

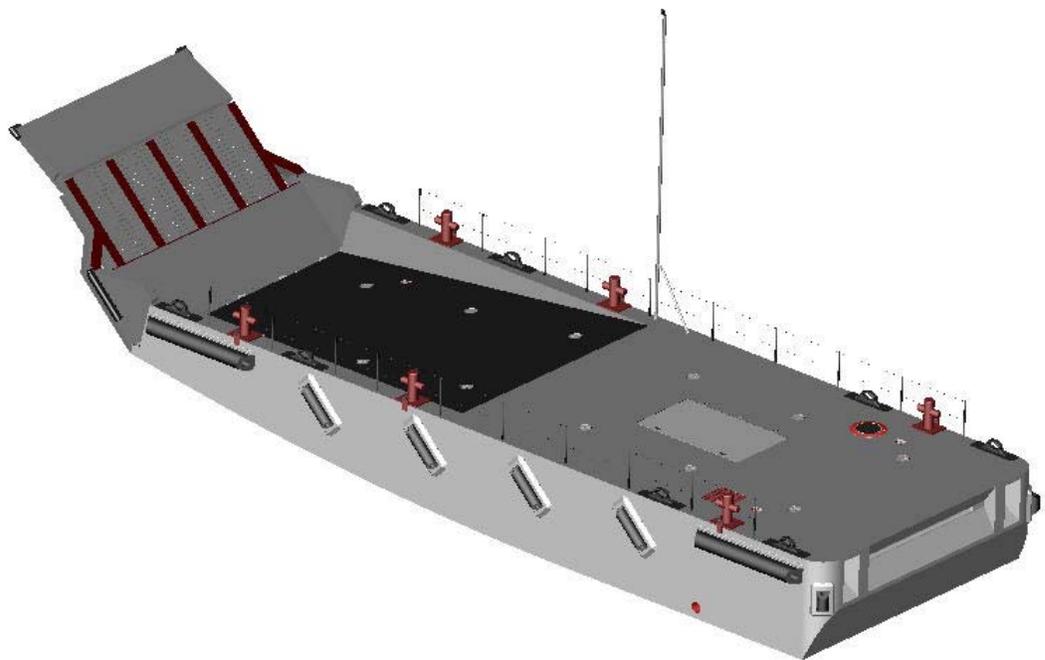


NAVAL FACILITIES ENGINEERING SERVICE CENTER
Port Hueneme, California 93043-4370

Technical Report TR-2202-AMP

DEVELOPMENT OF A BOW MODULE FOR THE SEABOSS CAUSEWAY FERRY

Final Report



by

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March 2002

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14. ABSTRACT This report describes the development of a bow module for the SEABOSS causeway ferry. A decision was made by the sponsor to develop a bow module that accommodates the majority of beaches where amphibious landings may occur and is practical to operate. This translated to a beach gradient of 1:50 or more. Flatter beach gradients may require a transition from the beach to deeper water by a pier-like facility, such as the floating causeway. The project effort included: a historical review of bow ramps for landing military vehicles on beaches; the development of design criteria for the bow module; the development of alternative concepts for the bow ramp and bow module; the evaluation and selection of a design concept for the bow module; and the preparation of detail design drawings for the bow module.					
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EXECUTIVE SUMMARY

The development of a beaching ramp capability for the SEABOSS causeway ferry (CF) bow module is reported. The SEABOSS bow module includes a bow thruster. SEABOSS is an advanced modular, floating causeway system that enables Logistics Over-the-Shore (JLOTS) operations to be executed in open-sea conditions through sea state 3 (SS 3). The SEABOSS beaching ramp is a key component of the self-powered causeway ferry. The primary mission of the SEABOSS CF is to discharge military vehicles from the CF to the beach. This operation is part of the capability to offload vehicular cargo from Military Pre-positioned Force (MPF) ships and Roll-On/Roll-Off (RO/RO) ships.

A historical review of vehicular beaching ramps for various types of vessels was conducted prior to the development of design concepts. Vehicular beaching ramps for the Navy's CFs have been used since the original Navy pontoon causeway system was developed during World War II. Beaching ramps for vessels of all types, including ships landing craft, and related applications were examined for both their good and bad features. Current users of the Navy's causeway system were consulted for their lessons learned from past operations.

Design criteria were developed for the beaching ramp. The beach slope and the draft of the CF are the parameters that have the greatest effect on the design of the beaching ramp. Analytical reviews of the capability of beaching vessels to land on various beach slopes clearly indicated that landing vehicles on beaches flatter than 1:100 slope would require a ramp too long for practical use. Therefore, the SEABOSS Project Management Office opted for a strategy to develop a beach ramp capability for beach slopes of 1:50 or steeper. This ramp would accommodate up to 75 percent of the beach gradients encountered in amphibious landings, as well as provide a ramp that is practical to stow, deploy, and use. Amphibious landing scenarios on flatter beaches will require the use of a transitional capability, such as the floating causeway moored to the beach. The SEABOSS bow module must interface with the landing ramp of the floating causeway.

Having established the critical design criteria, concept alternatives were developed for the bow module. Alternatives were for the rake angle, the beach ramp, the deployment/retraction mechanism, and a backup deployment system. The design team judged the alternatives according to a set of evaluation criteria developed for that purpose. Four alternative concepts were selected for final evaluation by the team. The selected concept proposed a hinged ramp with hydraulic ram actuators to deploy and retract the ramp. Hydraulic power to operate the rams is supplied by the diesel engine that drives the bow thruster. With the criteria and design concept established, the design details were executed by NFESC's design section. A complete set of drawings for the beaching ramp components of the bow module was provided. Detail drawings for the bow module structure and the bow thruster are to be developed by others.

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DEFINITIONS

Approach Angle	The supplement to the angle between an approach “road” and a sloping ramp. The approach angle refers to the maximum angle that a vehicle can negotiate with its front end as it moves forward onto a sloping ramp.
Bow Ramp	A hinged ramp structure that enables military vehicles to transition from the deck of the bow module to the beach or other designated floating structures.
Breakover Angle	Supplement to the angle between two ramps at different slopes.
Departure Angle	Supplement to the angle between a departure ramp and the departure “road”. The departure angle refers to the maximum angle that a vehicle can negotiate with its rear end as it moves forward off of a sloping ramp.
“Dry Ramp”	A ramp sufficiently close to the beach to enable military vehicles to reach the shore without the requirement for a fording kit. Generally, no more than 18 inches still water depth at the foot of the ramp is considered a dry ramp.
Gap Length	Distance from the beach end of the beaching ramp to the waterline on the beach, when the CF is fully grounded for offload.
Trafficability	Ability to move vehicles over a particular area.

ACRONYMS

BM	Bow module, a transition module with a floating hull structure and appurtenances, including the bow ramp, that enable the discharge/loading of military vehicles from/to the SEABOSS causeway ferry to the beach or to other designated floating structures.
CF	Causeway ferry consisting of a powered module, intermediate modules, and a bow module.
ELCAS(M)	Modular Elevated Causeway
FC	Floating Causeway
HET	Heavy Equipment Trailer (US Army)

MCS	Modular Causeway System (US Army)
MPF	Military Pre-positioning Force
RRDF	Roll-On Roll-Off Discharge Facility
RTCH	Rough Terrain Container Handler

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Chapter 1

INTRODUCTION

SEABOSS is being developed as an advanced modular causeway system that enables Logistics Over-the-Shore (JLOTS) operations to be executed in open-sea conditions through sea state 3 (SS 3). SEABOSS will replace the existing Navy Lightered (NL) causeway system. SEABOSS will provide a SS 3 capable ship-to-shore lighterage system to offload Military Prepositioned Force (MPF) ships and Roll-On/Roll-Off (RO/RO) ships.

SEABOSS BOW RAMP MISSION: Discharge cargo from causeway ferry (CF) and floating causeway (FC) to the beach on all beach slopes and interface with other SEABOSS systems. **Key Performance Parameters** include unassisted beaching and retracting while loaded or unloaded over beach gradients of 1:50 (threshold) and 1:100 (goal).

Recent efforts to modernize the Navy's and Army's lighterage systems have produced beaching ramps that fell short of the military user's mission requirements. Engineering and operational lessons learned from the test and evaluation of the CDI Marine designed prototype SEABOSS have indicated design improvements are required to improve the ability to transfer military vehicles from the CF to the beach. The SEABOSS Program Office commissioned NFESC to develop a bow module capable of achieving the mission requirements. This report describes the development and design of the SEABOSS bow ramp and bow module and the ability of the developed components to satisfy the mission requirements.

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Chapter 2

BACKGROUND

In September 1998, the Navy contracted with CDI Marine to develop a joint modular lighterage system (SEABOSS) capable of completing its mission requirements, even in SS 3 conditions. The contract was concluded after CDI was unable to satisfy some of the specified design requirements, including the ability to discharge military vehicles from the CF to the beach and to other causeway facilities. JMLS components to be upgraded, modified, or re-designed were allocated by the Naval Facilities Engineering Command (NAVFAC) Program Office to various Navy agencies for execution. NFESC was selected to execute the revised bow module design. The program was renamed SEABOSS by the Program Office to reflect changes in direction of the program.

The bow module is a key component of the self-powered CF. The CF is made up of end-linked SEABOSS lighters with a powered lighter at the stern and a bow module at the bow. The bow module is required to discharge rolling stock from the CF to the beach.

NFESC has an extensive history in the development and use of lighters for ship-to-shore transfer of military equipment. To execute the bow module development, NFESC engineers drew on their past experience, reviewed the history of beaching ramps, and took advantage of the lessons learned from the deficiencies experienced by past beaching ramp designs. Life cycle cost considerations were an integral part of the concept evaluation process. By following this approach and applying sound engineering judgement, NFESC sought an optimal configuration to meet user requirements.

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Chapter 3

HISTORICAL REVIEW OF BEACH RAMPS

NFESC's design approach for the bow module incorporates prior JMLS data and other efforts, including the lessons learned from similar ramps and bridging in the past. The functional and operational requirements have been reviewed with military users to assure that all requirements have been identified. Bow module criteria are derived from these requirements and key analyses.

The design goal of the SEABOSS program office is to have the capability to discharge wheeled vehicles from the CF to beaches with gradients of 1:400 and steeper. Beach gradient classifications are shown in Table 3-1. The beach gradient capability of existing military lighterage is estimated in Table 3-2. *The Army Trans-hydro Study 1975-1985 estimated that 90% of the world's beaches with potential to support JLOTS operations have beach gradients steeper than 1:60.* A recent Army study estimated the percent of use of beaches of various gradients in wartime and in peacetime. The study indicated that most usage will occur on "gentle" beach gradients of 1:30 to 1:60 in both cases (see Table 3-3). Note that 90% of peace time lighterage operations will be on beach gradients steeper than 1:60, compared to 60% in war time. Beach gradients steeper than 1:120 include 90% of war time operations.

Table 3-1. Beach Gradient Classification

Classification	Gradient (Slope)
Steep	> 1:15
Moderate	1:15 to 1:30
Gentle	1:30 to 1:60
Mild	1:60 to 1:120
Flat	<1:120

Ref. 1., "Joint Surf Manual," COMNAVSURFPAC/COMNAVSURFLANT Instruction 3840.1B, Jan 1987.

Table 3-2. Beach Gradient Capability of Lighters

Lighter Type	Capability
LCU	1:20 to 1:30
LCM 8	1:10 to 1:20
NL Causeway	1:40 to 1:60

Ref. 2. "LOTS Interface Systems Analysis," BDM Corp., 1984.

Table 3-3. Beach Gradients and Lighterage

Beach Gradient	War Time Use (%)	Peace Time Use (%)
>1:15 (Steep)	---	---
1:15 to 1:30 (Moderate)	10	20
1:30 to 1:60 (Gentle)	50	70
1:60 to 1:120 (Mild)	30	10
<1:120 (Flat)	10	---

Ref. 3. US Army JMLS Operational Mode Summary/Mission Profile (draft).

In an analysis by MAR, Inc., to determine the capability to install an elevated causeway on a shallow beach gradient, it was determined that many lighters grounded out at considerable distances from the beach. The results of their groundout distance estimates are provided in Table 3-4.

Table 3-4. Groundout Distance for Lighters

		Distance from Beach (ft) / Water Depth at Ramp (ft)				
		Beach Gradient				
Lighter	Draft (ft)	1:15	1:30	1:60	1:120	1:300
LCU	6.6	100/ dry	200/ 2.6	400/ 4.6	800/ 5.6	2000/ 6.2
LCM 8	4.6	70/ dry	140/ 2	280/ 3.3	550/ 4	1400/ 4.3
NL CWF	4.0	60/ 4	120/ 4	240/ 4	480/ 4	1200/ 4
NL CWF*	4.0	60/ dry	120/ dry	240/ 1	480/ 2.5	1080/ 3.4
**2 bow sections unloaded (1.3 ft draft); remaining 2 sections loaded 100 tons each.						
* NL CWF = Navy Lightered Causeway Ferry						

Ref.4. "ELCAS Installation on Shallow Beach Gradients," MAR, Inc. TR 960, Aug 1990.

The historical review determined that existing lighters ground out well short of the beach when gradients are flatter than 1:50. SEABOSS criteria specify that the CF draft up to 5 feet for beaching. At 5 feet of draft, the CF will require a substantial ramp length or a transition structure to enable wheeled vehicles to reach the beach. For the CF to get closer to the beach, it can approach the beach at its full speed of approximately 6 knots. Also, the load on the bow section can be arranged such that the bow module is trimmed to approximately the same angle as the beach slope. The precise groundout depth and consequent distance from the beach was computed for a range of beach gradients, and the results are reported later in this report. It was determined during the historical review that a single bow module cannot meet the requirements of all beach gradients. Steeper beaches (greater than 1:50) require a ramp to transition from the 8-foot high CF modules down to the beach. Flatter beaches require some type of transition between where

the CF grounds out and the beach. This could be a floating causeway, a fixed pier, or other type of transition structure.

Based on the foregoing review, it is concluded that:

- Current Army and Navy lighters do not have the capability to operate in areas where flat beach gradient conditions prevail.
- The existing JMLS beach ramp prototype developed by CDI Marine did not meet the specified requirements.
- A single bow module cannot meet the requirements to operate on flat beach gradients.

3.1 BEACHING RAMPS FOR STEEP TO MODERATE BEACH GRADIENTS

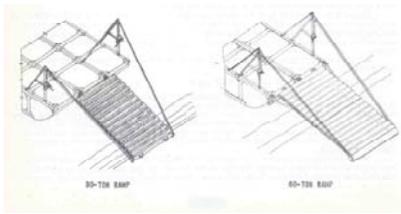
Most beaching ramps for lighters in the past were designed for operating on steep to moderate beach gradients. The Navy's modular floating causeway has its roots in World War II (WWII). Barge ferries were used even then. The beaching ramps were rather simple, but effective. Other shallow draft lighters were developed to effect the ship-to-shore delivery of cargo. Some of the beaching ramps used over the past 60 years, some of which are still in use, are shown in Figure 3-1. Other types of spanning structures can be adapted to function as beaching ramps, as well.

3.2 BEACHING RAMPS FOR MODERATE TO FLAT BEACH GRADIENTS

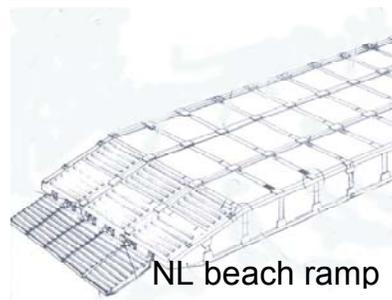
Flat beaches and deep draft lighters are a poor mix for efficient transfer of cargo from ship-to-shore because the lighters groundout far from shore on flat beaches. To cover the remaining distance requires some type of transition or linkage from the ground out point to the shore. Typical transition approaches may include:

- Fixed Piers
- Floating Causeways
- Aerial tramways or High Lines
- Helicopters
- Surface Effects Craft
- Dredging

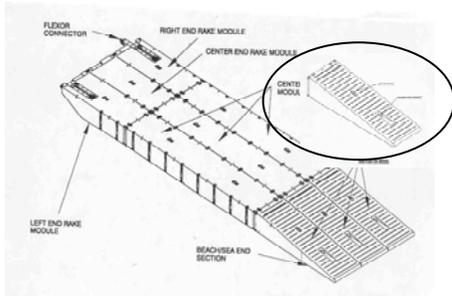
Figure 3-2 shows selected transitional capabilities that could satisfy this need. Most of these alternatives have major drawbacks that limit their applicability to military logistics over-the-shore (LOTS) scenarios, for which delivery logistics and installation expediency are of extreme importance. Shipping is critical because military cargo is displaced by logistics components. Rapid installation is essential to almost any military expeditionary mission. Other factors include cargo capacity and cost.



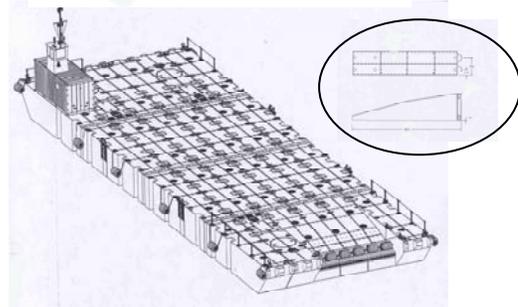
WW II CF beach ramp



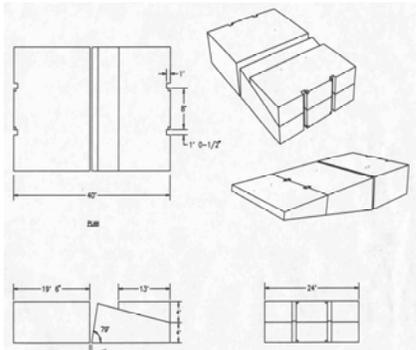
NL beach ramp



MCS beach ramp



JMLS beach ramp



ACBL beach ramp



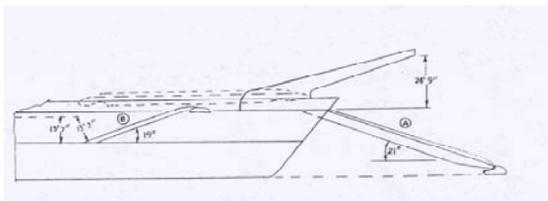
LCU 1610 bow ramp



LCU 2000 bow ramp

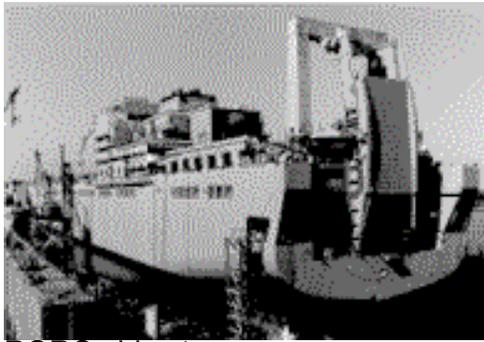


LSV bow ramp



1179 Class LST bow ramp

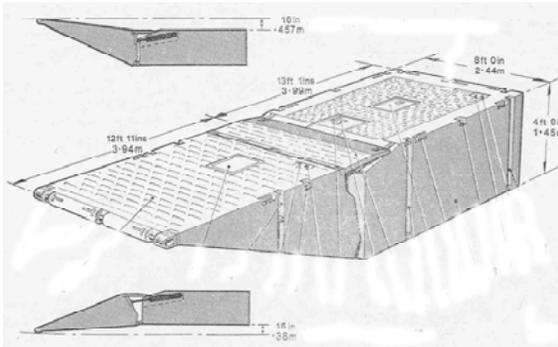
Figure 3-1. Beaching ramps for steep to moderate beach gradients past and present.



RORO ship stern ramp



NATO ACV bow ramp



MEXEFLOTE ramp



LCAC bow ramp



NL articulated bow ramp

Figure 3-1. Beaching ramps for steep to moderate beach gradients past and present (continued).



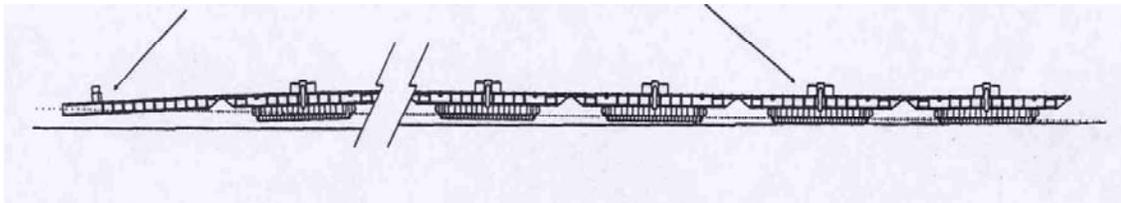
Floating causeway



U. S. Army ribbon bridge



Elevated causeway



Air cushion causeway ferry or floating causeway

Figure 3-2. Transitional or linking capabilities that have been used to assist in the transfer of wheeled cargo on moderate to flat beach gradients.

In the past, floating causeways linked end-to-end have been used for short-term applications. Causeways were originally used to provide a link for the WWII Landing Ship Tanks (LSTs), which drafted 6 to 8 feet at the bow. These applications were generally limited to causeway lengths on the order of 1000 to 1500 feet. On very flat beaches (1:400), floating causeways will ground out at 500 to 600 feet from the beach due to drafts of 1.5 to 2 feet, which means vehicles will have to ford the distance to the beach. Often, very flat beaches will have soft muddy bottoms, which would make it difficult for wheeled vehicles to drive from the floating causeway to the beach. Modifying the floating causeways with air cushion skirts has been proposed for this type of scenario to get the causeway beach end onto dry land.

Some additional approaches for intermediate to flat beach gradients are shown in Figure 3-3. Some approaches may solve one type of scenario, but not others. For example, dredging may be a good solution for sand bars, but not for mud bottoms.

3.3 LESSONS LEARNED

Experiences with beaching ramps and other types of unloading ramps during numerous amphibious scenarios over the past 60 years have produced both successes and failures. The accumulation of these experiences provides guidance for future applications and makes a significant contribution to the design philosophy for beaching ramps to be used in amphibious operations. This accumulation of experiences is known as “Lessons Learned” by the military. A partial list of beaching ramp lessons learned compiled by the design team is provided below.

- Bottom rake profile should “skim” over the beach when the CF grounds out, and avoid “digging in.”
- An articulated CF enhances the capability to navigate over/around sand bars.
- Need bow freeboard and bow rake to avoid submarining of bow.
- Wire rope winch systems often have problems spooling the wire rope while deploying or retracting the bow ramp, e.g., the LCM 8 landing craft.
- To operate effectively and safely, the CF operator needs good visibility over bow.
- Lighter loaded beach section(s) allow further advance on the beach.
- Ramp slopes should not exceed 13-15 degrees for vehicle traction.
- A backup capability to deploy/retract ramp is essential to maintain cargo discharge in the event the primary ramp deployment system is disabled.
- Low pivot points for ramps make for difficult interface with high landing points, e.g., ramp to high freeboard causeway.
- Ramp toe should provide sufficient bearing to prevent ramp from sinking in beach bottom.
- Ramp must accommodate flat, steep, and elevated departures for vehicles.
- Short floating beach ramps are difficult to attain level trim for end-to-end connection purposes.

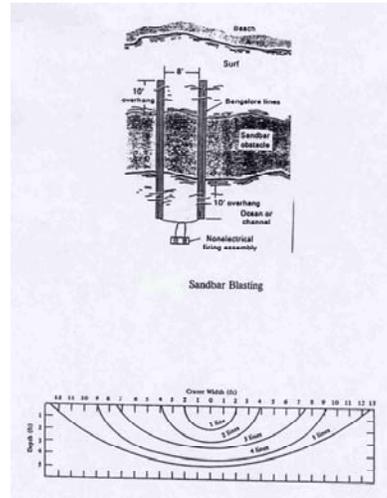
The bow module design philosophy embraced these lessons learned during the development process, as well as the input from active military users of causeways.



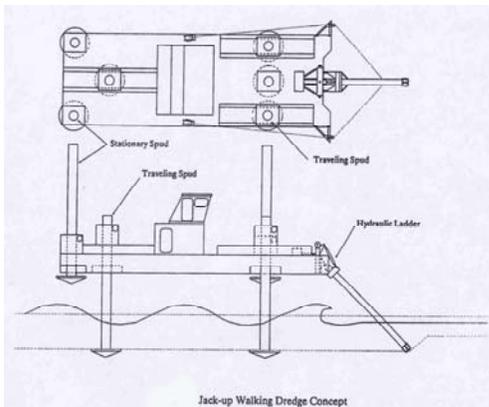
Concept A. Air cushion CF or floating causeway.



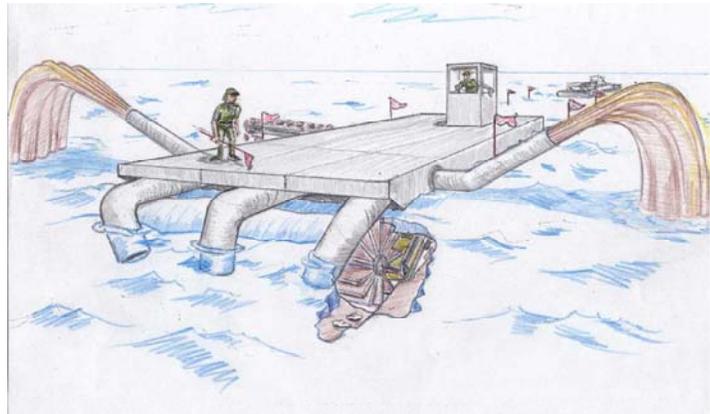
Concept B. Mobile bridging for moderately flat beach gradients.



Concept C. Channel blasting for stable beaches, sand bars.



Concept D. Walking dredge for moderately flat beaches.



Concept E. Beach Buffalo for dredging moderately flat beaches.

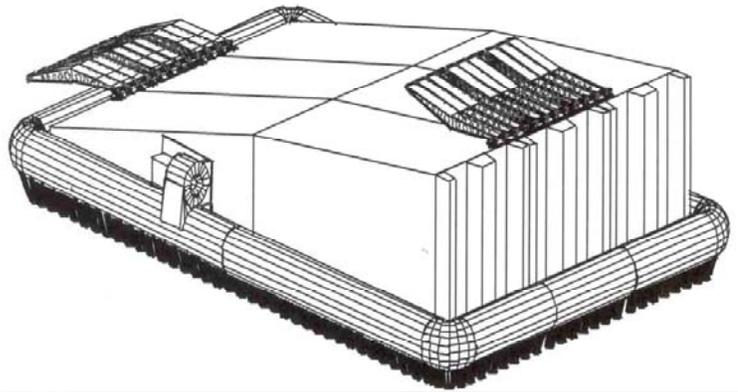
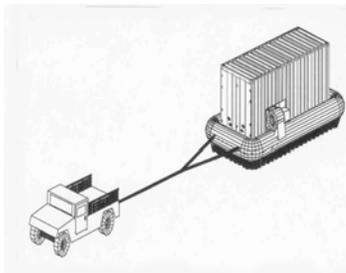
Figure 3-3. Alternative concepts for moderate to flat beach gradients.



Concept F. Supplemental buoyancy to decrease CF draft (for marginal beach gradients).



Concept G. Seawater supported link to the Beach (R&D concept).



Concept H. Proposed JMLS air cushion mobile beach ramp.

Figure 3-3. Alternative concepts for moderate to flat beach gradients (continued).

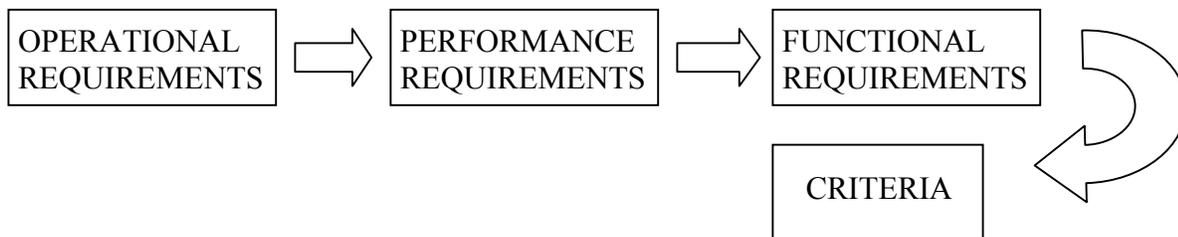
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Chapter 4

DESIGN CRITERIA DEVELOPMENT

The bow ramp is a component of the bow module (BM), and the BM is a component of the CF. The mission statement and the operational requirements apply to the CF. Operational requirements for the bow ramp and the BM apply insofar as they contribute toward the capability of the CF to complete its mission. The BM and/or the bow ramp cannot achieve the mission alone - only in concert with the other components of the CF.

The design team initially examined and defined the operational, performance, and functional requirements for a bow ramp to discharge military vehicular cargo from the CF. From those requirements, criteria were developed for the bow ramp:



The NFESC design team was assigned responsibility for configuring the module that would house the bow ramp; however, they were not held responsible for the design of the actual module. To acknowledge that distinction, the bow ramp module was called the bow module. In effect, the bow module would be designed around the bow ramp. A specification was developed for the bow ramp and the bow module to assure that the bow module design would be fully compatible with the bow ramp design. After the criteria were established, several analytical tasks were performed to develop the data required for the bow ramp design. Finally, the design was developed on paper.

4.1 OPERATIONAL REQUIREMENTS

The primary operational requirement for the CF is to transfer rolling stock from the roll-on/roll-off discharge facility (RRDF) to the beach. Operational requirements (OR) are broad statements of the military capability of a given system. In this case, the OR applies to the SEABOSS CF. The bow module is a critical subsystem of the CF that enables the CF to accomplish its mission as defined by the OR. The SEABOSS bow module mission might be stated as:

SEABOSS Beach Ramp Mission: Discharge cargo from the SEABOSS causeway ferry (CF) to the beach on all beach slopes and interface with other SEABOSS systems in conditions up to and including sea state 3.

4.2 PERFORMANCE REQUIREMENTS

Performance requirements begin to quantify the OR statement in terms of specific performance parameters that must be accomplished. Performance requirements for the SEABOSS bow module derive from the above mission statement. Obviously, the rolling stock must be transferred from the RRDF to the CF to complete its mission. However, the bow ramp project was limited to transfer of rolling stock to the beach and to other SEABOSS systems, such as other SEABOSS CFs, NL causeways, and the Army's Modular Causeway System (MCS). Table 4-1. Primary performance requirements for the bow ramp and the bow module are:

- Transportable by MPF and LMSR shipping
- Deployable by MPF and LMSR shipping
- Capable of assembly into CF in stream with SEABOSS assets
- Capability to operate in sea state 3
- Capability to maintain 6-knot CF speed when fully loaded
- Capability to beach and retract CF at all load conditions over all beach gradients.
- Capability to discharge military rolling stock from CF to beach
- Capability to achieve a wet ramp on beach gradient of 1:50 or steeper
- Capability to interface with other SEABOSS systems and Army MCS

A parallel development effort for a SEABOSS spanning ramp is developing the capability to transfer rolling stock from the RRDF to the CF.

The design parameters that pose the greatest challenge to proper functioning of the bow module are the beach slope, the CF draft, and the ability to operate in SS3. The mission states that the bow module must have the capability to discharge cargo on all beach slopes. Very flat beach slopes present significant problems for a loaded CF, which could draft as much as 5 or 6 feet. Table 4-1 shows the draft of different CF lengths loaded to the design payload of 400 short tons. Operational considerations dictate that the CF length exceed 200 feet. Several alternative configurations for the CF are shown in Figure 4-1. Since a 200-foot CF drafts only 4.2 feet and the CF operational length will exceed 200 feet, the SEABOSS Program Office made a decision that the CF design draft would be 4 feet instead of 5 feet.

Table 4-1. Draft of CF at Full Load for Various Lengths

Load (short ton)	CF Length (ft)	Draft (ft)
LIGHT	ANY	~1.6
400	200	~4.2
400	260	~3.6
400	340	~3.2
(SEABOSS CF Payload Requirement = 400 short tons)		

Early in the project, the effects of flat beach gradients and CF drafts were examined in an effort to determine the appropriate design configuration and length for the bow module. Tables 4-2 and 4-3 show the results of a parametric analysis for a 200-foot rigid CF and a 200-foot articulated CF with 4 feet of draft. Figures 4-2 and 4-3 show the minimum length for a beaching ramp with “dry” or “wet” ramps for both rigid and flexed CF at a range of drafts. The analysis determined that the beach ramp “gap length” becomes excessive at beach gradients flatter than 1:50. In the analysis, gap length is defined as the distance from the beach end of the beaching ramp to the waterline at the beach. For example, a 1:100 beach gradient with 4 feet CF draft requires a beach ramp longer than 100 feet. A sample output from the beaching ramp gap analysis is listed in Appendix A.

Table 4-2. Beaching Ramp Gap for 200-Foot Rigid CF with 4-Foot Draft

Ground Out Distance (ft)	Beach Gradient					
	1:400	1:200	1:100	1:50	1:25	1:125
Bow ground out distance	1,600	800	400	200	100	50
Trim gain	100	100	100	100	50	25
Skid distance	101	71	51	36	25	18
Distance to 18-in. depth	600	300	150	75	37.5	18.75
Dry ramp gap	1,399	629	249	64	-25	-18
Wet ramp gap	799	329	99	-11	-62.5	-36.75

Table 4-3. Beaching Ramp Gap for 200-Foot Flexed CF with 4-Foot Draft

Ground Out Distance (ft)	Beach Gradient					
	1:400	1:200	1:100	1:50	1:25	1:125
Bow ground out distance	1,580	780	380	180	80	30
Trim gain	22.5	22.5	22.5	22.5	22.5	22.5
Skid distance	183	131	95.3	68.9	47.5	32.9
Distance to 18'in. depth	600	300	150	75	37.5	18.7
Dry ramp gap	1,375	627	262	88.6	75	-25.4
Wet ramp gap	775	327	112	13.6	-27.5	-44.1

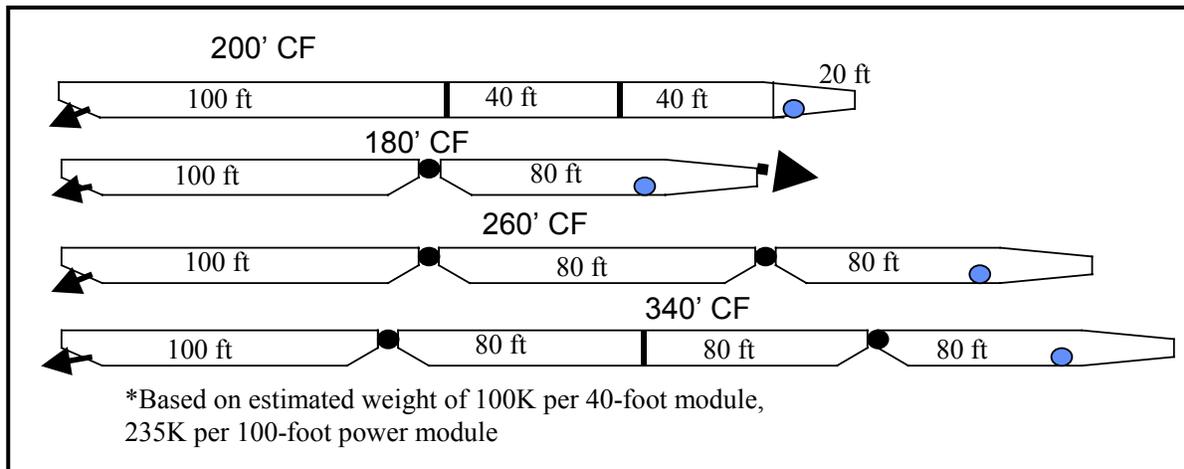


Figure 4-1. Alternative configurations for the JLMS CF.

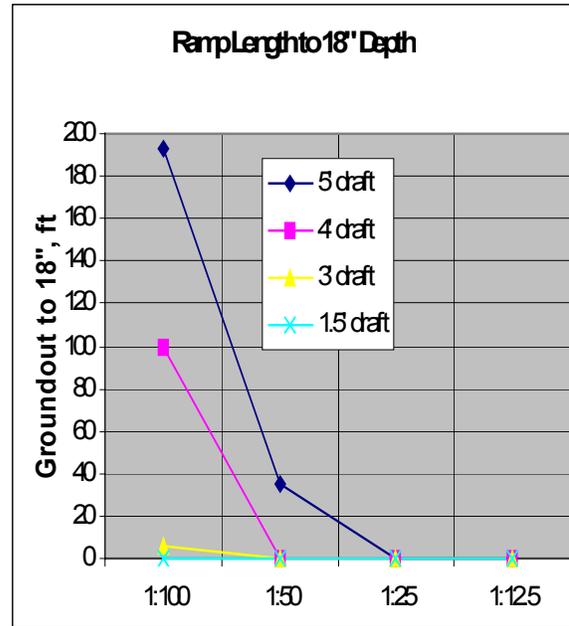
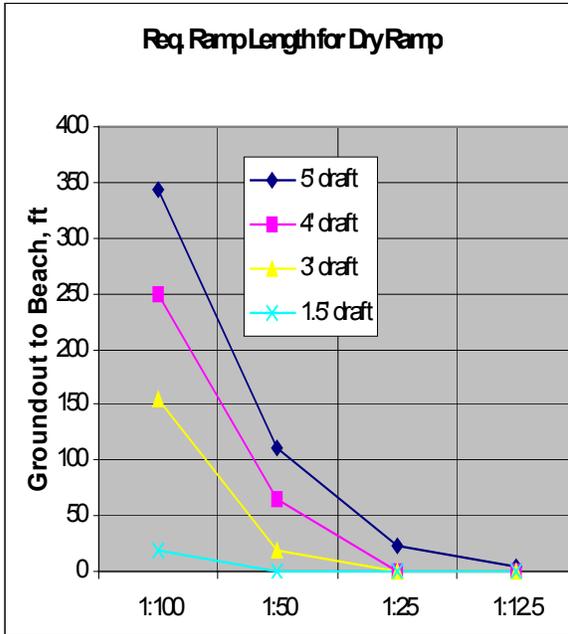


Figure 4-2. Minimum ramp lengths for “dry” and “wet” ramps for a rigid CF.

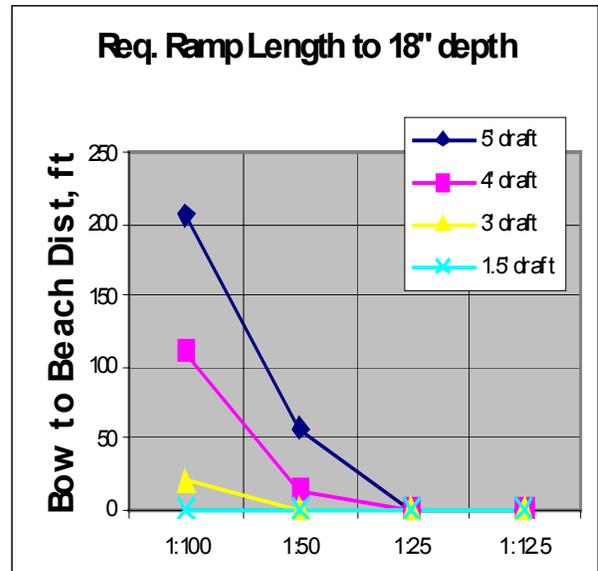
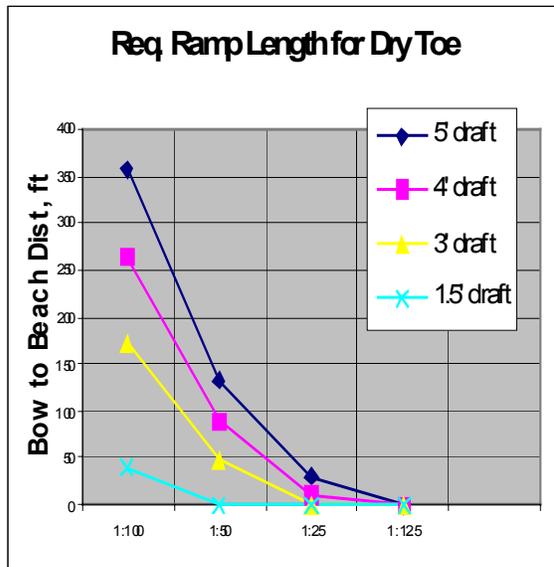


Figure 4-3. Minimum ramp lengths for “dry” and “wet” ramps for flexed CF.

Although a 100-foot-plus ramp can be developed, such a ramp length would greatly diminish the ramp's operational utility. The Army's study results of Table 3-3 indicate that 60% of the war time applications occurred on beach gradients steeper than 1:60, while 30% occurred on gradients between 1:60 and 1:120. In addition, weight and cube of a 100-foot plus ramp will impact on the transport logistics and SEABOSS CF assembly at sea. Based on these considerations, the SEABOSS Program Office elected a strategy to **develop a beach ramp capability for beach gradients steeper than 1:50**. For beach gradients between 1:50 and 1:200, adjunct hardware such as floating causeways would be required.

The rigid CF is a slight advantage for the required beach ramp length at a 4 foot draft; however, operational problems may result from trimming of the CF to parallel the beach gradient. Trimming lowers the freeboard of the CF stern, making the CF more vulnerable to breaking surf. The stern freeboard problem increases with length of a rigid CF. Further, the length of a rigid CF is limited by the ability to transport it by MPF or LMSR shipping. The articulated or flexed CF does not have the same disadvantages. See Figure 4-4. In addition, the flexed CF has some operational advantages in dealing with sand bars. See Figure 4-5. The SEABOSS Program Office accepted the design team's recommendation for a flexed CF.

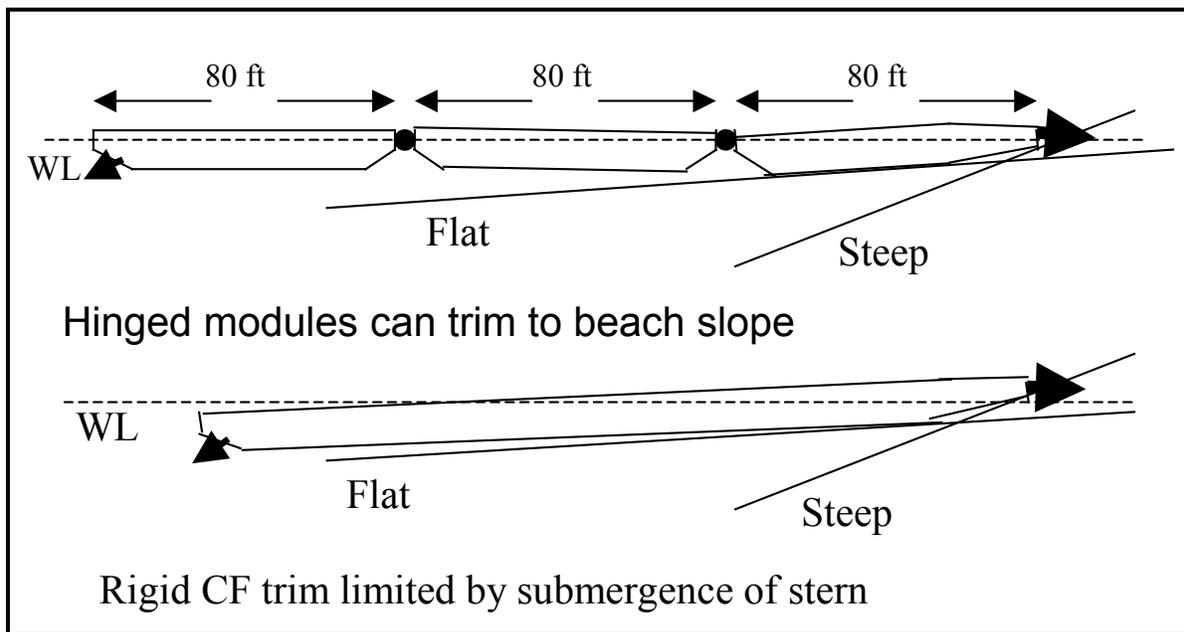


Figure 4-4. Effect of flexed CF compared to rigid CF.

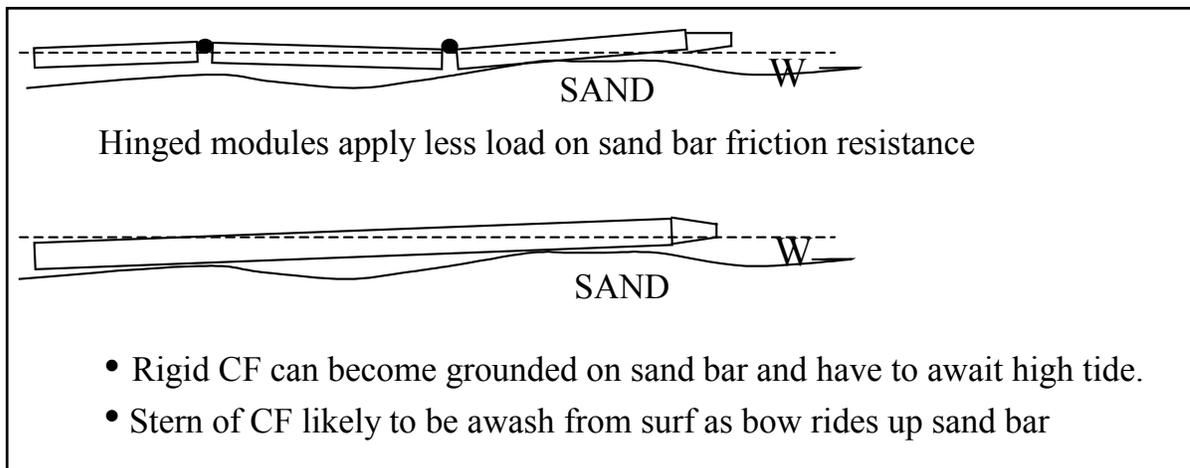


Figure 4-5. Comparison of hinged and rigid CF on a sand bar.

4.3 FUNCTIONAL REQUIREMENTS

Functional requirements take the performance requirements to the next level, as the system concept begins to take shape. Again, many of the functional requirements for the bow ramp subsystem enable the CF to accomplish its missions.

Operational requirements determine what missions the beach ramp system must accomplish. Functional and performance requirements evolve from these operational requirements and the hardware chosen to meet the operational requirements.

The beach gradient has a profound influence on the length requirements for a bow ramp. For example, steep beach gradients with a CF full-load draft of 4 feet require just a step down ramp from the 8-foot high deck. The step-down ramp with a slope limit of 7 degrees is long enough to reach a water depth considered to be a “dry ramp” for vehicular traffic. For the beach ramp, a dry ramp is defined as the maximum water depth at which applicable military vehicles can operate without a fording kit. At the other extreme, flat beach gradients with a CF full-load draft of 4 feet require a step-down ramp and a transition capability from the CF grounding water depth to a water depth considered to be a dry ramp.

From the beaching gap analysis, it was determined that a 1:50 beach slope requires a bow ramp length that closely matches the length required for a step-down ramp capability from an 8-foot high module. It should be noted that a significant majority of beach landings in war time have been on beach gradients steeper than 1:50. These data led the SEABOSS Program Office to opt for developing a primary bow module capability to operate on steep to moderate beaches. For beaches flatter than 1:50, CF to beach links or transitional capabilities will be required.

4.4 SEABOSS BOW MODULE CRITERIA

With further refinements, the requirements become quantitative. Criteria for the bow ramp and bow module were categorized as:

- Performance Criteria
- Environmental Criteria
- Logistics
- Operational Considerations
- SEABOSS Interfaces

A decision required of the SEABOSS Program Office was whether to specify a “dry ramp” or a “wet ramp” landing on the beach. A wet ramp refers to the condition at the end of the ramp. Once the CF has grounded and can advance no further toward the beach, the ramp must be capable of discharging its cargo to the beach. For this design effort, a “wet ramp” was defined as 18 inches of water depth at the end of the beaching ramp. This depth was chosen because all military vehicles to be transported by the CF can ford 18 inches of water, with some having significantly greater water depth. Referring to the previous charts for dry versus wet ramps, dry ramps increase the bow ramp length by approximately 50 feet. Bow ramps required to meet the dry ramp criteria would be much longer, hence, much less practical in operational use. This rationale led the Program Office to elect the “wet ramp” criteria for the SEABOSS bow module. A summary of bow ramp length requirements for “wet” and “dry” ramp on 1:50 beach slope is listed below.

“WET” RAMP AT 4 FEET DRAFT (FULL LOAD) ON 1:50 BEACH

- Deck taper length of 32.6’ determined by 7-degree breakover angle limit and 4-foot drop.
- For 7-degree max ramp slope, bow ramp length = 32.6 feet.
- Some ramp sections should go to 14 degrees slope to reduce bow ramp length.
- Momentum beaching of CF leaves “wet” gap of 14 feet.
- Vehicle trafficability (7-degree breakover, 14 degree slope) establish ramp length.

“DRY” RAMP AT 4 FEET DRAFT (FULL LOAD) ON 1:50 BEACH

- Momentum beaching of CF leaves “dry” gap of 89 feet.
- Ramp length determined by dry gap, trafficability issues are secondary

The primary criteria for the bow module centered around the issues related to deployment/retraction time, reliability, and trafficability by the military vehicles to be transported by the CF. Amphibious Construction Battalion (PHIBCB) users provided considerable input for deployment/retraction time. Bow ramp reliability was addressed in two ways – by selecting a reliable primary deployment system and by providing a backup deployment system. Historical ramp applications provided guidance for the ramp slope limits and ramp breakover angles.

The function and performance of the bow ramp cannot be divorced from the bow module, which houses and supports the ramp and provides one half of the 8-foot step down from the CF deck. Consequently, performance specifications for the bow ramp were combined with those of the bow module, even though the SEABOSS bow ramp project included a detailed design for the bow ramp, but not for the bow module.

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Chapter 5

CONCEPT ALTERNATIVES

Early in the project, the SEABOSS Program Office agreed that the capability to discharge cargo from a CF to the beach on all beach slopes was not practical within the SEABOSS deployment concept. Beach slopes of 1:50 or steeper were selected for the basic SEABOSS CF bow module, based on NFESC generated data. The data indicated that the bow ramp for steeper beaches could be kept to a reasonable length and maintain the SEABOSS logistics concept. Flatter beach slopes would require a shore link from the beach to the water depth where the CF grounds out. Floating pontoon causeways have performed this function for LST and deeper draft lighters in the past. Alternatives to be explored for moderate to flat beaches will be of this type.

5.1 CONCEPTS FOR STEEP TO MODERATE BEACH

Brainstorming sessions generated bow ramp concepts and concept approaches. It was apparent that the bow ramp could not be separated from the module that housed and supported the ramp. To that end, deck taper was used to bring the module deck height down from 8 feet to 4 feet. A built-in deck taper reduces the “active,” (deployed) length of the bow ramp. The bow ramp length begins at the end of the deck taper and effects the remaining 4-foot drop to the beach. Deck taper and ramp slopes are limited by the requirement for trafficability by a wide range of military vehicles. An analysis of the trafficability of ramp breakover angles and ramp departure angles is provided in Appendix B. The Rough Terrain Container Handler (RTCH) is one of the design drivers for structural design of the bow module.

The concept selection/evaluation process explored several functional elements or subsystems of the bow ramp and bow module. Alternatives for these subsystems were conceived and evaluated as part of the overall beach ramp/module system. The subsystems included:

- Bottom Rake Configuration
- Deck Taper Configuration
- Beach Ramp Deployment/Retraction
- Beach Ramp Power
- Beach Ramp Toe

Figure 5-1 shows some of the bottom rake configurations and deck taper alternatives considered for the bow module. Figure 5-2 illustrates the effects on beaching of the bottom rake on the bow module and the trim angle of a CF. Several considerations for rake selection are as follows:

- Ideally, the rake angle matches the beach slope
- Practically, the rake angle is greater than the beach slope
- For CF untrimmed, rake length adds to the effective length of the beach ramp
- For CF trimmed to the beach slope, rake length does not add to ramp length
- Flat rake angles plow into steep beaches, but slide easily over flat beaches
- Steep rake angles drag on flat beaches
- Rake edges should be rounded and fared to enhance sliding of CF toward beach
- Rounded or curved rake may have some advantage on steep beach slopes
- Hydrodynamic effects of the raked bow shape are minor
- Flat rake angle provides most advantage to advance CF toward the beach

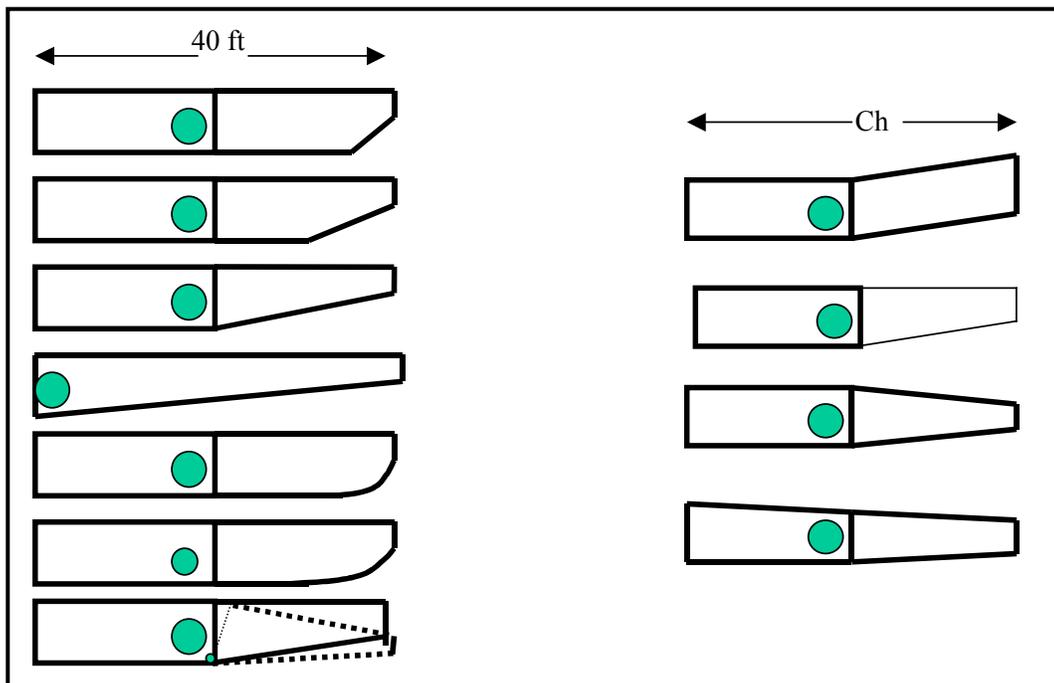


Figure 5-1. Bottom rake and deck taper configuration alternatives for beach ramps.

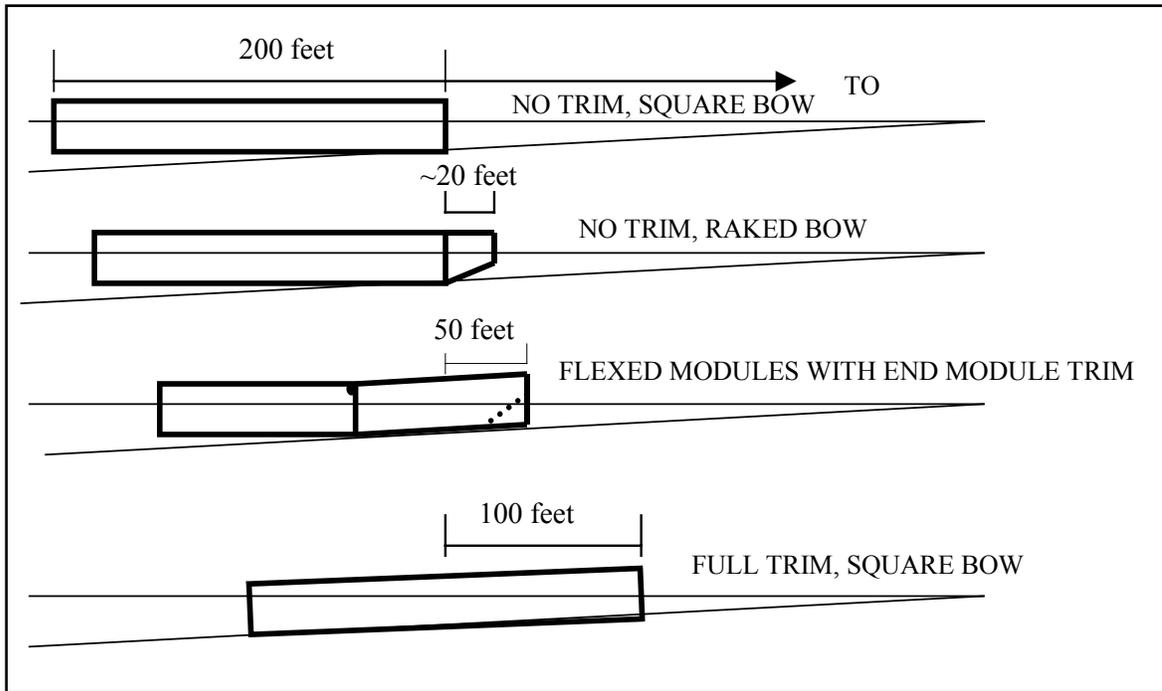


Figure 5-2. Effect of bottom rake and trim on beaching of CF.

The types of deployment/retraction alternatives considered for the bow ramp are:

Deployment/Retraction Alternatives

- Winch and Wire Rope
- Windlass and Chain
- Hydraulic Cylinders
- Worm or Screw Drive
- Block and Tackle Rigging
- Various Mechanical Linkages

Figure 5-3 illustrates several deployment/retraction alternative concepts for the bow ramp. Table 5-1 shows some of the power transmission choices considered for the bow ramps. Some of the deployment/retraction alternative selection factors are

- Estimated force to deploy/retract ramp is high (estimated 30,000 pounds).
- Some safety issues with winch and windlass systems have been experienced.
- Travel distance to deploy/retract the ramp is in the order of 3 to 6 feet.
- A mechanism like hydraulic cylinders or worm drives seems appropriate.
- Distance from prime mover at bow thruster to beach ramp discourages mechanical linkages.
- Hydraulics, pneumatics, or electrical power transmission favored.

- Electrical application not suited for the amphibious environment and PHIBCBs are not accustomed to this type of electrical component.
- Pneumatic cylinders would get too large for the high loads required. Also, pneumatic devices have potential for “explosive” failures.
- Hydraulic cylinders left as leading choice. Environmentally safe hydraulic oils are available.

Table 5-1. Power Transmission Alternatives for a Beach Ramp Deployment/Retraction Mechanism

Mechanism	Power Transmission			
	Hydraulic	Electrical	Pneumatic	Mechanical
Winch and Wire Rope	X	X	X	X
Windlass and Chain	X	X	X	X
Hydraulic Cylinders	X			
Pneumatic Cylinders			X	
Screw or Worm Drive	X	X	X	X
Mechanical Linkage				X

High capacity, reliability, relative simplicity, and familiarity of similar hydraulics in existing PHIBCB equipment drove the design team to choose hydraulic cylinders as the bow ramp deployment/retraction mechanism. Figure 5-4 shows several alternative configurations for the ramp structure. Single spans, folding spans, cantilever spans, and other variations were considered. When the final ramp length was determined, a single-hinged span provided sufficient structure and maintained the philosophy of simplicity.

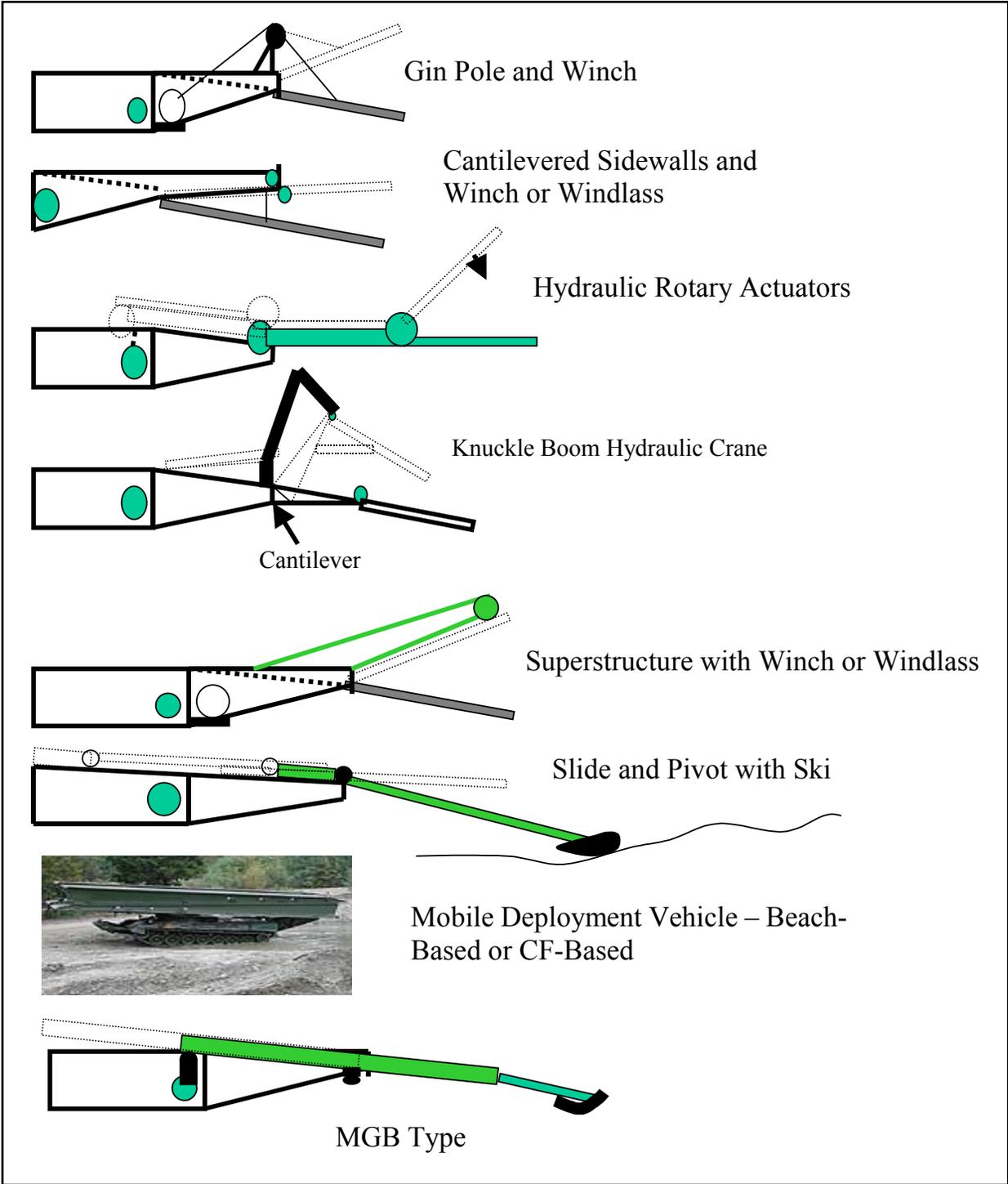


Figure 5-3. Beach ramp deployment/retraction alternative concepts.

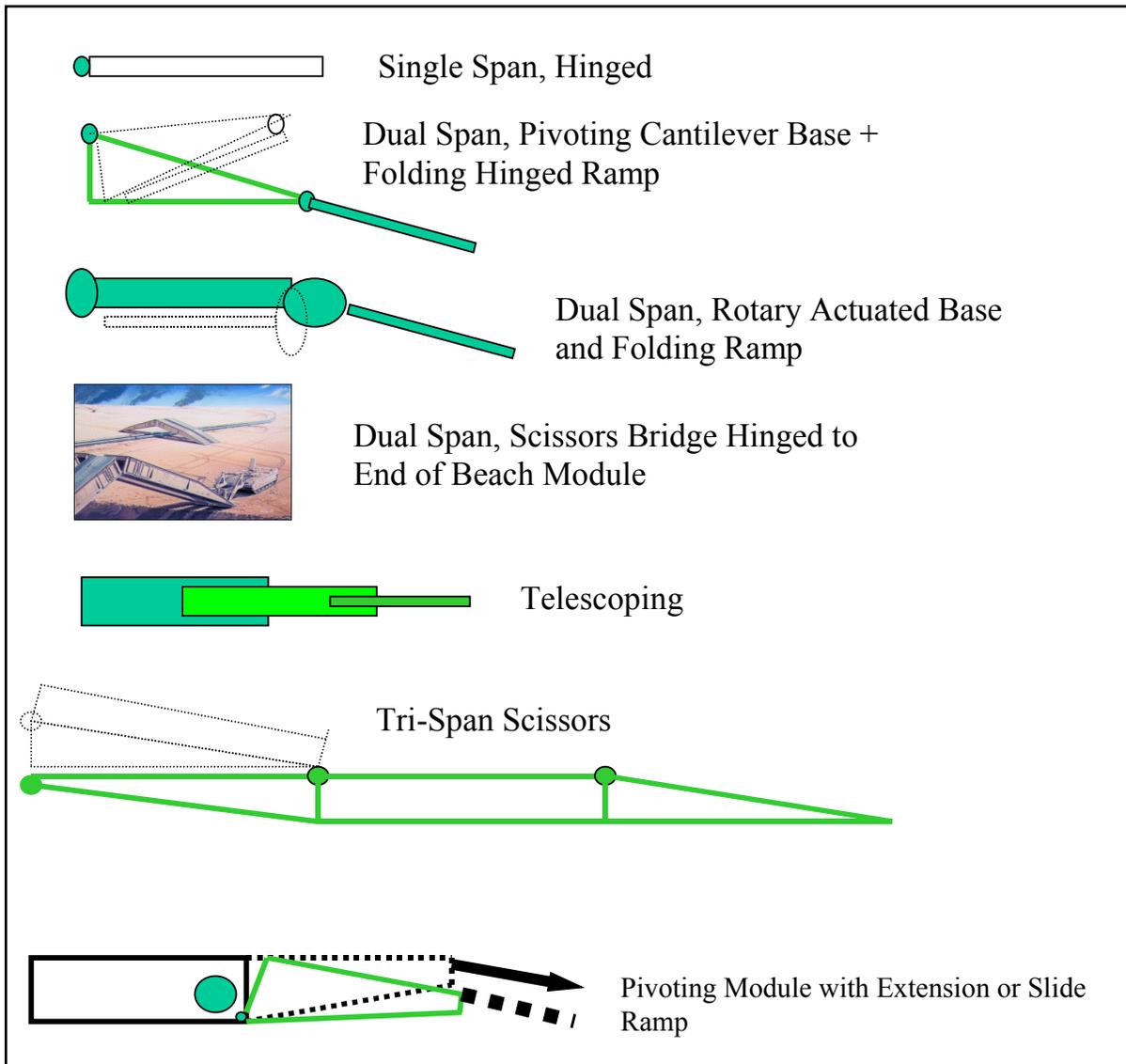


Figure 5-4. Beach ramp structure – alternative concepts.

Heavy vehicle loads on the bow ramp require some type of bearing plate/footing at the beach end of the ramp because uncompacted soils are often encountered at the beach discharge site. Also, multiple passes of vehicular traffic tend to cause ruts in the beach materials at the ramp foot. Some type of beaching landing mat could be provided; however, it makes sense to include the beach ramp footing as part of the beach ramp. We elected to call this footing the ramp “toe.” The ramp toe serves to minimize the ramp embedment into uncompacted soils and to provide a transition for vehicle traffic down the sloped beach ramp. Figure 5-5 shows the general configuration of the ramp toe. Note that the ramp toe is pivoted to orient the bearing plate to the surface. To accommodate tilted surfaces, the ramp toe is segmented into four independently hinged units.

After the key functional elements of the bow ramp design were examined, the team generated alternative beach ramp/module concepts. The concepts for steep to moderate beach gradients are shown in Figure 5-6. As noted above, a number of concepts came from the brainstorming sessions. The military users of the SEABOSS systems provided a concept that suited their operational functions. Other concepts were a fallout of merged elements of concepts that were flawed in some way. Presentation of concepts to different audiences invariably elicited “improvements.”

5.2 CONCEPTS FOR MODERATE TO FLAT BEACH GRADIENTS

A bow module designed to operate on steep to moderate beaches leaves a strategic gap in the operating capability to transfer cargo from ship to shore on flatter beaches. Clearly, it would be a logistic nightmare to fit the CF with a 100 to 150-foot ramp capable of achieving even a wet ramp on beach gradients greater than 1:50. No amphibious lighter in history has accomplished such a feat. In essence, the requirement to land equipment on the beach led to the birth of the floating causeway system in World War II. The LSTs, which were medium small ships, needed a way to land the equipment for the Marine Corps. The difference now is only one of degree. The LSTs drew 6 to 8 feet of water at the bow, while the SEABOSS CF draws only 4 feet. The SEABOSS CF can land on steep beaches, but not on flatter beaches. The missing capability is unresolved.

Is there something better than the time-honored floating causeways? Figure 3-3 shows a number of alternatives to fill the beaching gap. One approach that has been looked at and

prototyped by the military on several occasions is the air cushion lighter. In fact, a high-speed air cushioned lighter, the LCAC, is a key element of the current amphibious assault strategy. Several concepts used the air cushion approach. Air cushion causeways would enable the CF to push closer to the beach. This project did not attempt to estimate the beach gradient that could be overcome by this approach. A variation of the air cushion approach would

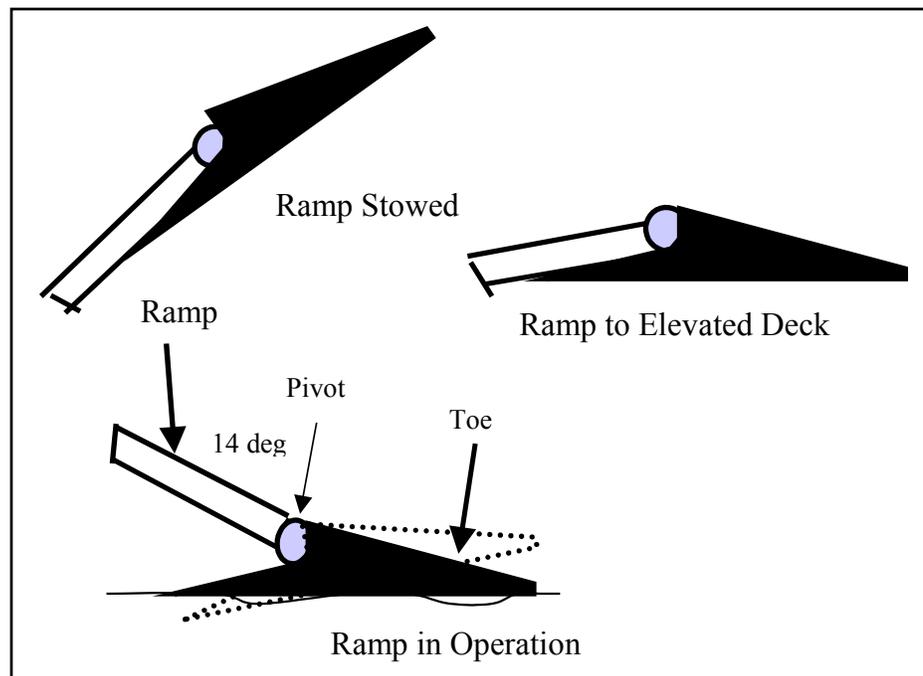


Figure 5-5. Beach ramp toe in various deployment modes.

be to air cushion the forward causeways only. One other air cushion approach was suggested by CDI Marine, the previous contractor who developed many JMLS components.

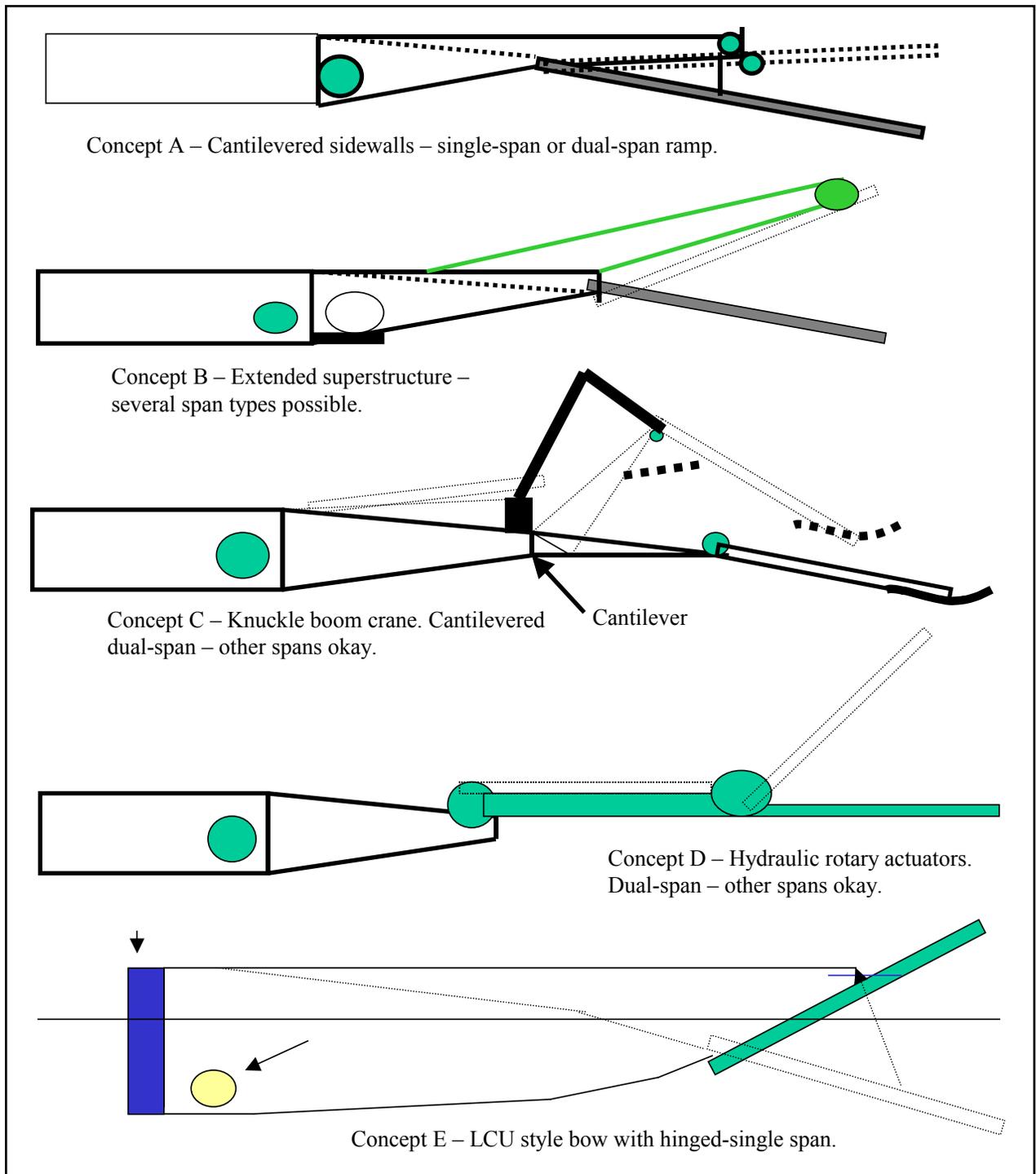
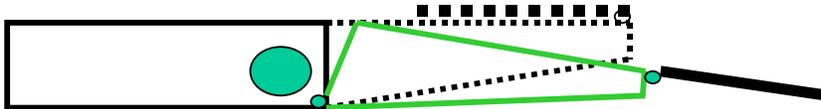
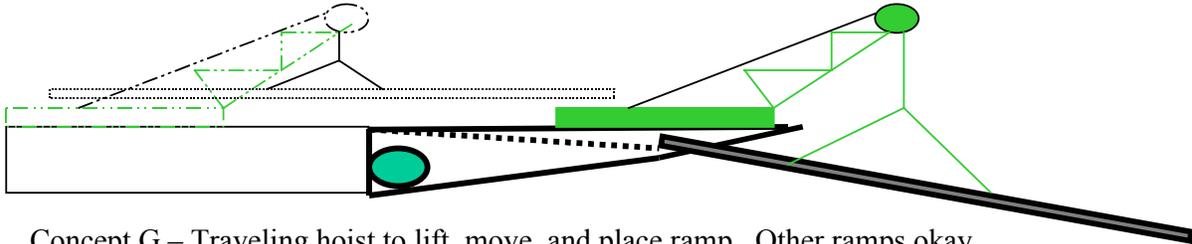


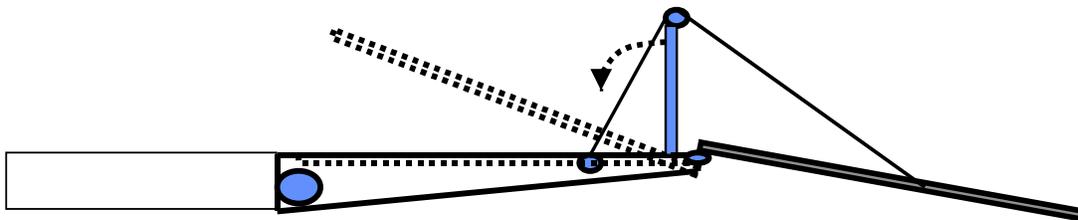
Figure 5-6. Alternative concepts for steep- to moderate-beach gradients.



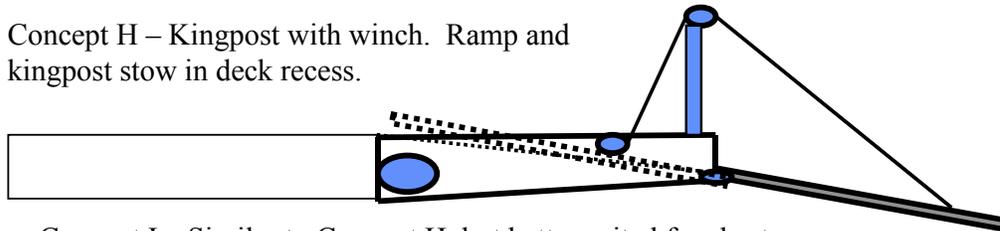
Concept F – Pivoting module with short flip-down ramp. Other ramps okay.



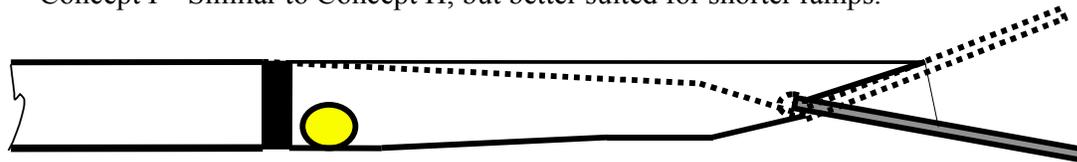
Concept G – Traveling hoist to lift, move, and place ramp. Other ramps okay.



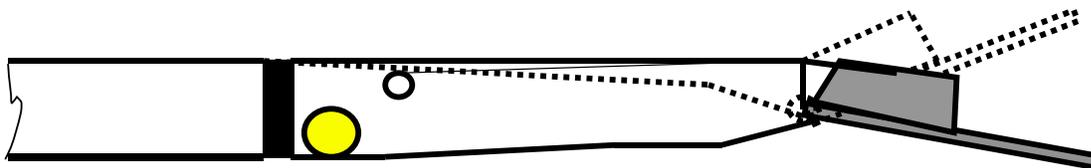
Concept H – Kingpost with winch. Ramp and kingpost stow in deck recess.



Concept I – Similar to Concept H, but better suited for shorter ramps.



Concept J – Extended gunwales to deploy ramp. Remove ramp for transport.



Concept K – Variation of Concept J. Extended gunwales part of ramp.

Figure 5-6. Alternative concepts for steep- to moderate-beach gradients (continued).

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Chapter 6

CONCEPT EVALUATION

The concept evaluation was guided by the criteria for the specification, which are:

- Performance Criteria
- Environmental Criteria
- Logistics
- Operational Considerations
- SEABOSS Interfaces

Some of the bow ramp and bow module issues that will influence the selection process are:

- Backup beach ramp deployment/retraction method required for operational use.
- Stacking of bow modules required for transport by MPR or LMSR shipping.
- Maximum slope for other ramps include C5A, 13 degrees, and MPF(E), 15 degrees
- Target bow ramp slope for 14 degrees on a flat beach. Ramp slope decreases as beach slope gets steeper.
- Bottom rake of bow module will affect additional trim toward bow.
- Bow thruster weight is unlikely to provide level trim in 80-foot bow module.
- Ramp module trim must be near level to connect to other CF modules.
- Other design considerations of the bow module may be necessary to enable flex connection to CF modules. Tapering the flex end and lowering the flex connector is one option.

Members of the SEABOSS design team that developed the bow module alternative concepts participated in the evaluation and down selection of the alternatives.

6.1 TRADE-OFF ANALYSES

A number of trade-off analyses were conducted to evaluate key components or subsystems of the bow module system. One of the leading trade-offs was the selection of the bow module configuration. Figure 6-1 graphs the minimum ramp length required for various slopes and vertical drops. This data was used to consider the height of the bow ramp hinge on the module and the deck taper angle. Figure 6-2 shows some bow module configurations that were considered.

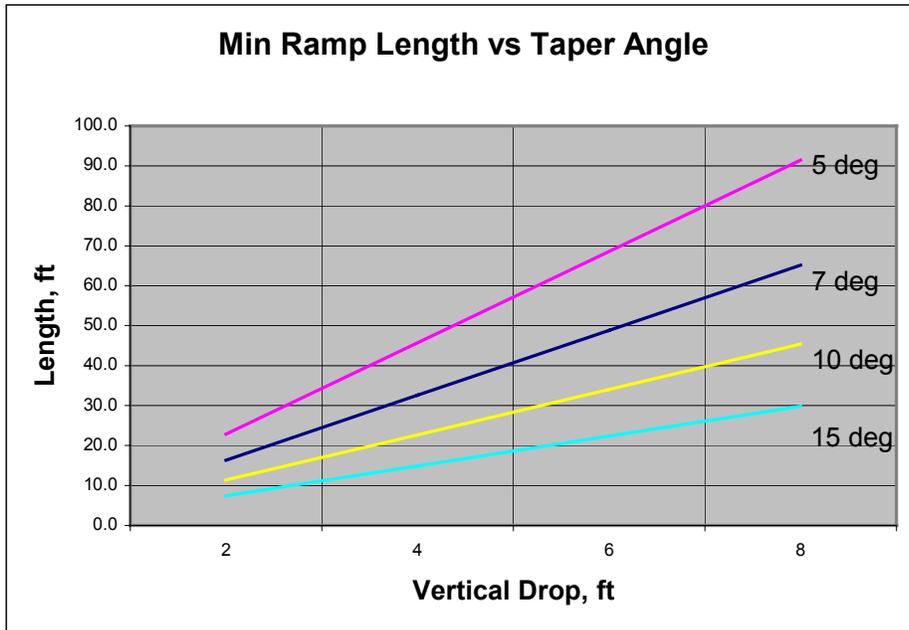


Figure 6-1. Minimum ramp length as a function of the vertical drop at various ramp slopes.

A comparative analysis was made between a 40-foot module and 80-foot module for the bow module length and is listed below.

- Space-wise, beach ramp functions and bow thruster components can be contained in a 40-foot module space.
- A 40-foot module would be very difficult to assemble to CF in SS 3.
- A 40-foot module would likely be mated to another 40-foot to make an 80-foot operational bow module.
- Could require special 40-foot module, if no 40-foot modules in SEABOSS system.
- Bow thruster components should be located in “non ramp” module of 40+40 module.
- Bow ramp and bow thruster components very likely to result in uneven trim of 80-foot beaching module, regardless of the component placement in the module.
- Uneven trim of bow module will add to flex connection difficulty.
- Hydraulic lines should avoid penetration of external bulkheads.
- Comparison favors single unit 80-foot bow module.

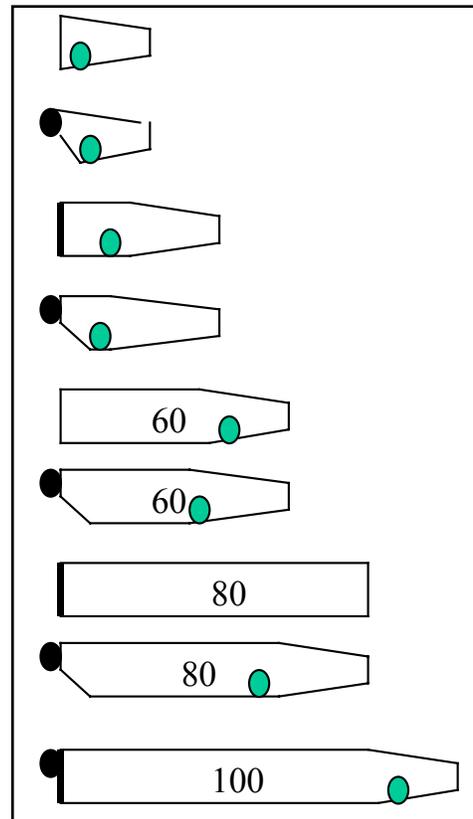


Figure 6-2. Bow ramp module length and CF connection alternatives.

It should be noted that all module widths considered are 24 feet. Although ISO compatibility is not strictly specified in this project, it is recommended when it does not adversely effect the component or system. Transport compatibility is never a bad thing in the logistics business.

After settling on an 80-foot overall length by 24-foot width for the nominal size and configuration for the bow module, the overall CF configuration became an issue. Figure 6-3 depicts several CF configurations that weighed in the decision making. Figure 6-4 shows the parametric computation of bow ramp length requirement after the key decisions were made on bow module length, bottom rake, ramp deployment/retraction, and CF configuration.

Pilot visibility is important in a long, low profile lighter like the CF. In its stowed position, the bow ramp projects well above the deck level of the CF. Figure 6-5 shows the ramp extending about 8 feet above the deck. Coast Guard recommendations were used for guidance for pilot visibility. Ultimately, the choice was to provide louvered openings in the bow ramp structure via deck gratings for the needed visibility.

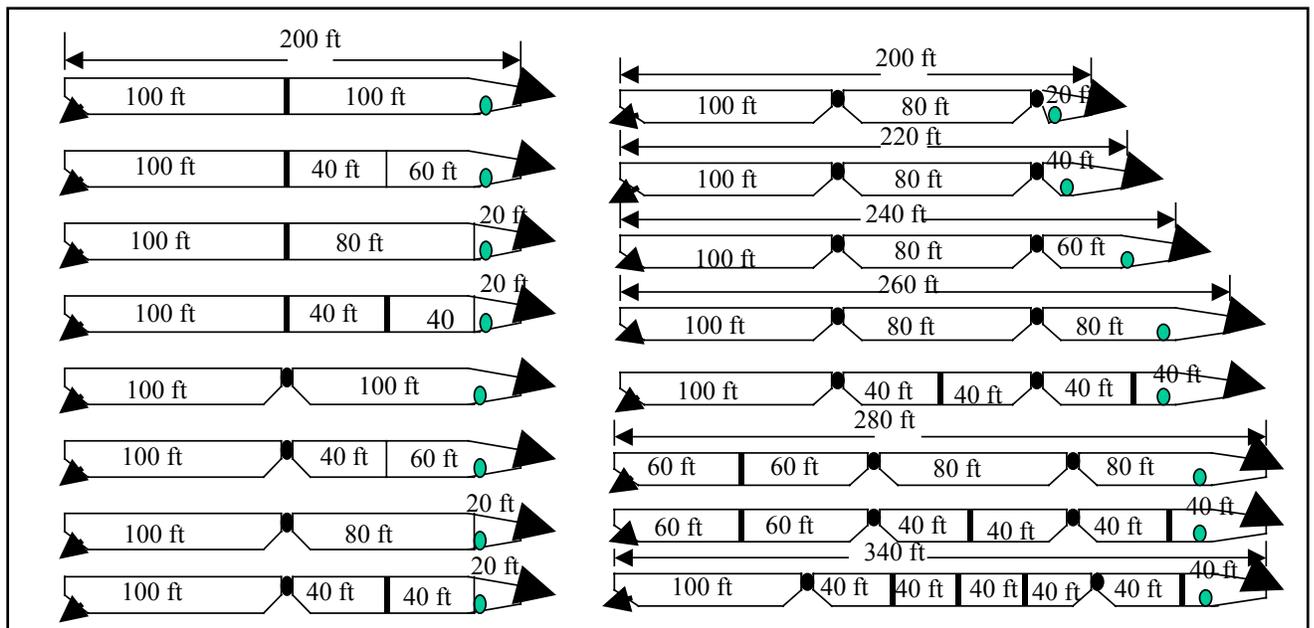


Figure 6-3. Rigid and flexed alternative JMLS CF configurations.

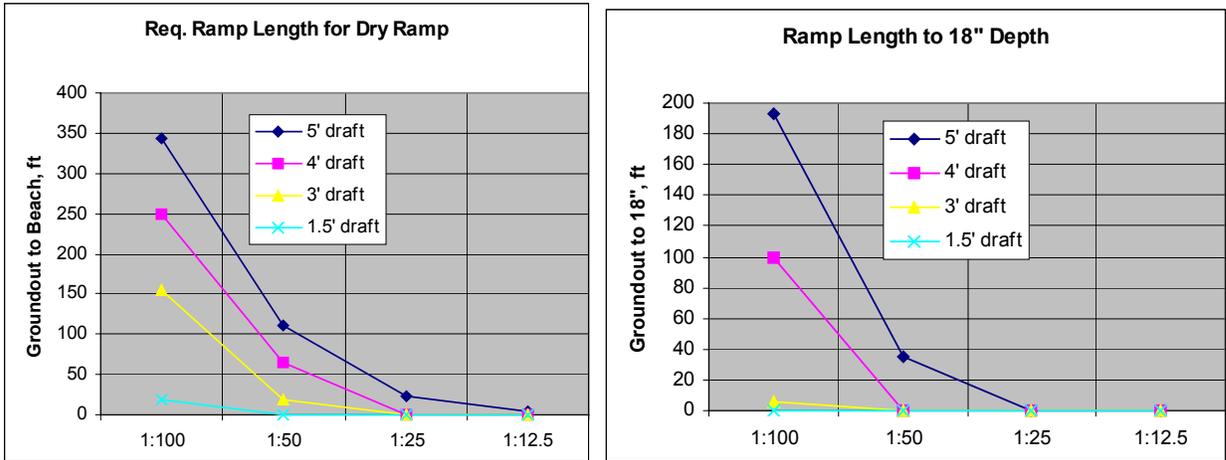


Figure 6-4. Distance from the beach to the bow of a grounded CF and distance from 18-inch water depth to the bow of a grounded CF for various CF drafts.

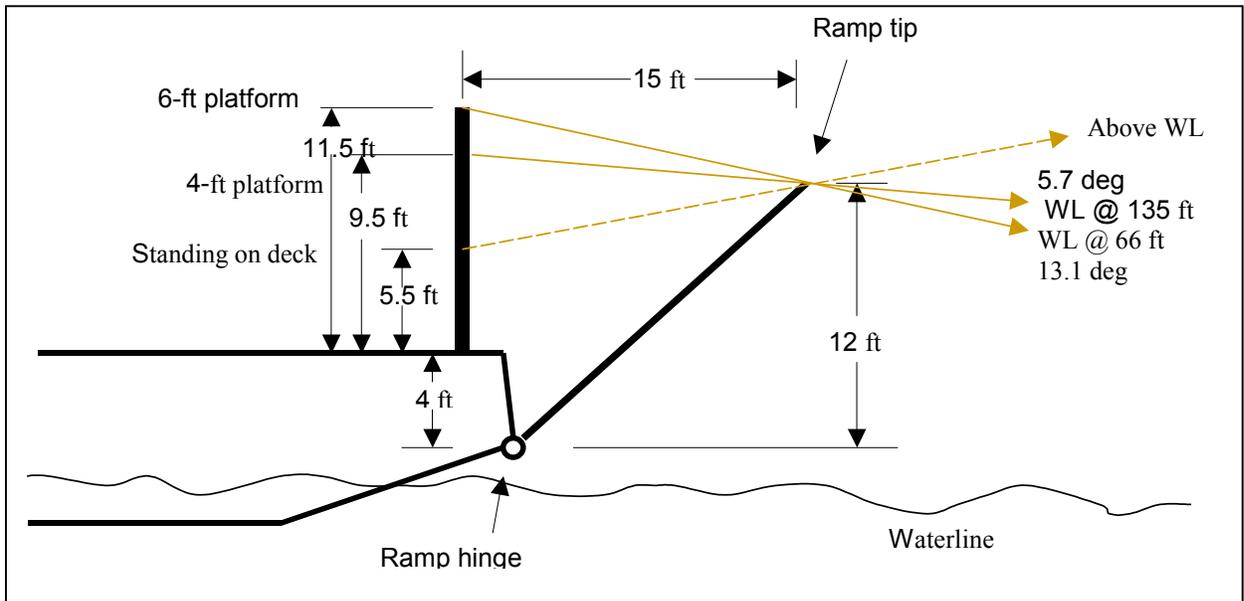


Figure 6-5. Pilot visibility considerations over beaching ramp.

Table 6-1. Alternatives for a Backup Beaching Ramp Deployment/Retraction System

Alternative	Description
Use existing hydraulic cylinders	Insert portable hydraulic pump to power existing cylinders locally.
Threaded rod jacking mechanism	Use turn-of-nut or worm gear drives to power threaded rods. Replace existing cylinders.
Mechanical leverage	Use block-and-tackle or other leverage to retract ramp via securing padeyes.
Pivot lever	Use hinged pivot to gain leverage to retract ramp. Winch or come-a-long provide power.
Port-a-power	Use portable hydraulic cylinders in place of existing hydraulic cylinders.
Repair/replace	Develop high level repair capability and deploy spares for critical systems.

Table 6-2. Failure Modes Analysis of JMLS Beaching Ramp System

Failure	Probability of Failure	Onboard Spare	Probable Fix During Operation
Prime mover	Low	No	Repair
Hydraulic pump	Medium low	Yes	Replace
Hydraulic reservoir	Medium low	No	Repair
Hydraulic lines	Medium low	Yes	Replace
Fluid contamination	Medium high	Yes	Repair
Hydraulic cylinder	Low	Yes?	Replace
Hydraulic hose	High	Yes	Replace
Hydraulic valves	Medium high	Yes	Replace
Hydraulic flow divider	Medium low	Yes	Replace
Ramp damage	Low	No	Repair
Securing system damage	Medium	Yes	Replace
Padeye damage	Medium low	No	Repair

Table 6-3. Assessment of Alternatives for Beaching Ramp Failure Modes

Failure	Probability of Failure	Spare	Fix	Does Alternative Fix the Failure?					
				A	B	C	D	E	F
Prime mover	Low	No	Repair	Y	Y	Y	Y	Y	?
Hydraulic pump	Medium low	Yes	Replace	Y	Y	Y	Y	Y	Y
Hydraulic reservoir	Medium low	No	Repair	Y	Y	Y	Y	Y	?
Hydraulic lines	Medium low	Yes	Replace	Y	Y	Y	Y	Y	Y
Fluid contamination	Medium high	Yes	Repair	N	Y	Y	Y	N	Y
Hydraulic cylinder	Low	Yes?	Replace	N	Y	Y	Y	Y	Y?
Hydraulic hose	High	Yes	Replace	Y	Y	Y	Y	Y	Y
Hydraulic valves	Medium high	Yes	Replace	Y	Y	Y	Y	Y	Y
Flow divider	Medium low	Yes	Replace	Y	Y	Y	Y	Y	Y
Ramp	Low	No	Repair	N	N	N	N	N	N
Security system	Medium	No	Repair	N	N	N	N	N	Y
Padeye	Medium low	No	Repair	N	N	Y	Y	N	Y

The backup deployment/retraction system for the bow ramp proved to be one of the more difficult design decisions to make in the project. The CF is a critical element of ship-to-shore logistics. It is unacceptable for failure of the primary deployment/retraction system to completely disable the CF. Table 6-1 shows several alternative approaches. A failure modes analysis was performed on the bow module to help determine which alternative would address the most failures. Table 6-2 shows the primary failure modes anticipated. Each of the alternatives of Table 6-1 was assessed against the failure modes of Table 6-2. The results are presented in Table 6-3. The pivot lever concept was judged to provide the best overall solution. Figure 6-6 is a schematic of the pivot lever alternative.

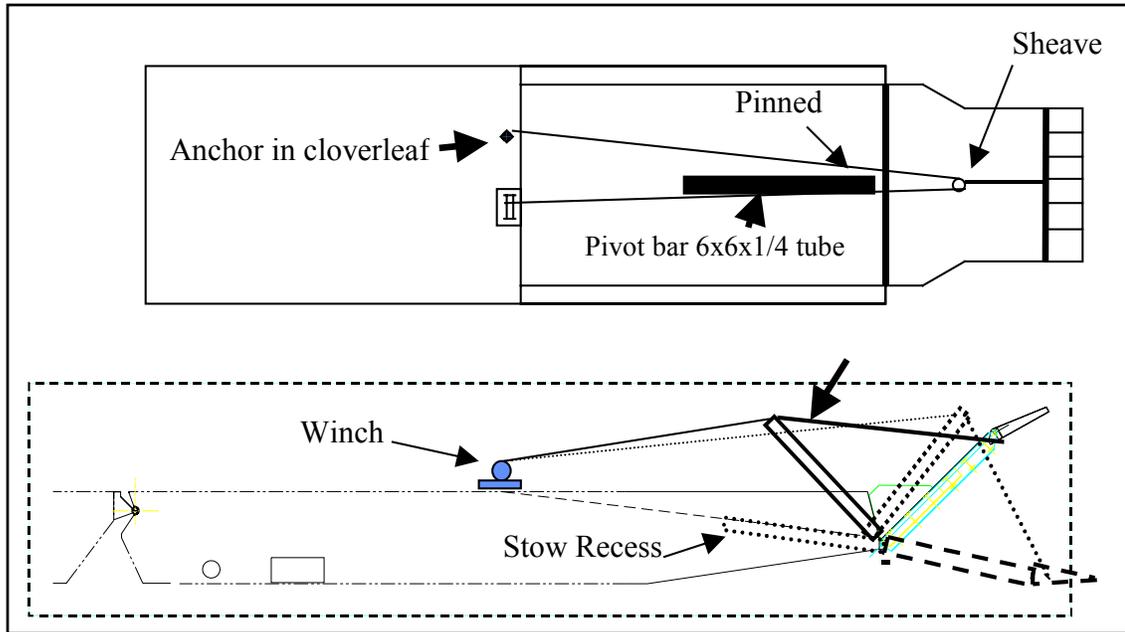


Figure 6-6. JMLS beach ramp backup deployment system.

6.2 CONCEPT SELECTION

To a large degree the final bow ramp and bow module were the result of an evolutionary process of trade-offs for ramp and module components and subsystems. Table 6-4 lists the general factors used to evaluate the concept alternatives. Refer to Appendix C for detailed beach ramp evaluation factors. The design team reviewed and discussed the alternatives to three or four concepts, which would be subjected to a detailed evaluation. Four finalists were selected. They are:

- C - Knuckle Boom Crane
- D - Hydraulic Rotary Actuators
- J - Extended Gunwales with hoist
- K - Variation of J with gunwales built to ramp

Table 6-4. Beach Ramp Evaluation Factors

Item	Evaluation Factors
CF Configuration	Transportability as other SEABOSS, beaching/retraction, MSI 9/ SS3
Beach Module Configuration	ISO compatible, trafficability, speed
Ramp Deployment	Simplicity, rapid deployment, redundancy, RAM
Ramp Capability	Length, structurally sound, stowable
System Performance	Effect on CF, SEABOSS interface capable, logistically supportable

Figure 6-7 depicts the four finalists. These concepts were assessed independently in accordance with the evaluation factors in Appendix C. Each concept had its supporters, but concept K prevailed. Figure 6-8 illustrates the basic features of the selected concept.

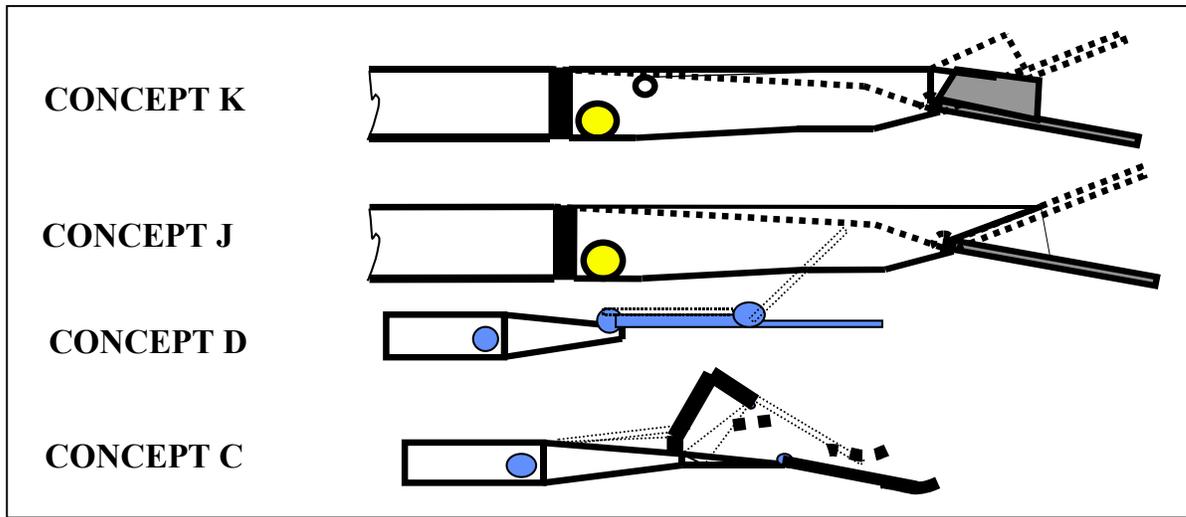


Figure 6-7. Concepts down selected from original alternatives.

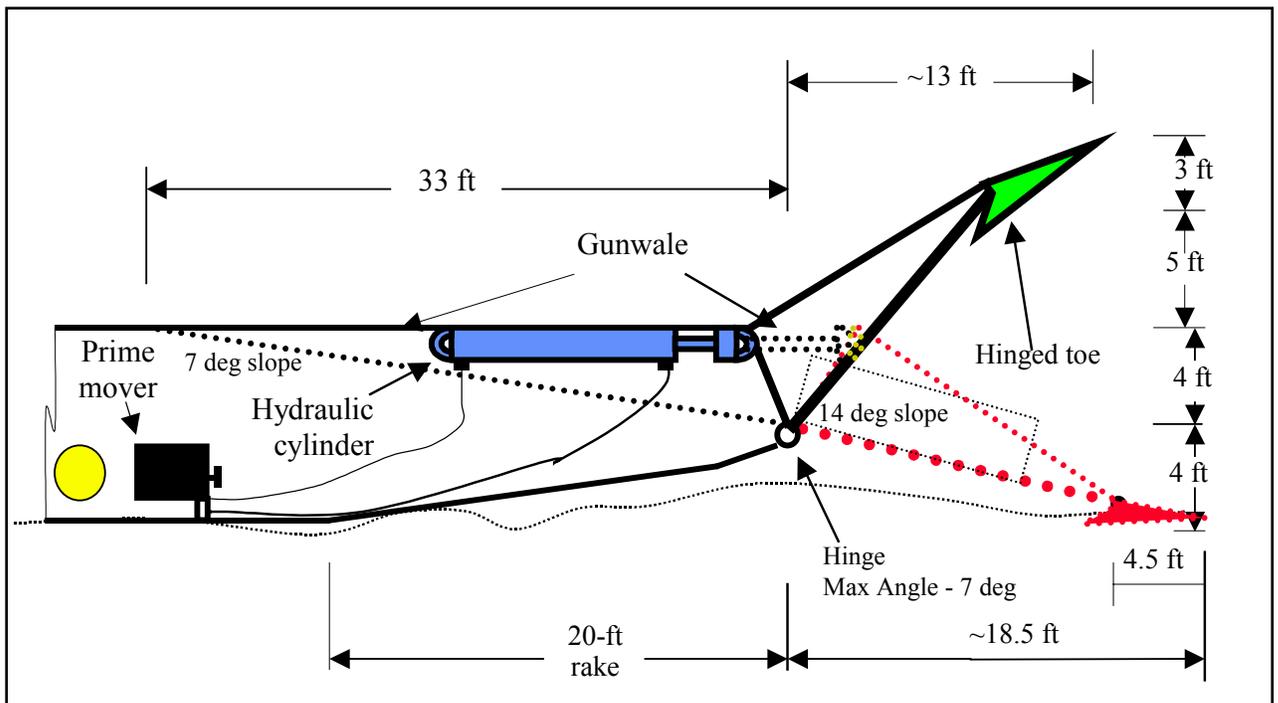


Figure 6-8. Proposed beaching ramp geometry and general arrangement.

Chapter 7

DESIGN EXECUTION

The development process for the bow module was quite extensive for this project. Initially, the operational needs and the environmental factors were explored with the military users to get a better perspective of the system to be developed. A review of beaching ramps and related applications, going back to the origination of the Navy's pontoon causeway in World War II, revealed what has been used in the past and how successful (or unsuccessful) they are. Military users were consulted to determine their future needs and to review their "lessons learned" of the past. From this data and other analyses, the beaching ramp criteria were refined for this SEABOSS application. The design team concluded that two approaches are required for the range of steep to flat slopes. At beach slopes less than 1:50, ramp lengths remain reasonable, while flatter beach slopes would require ramps of 100 feet or more. For flatter beaches, floating causeways should span the shallow gap to interface with the CF bow module. Trade-offs pared down the list of alternatives, leading to the concept selected for detailed design.

The design concept and the general arrangement of the bow module were completed by the design team. A member of the NFESC design team translated the design concept to a detailed drawing and parts listing. One of the design tasks was to assure that the trafficability requirements to discharge the military wheeled vehicles were met. Figure 7-1 shows the bow module profile on a flat beach. Figure 7-2 depicts the parameters for determination of breakover angles, approach angles, and departure angles for a typical trailer truck. Figure 7-3 shows the calculated final weight and horizontal center of gravity of the bow module. Figure 7-4 shows the estimated weight and trim for the bow module. The "SEABOSS bow ramp design drawings" are provided in Appendix D. The "Specification for SEABOSS CF Bow Module" is provided in Appendix E.

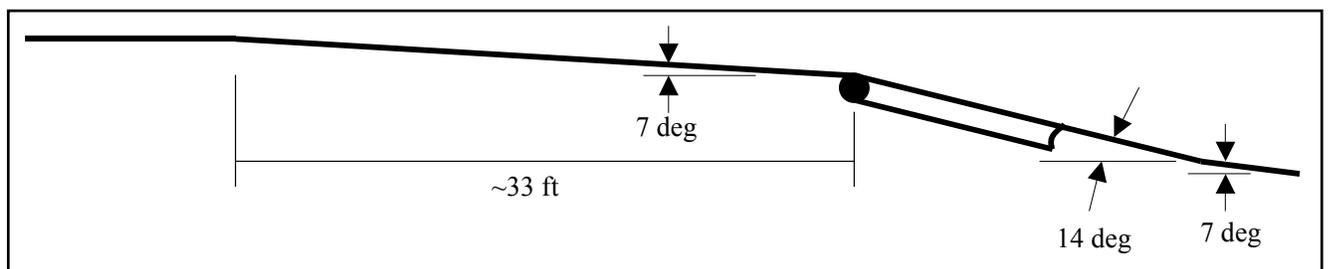


Figure 7-1. Beaching ramp module slope profile on a flat beach.

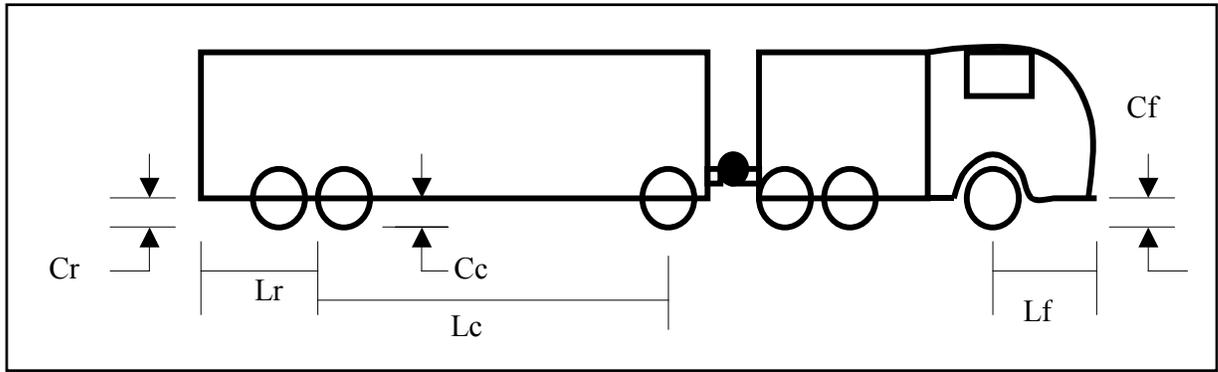


Figure 7-2. Vehicle clearance and axle spacing geometry.

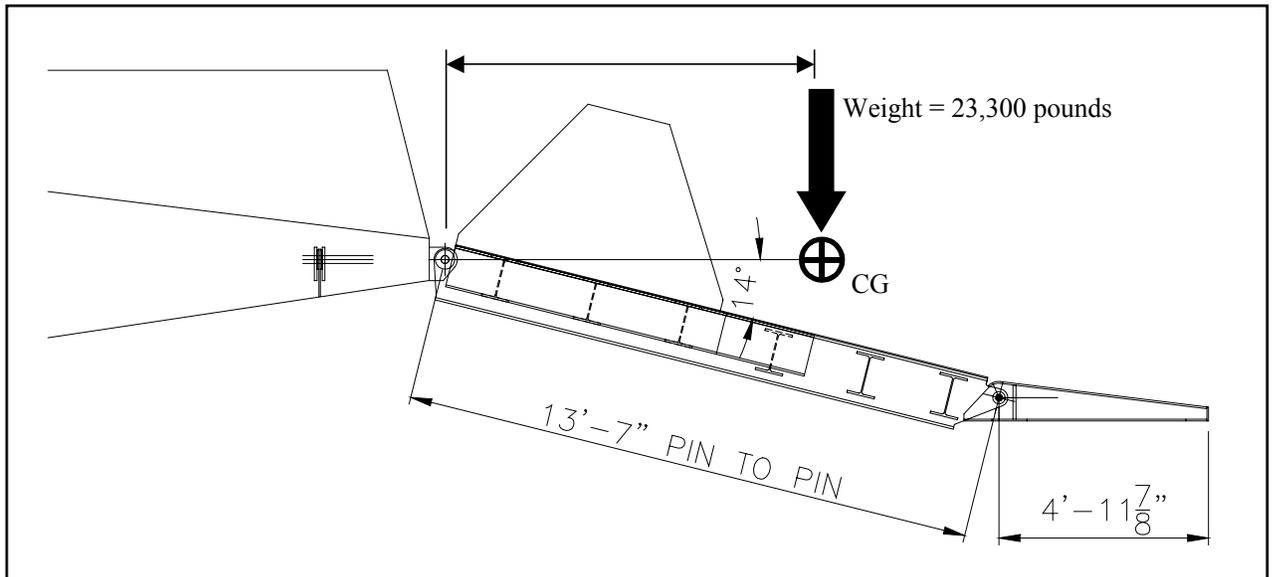
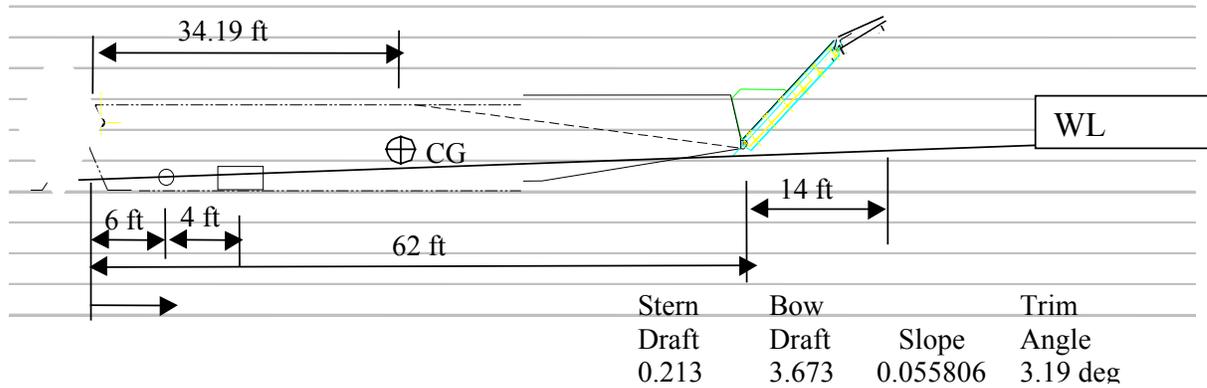


Figure 7-3. JMLS beaching ramp weight and center of gravity (horizontal).



Estimate the weight and trim of the JMLS bow module:

Component	Weight	X to CG	Moment	Bow Module Weight Estimate	
Bow ramp	22,000	69	1,518,000	40-ft module weight	100,000
Bow thruster	5,000	6	30,000	8 side connections	-24,000
Bow thruster power	5,000	10	5,000	40-ft module w/o side conn.	76,000
Flexor and receiver	4,000	2.5	10,000	Length of bow = 80-18	62
Bow module	<u>118,000</u>	31	<u>3,658,000</u>	Bow module	
				Wt = 62/40*76000	117,800
	154,000	34.19481	5,266,000		

Figure 7-4. JMLS beaching module weight and trim estimate.

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Chapter 8

BIBLIOGRAPHY

AFSC. Design Handbook DH 1-11, Air Transportability, Dept. of the Air Force, Aeronautical Systems Division, Wright-Patterson Air Force Base, 15 June 1983.

MAR, Inc., Technical Report No. 960 "ELCAS Installation on Shallow Beach Gradients," August 1990, Severna Park, MD (DTRC Contract No. N00167-86-D-0119/0114).

Marine Corps. Technical Manual, TM 11275-15/3c, "Principal Technical Characteristics of U.S. Marine Corps Engineer Equipment," September 1991.

Marine Corps. Technical Manual, TM 11240-15/4B, August 1994.

Marine Corp. Technical Manual, Motor Transport Technical Characteristics Manual.

Naval Civil Engineering Laboratory. Technical Memorandum No. 55-83-10. A Lightweight Ramp for Amphibious Missions, by B. R. Karrh, November 1983.

Naval Civil Engineering Laboratory. Memorandum "Beach Ramp Concept Study for the Navy's Elevated Causeway System," September 1979 (unpublished).

Naval Facilities Engineering Command. MIL-HDBK-1791, Handbook for Designing for Internal Aerial Delivery of Fixed Wing Aircraft.

Naval Facilities Engineering Service Center. Memorandum "NL Articulating Ramp," of 27 May 1998, by P. R. Kane and B.R. Karrh, Port Hueneme, California.

Naval Sea Systems Command (PMS 385). "Circular of Requirements for Conversion of an Existing Ship to an Enhanced Maritime Pre-Positioning Force Ship, MPF(E)," Arlington, Virginia, November 1995.

Operational Requirements Document for Joint Modular Lighter System (JMLS), Version 6, 11/17/00 [draft].

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Appendix A CAUSEWAY FERRY MOMENTUM BEACHING ANALYSIS

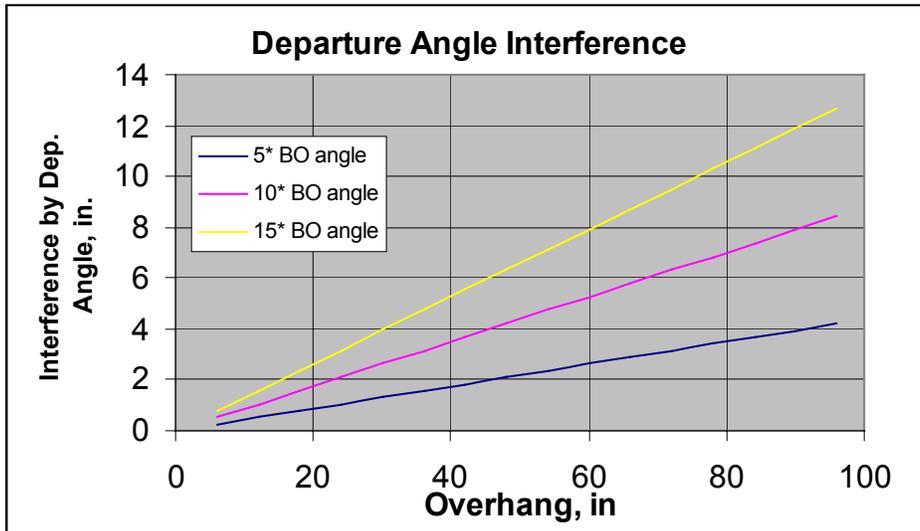
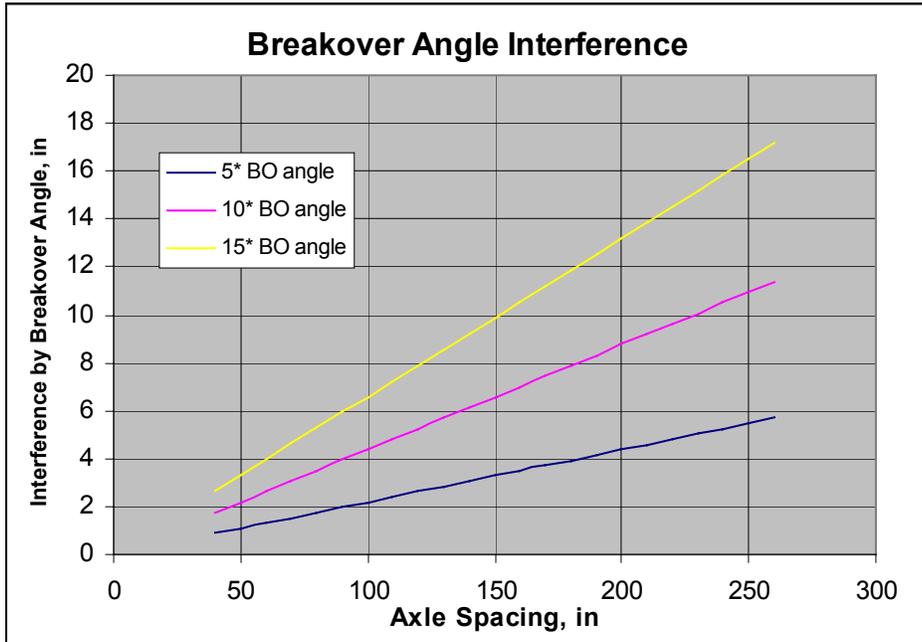
MOMENTUM BEACHING ANALYSIS OF FLEXED CF					4 FEET DRAFT				
@									
Draft=	1.5	3			3	57.24763			
W1=	184320	W2=	368640	W3=	414720	Friction Factor=	0.5		
	N= normal force= f(x) Speed=				6 knots = 10.13333 f/sec				
dT=	0.1	Beach Slope= 1:50=			0.01	0.578 deg	Thrust, P=	20,000 lb	
Station	T+dT	Vi	Xi-1	Xi	Yi	Ri	Ai	Xi+1	
-1	-0.1								
0	0	10.13333	-1.01333	0	0	0	0	1.013333	
1	0.1	10.13333	0	1.013333	0.010133	-311.296	-0.01036	2.026563	
2	0.2	10.1323	1.013333	2.026563	0.020266	-618.471	-0.02058	3.039587	
3	0.3	10.13024	2.026563	3.039587	0.030396	-921.55	-0.03067	4.052304	
4	0.4	10.12717	3.039587	4.052304	0.040523	-1220.56	-0.04061	5.064615	
5	0.5	10.12311	4.052304	5.064615	0.050646	-1515.52	-0.05043	6.076422	
6	0.6	10.11807	5.064615	6.076422	0.060764	-1806.47	-0.06011	7.087628	
7	0.7	10.11206	6.076422	7.087628	0.070876	-2093.42	-0.06966	8.098137	
8	0.8	10.10509	7.087628	8.098137	0.080981	-2376.42	-0.07908	9.107856	
9	0.9	10.09718	8.098137	9.107856	0.091079	-2655.49	-0.08836	10.11669	
10	1	10.08835	9.107856	10.11669	0.101167	-2930.67	-0.09752	11.12455	
11	1.1	10.0786	10.11669	11.12455	0.111245	-3201.98	-0.10655	12.13134	
12	1.2	10.06794	11.12455	12.13134	0.121313	-3469.45	-0.11545	13.13698	
13	1.3	10.0564	12.13134	13.13698	0.13137	-3733.13	-0.12422	14.14138	
14	1.4	10.04397	13.13698	14.14138	0.141414	-3993.05	-0.13287	15.14445	
15	1.5	10.03069	14.14138	15.14445	0.151444	-4249.24	-0.1414	16.1461	
16	1.6	10.01655	15.14445	16.1461	0.161461	-4501.74	-0.1498	17.14626	
17	1.7	10.00157	16.1461	17.14626	0.171463	-4750.59	-0.15808	18.14484	
18	1.8	9.98576	17.14626	18.14484	0.181448	-4995.81	-0.16624	19.14175	
19	1.9	9.969136	18.14484	19.14175	0.191418	-5237.45	-0.17428	20.13692	
20	2	9.951708	19.14175	20.13692	0.201369	-5475.55	-0.1822	21.13027	
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22	2.2	9.914487	21.13027	22.12172	0.221217	-5941.25	-0.1977	23.11119	
23	2.3	9.894717	22.12172	23.11119	0.231112	-6168.94	-0.20527	24.09861	
24	2.4	9.87419	23.11119	24.09861	0.240986	-6393.24	-0.21274	25.0839	
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27	2.7	9.808174	26.06699	27.04781	0.270478	-7046.16	-0.23446	28.02628	
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29	2.9	9.760579	28.02628	29.00234	0.290023	-7465.18	-0.24841	29.97591	
30	3	9.735738	29.00234	29.97591	0.299759	-7669.94	-0.25522	30.94694	
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32	3.2	9.684023	30.94694	31.91534	0.319153	-8070.12	-0.26854	32.88105	
33	3.3	9.657169	31.91534	32.88105	0.328811	-8265.63	-0.27504	33.84402	
34	3.4	9.629665	32.88105	33.84402	0.33844	-8458.13	-0.28145	34.80417	

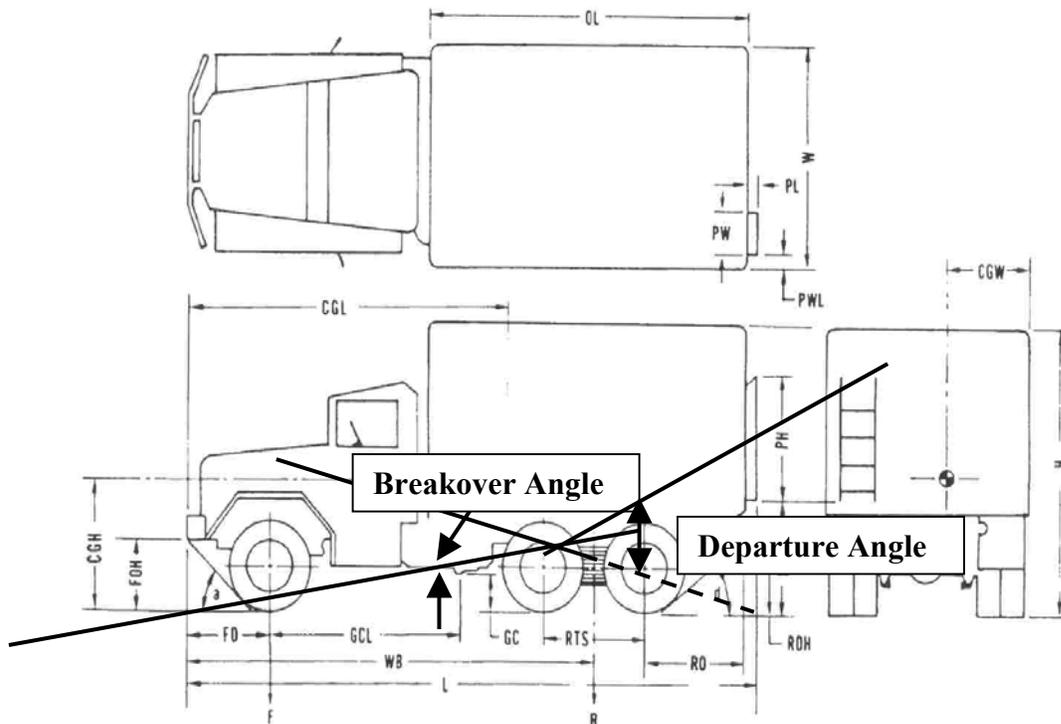
Sample computation for numerical analysis of momentum beaching of a causeway at 6 knots (full speed).

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APPENDIX B

TRAFFICABILITY ANALYSIS





LEGEND

- | | |
|----------------------------------|---------------------------------|
| OL - overall length body | WB - wheel base |
| W - overall width | FO - front overhang |
| PW - projection width | FOH - front overhang height |
| PWL - projection width location | RO - rear overhang |
| PH - projection height | ROH - rear overhang height |
| PHL - projection height location | GC - ground clearance |
| PL - projection length | GCL - ground clearance location |
| H - overall height | RTS - rear tire separation |
| L - overall length | a - angle of approach |
| CGL - center of gravity length | d - angle of departure |
| CGW - center of gravity width | F - front axle load |
| CGH - center of gravity height | R - rear tandem load |

Breakover Interference = Axle Spacing x tan (Breakover Angle/2)

Departure Interference = Overhang Length x tan (Departure Angle/2)

Appendix C

CONCEPT SELECTION CRITERIA

BOW MODULE EVALUATION FACTORS

Weight Factor

A. CF Configuration

- 1 . Transportable by military shipping - size, weight, stow, deploy
- 2 . Capability to be assembled into CF in SS 3
- 3 . Capability to transport 400 ST of cargo in SS 3
- 4 . Capability to attain 6 knot speed fully loaded in SS 3
- 5 . Capability to dock and hold position @ ELCAS and ships in SS 3
- 6 . Capability for unassisted beaching/retracting - fully loaded on slopes to 1:50
- 7 . Capability to withstand surf to MSI 9 surf when beached
- 8 . Capability for dozer assisted beaching/retracting
- 9 . Capability to interface with other SEABOSS systems (RRDF, FC)

B. Beach Module Hull Configuration

- 1 . Transportable by military shipping - size, weight, stow, deploy
- 2 . Capability for assembly into CF in SS 3
- 3 . Capability to contain ramp, deployment equipment, bow thruster
- 4 . Capability to load/offload military vehicles when beached and interfacing with RRDF and FC
- 5 . Capability of bow to slide over beach gradients rather than plowing in
- 6 . Capability to discharge military vehicles to beach and other SEABOSS systems
- 7 . Hydrodynamic response of module

C. Ramp Deployment Mode

- 1 Simplicity of operation
- 2 Rapid deployment capability
- 3 Backup deployment mode
- 4 Dozer push compatible
- 5 Operationally compatible
- 6 Reliable, maintainable

D. Ramp Capability

- 1 Beach gap length capability
- 2 Deployability
- 3 Durability
- 4 Stowability
- 5 Structural capability
- 6 Toe bearing capability
- 7 Bow function capability
- 8 Dozer push compatible

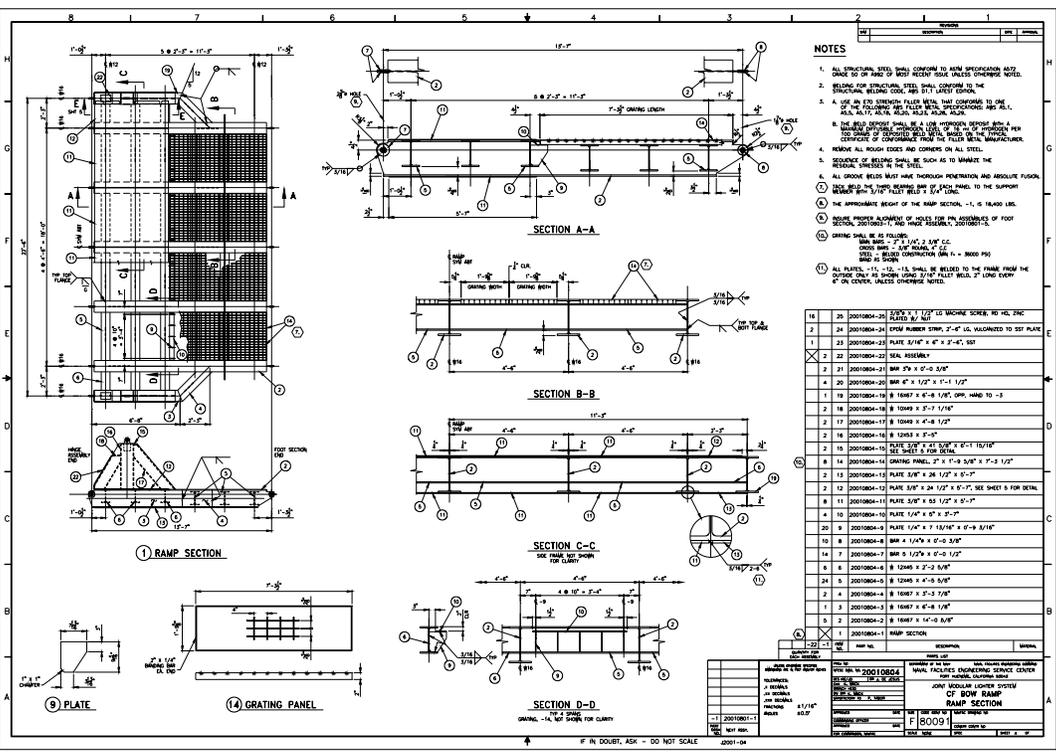
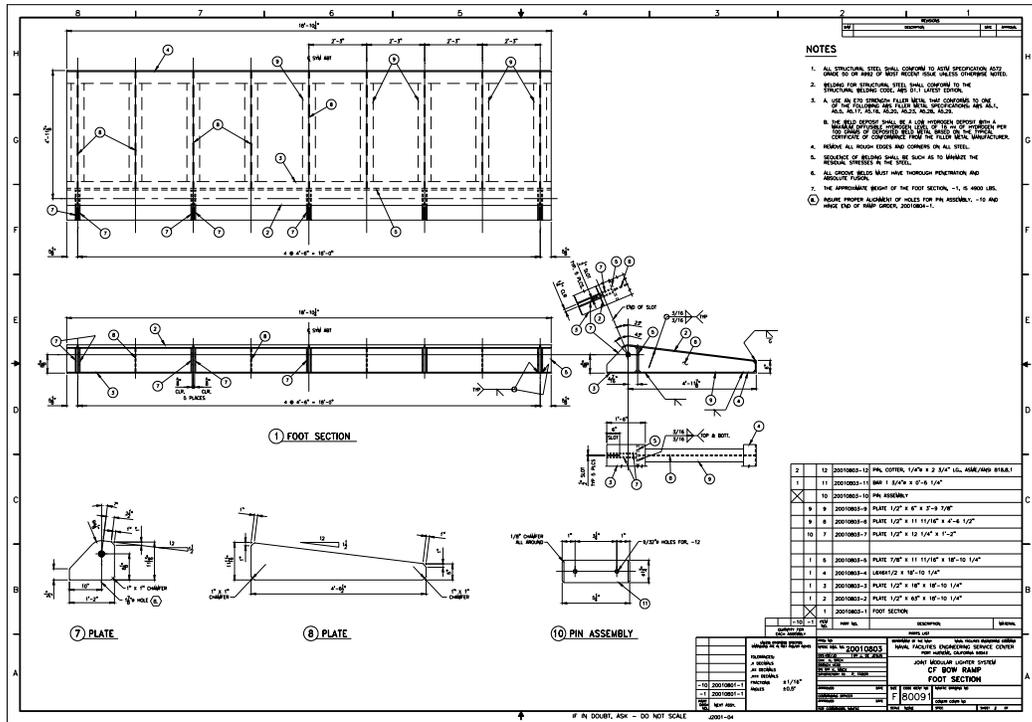
5. Weight < Twin Crane Capacity

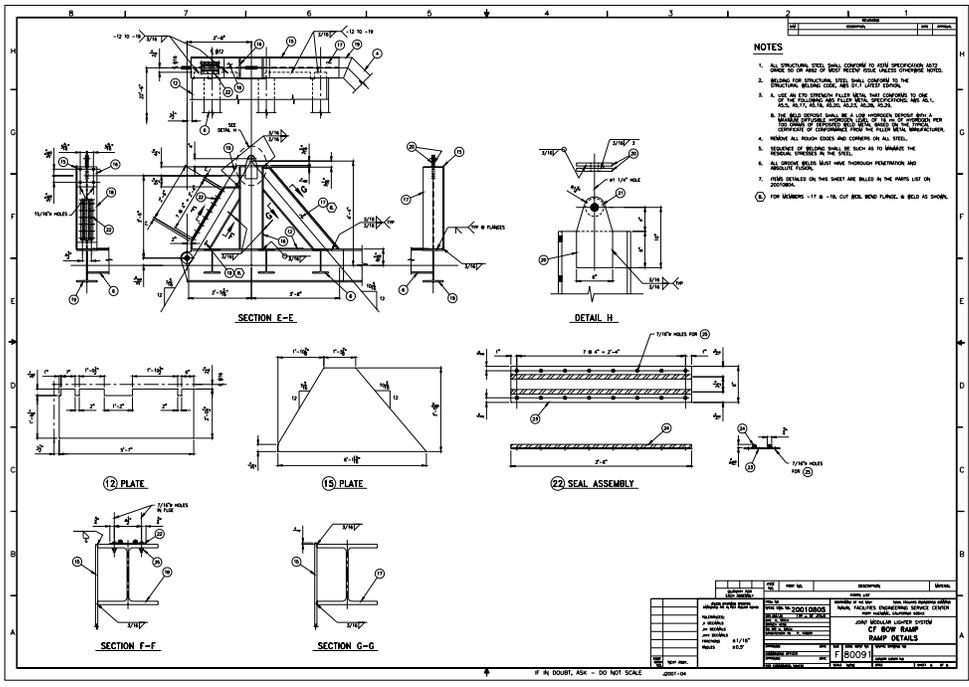
B. Logistics Impact

- Beach ramp configuration and properties, including length required to meet beach gradient requirements per the ORD
- General hull form (length, width, weight, draft, flexibility, geometry) and its impact on beaching
- Trafficability of beach ramp geometry (break-over angles)
- Deployment mechanism, powered or non-powered
- Bow thruster
- Type, size, and placement
- Use of thrusters (bow and/or propulsion) to move sand as a dredge

The following performance factors will be used to evaluate alternatives:

- Effect on assembly of the SEABOSS CF
- Ability to discharge cargo on beaches with steep or flat Gradients
- Time to deploy and retract
- Ability to operate in current, tides, surf conditions (MSI 9), waves, and wind
- Ability to breach surf zone obstructions, sand bars, and reefs
- Ability to interface with other SEABOSS systems, such as the RRDF, FC, and other water craft without degrading their performance
- Logistics impact
- Cost





- NOTES**
1. ALL DIMENSIONS UNLESS OTHERWISE SPECIFIED ARE IN INCHES. DIMENSIONS IN PARENTHESES ARE IN MILLIMETERS.
 2. MATERIALS AND FINISHES SHALL BE AS SHOWN IN THE SPECIFICATIONS UNLESS OTHERWISE NOTED.
 3. ALL DIMENSIONS SHALL BE TO THE CENTERLINE UNLESS OTHERWISE NOTED.
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Appendix E

SPECIFICATION FOR SEABOSS CF BOW RAMP MODULE

000 GENERAL GUIDANCE AND ADMINISTRATION

70 General Requirements for Design and Construction - General Guidance and Administration from the _____ (system spec) specification shall apply to the Causeway Ferry (CF) Bow module (BM). The bow module and bow ramp shall be designed to the structural and hydrodynamic specifications of standard SEABOSS modules as listed in Specification _____ (spec for deck and hull design loads for standard SEABOSS modules). Generally, the requirements specified herein will be in addition to the specifications for standard SEABOSS modules, although some specifications may be repeated to assure clarity. A government developed design concept for a CF bow module is provided for information only in Appendix As. A list of acronyms and definitions used in this specification is provided in Appendix Bs. Appendix Cs provides a list of lessons learned from previous beach ramp design applications. Vehicle types to transit the BM include tractor (e.g., USMC type M818 or M931A2)/trailer (e.g. USMC M870 or M870A1 type) with fully loaded 40-foot container, Rough Terrain Container Handler (RTCH) unloaded, 5-Ton Stake Truck, HUMMVEE, water buffalo, Heavy Equipment Trailer (HET), M1A1 Tank, USMC Logistics Vehicle System (LVS) MK48. Appendix Ds (from reference 2) lists USMC motor transport vehicles. Appendix Es is a list of reference documents used to assist the development of this specification.

92 Shipboard Tests – For shipboard tests components may be tested as part of the bow module. These tests shall be performed after installation of the component in the BM.

92.1 Bow Thruster Functional Test – The installed bow thruster system shall be tested for functional performance and operation of the controls prior to ship trials. Performance characteristics of the thruster and engine shall be validated by the respective manufacturers.

92.2 Bow Ramp Functional Tests – The installed bow ramp shall be tested for functional and operational performance prior to ship trials using the onboard control system. Representative military vehicles, including the Rough Terrain Container Handler (RTCH) and the Army’s Heavy Equipment Trailer (HET) (if available), shall load and discharge over the bow ramp at positions representative of flat beaches, steep beaches, and a pier deck two feet above the bow module deck.

94 Ship Trials – For ship trials the bow module shall be tested as an integral part of the SEABOSS causeway ferry. Testing shall include transportability of modules by Military Pre-positioned Force (MPF) shipping. Trials shall be conducted under conditions that permit evaluation of performance in sea state 3 and Modified Surf Index (MSI) 11.

94.1 Transportability Testing – Ship trials for transportability by MPF shipping shall include lifting modules by MPF crane(s), stacking modules on deck, securing for transport, offloading over the side, and assembly of the CF while afloat.

94.2 Speed Trials – CF speed trials shall include runs fully loaded (400 ST) and unloaded and with and without the bow module to determine that BM does not degrade the speed of the CF by more than 5 % for each condition.

94.3 Beaching Trials – The CF shall demonstrate the capability to retract from the beach under all beaching conditions and tidal ranges. A fully loaded CF with the bow ramp shall beach on flat (1:50 slope) and steep (1:10 slope) beaches to determine the ability to achieve a “dry ramp.” The CF may approach the beach at any speed up to full speed (6 knots) to achieve the dry ramp. A “dry ramp” requires that the water depth at the end of the bow ramp does not exceed 18 inches, which can be forded by military vehicles expected to use the ramp. The bow ramp shall be fully deployed from a stowed position to ready to discharge vehicles in each of the above scenarios. After each beaching trial, the bow ramp shall be retracted to the fully stowed position and the CF shall retract from the beach. Assist by dozers or warping tug is allowed for retraction only.

94.4 Docking Trials – The CF with the bow module shall demonstrate the capability to dock and moor at the SEABOSS Roll-on/Roll-off Discharge Facility (RRDF), the Navy Lightered (NL) RRDF, the Modular Causeway System (MCS) RRDF, the NL Floating Causeway (FC), the SEABOSS FC, the MCS FC and similar floating platforms up to two feet higher than the hinge point of the BM.

94.5 Vehicle load and discharge tests – Military vehicles, including the RTCH and the dozer, shall be loaded and discharged over the bow ramp under conditions representative of flat beaches (as in Beaching Trials), steep beaches, and a pier deck two feet above the bow ramp hinge point (as in Docking Trials). These tests may be performed in conjunction with the beaching and docking trials above.

95 Test Requirements – Assets, facilities, personnel, resources, and support equipment required to execute the Shipboard Tests and the Ship Trials are identified in this section.

95.1 Transportability Tests – These tests require an MPF ship, dock access, other SEABOSS modules, operators and support tugs, stacking dunnage, tie-downs, mooring and rigging gear, CF modules,

95.2 Speed Trials - Operators and support tugs, modules for complete CF, measured course, dock access, ballast material

95.3 Beaching Trials - Operators and support tugs, modules for complete CF, beach support equipment, beach access, dock access, ballast material

95.4 Docking Trials - Operators and support tugs, modules for complete CF, floating platform with deck two feet higher than bow module deck (RRDF, FC, etc.), dock access,

95.5 Vehicle load and discharge tests – Representative military equipment (6-8 units), RTCH, Dozer, and HET (if available).

HULL STRUCTURE

100 General Requirements for Hull Structure

100.1 When stowed, the bow ramp shall be integrated into the bow module hull such that it functions as the bow of the causeway ferry (CF) while underway. The angle or shape of the bow ramp shall minimize form drag resistance on the CF, insofar as other operational requirements are not compromised.

100.2 The arrangement of the bow thruster and other components in the BM shall effect draft and trim in a manner to enhance connection to an adjacent SEABOSS floating causeway

module with the SEABOSS flexible connectors, insofar as other criteria are not significantly impacted.

100.3 The BM shall have the capability to interface with the flexible connection system to be designed for CF modules; the bow module stern shear connector shall be of the female receiver type. See Section ____.

100.4 By arranging the loads on the CF, the BM shall be capable of attaining a hull bottom trim parallel to any beach gradient from 0 to 1:30.

100.5 Deck breakover angles on the BM departure roadway and between the departure roadway and the bow ramp shall not exceed 7 degrees; length between successive breakover angles shall be 20 feet or more.

100.6 Maximum slope of the bow module departure pathway and the bow ramp shall not exceed 14 degrees from horizontal when discharging onto a near zero gradient beach.

100.7 The BM shall be capable of achieving a "dry ramp" on mud or sandy beaches with beach gradients of 1:50 or less. See DEFINITIONS in Appendix Bs for "dry ramp".

100.9 Military Vehicle Trafficability Requirements

100.9.1 Definitions for trafficability requirements shall be as defined by the sketch shown in Appendix Ds.

100.9.2 The bow ramp and bow module shall be capable of discharging and embarking military vehicular cargo to the beach, the SEABOSS RRDF, or the FC ramp module at all operational drafts. The bow module shall be capable of discharging and embarking the US Army's Heavy Equipment Trailer (HET) under limited conditions suitable for operation of the HET.

100.10 When used as part of the CF, the bow ramp hinge shall not be fully submerged below the still water level at all CF load conditions (generally 4 feet maximum draft).

100.11 The bow ramp design shall provide for forward navigation visibility by CF operators during transit, maneuvering, docking, and beaching to enable safe operations.

100.11.1 For CF underway transit, use guidance provided by the US Coast Guard for passenger vessels over 328 feet long: "CG 46CFR Chapter 1 Subpart 72.04 – Navigation Bridge Visibility". This guidance specifies that the forward arc of visibility shall have no blind sector greater than 5 degrees caused by permanent obstructions.

100.11.2 For beaching, maneuvering and docking around other vessels and floating facilities, provision shall be made for visibility by a forward lookout. The lookout shall have direct wireless radio communication to the navigation bridge.

100.12 Fendering for the bow module shall be of the type and design as the standard SEABOSS modules (Specification ____).

100.12.1 Fendering shall be provided to protect the bow module while docking or when moored alongside ships, warping tugs, NL causeways, MCS, and SEABOSS RRDF and FC in sea state 3.

100.13 Deck Hardware for the bow module shall be of the same type and capacity as the standard SEABOSS modules. See Specification ____.

100.13.1 Vehicle tie-down fittings shall be located on the deck of the bow module (including the sloped deck) in the same pattern as the standard SEABOSS module, except for differences necessitated by overall length variations.

100.13.2 A total of six (6) portable bits shall be mounted on the bow module deck as follows: one bitt on each side 10 feet from the stern; 1 bitt on each side 40

feet from the stern; 1 bitt on each gunwale 10 feet from the bow. The bitts shall be 12-18 inches inboard from the side hull, except the two bitt locations on the gunwales may be adjusted for geometric and structural necessity. The bitts shall be the same type and capacity of those of standard SEABOSS modules. See Specification _____.

100.13.3 Two (2) [open or closed?] ____ -inch chocks, one on each gunwale, shall be mounted at about two feet from the bow end of the gunwales. The chocks shall be located flush with the outboard edge for proper fairlead in all directions. The chocks shall be the same type and capacity of those of standard SEABOSS modules. See Specification _____.

100.13.4 Four (4) lifting eyes, designed for a single-point lift 20 feet above the deck, shall be mounted on the deck for lifting the bow module by MPF pedestal cranes in sea state 3. The lifting eyes shall be compatible with MPF and travel lift sling gear. The lifting eyes shall be located to get the center of gravity beneath the crane hook using standard SEABOSS lifting slings.

100.14 Lifelines shall be of the type specified for standard SEABOSS modules. They shall be made of Kevlar with bendable stanchions, including a waist rope and a hip rope with sister hooks.

100.15 The bow module shall be capable of push tow by the SEABOSS warping tug to enable maneuvering for CF assembly.

100.16 Bow and stern rake angles of the bow module shall be selected to minimize form and drag resistance or for compatibility with the flexible connector, as appropriate. The bow rake shall be formed to enhance the ability to slide up the beach when the CF beaches at speed. The bow rake angle may be modified to enhance beaching of the CF.

100.17 The bow module shall have a hard point on the bow to enable dozers to assist retraction of the CF by pushing.

111 Shell Plating

111.1 The leading edge of the raked bow end of bow module shall be shaped so that the module will slide over the bottom upon contact with the beach (rather than digging into the bottom) when beaching/retraction of the CF.

116 Framing for Shell Plating and Innerbottoms shall be designed for the environmental and operational forces specified for the standard SEABOSS modules. See Specification _____.

116.1 The bottom hull plate and framing shall be designed to resist the forces from beaching a fully loaded CF at 10 knots. Multiple beach landings and corrosion shall not degrade the structural integrity of the bottom hull plate shell over the 20-year life of the module.

130 Decks and Platforms

130.1 Bow Ramp

130.1.1 The bow module shall be capable of discharging and embarking military vehicular cargo to the beach, the SEABOSS RRDF, or the FC ramp module at all operational drafts, including US Army's Heavy Equipment Trailer (HET) under limited conditions suitable for operation of the HET.

130.1.2 The deck breakover angle between the departure roadway and the bow ramp shall not exceed 7 degrees.

130.1.3 Maximum slope of the bow module departure pathway and the bow ramp shall not exceed 14 degrees from horizontal when discharging onto a near zero gradient beach.

130.1.4 The bow module design shall provide a roadway width of no less than 22 feet over its full length.

130.1.5 The width of the bow ramp along its full length shall not be less than the width of the RTCH plus 4 feet.

130.1.6 Bow Ramp Deployment

130.1.6.1 The bow ramp shall be capable of being deployed with or without power and ready to operate from its stowed position in 2 minutes or less. The bow ramp shall be capable of being retracted and stowed for transit in 4 minutes or less. The bow ramp deployment system shall have the capability to fully lower or raise the bow ramp in 30 seconds or less.

130.1.6.2 The preferred actuation (lowering and raising) method of the bow ramp is by hydraulic cylinders. Power to operate the hydraulics will be supplied from the bow thruster prime mover co-located inside the bow module. The bow ramp actuation components shall be contained in the gunwale section of the BM. Bio-degradable hydraulic oil shall be specified for all hydraulic systems.

130.1.6.3 After raising the bow ramp for CF transit, the bow ramp shall be stowed via a dogging/locking mechanism that does not require the active use of the deployment system and can be accomplished by one person in a reasonable and safe manner.

130.1.6.4 A backup bow ramp deployment/retraction system shall be provided in the event the primary deployment system becomes inoperative. The backup system shall have the capability to lower, raise, and stow the ramp without external power. The backup system shall be capable of being removed from stowage and rigged in less than 20 minutes. After initial rigging, the backup system shall be capable of deploying the stowed bow ramp in 5 minutes or less, and shall be capable of retracting and stowing the bow ramp in no more than 30 minutes. A concept that meets the above requirements is depicted in Figure ____.

130.1.6.5 The configuration of the bow ramp and the selection of fendering shall enable the CF to approach and moor alongside ships and to conduct lift on/lift off operations in sea state 3, while minimizing damage to the CF, the bow ramp, and the ship.

130.1.6.6 The departure angle between the bow ramp and the beach shall not exceed 14 degrees. A pivoting foot/toe will be provided at the outboard end of the bow ramp to minimize (transition) the departure angle from the bow ramp to the beach.

130.2 The deck of the bow module and the bow ramp itself shall be surfaced to enable tracked and rubber tired vehicles and personnel to transit the bow ramp under expected operating and environmental conditions without losing traction.

180.1 A structural foundation suitable for a hard point to push the CF off the beach with bulldozers shall be provided at the bow of the bow module.

180.2 A structural foundation to accommodate the forces developed by the flexible connector system shall be provided at the stern of the bow module.

180.3 A structural foundation to support the forces on the bow ramp during all operational modes shall be provided at the bow of the bow module.

180.4 A structural foundation to support the forces developed by the bow ramp deployment system shall be provided in the gunwales of the bow module.

180.5 Structural foundations shall be provided for vehicle tie-downs, mooring fittings (bits and chocks), fenders, and lifting points. These foundations shall be the same as those for standard SEABOSS modules. See Specification _____ (see spec for SEABOSS deck hardware) for further information.

192 Compartment Tightness

192.1 Internal compartments of the bow module shall be watertight with access between compartments in the same manner as standard SEABOSS modules. See Specification _____.

192.2 Internal machinery, piping, electrical wiring, and hydraulic systems shall be fitted between watertight compartments in the same manner as the SEABOSS warping tug. See Specification _____.

192.2 A watertight sealing mechanism shall be provided between the bow ramp and the bow module hull when the bow ramp is in the stowed position.

PROPULSION PLANT

200 General Requirements for Machinery Plant

200.1 Sufficient power shall be provided to power the bow module bow thruster, the bow ramp deployment system, the deck lighting, the navigation lighting, and the fire pump. See Specification _____ for bow thruster.

200.2 Machinery spaces shall be unmanned during operations, but shall be accessible for human entry in emergencies.

233 Propulsion Internal Combustion Engines

233.1 The electric motor driven bow thruster and the internal combustion engine/generator that supplies power for the bow thruster are contained in the bow module as specified by Specification _____.

233.2 Power to operate the bow ramp and lighting shall be available from the internal combustion engine/generator that supplies power bow thruster.

233.3 The internal combustion engine/generator that supplies power for the bow thruster shall supply sufficient power to raise or lower the bow ramp in 30 seconds or less. The time to raise or lower the bow ramp may be increased by as much as 50% when operated concurrently with the bow thruster.

252 Machinery Control Stations

252.1 A local control station to operate the bow thruster and the bow ramp shall be provided on the starboard gunwale of the bow module. The control station shall incorporate a tethered control head with a tether length of 25 feet. The control station and the tethered control head shall be resistant to the effects of weather, the marine environment, and JLOTS operational conditions.

ELECTRICAL PLANT

331 General Requirements for Lighting Systems – Distribution and Control

331.1 Lighting suitable for night cargo offload and backload operations over the bow ramp shall be provided with the bow module.

331.1.1 Lighting components shall be mounted on the gunwales of the bow module and shall be recessed and protected from damage. Lights shall be directed to provide lighting for operations when the ramp is in the deployed mode.

331.1.2 Power for lighting shall be provided by a generator mounted on the bow thruster's internal combustion engine.

332 Illumination Requirements

332.2 Lighting for the cargo operations over the bow ramp shall be sufficient to enable operators and personnel to see obstacles and work safely in the environment.

COMMAND AND SURVEILLANCE

422 Navigation Lights, Signal Lights, Searchlights, and Lights for Night Flight Operations

422.1 Provision shall be made to mount a 135 degree, battery powered portable range light suitable for CF operations on the starboard gunwale of the bow module. The range light shall be mounted in accordance with US Coast Guard regulations for craft over 50 meters long.

AUXILIARY SYSTEMS

502 Auxiliary Machinery

502.1 A bow thruster as specified by Specification ____ shall be installed in the stern of the bow module.

503 Pumps

503.1 A portable 81 gpm, 95 psi salt water wash down pump with a riser and hose shall be provided with the bow module. See Specification ____.

529 Drainage and Ballasting Systems (Surface Ships)

529.1 One way scuppers shall be provided to drain accumulated water overboard from the bow ramp cavity.

593 Environmental Pollution Control Systems

593.1 Cleanup gear shall be provided in the event of hydraulic oil spillage.

OUTFITTING AND FURNISHING

603 Draft Marks

603.1 Draft marks shall be provided as specified for other SEABOSS modules.

671 Special Stowage Arrangements

671.1 Stowage and hangers/brackets shall be provided inside the bow module for the following components: BM lifelines, 24 each 35,000 pound capacity tie-down gripes, emergency bow ramp deployment/retraction gear (contractor provided), range light, boat hook, 6 each ____ diameter portable fenders, salt water wash down pump (size?). The existing SEABOSS hatch design should be considered as a model.

ARMAMENT

700 Provide two multi-purpose gun mounts on each of the port and starboard gunwales.

INTEGRATION / ENGINEERING

800 Special Technical Data Requirements

800.1 Transportability Requirements

800.1.1 The bow ramp and module shall be deck transportable on MPF shipping.

800.1.2 The bow module including the bow ramp shall be fully contained within an 80-foot length envelope on deck of MPF ships.

800.1.3 The bow module shall not exceed 103 LT and shall be capable of being lifted on/off MPF ships with their onboard pedestal cranes, using either a single hook or dual hook 4-point lift at 20 feet above the deck.

800.1.4 The bow module shall be capable of stacking up to three high on the deck of MPF ships (in any position) with bow modules or any other SEABOSS modules.

800.1.5 The bow module shall be fitted with lifting eyes suitable for lifting as described in 800.1.3.

800.1.6 The bow module shall be liftable and transportable by the Travelift used by the PHIBCBs to manage SEABOSS causeway assets. A 6-point lift may be required.

800.2 System Interface Requirements

800.2.1 Beach Interface Requirements – As part of the SEABOSS CF, the bow module shall have the capability to beach and discharge military equipment on beaches under SEABOSS system specified environmental conditions.

800.2.1.1 The bow module shall enable a fully loaded CF to beach at full speed and achieve a dry ramp with beach slopes to 1:50.

800.2.1.2 As part of the SEABOSS CF, the bow module with its bow ramp shall be capable of discharging military vehicles onto beaches with slopes between 1:10 and 1:50.

800.2.2 Other SEABOSS System Interfaces

800.2.2.1 The bow module shall interface with the CF through the female shear receiver of the SEABOSS flexible connection system.

800.2.2.2 The bow ramp and bow module shall have the capability to interface with the SEABOSS RRDF and floating causeway ramp module to enable the transfer of military vehicles to/from the CF.

800.2.3 Interface with US Army Modular Causeway System (MCS) – As part of the SEABOSS CF, the bow module shall be capable of discharging/receiving military vehicles to/from the MCS via the landing ramp.

800.2.4 Interface with NL Causeway systems – As part of the SEABOSS CF, the bow module with its bow ramp shall be capable of discharging/receiving military vehicles to/from NL causeway floating facilities.

800.2.5 Interface with ELCAS(M) - As part of the SEABOSS CF, the bow module with its bow ramp shall be capable of docking and mooring to the ELCAS(M) to enable containers to be lifted on/off by ELCAS(M) crane.

800.2.6 Interface with DOD Shipping and Commercial Shipping - As part of the SEABOSS CF, the bow module with its bow ramp shall be capable of docking and mooring alongside DOD and commercial ships for the purpose of lifting containers on/off the deck.