

# **Thermal-Electrical FEA of Localized Heating for MEMS Packaging**

C.L. Xie and M. Hailat  
Noveltech, Inc., Plymouth, MI 48170

G. Newaz  
Wayne State University, Detroit, MI 48202

J. R. Mabesa Jr.  
U. S. Army RDECOM-TARDEC, Warren, MI 49397

Category: Advanced Modeling and Simulation

## **ABSTRACT**

Localized silicon fusion and eutectic bonding for MEMS packaging have been preliminarily investigated through the U.S. Army SBIR Phase I program entitled “Multi-Power Source for MEMS Packaging”, contract #: W56HZV-05-C-0092. This methodology allows localized heating at the bonding area without overheating the temperature-sensitive MEMS device. This paper presents the newly developed three-dimensional finite element analysis (FEA) of localized heating for MEMS packaging, for analysis of the electrical problem, thermal problem, and the coupling between the two problems. It was confirmed that high temperature is confined and controllable in the heater-on-circuit localized heating technology.

## **1. INTRODUCTION**

Micro electro-mechanical system (MEMS) represents the integration of mechanical components, sensors, actuators and electronics on a silicon wafer. MEMS devices are in demand for applications that range from automobiles and aerospace to biomedical, navigation and cell phones, including accelerometers, gyroscopes, pressure sensors, optical scanners, RF switches, etc [1-5]. While MEMS are shrinking sensors and actuators into micro and nanometer scales, MEMS packaging, the most expensive and time-consuming step in overall MEMS manufacturing, emerges as the bottleneck for successful device commercialization [6]. Usually, MEMS packaging starts after micromachining is complete or released. This post-packaging process must not damage either pre-fabricated MEMS microstructures or microelectronics. The key additional requirements on MEMS packaging beyond the

## Report Documentation Page

*Form Approved*  
*OMB No. 0704-0188*

Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.

1. REPORT DATE <b>27 NOV 2006</b>	2. REPORT TYPE <b>N/A</b>	3. DATES COVERED <b>-</b>	
4. TITLE AND SUBTITLE <b>Thermal-Electrical FEA of Localized Heating for MEMS Packaging</b>		5a. CONTRACT NUMBER	
		5b. GRANT NUMBER	
		5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S) <b>C.L. Xie; M. Hailat; G. Newaz; J. R. Mabesa Jr</b>		5d. PROJECT NUMBER	
		5e. TASK NUMBER	
		5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) <b>US Army RDECOM-TARDEC 6501 E 11 Mile Rd Warren, MI 48397-5000, USA Noveltech, Inc., Plymouth, MI 48170 Wayne State University, Detroit, MI 48202</b>		8. PERFORMING ORGANIZATION REPORT NUMBER <b>16351</b>	
		9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)	
		10. SPONSOR/MONITOR'S ACRONYM(S) <b>TACOM/TARDEC</b>	
		11. SPONSOR/MONITOR'S REPORT NUMBER(S) <b>16351</b>	
12. DISTRIBUTION/AVAILABILITY STATEMENT <b>Approved for public release, distribution unlimited</b>			
13. SUPPLEMENTARY NOTES <b>The original document contains color images.</b>			
14. ABSTRACT			
15. SUBJECT TERMS			
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT <b>SAR</b>
a. REPORT <b>unclassified</b>	b. ABSTRACT <b>unclassified</b>	c. THIS PAGE <b>unclassified</b>	
19a. NAME OF RESPONSIBLE PERSON			

packaging requirements of standard semiconductor devices are to maintain a cavity for the motion of the MEMS and to prevent contamination due to the sensitive nature of the MEMS' moving structures and their exposed surfaces. The rigorous MEMS packaging requirements involve wafer-level packaging, hermetic sealing, and long-term stability [7-12]. The processes may need to be done at 200~1000°C, however, the temperature-sensitive electronic circuitry and MEMS devices must be kept from overheating (<400°C). A potential solution is to develop localized heating method to ensure reliable bonding without affecting other components. This work is focusing to develop a methodology of the three-dimensional finite element analysis (FEA) for MEMS packaging on die level by localized heating and silicon-gold eutectic bonding, a heater-on-circuit technology is being investigated.

## **2. LOCALIZED HEATING AND Au-Si EUTECTIC BONDING**

Using microheaters instead of global heating furnaces, as shown in Fig.1 (a), provides localized heating. These microheaters are constructed in a way that heating is restricted in a small region surrounding by insulation materials. Based on the principle of silicon-gold eutectic bonding, gold microheaters was built and subject to be bonded to a cap substrate, A Si wafer was used as the substrate. A SiO<sub>2</sub> thin film was deposited on the Si wafer surface, which serves as the thermal and electric insulation. The gold resistive heater was sputtered on the top of the oxide layer. The gold microheater was used as the heating and bonding material. A silicon cap substrate was placed on the top of the microheater and in intimate contact. When an electrical current is applied, the temperature of the microheater rises to activate the bonding process. The gold in intimate contact with the silicon is heating up to at least 363°C, which causes the gold atoms to diffuse into the silicon. When the eutectic composition (19 at% of Silicon) is reached, as shown in Fig.1 (b), a liquid layer is formed at the interface and the eutectic alloy grows until the gold is exhausted. The alloy can then be cooled slowly, causing it to solidify and hence forming the bond.

Based on the principle of localized heating and Au-Si eutectic bonding, gold microheaters was built and subject to be bonded to a cap substrate, as illustrated in Fig. 2. A P-type Si wafer with (100) orientation was used as the substrate. A silicon dioxide (SiO<sub>2</sub>) thin film was deposited on the Si wafer surface, which serves as the thermal and electric insulation. Then, the gold resistive heater was sputtered on the top of the oxide layer. The microheater was patterned in a line-shape with contact pads in two ends. The gold microheater was used as the heating and bonding material. A silicon cap substrate was placed

on the top of the microheater and in intimate contact. When an electrical current is applied, the temperature of the microheater rises to activate the bonding process. The gold in intimate contact with the silicon is heating up to at least 363°C, which causes the gold atoms to diffuse into the silicon. This process is suitable to bond silicon wafer to wafer with hermetic packaging.

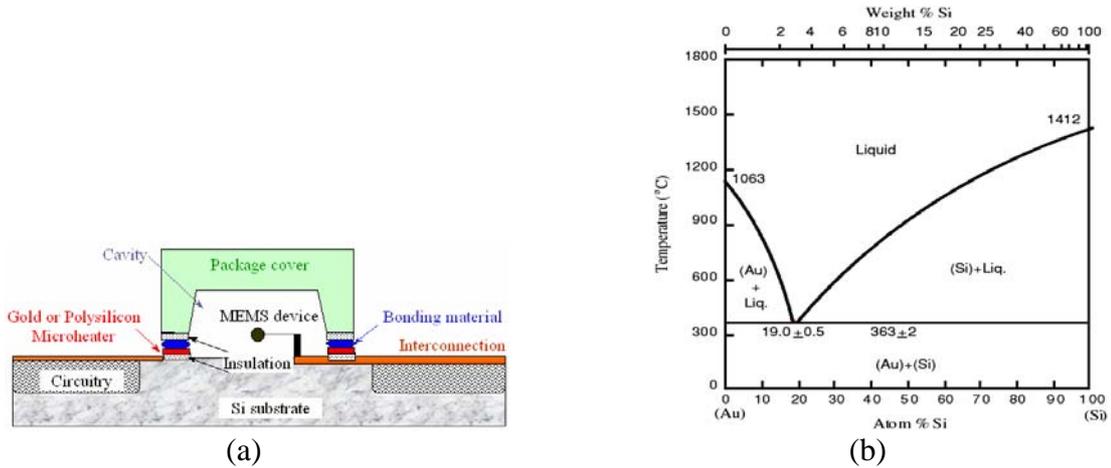


Fig. 1 (a) MEMS packaging by localized heating and bonding, (b) Binary phase Diagram of Au-Si alloy.

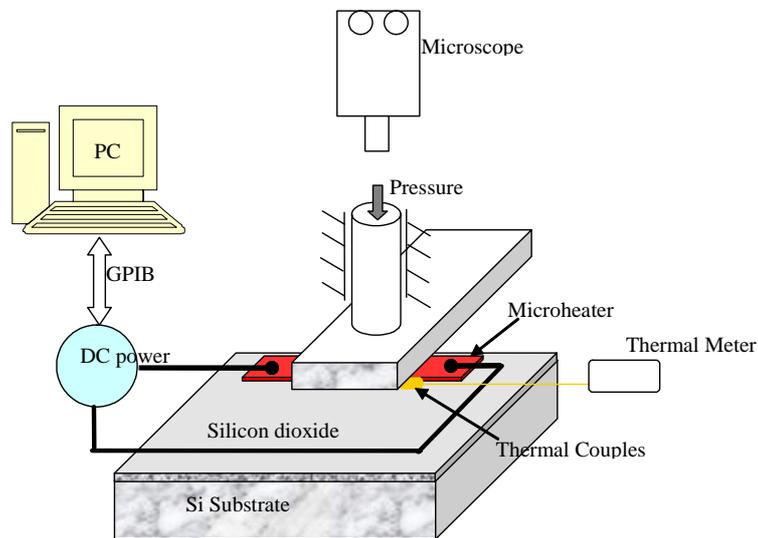


Fig.2 Schematic of the bonding stage.

### 3. THERMAL-ELECTRICAL FE MODELING OF LOCALIZED HEATING FOR MEMS PACKAGING

A three-dimensional finite element (FE) modeling was established for analysis of the coupled thermal-electrical problems of MEMS packaging. Joule heating arises when the energy dissipated by an electrical current flowing through the gold microheater is converted into thermal energy for bonding.

#### 3.1 Line-shape Model

The cross-sectional view of a line-shape model is shown in Fig.3 (a). The structure configuration and dimensions of the model were designed based on our fusion bonding experimental setup described above. ABAQUS/Standard was used for analysis of the coupled thermal-electrical procedure, including analysis of the electrical problem, the thermal problem, and the coupling between the two problems [13]. The physical properties used in the simulation are listed in Table 1.

Fig.3 (b) shows temperature distribution on a gold microheater with the dimensions of  $100 \times 8 \times 1.5 \mu\text{m}$ . It was found that under an input current of 1.3Amp, the heater could generate a temperature of about  $450^\circ\text{C}$ . The simulated heat transfer is shown in Fig.3 (a) and b) illustrating the isotherms of the silicon-gold bonding process. The steady-state isotherms on the cross section diagram clearly demonstrate that the high temperature region is confined in a small area surrounding the heater. When temperature on the center of the microheater reaches  $450^\circ\text{C}$ , the temperature is only  $50^\circ\text{C}$ , in a distance of less than  $1\mu\text{m}$  into the insulation layer. The most area of the silicon substrate maintains at room temperature during the process. Therefore, localized heating can be achieved without affecting the microelectronics or other temperature sensitive materials at the wafer-level. It was confirmed that high temperature is confined and controllable in the heater-on-circuit localized heating technology.

Table 1. Physical properties

	Thermal conductivity W/(m K)		Electrical conductivity ( $1/\Omega\text{-m}$ )		Specific heat cal/(g K)		Density ( $\text{g/cm}^3$ )
Gold	317.0	at 313K	$4.5 \times 10^7$	at 313K	108.0	at 313K	19.32
	304.0	at 500K	$1.1 \times 10^7$	at 1000K	205.0	at 1100K	
	284.0	at 800K					
	255.0	at 1200K					
Silicon	136.0	at 313K	$1.6 \times 10^{-3}$	at 313K	0.180	at 298K	2.2
	105.0	at 800K	$3.0 \times 10^{-4}$	at 1100K	0.253	at 1800K	
Silicon dioxide	1.4	at 313K	$1.0 \times 10^{-6}$	at 313K	700.0		2.2

0.1 at 800K  $1.0 \times 10^{-5}$  at 110K

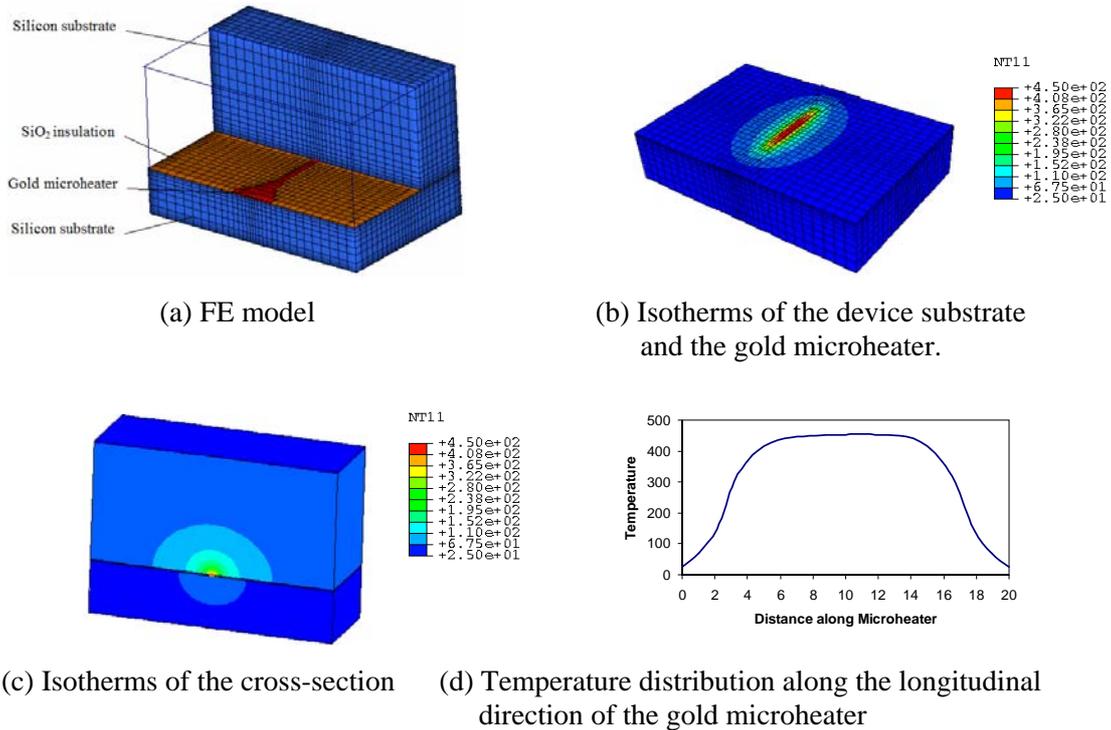
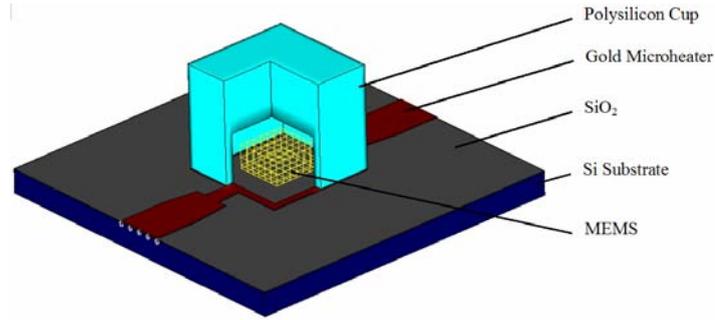


Fig.3 Line-shape FE modeling of localized heating

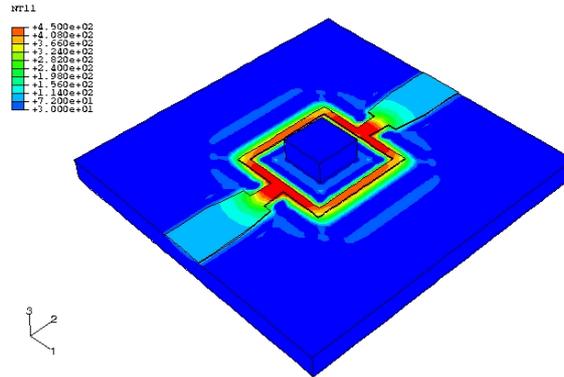
### 3.2 Cup Model

A three-dimensional FE modeling was established for MEMS packaging with localized heating/bonding. It consists of MEMS, Si substrate, SiO<sub>2</sub> insulation, microheater, and polysilicon cup, as shown in Fig.4 (a). The MEMS' dimensions are 60×60×30μm. The cross-section and the edge dimensions of the gold microheater in the bonding area are 10×1.5×120μm. The simulation results as shown in Fig. 4 (b-c) infer that:

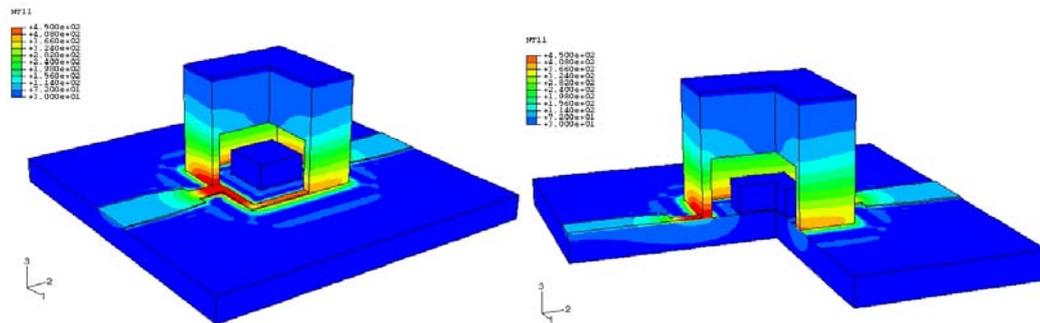
- 1) The temperature of the MEMS inside the package remains below 30°C while the temperature of bonding area is above 450°C in steady status, which confirmed the concept of localized heating.
- 2) The distribution of temperature on the microheater is not uniform. The temperature of the corner is lower than that of the center because of the difference of cross-section area.



(a) Cup Shape Model



(b) Isotherms of the device substrate and the gold microheater



(c) Isotherms of the MEMS, substrate and gold microheater

Fig.4 Cup model of MEMS packaging with localized heating

#### 4. DISCUSSIONS AND CONCLUSION

MEMS post-packaging by localized heating and bonding provides unique opportunities in developing packaging processes for microsystems with theoretical, experimental and engineering challenges. The phase I work addressed the fundamental issues and approaches in the packaging of MEMS devices and provides directions for future research. From the thermal-electrical modeling of localized heating, it was confirmed that high temperature is confined and temperature is controllable.

In order to achieve a successfully localized heating and bonding technology applied to a uniform, high-yield, reproducible, Au-Si eutectic bonding for wafer-level MEMS vacuum packaging, several fundamental and challenging problems should be carefully studied in both theoretical and experimental regimes. Specific areas to be explored are as follows:

- 1) Characterizations of localized bonding mechanisms such as the bond quality and uniformity between silicon-gold, and polysilicon-gold.
- 2) Investigations of the effects of temperature, environment, time, applied pressure and surface roughness on the bonding processes.
- 3) Investigations of long term stability of localized bonds such as tensile and shear tests, hermeticity, leakage with respect to time and harsh environment and accelerated test.
- 4) Schemes and processes for massively parallel MEMS post-packaging by localized heating and bonding that can be conducted as batch fabrication.

## **ACKNOWLEDGEMENTS**

This work was supported by the U.S. Army Tank Automotive Research, Development and Engineering Center (TARDEC) through an the SBIR Phase I Program, contract #: W56HZV-05-C-0092.

## **References**

- [1] S. Senturia, "Microsystem Design", Kluwer Academic Publishers, 2001.
- [2] M. Gad-El-Hak, "The MEMS Handbook", Boca Raton, 2002.
- [3] J.A. Pelesko and D.H. Bernstein, "Modeling of MEMS and NEMS", Boca Raton, 2003.
- [4] Tai-Ran Hus, "MEMS & Microsystems Design and Manufacture", McGraw Hill, 2002.
- [5] J.W. Gardner, V.K. Varadan and O.O. Awadelkarim, "Microsensors MEMS and Smart Devices", John Wiley & Sons, 2001.
- [6] L. Lin, "Thermal Challenges in MEMS Applications: Phase Change Phenomena and Thermal Bonding Processes," *Microelectronics Journal*, 34, (2003), pp. 179-185.
- [7] L. Lin, "MEMS Post-Packaging by Localized Heating and Bonding, *IEEE Transactions on Advanced Packaging*", 23 (4), (2000), pp.608-616.

- [8] C.T. Pan, "Selective low temperature microcap packaging technique through flip chip and wafer level alignment", *J. Micromech. Microeng.* 14, (2004), pp. 522–529.
- [9] L. Pan, P. Yuen, L. Lin and E.J. Garcia, "Flip Chip Electrical Interconnection by Selective Electroplating and Bonding," *Microsystem Technologies Journal*, 10 (1), (2003), pp. 7-10.
- [10] L. W. da Silva, M. Kaviany, "Micro-thermoelectric cooler: interfacial effects on thermal and electrical transport", *International Journal of Heat and Mass Transfer*, 47, (2004), pp. 2417–2435.
- [11] D. Joachim and L. Lin, "Characterization of Selective Polysilicon Deposition for MEMS Resonator Tuning," *IEEE/ASME Journal of Microelectromechanical Systems*, 12, (2003), pp. 193-200.
- [12] B. Sridharan, C.J. Kim and L. Huang, "Post-packaging Release -A New Concept for Surface-micromachined Devices", *Tech. Dig., Solid-State Sensor and Actuator Workshop*, Hilton Head Island, SC, June 1998, pp. 225-228.
- [13] ABAQUS reference manuals, 2001, Providence ~RI!: Hibbitt, Karlsson and Sorenson, Inc.