes important to the extreme value response.
- In agreement with experiments, the simulations for IN100 predict that cube slip may play an important role in fatigue damage formation particularly when there are multiple grains oriented for cube slip clustered in the same region or clusters of grains oriented for cube slip surrounded by other grains oriented favorably for octahedral slip [14]. Thus, as fatigue crack formation is dominated by the presence of non-metallic inclusions or voids for this particular material system, we expect that given two inclusions of similar character that fatigue cracks will form preferentially near the inclusion that is surrounded by grains or grain clusters unfavorably oriented for octahedral slip.
- In agreement with experiments, the simulations for Ti-6Al-4V predict that primary  $\alpha$  grains oriented favorably for basal slip (with a Schmid factor for basal slip between 0.45 and 0.5) have a much higher probability of being associated with the regions of extreme value behavior than in the overall microstructure [15, 16]. Additionally, hard-soft grain interactions between primary  $\alpha$  grains oriented favorably for basal slip and primary  $\alpha$  grains oriented favorably for pyramidal  $\langle a+c \rangle$  or  $\alpha+\beta$  colonies oriented favorably for bcc BOR modified slip are important relative to increased driving forces for fatigue crack formation [17, 42].

## Acknowledgements

The authors would like to acknowledge the support of the NSF Center for Computational Materials Design, a joint Penn State–Georgia Tech I/UCRC, for development of extreme value HCF and VHCF statistical methods informed by microstructure-sensitive computational models. In addition, Craig P. Przybyla is grateful for the financial support of the Graduate Coop Program at the Air Force Research Laboratory at Wright-Patterson Air Force Base, Dayton, Ohio.

## References

- [1] S. Suresh, *Fatigue of Materials*, 2nd ed. Cambridge: Cambridge University Press, 1998.
- [2] D. L. McDowell, "Basic issues in the mechanics of high cycle metal fatigue," *International Journal of Fracture*, vol. 80, pp. 103-45, 1996.
- [3] Y. Murakami, S. Kodama, and S. Konuma, "Quantitative evaluation of defects of non-metallic inclusions on fatigue strength of high strength steels. I: Basic fatigue mechanism and evaluation of correlation between the fatigue fracture stress and the size and location of non-metallic inclusions," *International Journal of Fatigue*, vol. 11, pp. 291-298, 1989.
- [4] S. Beretta and Y. Murakami, "Statistical analysis of defects for fatigue strength prediction and quality control of materials," *Fatigue & Fracture of Engineering Materials & Structures*, vol. 21, pp. 1049-1065, 1998.
- [5] H. V. Atkinson and G. Shi, "Characterization of inclusions in clean steels: a review including the statistics of extremes methods," *Progress in Materials Science*, vol. 48, pp. 457-520, 2003.
- [6] C. Przybyla, R. Prasannavenkatesan, N. Salajegheh, and D. L. McDowell, "Microstructure-sensitive modeling of high cycle fatigue," *International Journal of Fatigue*, vol. 32, pp. 512-525, 2009.
- [7] C. P. Przybyla and D. L. McDowell, "Microstructure-Sensitive Extreme Value Probabilities for High Cycle Fatigue of Ni-Base Superalloy IN100," *International Journal of Plasticity*, in press, 2009 doi:10.1016/j.ijplas.2009.08.001.
- [8] J. M. Hyzak and I. M. Bernstein, "The effect of defects on the fatigue crack initiation process in 2 p/m super-alloys. 1. Fatigue origins," *Metallurgical Transactions a-Physical Metallurgy and Materials Science*, vol. 13, pp. 33-43, 1982.
- [9] M. Goto and D. M. Knowles, "Initiation and propagation behaviour of microcracks in Ni-base superalloy Udimet 720 Li," *Engineering Fracture Mechanics*, vol. 60, pp. 1-18, 1998.
- [10] H. T. Pang and P. A. S. Reed, "Fatigue crack initiation and short crack growth in nickel-base turbine disc alloys-the effects of microstructure and operating parameters," *International Journal of Fatigue*, vol. 25, pp. 1089-1099, 2003.
- [11] S. K. Jha, M. J. Caton, J. M. Larsen, A. H. Rosenberger, K. Li, and W. J. Porter, "Superimposing mechanisms and their effect on the variability in fatigue lives of a nickel-based superalloy," in *Materials Damage Prognosis*, J. M. Larsen, L. Christodoulou, J. R. Calcaterra, M. L. Dent, M. M. Derriso, W. J. Hardman, J. W. Jones, and S. M. Russ, Eds.: TMS (The Minerals, Metals & Materials Society), 2005.
- [12] J. S. Miao, T. M. Pollock, and J. W. Jones, "Crystallographic fatigue crack initiation in nickel-based superalloy Rene 88DT at elevated temperature," *Acta Materialia*, vol. 57, pp. 5964-5974, 2009.
- [13] D. Bettge and W. Österle, "'Cube slip' in near-[111] oriented specimens of a single-crystal nickel-base superalloy," *Scripta Materialia*, vol. 40, pp. 389-395, 1999.
- [14] K. Li, N. E. Ashbaugh, and A. H. Rosenberger, "Crystallographic Initiation of Nickel-Base Superalloy IN100 at RT and 538°C Under Low Cycle Fatigue Conditions," in *Superalloys 2004*, K. A. Green, T. M. Pollock, H. Harada, T. E. Howson, R. C. Reed, J. J. Schirra, and S. Walston, Eds. Champion, Pennsylvania: The Minerals, Metals & Materials Society (TMS), 2004.
- [15] F. Bridier, P. Villechaise, and J. Mendez, "Analysis of slip and crack initiation processes activated by fatigue in a  $\alpha/\beta$  titanium alloy in relation with local crystallographic orientation," presented at 9th International Fatigue Congress, Atlanta, GA, 2006.
- [16] F. Bridier, P. Villechaise, and J. Mendez, "Slip and fatigue crack formation processes in an  $\alpha$  titanium alloy in relation to crystallographic texture on different scales," *Acta Materialia*, vol. 56, pp. 3951-3962, 2008.
- [17] J. L. Gilbert and H. R. Piehler, "On the nature and crystallographic orientation of subsurface cracks in high cycle fatigue of Ti-6Al-4V," *Metallurgical Transactions A-Physical Metallurgy and Materials Science*, vol. 24, pp. 669-680, 1993.
- [18] C. J. Szczepanski, S. K. Jha, J. M. Larsen, and J. W. Jones, "Microstructural influences on very-high-cycle fatigue-crack initiation in Ti-6246," *Metallurgical and Materials Transactions A-Physical Metallurgy and Materials Science*, vol. 39A, pp. 2841-2851, 2008.
- [19] S. K. Jha and J. M. Larsen, "Random heterogeneity scales and probabilistic description of the long-lifetime regime of fatigue," in *Fourth International Conference on Very High Cycle Fatigue (VHCF-4)*, J. E. Allison, J. W. Jones, J. M. Larsen, and R. O. Ritchie, Eds. Ann Arbor, Michigan, USA: The Minerals, Metals and Materials Society (TMS), 2007, pp. 385-96.
- [20] D. L. McDowell, "Simulation-based strategies for microstructure-sensitive fatigue modeling," *Materials Science and Engineering A*, vol. 468-470, pp. 4-14, 2007.
- [21] A. Fatemi and D. F. Socie, "A critical plane approach to multiaxial fatigue damage including out-of-phase loading," *Fatigue and Fracture of Engineering Materials and Structures*, vol. 11, pp. 149-65, 1988.
- [22] R. Prasannavenkatesan, J. X. Zhang, D. L. McDowell, G. B. Olson, and H. J. Jou, "3D modeling of subsurface fatigue crack nucleation potency of primary inclusions in heat treated and shot peened martensitic gear steels," *International Journal of Fatigue*, vol. 31, pp. 1176-1189, 2009.
- [23] R. Döring, J. Hoffmeyer, T. Seeger, and M. Vormwald, "Short fatigue crack growth under nonproportional multiaxial elastic-plastic strains," *International Journal of Fatigue*, vol. 28, pp. 972-982, 2006.

- [24] J. Hoffmeyer, R. Döring, T. Seeger, and M. Vormwald, "Deformation behaviour, short crack growth and fatigue lives under multiaxial nonproportional loading," *International Journal of Fatigue*, vol. 28, pp. 508-520, 2006.
- [25] M. Shenoy, J. Zhang, and D. L. McDowell, "Estimating fatigue sensitivity to polycrystalline Ni-base superalloy microstructures using a computational approach," *Fatigue & Fracture of Engineering Materials & Structures*, vol. 30, pp. 889-904, 2007.
- [26] F. P. E. Dunne, A. J. Wilkinson, and R. Allen, "Experimental and computational studies of low cycle fatigue crack nucleation in a polycrystal," *International Journal of Plasticity*, vol. 23, pp. 273-295, 2007.
- [27] K. O. Findley and A. Saxena, "Low cycle fatigue in Rene 88DT at 650 degrees C: Crack nucleation mechanisms and modeling," *Metallurgical and Materials Transactions A-Physical Metallurgy and Materials Science*, vol. 37A, pp. 1469-1475, 2006.
- [28] E. J. Gumbel, *Statistics of Extremes*. New York: Columbia University Press, 1958.
- [29] S. Torquato, *Random heterogeneous materials : microstructure and macroscopic properties*. New York: Springer, 2002.
- [30] J. Miao, T. M. Pollock, and J. W. Jones, "Fatigue crack initiation in nickel-based superalloy René 88 DT at 593°C," presented at Superalloys, Champion, Pennsylvania, 2008.
- [31] A. Brahme, M. H. Alvi, D. Saylor, J. Fridy, and A. D. Rollett, "3D reconstruction of microstructure in a commercial purity aluminum," *Scripta Materialia*, vol. 55, pp. 75-80, 2006.
- [32] M. Groeber, S. Ghosh, M. D. Uchic, and D. M. Dimiduk, "A framework for automated analysis and simulation of 3D polycrystalline micro structures. Part 1: Statistical characterization," *Acta Materialia*, vol. 56, pp. 1257-1273, 2008.
- [33] M. Groeber, S. Ghosh, M. D. Uchic, and D. M. Dimiduk, "A framework for automated analysis and simulation of 3D polycrystalline micro structures. Part 2: Synthetic structure generation," *Acta Materialia*, vol. 56, pp. 1274-1287, 2008.
- [34] "MATLAB," 7.6.0.324 (R2008a) ed: The MathWorks, Inc., 2008.
- [35] M. Shenoy, J. Zhang, and D. L. McDowell, "Estimating fatigue sensitivity to polycrystalline Ni-base superalloy microstructures using a computational approach," *Fatigue and Fracture of Engineering Materials and Structures*, vol. 30, pp. 889-904, 2007.
- [36] M. Shenoy, Y. Tjijptowidjojo, and D. McDowell, "Microstructure-sensitive modeling of polycrystalline IN 100," *International Journal of Plasticity*, vol. 24, pp. 1694-1730, 2008.
- [37] "ABAQUS," 6.7-3 ed. Providence, RI: Simulia, 2007.
- [38] F. Bridier, D. L. McDowell, P. Villechaise, and J. Mendez, "Crystal plasticity modeling of slip activity in Ti-6Al-4V under high cycle fatigue loading," 2008.
- [39] A. Haldar and S. Mahadevan, *Probability, Reliability and Statistical Methods in Engineering Design*. New York: John Wiley & Sons, Inc., 2000.
- [40] D. L. McDowell and J. Y. Berard, "A  $\Delta J$ -based approach to biaxial fatigue," *Fatigue and Fracture of Engineering Materials and Structures*, vol. 15, pp. 719-41, 1992.
- [41] K. Li, N. E. Ashbaugh, and A. H. Rosenberger, "Crystallographic initiation of nickel-base superalloys IN100 at RT and 538°C under low cycle fatigue conditions," presented at Superalloys, Champion, Pennsylvania, 2004.
- [42] I. Bantounas, D. Dye, and T. C. Lindley, "The effect of grain orientation on fracture morphology during high-cycle fatigue of Ti-6Al-4V," *Acta Materialia*, vol. 57, pp. 3584-3595, 2009.
- [43] V. Hasija, M. J. Mills, D. S. Joseph, and S. Ghosh, "Deformation and creep modeling in polycrystalline Ti-6Al alloys," *Acta Materialia*, vol. 51, pp. 4533-4549, 2003.
- [44] G. Venkataramani, D. Deka, and S. Ghosh, "Crystal plasticity based Fe model for understanding microstructural effects on creep and dwell fatigue in Ti-6242," 2006.
- [45] G. Venkataramani, S. Ghosh, and M. Mills, "A size-dependent crystal plasticity finite-element model for creep and load shedding in polycrystalline titanium alloys," *Acta Materialia*, vol. 55, pp. 3971-3986, 2007.
- [46] F. P. E. Dunne and D. Rugg, "On the mechanisms of fatigue facet nucleation in titanium alloys," *Fatigue and Fracture of Engineering Materials and Structures*, vol. 31, pp. 949-958, 2008.
- [47] F. P. E. Dunne, D. Rugg, and A. Walker, "Lengthscale-dependent, elastically anisotropic, physically-based hcp crystal plasticity: Application to cold-dwell fatigue in Ti alloys," *International Journal of Plasticity*, vol. 23, pp. 1061-1083, 2007.