

**A MECHANISTIC STUDY OF THE BRITTLE TO DUCTILE TRANSITION  
IN HIGH MELTING POINT INTERMETALLIC COMPOUNDS**

**A Report on a Program of Research Conducted at  
The University of Illinois  
Department of Materials Science and Engineering**

**Principal Investigator:  
Hamish L. Fraser**

**Office of Naval Research, Grant Number: N00014-89-J-1233**

***Preamble***

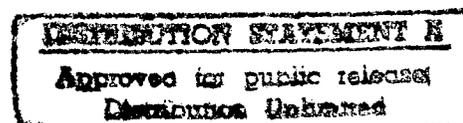
This report describe the work done on an ONR grant involving a study of high melting point intermetallic compounds. This grant was supposed to be of a three year duration, but lasted only approximately nine months because the Principal Investigator accepted a position on the faculty of the Ohio State University. The program was transferred to the Ohio State University, and was eventually renewed and enlarged in scope - a successful program.

***Aims of the Program***

The previous program of research was aimed at developing a fundamental understanding of the mechanisms of plastic deformation in certain high melting point intermetallic compounds. The results of this study were to have lead in part to a more detailed understanding of the factors that influence the lack of ductility exhibited at ambient temperatures by these types of compound.

In order to study the deformation mechanisms of these materials at ambient temperatures, where they exhibit brittle behavior, it was proposed that ductile phase toughening should be employed so that some degree of plastic deformation might be induced in the brittle compounds. It was hoped that from a detailed analysis of defects in the deformed samples the various factors influencing the deformation mechanisms would become apparent. In the case of the higher temperature deformation experiments, a determination of the contribution of diffusive mechanisms to plastic deformation was to be made.

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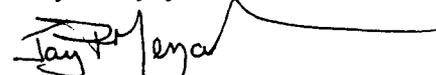
SUBJECT: ONR Grant N00014-89-J-1233 - Final Report

Dear Dr. Polk:

In accordance with the terms of the subject grant, enclosed are three (3) copies of the final technical report that have been prepared by Professor Hamish Fraser, the principal investigator. Please accept our apologies for the lateness of this report. I trust this will allow for the official close-out of the subject grant to be completed. Additional copies of the final report have been distributed as indicated below.

Should you have any questions concerning the technical content of the report, please contact Professor Fraser at Ohio State University at (614)292-2708. If I can be of assistance, please feel free to contact me at (217)244-6422.

Very truly yours,



Jay P. Menacher  
Assistant to the Head

enclosures

cc: ONR/Administrative Grants Officer/Chicago (1)  
Naval Research Laboratory/Director (6)  
Defense Technical Information Center (12)  
UIUC Grants & Contracts (1)  
H. Fraser

The effect of extrinsic factors such as the possible detrimental rôle of interstitial impurities and the influence of alloying elements on microstructure was to be examined. Alloying additions were to be made in response to the results of the work aimed at determining the mechanisms of plastic deformation; the specific additions were to be chosen on the basis of their intended rôle (e.g. modification of crystal structure) and the results of calculations being performed elsewhere concerning the influence of electronic structure on crystal structure and mechanical properties.

Finally, the creep properties of two types of alloy samples were to be determined.

## 2.2 Summary of Results

The original proposal called for studies of  $\text{Al}_3\text{Nb}$ ,  $\text{RuTi}$ ,  $\text{V}_3\text{Si}$ ,  $\text{Ti}_5\text{Si}_3$  and  $\text{Nb}_3\text{Al}$ . Work for the nine month program was initiated on  $\text{Al}_3\text{Nb}$ ,  $\text{Ti}_5\text{Si}_3$ ,  $\text{V}_3\text{Si}$  and  $\text{Nb}_3\text{Al}$ .

In the case of the compound  $\text{Al}_3\text{Nb}$ , There appears to be a tendency for the compound  $\text{Al}_3\text{Ti}$  to tolerate ribbons of anti-phase boundaries (APB's) on (001), whereas the opposite trend for is observed in  $\text{Al}_3\text{V}$ , and also ordered microtwinning occurs commonly in  $\text{Al}_3\text{Ti}$ , whereas this deformation mechanism is absent in  $\text{Al}_3\text{V}$ . The difference in this behavior may be accounted for as follows. Thus, the formation of ribbons of APB on (001), is consistent with a significant difference in the APB energy between the two compounds. Careful consideration of the stacking sequences about these faults in  $\text{DO}_{22}$  crystals shows that the formation of an APB on the (001) plane produces a thin ribbon of  $\text{DO}_{23}$  structure. It is proposed here that the difference in the APB energy on the (001) planes is due to the relative stability of the  $\text{DO}_{22}$  structure compared to that of the  $\text{DO}_{23}$  structure for these compounds. Thus, Carlsson and Meschter (1989) have performed calculations, based on the augmented spherical wave method, of the variation in energy of these two structures compared with the  $\text{L1}_2$  structure for several  $\text{Al}_3\text{X}$  compounds. These results have been used here to deduce the energy differences between the  $\text{DO}_{22}$  and  $\text{DO}_{23}$  structures for the various compounds, shown in Table 1. As can be seen, for  $\text{Al}_3\text{Ti}$  the energy difference between the two crystal structures is rather small, and so it seems reasonable to assume that the APB energy would be rather low. However, for the case of  $\text{Al}_3\text{V}$  this difference in energy of the two structures is relatively large, and so therefore the apparently high value for the APB on (001) for this compound may be understood. It is, of course, tempting to interpret the difference in the twinning behavior in the same way. In the case of the twinning shear provided by glide of dislocations with  $\mathbf{b}=\frac{1}{6}\langle 111 \rangle$  on {112} in the  $\text{DO}_{22}$  structure, ribbons of material with the  $\text{Cu}_3\text{Ti}$ -type structure are produced. The differences in energy between the two structures  $\text{DO}_{22}$  and  $\text{Cu}_3\text{Ti}$ -type for these two compounds have not been computed. However, it is significant that the compound  $\text{Al}_3\text{Ti}$  with

the DO<sub>22</sub> structure appears to be less stable relative to several other structures, such as L1<sub>2</sub> or DO<sub>23</sub>, as suggested by the results of calculations (Carlsson and Meschter 1989). If it is assumed that this trend concerning relative phase stability applies also to a comparison of the Cu<sub>3</sub>Ti-type and DO<sub>22</sub> structures for these two compounds, then it follows that the energy associated with the formation of a twin will be significantly lower in Al<sub>3</sub>Ti than in Al<sub>3</sub>V.

	Ti	V
E(DO <sub>22</sub> )-E(L1 <sub>2</sub> )	-0.059	-0.175
E(DO <sub>23</sub> )-E(L1 <sub>2</sub> )	-0.026	-0.067
E(DO <sub>22</sub> )-E(DO <sub>23</sub> )	-0.033	-0.108

Table 1. The energy differences (in eV/atom plane) between the various structures listed for Al<sub>3</sub>X (where X is Ti or V). The data in the first two rows have been obtained from the results of Carlsson and Meschter (1989), whereas the final row contains values deduced from these latter rows. Note that the DO<sub>22</sub> structure is the most stable from the point of view of free energy.

It is proposed then that the occurrence of order twinning in compounds with the DO<sub>22</sub> crystal structure is influenced by the difference in energy between this structure and the Cu<sub>3</sub>Ti-type structure, and so for compounds where the deformation mechanisms are dominated by twinning it is expected that there would be a relatively small difference in energy between these two structure types. One such compound is Ni<sub>3</sub>V which is relatively ductile and where plastic deformation is effected in the main by twinning (e.g. Liu 1984). The energy differences between the two structure types (DO<sub>22</sub> and Cu<sub>3</sub>Ti-type) have not been calculated for this compound, but the fact that this difference may be relatively small may be deduced by reference to the *structure map* proposed by Pettifor (1986 and 1988) for the AB<sub>3</sub> compounds. There are a number of compounds exhibiting the Cu<sub>3</sub>Ti-type structure adjacent to the group of compounds having the DO<sub>22</sub> structure. This is consistent with there being a small energy difference between these two structures in the case of Ni<sub>3</sub>V.

We have determined that the compound Al<sub>3</sub>Nb deforms in similar manner to Al<sub>3</sub>V, and therefore it is reasonable to assume that this compound is reasonably stable in the DO<sub>22</sub> form. It has been a popular thesis that, to increase ductility, alloying should be used to effect changes in crystal structures of compounds, such as those with the DO<sub>22</sub> structure, to ones of higher

symmetry, e.g. cubic  $L1_2$ . The present results suggest that rather than attempting to cause a change in structure, it may be more profitable in terms of ductility to add alloying elements that result in a reduction in the relative energies of the  $DO_{22}$  and  $Cu_3Ti$ -type structures, and so promote the degree of twinning during plastic deformation in the  $DO_{22}$  structure. However, despite this conjecture, it has not been possible to alloy  $Al_3Nb$  such that these changes have occurred!

A part of the study which has proven to be the most tedious involves the compound  $Ti_5Si_3$  since it has been almost impossible to cause plastic deformation. Thus, our scheme has been to produce the compound in the presence of  $\alpha$ -Ti, where this latter phase was added to provide ductile phase toughening. It was hoped that the total strain experience by samples during compression testing might be increased by the presence of such a phase so that some deformation might occur in the harder, more brittle, phase. However, we have no evidence that in our experiments plastic strain has been produced in  $Ti_5Si_3$ . These experiments were terminated in view of the very exciting results obtained in the case of our studies of  $Nb_3Al$ , described below. Samples of  $V_3Si$  were also found to be rather brittle.

A very exciting set of results have been obtained from experiments involving the compound  $Nb_3Al$ ; these are summarized briefly here.  $Nb_3Al$  was chosen for study on the basis of its melting point ( $\approx 2000^\circ C$ ), the range of composition over which the compound is stable, and because of a relatively low density (for example when compared to Ni-base superalloys). However, the binary compound in its stable form has the A15 crystal structure, and in common with many other compounds with this structure, it is very brittle at ambient temperatures. The brittle to ductile transition temperature is  $\approx 1000^\circ C$ . The exciting result of the present work is that we have been able to form a metastable form of  $Nb_3Al$ , having the B2 crystal structure, in rapidly solidified ribbons of Nb-Al alloys. On thermal cycling between room temperature and either  $800^\circ C$  or  $1100^\circ C$ , the grains of the B2 phase become more heavily dislocated, presumably because of the mismatch in coefficients of thermal expansion between the A15 and B2 phases. This is a very exciting result because it shows that the B2 phase can be readily deformed. This fact is to be exploited in a subsequent ONR program.

### *References*

- Carlsson, A.E. and Meschter, P.J., 1989, *Mater. Res.* **4** (5), 1060.  
Liu, C.T., 1984, *Intl. Metals Rev.*, **29**, 168.  
Pettifor, D.G., 1986, *J.Phys.C.*, **19**, 285.

Pettifor, D.G., 1988, Mat. Sci. and Tech., **4**, 675.

*Papers Published as a Result of this Program*

"Factors Influencing the Deformation Mechanisms in the Intermetallic Compounds  $\text{Al}_3\text{Ti}$  and  $\text{Al}_3\text{V}$ ", Phil. Mag. Letts, 1990, **62**,143.

*Students Supported by this Program*

Robert Wheeler  
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