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Finite element analysis of static and dynamic fracture of brittle microcracking
solids was performed. The continuum constitutive modeling for rate-dependent
fracture of brittle microcracking solids is discussed. The rate-type constitutive
equation that is proposed takes into account the rate effect on microcracking
and plastic deformation. In order to test the validity of the proposed modeling,
numerical studies were conducted on a bar under uniaxial tension, a beam under
pure bending, and on the phenomenon of microcracking around the tip of a macrocrack
under mode-I loading. Finite element analysis of stationary and rapidly-propagating
macrocracks under dynamic loading. The microcrack toughening effect is discussed,
along with the influence on it of the size of the microcracked process zone and
the various parameters in the microcrack density evolution equation, through the
observation of the behavior of the general crack-tip energy-release parameter,
the T integral. Some important aspects associated with the transformation induced
plasticity in Al2O3-ZrO2 are analyzed using a computer simulation based on Finite
Element Method (FEM).

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BRIEF OUTLINE OF RESEARCH FINDINGS

*Finite Element Analysis of Static and Dynamic Fracture of Brittle Microcracking Solids: Part 1:*
The continuum constitutive modeling for rate-dependent fracture of brittle microcracking solids is discussed. The rate-type constitutive equation that is proposed takes into account the rate effect on microcracking and plastic deformation. In order to test the validity of the proposed modeling, numerical studies are conducted on a bar under uniaxial tension, a beam under pure bending, and on the phenomenon of microcracking around the tip of a macrocrack under mode-I loading.

*Finite Element Analysis of Static and Dynamic Fracture of Brittle Microcracking Solids: Part 2:*
The continuum constitutive modeling for rate-dependent fracture of brittle microcracking solids, which was described in part 1 of this paper, is applied to the finite element analysis of stationary and nonstationary macrocracks in a single-edge-notched three-point bend specimen under a
static loading. The microcrack damage zones near the macro-crack-tip can be classified as being "large-scale." The microcrack toughening effect in stationary cracks is observed through the behavior of the crack tip energy flux parameter, the $T^*$ integral. The numerical results of the nonstationary crack analysis are compared with the available experimental results for a silicon carbide specimen.

**Finite Element Analysis of Static and Dynamic Fracture of Brittle Microcracking Solids: Part 3:**

The continuum constitutive modeling for rate-dependent fracture of brittle microcracking solids, which was described in part 1 of this paper, is applied to the finite element analysis of stationary and rapidly-propagating macrocracks under dynamic loading. The microcrack toughening effect is discussed, along with the influence on it of the size of the microcracked process zone and the various parameters in the microcrack density evolution equation, through the observation of the behavior of the general crack-tip energy-release parameter, the $T^*$ integral.

**Computer Simulation of Transformation Induced Plasticity using Finite Element Method:**

Some important aspects associated with the transformation induced plasticity in $\text{Al}_2\text{O}_3$-$\text{ZrO}_2$ are analyzed using a computer simulation based on Finite Element Method (FEM). These aspects include: (i) an estimation of the residual stress in the second phase, arising during post fabrication cooling, which affects the critical stress for transformation, (ii) the constitutive behavior of the material during the dilatational transformation of $\text{ZrO}_2$ and (iii) the crack deflection due to the transformation. This simulation study was conducted for angular as well as spherical shapes of second phase particles and also for varying volume fractions of the second phase, using a master finite element mesh. Apart from this numerical experiment, analytical expressions were derived for the residual stress and the constitutive behavior, assuming a spherical shape for the second phase particles. The analysis of the constitutive behavior mainly consists of an estimation of the composite modulus and of the irreversible strain due to the transformation. The comparison of the analytical solutions with the results obtained through the simulation shows a very good agreement. Using the simulation of crack deflection, the increase in crack surface area due to the transformation was computed, to approximately estimate the improvement in fracture toughness due to the crack deflection mechanism.

**Fracture Toughness Enhancement Mechanisms in Ceramic Composites:**

The transformation toughening and microcracking have been found to be the key phenomena in enhancing the fracture toughness of ceramic composite materials. The transformation toughening phenomenon is generally seen in ceramic materials which contain tetragonal zirconia phase ($t$-$\text{ZrO}_2$). The tetragonal zirconia particles transform to monoclinic structure under high stress. In the case of crack propagation, the transformation results in a significant amount of irreversible strain around the crack tip, thereby enhancing the fracture toughness. On the other hand, the microcrack toughening enhances the fracture toughness of the ceramic materials by reducing the stress intensity at the crack tip, and this phenomenon is associated with the reduction of the elastic moduli of microcracked material. Also, coupled microcracking and transformation-toughening phenomenon has also been reported, that is, the phase transformation of zirconia particles induces microcracking in the matrix material, thereby resulting in a larger amount of irreversible strain than that of the transformation alone. These deformation mechanisms are not additive and the coupling effect is not well understood.

In this study, a nonlinear constitutive model for the transformation induced plasticity is presented. This nonlinear constitutive model is implemented in a nonlinear finite element method and applied to crack problems. Stationary crack and steady state crack propagation problems are analyzed to estimate the fracture toughness enhancement due to the transformation effect. The constitutive equations derived in this investigation are in the rate (incremental) form, and are ideally suited for implementing in the existing nonlinear finite element codes. It is assumed that the transformation plasticity is dilatationally nonlinear and distortionally linear, and exhibits dilatational strain softening. Dilatational irreversible strain, for the coupled microcracking-transformation case, as a function of volume fraction of transformed zirconia is also derived. With this investigation, a better insight into the mechanisms of fracture toughness enhancement in certain ceramic materials is found.
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1. Finite Element Analysis of Static and Dynamic Fracture of Brittle Micro-cracking Solids: Part 1: Formulation & Numerical Examples; International Journal of Plasticity (accepted for publication); (By Y. Toi and S.N. Atluri)


8) SCIENTIFIC PERSONNEL SUPPORTED BY THIS PROJECT AND DEGREES AWARDED DURING THIS REPORTING PERIOD:

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BRIEF OUTLINE OF RESEARCH FINDINGS

1) Contact with Army Laboratory Personnell:

Dr. R. Ahmad of ARO, and Dr. Tony Chou of Army Materials Technology Labs, visited Georgia Tech in February 1989. A presentation was made by S.N. Atluri.

2) Brief outline of Research:

The continuum constitutive modeling for rate dependent fracture of brittle microcracking solids has been pursued. A rate-type constitutive equation that takes into account the rate effect on microcracking has been proposed. Its computational implementation via a finite element method has been undertaken. A computational method for the analysis of stationary as well as dynamically propagating macrocracks has been formulated. The effect on microcracking surrounding a macrocrack is being studied through as analysis of the behavior of the general crack-tip energy-release-rate parameter, the $T^*$ integral.