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THE OBJECTIVE OF THIS CMP IS TO: VERIFY AND EVALUATE POTENTIAL AIR QUALITY HEALTH HAZARDS, TO VERIFY PROGRESS THAT HAS BEEN MADE TO DATE IN REMOVING CONTAMINANTS RESULTING FROM PREVIOUS ACTIVITIES, TO PROVIDE BASELINE DATA FOR THE EVALUATION OF PROGRESS THAT WILL BE MADE IN FUTURE REMEDIAL ACTIVITIES, TO DEVELOP REAL-TIME GUIDELINES, STANDARD PROCEDURES AND DATA COLLECTION METHODS, AS APPROPRIATE, TO INDICATE IMPACTS OF ONGOING REMEDIAL ACTIONS, AND TO VALIDATE AND DOCUMENT DATABASE RELIABILITY.

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APPENDIX A

TOTAL SUSPENDED PARTICULATES (TSP) DATA
A1 Summary
A2 Listing
A1 Summary
(on diskette file APPA1.TXT)
A2 Listing
(on diskette file APPA2.TXT)
APPENDIX B

RESPIRABLE PARTICULATES OF LESS THAN
10 MICRONS (PM-10) DATA

B1  Summary
B2  Listing
BI Summary
(on diskette file APPB1.TXT)
B2  Listing
(on diskette file APPB2.TXT)
APPENDIX C

ARSENIC, METALS AND MERCURY DATA
(Use data have not been finalized by RMA)

Cl  Listing
C1 Listing
(on diskette file APPC1.TXT)
APPENDIX D

ASBESTOS DATA
D1 Listing
DI Listing
(on diskette file APPD.TXT)
APPENDIX E

VOLATILE ORGANIC COMPOUNDS (VOC) DATA
(These data have not been finalized by PMRMA)
E1    Listing
E1 Listing
(on diskette file APPE.TXT)
APPENDIX F

SEMI-VOLATILE ORGANIC COMPOUNDS (SVOC) DATA
(These data have not been finalized by PMRMA)

F1 Listing
Listing
(on diskette file APPF.TXT)
APPENDIX G

ORGANOCHLORINE PESTICIDES (OCP) DATA
(These data have not been finalized by PMRMA)

G1 Listing
G1 Listing
(on diskette file APPG.TXT)
APPENDIX H

QUALITY ASSURANCE/QUALITY CONTROL

H1  Precision Calculation
H2  Daily Zero and Span Data for
    Continuous Gaseous Monitors
H3  Audit Results
HI Precision Calculation
OZONE PRECISION CALCULATIONS
CMP - FY90

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AVERAGE % DIFFERENCE: 3.36
STANDARD DEVIATION: 2.70

UPPER 95% PROBABILITY LIMIT: 8.5
LOWER 95% PROBABILITY LIMIT: -1.92
### CARBON MONOXIDE PRECISION CALCULATIONS

**CMP - FY90**

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**AVERAGE % DIFFERENCE** -5.38

**STANDARD DEVIATION** 1.98

**UPPER 95% PROBABILITY LIMIT** -1.50

**LOWER 95% PROBABILITY LIMIT** -9.25
# Sulfur Dioxide Precision Calculations

**CMP - FY' 0**

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- Average % Difference: 3.61
- Standard Deviation: 6.73
- Upper 95% Probability Limit: 9.50
- Lower 95% Probability Limit: -16.80
### NITROGEN OXIDES PRECISION CALCULATIONS

CMP - FY90

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**AVERAGE % DIFFERENCE**  
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**STANDARD DEVIATION**  
7.37

**UPPER 95% PROBABILITY LIMIT**  
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**LOWER 95% PROBABILITY LIMIT**  
-19.58
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Lower 95% Prob. Limit: -10.16

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**Average % Difference**: -3.53

**Standard Deviation**: 15.01

**Upper 95% Prob. Limit**: 10.31

**Lower 95% Prob. Limit**: -23.51

**Number of Precision Checks**: 56

**Number of Paired Samples Less Than 20 ug/m³**: 36
## Metals and Arsenic Precision Calculations

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## METALS AND ARSENIC PRECISION CALCULATIONS (CONTINUED)

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**Average % Difference:** -10.30  35.79  0.47  9.53  21.89

**Standard Deviation:** 19.02

**Upper 95% Prob. Limit:** 26.69

**Lower 95% Prob. Limit:** -26.03

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1 Number of paired samples is 21.
Number of samples above the LCRL = 0.
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(in fibers/mL)

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*Number of tested samples is 18.
Number of samples above LCRL = 0.*
### VOC Precision Calculations for FY90

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-40.26  LT CRL  LT CRL  8.93  LT CRL  39.80  -6.61  -61.05  -0.21  LT CRL  LT CRL  LT CRL
49.94  LT CRL  LT CRL  LT CRL  LT CRL  LT CRL  70.32  7.94  -71.03  LT CRL  LT CRL  LT CRL
11.84  LT CRL  LT CRL  LT CRL  LT CRL  LT CRL  -20.49  29.86  -30.73  -55.93  LT CRL  LT CRL  LT CRL
21.94  LT CRL  LT CRL  LT CRL  LT CRL  LT CRL  39.73  -0.28  -0.28  -57.40  LT CRL  LT CRL  LT CRL
-0.35  LT CRL  LT CRL  LT CRL  LT CRL  LT CRL  -28.91  -0.35  100.26  10.11  LT CRL  LT CRL  LT CRL

### Average 2 Difference

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**Analysis of all values including greater than**

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#### Percent Differences

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| LT CRL | LT CRL | 0.68 | 0.68 | LT CRL | LT CRL | 0.68 | LT CRL | 29.24 |
| LT CRL | LT CRL | 0.68 | 0.68 | LT CRL | LT CRL | 0.68 | LT CRL | 29.24 |
| LT CRL | LT CRL | 87.20 | 67.21 | LT CRL | LT CRL | 0.61 | LT CRL | 29.17 | LT CRL | 0.61 |
| LT CRL | LT CRL | 0.21 | 0.21 | LT CRL | LT CRL | 0.21 | LT CRL | 18.39 |
| LT CRL | LT CRL | 0.21 | 0.21 | LT CRL | LT CRL | 0.21 | LT CRL | 18.39 |
| LT CRL | LT CRL | -39.87 | -108.93 | LT CRL | LT CRL | 0.14 | LT CRL | -36.5 | -36.5 |
| LT CRL | LT CRL | 1.25 | 45.40 | LT CRL | LT CRL | 52.90 | LT CRL | -4.90 | LT CRL | -4.90 |
| LT CRL | LT CRL | 44.62 | 38.75 | LT CRL | LT CRL | 67.83 | LT CRL | -30.75 | LT CRL | -29.67 |
| LT CRL | LT CRL | 89.44 | 99.79 | LT CRL | LT CRL | 79.76 | LT CRL | 6.46 | LT CRL | 6.46 |
| LT CRL | LT CRL | 85.44 | 60.35 | LT CRL | LT CRL | 130.38 | LT CRL | 66.35 | 7.49 | 102.77 |

#### Average 2 Difference

| 21.75 | -2.98 | 11.36 | -3.79 | 13.25 | -22.39 | 25.74 |

#### Number of Paired Samples

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AVERAGE 2 DIFFERENCE: 11.40

NUMBER OF PAIRED SAMPLES: 3
### VOC Precision Calculations for FY90 (Continued)

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|       | 17-Dec-90| A05  | 24577 | LT CRL | LT CRL | GT CRL | GT CRL | LT CRL | GT CRL | LT CRL | GT CRL | 0.316 | GT CRL |
|       | 16-Mar-90| A05  | 24619 | LT CRL | LT CRL | GT CRL | GT CRL | LT CRL | GT CRL | LT CRL | GT CRL | 0.316 | GT CRL |
|       | 21-May-90| A05  | 24657 | LT CRL | LT CRL | GT CRL | GT CRL | LT CRL | LT CRL | GT CRL | LT CRL | 0.316 | GT CRL |
|       | 27-Jun-90| A05  | 24678 | LT CRL | LT CRL | GT CRL | GT CRL | 0.376 | LT CRL | GT CRL | LT CRL | 0.316 | GT CRL |
|       | 28-Jun-90| A05  | 24684 | LT CRL | LT CRL | GT CRL | GT CRL | 0.412 | LT CRL | GT CRL | LT CRL | 0.316 | GT CRL |
|       | 18-Jul-90| A05  | 24694 | LT CRL | LT CRL | 0.307 | GT CRL | 0.107 | LT CRL | 0.425 | LT CRL | 0.594 | LT CRL | GT CRL |
|       | 27-Jul-90| A05  | 24715 | LT CRL | LT CRL | 0.437 | GT CRL | LT CRL | 0.567 | LT CRL | 0.486 | LT CRL | GT CRL |
|       | 02-Aug-90| A05  | 24726 | LT CRL | LT CRL | 0.572 | GT CRL | LT CRL | LT CRL | GT CRL | LT CRL | 0.109 | GT CRL |
|       | 09-Aug-90| A05  | 24735 | LT CRL | LT CRL | 0.680 | GT CRL | LT CRL | 0.204 | LT CRL | 0.210 | CTRL | 0.156 | 0.707 |
|       | 11-Sep-90| A010 | 24743 | LT CRL | LT CRL | 0.180 | GT CRL | 0.204 | LT CRL | 0.210 | LT CRL | 0.156 | 0.707 |

### Percent Differences

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**Note:** The data includes various precision calculations for different dates and sites, with specific values for each calculation.
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**PERCENT DIFFERENCES**

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**AVE. % DIFFERENCE** 3.95 -20.68
H2 Daily Zero and Span Data for Continuous Gaseous Monitors
Daily Ozone Zero Values for FY90
Daily Carbon Monoxide Zero Values for FY90
Daily Sulfur Dioxide Zero Values for FY90

Zero Value Conc. in PPM

Day of Year

OCT  NOV  DEC  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP
Daily Nitric Oxide Zero Values for FY90

Zero Value Conc. in PPM

OCT  NOV  DEC  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP
Day of Year
Daily Nitrogen Oxides Zero Values for FY90
Daily Nitrogen Dioxide Zero Values for FY90

Zero Value Conc. in PPM

OCT  NOV  DIC  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP

Day of Year
Daily Ozone Spans for FY90

90% of Full Scale Line

70% of Full Scale Line

Span Value Conc. in PPM

0.6
0.4
0.2
0

OCT NOV DEC JAN FEB MAR APR MAY JUN JUL AUG SEP
Day of Year
Daily Carbon Monoxide Spans for FY90

Span Value Conc. in PPM

90% of Full Scale Line

70% of Full Scale Line

OCT NOV DEC JAN FEB MAR APR MAY JUN JUL AUG SEP
Day of Year
Daily Sulfur Dioxide Spans for FY90

Span Value Conc. in PPM

90% of Full Scale Line

70% of Full Scale Line

Day of Year

OCT  NOV  DEC  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP
Daily Nitric Oxide Spans for FY90

Span Value Conc. in PPM

OCT  NOV  DEC  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP

Day of Year
Daily Nitrogen Dioxide Spans for FY90

Span Value Concentration in PPM

0.6

0.5

0.4

0.3

0.2

0.1

0.0

0

70% of Full Scale Line

90% of Full Scale Line

OCT NOV DEC JAN FEB MAR APR MAY JUN JUL AUG SEP

Day of Year
Daily Nitrogen Oxides Spans for FY90

- 50% of Full Scale Line
- 70% of Full Scale Line

Span Value Conc. in PPM

Day of Year

OCT  NOV  DEC  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP
Audit Results
Summary Tables from
First Quarter 1990 Audit Report
### TABLE 4.1-1  (Sheet 1 of 2)
**HIGH VOLUME SAMPLERS**
**TSP - PM$_{10}$ - PUF**
**AUDIT SUMMARY**

#### TSP SAMPLERS

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<th>Operator Determined Flow (SCFM)</th>
<th>Percent Difference</th>
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### TABLE 4.1-1 (Sheet 2 of 2)
**HIGH VOLUME SAMPLERS**
**TSP - PM$_{10}$ - PUF**
**AUDIT SUMMARY**

#### PM$_{10}$-SAMPLERS

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SAMPLE PUMPS
ASBESTOS - VOC - MERCURY
AUDIT SUMMARY

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### Table 4.3-1 (Sheet 1 of 2)
Meteorological System Audit Results Summary

#### Wind Speed (MPH)

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#### Linearly Check

- Oriented to True North
- Starting Torque g.cm

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<th>Response</th>
<th>Difference</th>
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<td>Yes</td>
<td>4.6</td>
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<td>MET 3</td>
<td>+2</td>
<td>Yes</td>
<td>4.5</td>
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#### Temperature (°C)

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<tr>
<th>Site</th>
<th>Low Point</th>
<th>Audit</th>
<th>Response</th>
<th>Difference</th>
<th>Mid Point</th>
<th>Audit</th>
<th>Response</th>
<th>Difference</th>
<th>High Point</th>
<th>Audit</th>
<th>Response</th>
<th>Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>MET 1 (2M)</td>
<td>0.5</td>
<td>0.5</td>
<td>0.0</td>
<td>20.7</td>
<td>20.9</td>
<td>+0.2</td>
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<td>31.0</td>
<td>+0.1</td>
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<tr>
<td>MET 3</td>
<td>0.1</td>
<td>-0.1</td>
<td>-0.2</td>
<td>20.6</td>
<td>20.7</td>
<td>+0.1</td>
<td>31.0</td>
<td>31.0</td>
<td>0.0</td>
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<td></td>
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<tr>
<td>MET 1 (10M)</td>
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<td>0.2</td>
<td>0.0</td>
<td>20.7</td>
<td>20.9</td>
<td>+0.2</td>
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#### Relative Humidity

<table>
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<th>Response</th>
<th>Dew Point</th>
<th>Difference</th>
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</thead>
<tbody>
<tr>
<td></td>
<td>RH</td>
<td>Dev Point</td>
<td>RH</td>
<td>Dew Point</td>
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0040
<table>
<thead>
<tr>
<th>SOLAR RADIATION (LAMPS)</th>
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<table>
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<tr>
<th>RAIN FALL (H2O)</th>
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</thead>
<tbody>
<tr>
<td>Audit Value</td>
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<tr>
<td>Site</td>
</tr>
<tr>
<td>MET 1</td>
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<tr>
<td>MET 3</td>
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</table>

(1) MLN = [(RPM/3RPM/H2)/ 6.95] + 0.5.

(2) Acceptable W/S starting Torque =0.2g.cm.

(3) Water was left in bucket after final tip, indicating a response between 0.12 and 0.13.
# TABLE 4.1-1

**HIGH VOLUME SAMPLERS**

TSP - PM<sub>10</sub> - PUF

**AUDIT SUMMARY**

<table>
<thead>
<tr>
<th>Site</th>
<th>Audit Flow (SCFM)</th>
<th>Operator Determined Flow (SCFM)</th>
<th>Percent Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>1A</td>
<td>39.9</td>
<td>40.3</td>
<td>+1.0</td>
</tr>
<tr>
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<td>41.7</td>
<td>40.2</td>
<td>-3.6</td>
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<tr>
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<td>40.9</td>
<td>40.2</td>
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<td>40.1</td>
<td>+0.9</td>
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<td>39.2</td>
<td>40.3</td>
<td>+2.9</td>
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<tr>
<td>5B</td>
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<td>40.4</td>
<td>0.0</td>
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<td>40.6</td>
<td>40.0</td>
<td>-1.4</td>
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<td>39.7</td>
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<td>+0.9</td>
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<tr>
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<td>40.1</td>
<td>40.2</td>
<td>+0.3</td>
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<td>40.7</td>
<td>40.1</td>
<td>-1.5</td>
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<tr>
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<td>0.0</td>
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<td>39.9</td>
<td>40.0</td>
<td>+0.4</td>
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<td>40.0</td>
<td>+0.8</td>
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<td>M2A</td>
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<td>M3A</td>
<td>39.8</td>
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<tr>
<td>M4A</td>
<td>39.1</td>
<td>39.9</td>
<td>+2.1</td>
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### TABLE 4.1-1 (Sheet 2 of 2)
**HIGH VOLUME SAMPLERS**
**TSP - PM$_{10}$ - PUF**
**AUDIT SUMMARY**

#### PM$_{10}$ SAMPLERS

<table>
<thead>
<tr>
<th>Site</th>
<th>Audit Flow (SCFM)</th>
<th>Operator Determined Flow (SCFM)</th>
<th>Percent Difference</th>
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</thead>
<tbody>
<tr>
<td>1A</td>
<td>34.6</td>
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<tr>
<td>2B</td>
<td>35.4</td>
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<td>-1.2</td>
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<td>3B</td>
<td>35.1</td>
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<td>0.0</td>
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<td>5C</td>
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<td>-0.5</td>
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<tr>
<td>5D</td>
<td>35.0</td>
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<td>-1.6</td>
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<tr>
<td>9B</td>
<td>34.9</td>
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<td>+1.0</td>
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#### PUF SAMPLERS

<table>
<thead>
<tr>
<th>Site</th>
<th>Audit Flow (SLM)</th>
<th>Operator Determined Flow (SLM)</th>
<th>Percent Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>1C</td>
<td>200.8</td>
<td>207.6</td>
<td>+3.4</td>
</tr>
<tr>
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<td>201.0</td>
<td>212.6</td>
<td>+6.0</td>
</tr>
<tr>
<td>3C</td>
<td>185.8</td>
<td>193.1</td>
<td>+3.9</td>
</tr>
<tr>
<td>5P</td>
<td>203.6</td>
<td>207.5</td>
<td>+2.2</td>
</tr>
<tr>
<td>5G</td>
<td>187.5</td>
<td>179.5</td>
<td>-4.3</td>
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<tr>
<td>M1C</td>
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<td>199.7</td>
<td>+3.1</td>
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<tr>
<td>M2C</td>
<td>206.0</td>
<td>207.4</td>
<td>+0.5</td>
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<tr>
<td>M3C</td>
<td>200.0</td>
<td>202.2</td>
<td>+0.8</td>
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<tr>
<td>M4C</td>
<td>203.0</td>
<td>207.3</td>
<td>+1.9</td>
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TABLE 4.2-1
SAMPLE PUMPS
ASBESTOS - VOC - MERCURY
AUDIT SUMMARY

<table>
<thead>
<tr>
<th>Instrument/ID</th>
<th>Audit Flow (SCCM)</th>
<th>Operator Flow (SCCM)</th>
<th>Percent Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Micromax 11199</td>
<td>6753</td>
<td>7000</td>
<td>+3.6</td>
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<td>Micromax 07792</td>
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<td>7000</td>
<td>+4.1</td>
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<td>Micromax 03311</td>
<td>6860</td>
<td>7000</td>
<td>+3.6</td>
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<td>7000</td>
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<td>Micromax 03312</td>
<td>6866</td>
<td>7000</td>
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<td>293</td>
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S/N: 3327
### TABLE 4.3-1 (Sheet 1 of 2)
METEOROLOGICAL SYSTEM AUDIT RESULTS SUMMARY

#### WIND SPEED (MPH)

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<thead>
<tr>
<th>Input</th>
<th>119.8 RPM 6.2 MPH(1)</th>
<th>301.0 RPM 14.9 MPH(1)</th>
<th>601.9 RPM 29.4 MPH(1)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Site</td>
<td>Response (MPH)</td>
<td>Difference (MPH)</td>
<td>Response (MPH)</td>
</tr>
<tr>
<td>MET 2</td>
<td>6.2</td>
<td>0.0</td>
<td>14.7</td>
</tr>
<tr>
<td>MET 4</td>
<td>5.8</td>
<td>0.4</td>
<td>14.6</td>
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</table>

#### WIND DIRECTION (°)

<table>
<thead>
<tr>
<th>Site</th>
<th>North</th>
<th>Difference</th>
<th>East</th>
<th>Difference</th>
<th>South</th>
<th>Difference</th>
<th>West</th>
<th>Difference</th>
<th>Oriented to True North</th>
<th>Starting Torque g.cm</th>
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</thead>
<tbody>
<tr>
<td>MET 2</td>
<td>1</td>
<td>+1</td>
<td>92</td>
<td>+2</td>
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<td>+3</td>
<td>273</td>
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<tr>
<td>MET 4</td>
<td>365</td>
<td>+5</td>
<td>93</td>
<td>+3</td>
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<td>+1</td>
<td>268</td>
<td>-2</td>
<td>Yes</td>
<td>5.6</td>
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</table>

#### TEMPERATURE (°C)

<table>
<thead>
<tr>
<th>Site</th>
<th>Low Point</th>
<th>Mid Point</th>
<th>High Point</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Audit</td>
<td>Response</td>
<td>Difference</td>
</tr>
<tr>
<td>MET 2</td>
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<td>(31.4°F)/-0.1</td>
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</tr>
<tr>
<td>MET 4</td>
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<td>(32.1°F)/-0.1</td>
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</table>

#### BAROMETRIC PRESSURE ("Hg)

<table>
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<tr>
<th>Site</th>
<th>Audit</th>
<th>System</th>
<th>Difference</th>
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<tr>
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0040-3
### SOLAR RADIATION (LANGLEY)

<table>
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### RAIN FALL ("H2O")

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<tr>
<th>Site</th>
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<th>System Response</th>
<th>Rain Equivalent</th>
<th>% Difference</th>
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<tbody>
<tr>
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<td>.12</td>
<td>.12</td>
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<tr>
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<td>.22</td>
<td>.23</td>
<td>.23</td>
<td>4.5</td>
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</table>

(1) MPH = [(RPM/3950) / 6.95] + 0.5.
(2) Acceptable W/S starting Torque <0.2g.cm.
Summary Tables from
Third Quarter 1990 Audit Report
### TABLE 4.1-1 (Sheet of 2)

HIGH VOLUME SAMPLERS  
TSP - PM$_{10}$ - PUF  
AUDIT SUMMARY

#### TSP SAMPLERS

<table>
<thead>
<tr>
<th>Site</th>
<th>Audit Flow (SCFM)</th>
<th>Operator Determined Flow (SCFM)</th>
<th>Percent Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>1A</td>
<td>40.7</td>
<td>40.1</td>
<td>-1.5</td>
</tr>
<tr>
<td>2A</td>
<td>40.5</td>
<td>40.0</td>
<td>-1.2</td>
</tr>
<tr>
<td>3A</td>
<td>42.4</td>
<td>40.1</td>
<td>-5.3</td>
</tr>
<tr>
<td>4A</td>
<td>39.7</td>
<td>39.9</td>
<td>+0.6</td>
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<td>5A</td>
<td>40.7</td>
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<td>+1.5</td>
</tr>
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<td>5B</td>
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<td>39.6</td>
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<td>+1.2</td>
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<tr>
<td>7A</td>
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<td>39.9</td>
<td>-7.1</td>
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<tr>
<td>8A</td>
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<td>-6.5</td>
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<td>+1.8</td>
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<td>-2.3</td>
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<td>+0.3</td>
</tr>
<tr>
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<td>40.1</td>
<td>+0.7</td>
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<tr>
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<tr>
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TABLE 4.1-1 (Sheet 2 of 2)

HIGH VOLUME SAMPLERS
TSP - \( \text{PM}_{10} \) - PUF

AUDIT SUMMARY

<table>
<thead>
<tr>
<th>PM(_{10}) SAMPLERS</th>
<th>Operator Determined Flow (SCFM)</th>
<th>Site</th>
<th>Audit Flow (SCFM)</th>
<th>Percent Difference</th>
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<tbody>
<tr>
<td>1B</td>
<td>33.5</td>
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<tr>
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<td>33.4</td>
<td>+0.7</td>
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</tr>
<tr>
<td>3B</td>
<td>33.3</td>
<td>32.9</td>
<td>-0.6</td>
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<tr>
<td>5C</td>
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<td>34.0</td>
<td>+2.7</td>
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<tr>
<td>5D</td>
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<td>33.8</td>
<td>-0.1</td>
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<tr>
<td>9B</td>
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<td>33.4</td>
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<td>M1B</td>
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<table>
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<th>Site</th>
<th>Audit Flow (SLM)</th>
<th>Percent Difference</th>
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<tr>
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<td>Operator Flow (SCCM)</td>
<td>Percent Difference</td>
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<td>-------------------</td>
<td>----------------------</td>
<td>--------------------</td>
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</tr>
<tr>
<td>Micromax 03311</td>
<td>7110</td>
<td>7000</td>
<td>-1.5</td>
<td></td>
</tr>
<tr>
<td>Micromax 03316</td>
<td>7512</td>
<td>7000</td>
<td>-6.8</td>
<td></td>
</tr>
<tr>
<td>Micromax 03314</td>
<td>6908</td>
<td>7000</td>
<td>+1.3</td>
<td></td>
</tr>
<tr>
<td>Micromax 03312</td>
<td>6918</td>
<td>7000</td>
<td>+1.2</td>
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</tr>
<tr>
<td>Sierra 821-2</td>
<td>289</td>
<td>300</td>
<td>+3.8</td>
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</table>

S/N: 3327
### TABLE 4.3-1 (Sheet 1 of 2)
METEOROLOGICAL SYSTEM AUDIT RESULTS SUMMARY

#### WIND SPEED (MPH)

<table>
<thead>
<tr>
<th>Site</th>
<th>119.93 RPM</th>
<th>300.12 RPM</th>
<th>500.20 RPM</th>
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</thead>
<tbody>
<tr>
<td></td>
<td>Input</td>
<td>6.2 MPH</td>
<td>14.9 MPH</td>
</tr>
<tr>
<td>MET 1</td>
<td>6.1</td>
<td>14.8</td>
<td>29.1</td>
</tr>
<tr>
<td>MET 3</td>
<td>6.2</td>
<td>14.5</td>
<td>29.1</td>
</tr>
</tbody>
</table>

#### WIND DIRECTION (*°)

<table>
<thead>
<tr>
<th>Site</th>
<th>North</th>
<th>East</th>
<th>South</th>
<th>West</th>
<th>Oriented to True North</th>
<th>Starting Torque g-cm</th>
</tr>
</thead>
<tbody>
<tr>
<td>MET 1</td>
<td>0</td>
<td>+1</td>
<td>+2</td>
<td>273</td>
<td>Yes</td>
<td>5.0</td>
</tr>
<tr>
<td>MET 3</td>
<td>2</td>
<td>+3</td>
<td>-1</td>
<td>274</td>
<td>Yes</td>
<td>6.0</td>
</tr>
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</table>

#### TEMPERATURE °C (°F)

<table>
<thead>
<tr>
<th>Site</th>
<th>Low Point</th>
<th>Mid Point</th>
<th>High Point</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Audit</td>
<td>Response</td>
<td>Difference</td>
</tr>
<tr>
<td>MET 1</td>
<td>0.1 (32.2)</td>
<td>0.3 (32.6)</td>
<td>2</td>
</tr>
<tr>
<td>MET 3</td>
<td>0.5 (32.9)</td>
<td>0.6 (33.1)</td>
<td>+0.1</td>
</tr>
<tr>
<td>MET 1</td>
<td>No data</td>
<td>No data</td>
<td>No data</td>
</tr>
<tr>
<td>MET 1</td>
<td>0.2 (32.7)</td>
<td>0.3 (32.5)</td>
<td>+0.1</td>
</tr>
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</table>

#### RELATIVE HUMIDITY

<table>
<thead>
<tr>
<th>Site</th>
<th>Audit</th>
<th>RH</th>
<th>Dew Point</th>
<th>Response</th>
<th>RH</th>
<th>Dew Point</th>
<th>Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>MET 1</td>
<td>51.9</td>
<td>-8.1°C</td>
<td>49.5</td>
<td>-9.2</td>
<td>-1.1°C</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

0040-4
TABLE 4.1-1 (Sheet 2 of 2)
METEOROLOGICAL SYSTEM RESULTS AUDIT SUMMARY

SOLAR RADIATION (KANGELY PER HOUR)

<table>
<thead>
<tr>
<th>Sensor</th>
<th>Covered</th>
<th>System</th>
</tr>
</thead>
<tbody>
<tr>
<td>MET 3</td>
<td>-</td>
<td>0.00</td>
</tr>
</tbody>
</table>

RAIN FALL (*H2O)

<table>
<thead>
<tr>
<th>Site</th>
<th>Volume (cc)</th>
<th>Rain Equivalent</th>
<th>System Response</th>
<th>% Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>MET 1</td>
<td>100</td>
<td>.13</td>
<td>.12</td>
<td>.01 (3)</td>
</tr>
<tr>
<td>MET 3</td>
<td>100</td>
<td>.13</td>
<td>.14</td>
<td>.01</td>
</tr>
</tbody>
</table>

1. MPH = [([RPM/3RPM] / 6.95) + 0.5).
2. Acceptable W/S starting Torque < 0.2 g.cm.
3. Water was left in bucket after final tip indicating a response between 0.12 and 0.13.
Summary Tables from
Fourth Quarter 1990 Audit Report
TABLE 4.1-1 (Sheet 1 of 2)
HIGH VOLUME SAMPLERS
TSP - PM$_{10}$ - PUF
AUDIT SUMMARY

**TSP SAMPLERS**

<table>
<thead>
<tr>
<th>Site</th>
<th>Audit Flow (SCFM)</th>
<th>Operator Determined Flow (SCFM)</th>
<th>Percent Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>1A</td>
<td>41.1</td>
<td>39.3</td>
<td>-4.4</td>
</tr>
<tr>
<td>2A</td>
<td>40.8</td>
<td>39.9</td>
<td>-2.1</td>
</tr>
<tr>
<td>3A</td>
<td>44.0</td>
<td>42.5</td>
<td>-3.5</td>
</tr>
<tr>
<td>4A</td>
<td>43.4</td>
<td>40.3</td>
<td>-7.2</td>
</tr>
<tr>
<td>5A</td>
<td>41.3</td>
<td>40.6</td>
<td>-1.6</td>
</tr>
<tr>
<td>5B</td>
<td>40.2</td>
<td>40.7</td>
<td>+1.3</td>
</tr>
<tr>
<td>6A</td>
<td>41.2</td>
<td>40.8</td>
<td>-0.9</td>
</tr>
<tr>
<td>7A</td>
<td>43.4</td>
<td>41.5</td>
<td>-4.5</td>
</tr>
<tr>
<td>8A</td>
<td>43.0</td>
<td>41.5</td>
<td>-3.4</td>
</tr>
<tr>
<td>9A</td>
<td>41.8</td>
<td>40.0</td>
<td>-4.3</td>
</tr>
<tr>
<td>10A</td>
<td>40.1</td>
<td>38.5</td>
<td>-3.9</td>
</tr>
<tr>
<td>11A</td>
<td>41.3</td>
<td>40.0</td>
<td>-3.2</td>
</tr>
<tr>
<td>12A</td>
<td>41.3</td>
<td>40.7</td>
<td>-1.5</td>
</tr>
<tr>
<td>M1A</td>
<td>38.1</td>
<td>38.4</td>
<td>+0.8</td>
</tr>
<tr>
<td>M2A</td>
<td>40.3</td>
<td>40.3</td>
<td>0.0</td>
</tr>
<tr>
<td>M3A</td>
<td>39.3</td>
<td>39.9</td>
<td>+1.5</td>
</tr>
<tr>
<td>M4A</td>
<td>39.0</td>
<td>39.7</td>
<td>+1.7</td>
</tr>
</tbody>
</table>
# Table 4.1-1 (Sheet 2 of 2)

**High Volume Samplers**

**TSP - PM$_{10}$ - PUF**

## Audit Summary

### PM$_{10}$samplers

<table>
<thead>
<tr>
<th>Site</th>
<th>Audit Flow (SCFM)</th>
<th>Operator Determined Flow (SCFM)</th>
<th>Percent Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>1B</td>
<td>33.4</td>
<td>33.3</td>
<td>-0.2</td>
</tr>
<tr>
<td>2B</td>
<td>34.1</td>
<td>32.8</td>
<td>-3.9</td>
</tr>
<tr>
<td>3B</td>
<td>34.3</td>
<td>33.6</td>
<td>-2.1</td>
</tr>
<tr>
<td>5C</td>
<td>34.4</td>
<td>34.6</td>
<td>+0.6</td>
</tr>
<tr>
<td>5D</td>
<td>34.8</td>
<td>34.5</td>
<td>-0.7</td>
</tr>
<tr>
<td>9B</td>
<td>34.4</td>
<td>34.3</td>
<td>-0.2</td>
</tr>
<tr>
<td>10B</td>
<td>32.9</td>
<td>32.3</td>
<td>-1.8</td>
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</tbody>
</table>

### PUF samplers

<table>
<thead>
<tr>
<th>Site</th>
<th>Audit Flow (SLM)</th>
<th>Operator Determined Flow (SLM)</th>
<th>Percent Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>1C</td>
<td>198</td>
<td>196</td>
<td>-1.0</td>
</tr>
<tr>
<td>2C</td>
<td>184</td>
<td>183</td>
<td>-0.6</td>
</tr>
<tr>
<td>3C</td>
<td>194</td>
<td>199</td>
<td>+2.7</td>
</tr>
<tr>
<td>5E</td>
<td>201</td>
<td>198</td>
<td>-1.5</td>
</tr>
<tr>
<td>5F</td>
<td>191</td>
<td>188</td>
<td>-1.5</td>
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<tr>
<td>5G</td>
<td>180</td>
<td>178</td>
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</tr>
<tr>
<td>M1C</td>
<td>181</td>
<td>215</td>
<td>+18.8</td>
</tr>
<tr>
<td>M2C</td>
<td>187</td>
<td>183</td>
<td>-2.0</td>
</tr>
<tr>
<td>M3C</td>
<td>184</td>
<td>190</td>
<td>+3.2</td>
</tr>
<tr>
<td>M4C</td>
<td>187</td>
<td>187</td>
<td>0.0</td>
</tr>
<tr>
<td>Instrument/ID</td>
<td>Audit Flow (SCCM)</td>
<td>Operator Flow (SCCM)</td>
<td>Percent Difference</td>
</tr>
<tr>
<td>------------------</td>
<td>-------------------</td>
<td>----------------------</td>
<td>--------------------</td>
</tr>
<tr>
<td>Micromax 11199</td>
<td>6295</td>
<td>6800</td>
<td>+8.0</td>
</tr>
<tr>
<td>Micromax 07792</td>
<td>6098</td>
<td>6500</td>
<td>+6.6</td>
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<tr>
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<td>6024</td>
<td>6400</td>
<td>+6.2</td>
</tr>
<tr>
<td>Micromax 03316</td>
<td>6117</td>
<td>6600</td>
<td>+7.9</td>
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<td>Micromax 03314</td>
<td>6367</td>
<td>6700</td>
<td>+5.2</td>
</tr>
<tr>
<td>Micromax 03312</td>
<td>6175</td>
<td>6800</td>
<td>+10.2</td>
</tr>
<tr>
<td>Sierra 821-2</td>
<td>299</td>
<td>302</td>
<td>+1.0</td>
</tr>
<tr>
<td>S/N: 3327</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>
TABLE 4.3-1 (Sheet 1 of 2)
METEOROLOGICAL SYSTEM AUDIT RESULTS SUMMARY

| WIND SPEED (MPH) | 119.9 RPM 6.3 MPH<sup>10</sup> | 300.1 RPM 14.9 MPH<sup>10</sup> | 600.2 RPM 29.3 MPH<sup>10</sup> | Starting 
<table>
<thead>
<tr>
<th>Met 1</th>
<th>Response (MPH)</th>
<th>Difference (MPH)</th>
<th>Response (MPH)</th>
<th>Difference (MPH)</th>
<th>Response (MPH)</th>
<th>Difference (MPH)</th>
<th>Torque g-cm&lt;sup&gt;10&lt;/sup&gt;</th>
</tr>
</thead>
<tbody>
<tr>
<td>MET 1</td>
<td>6.1</td>
<td>-0.2</td>
<td>14.3</td>
<td>-0.1</td>
<td>29.1</td>
<td>-0.2</td>
<td>&lt;0.2</td>
</tr>
<tr>
<td>MET 2</td>
<td>6.1</td>
<td>-0.2</td>
<td>14.7</td>
<td>-0.2</td>
<td>29.2</td>
<td>-0.1</td>
<td>&lt;0.2</td>
</tr>
<tr>
<td>MET 3</td>
<td>6.2</td>
<td>-0.1</td>
<td>14.8</td>
<td>-0.1</td>
<td>29.1</td>
<td>-0.2</td>
<td>&lt;0.2</td>
</tr>
<tr>
<td>MET 4</td>
<td>5.8</td>
<td>-0.3</td>
<td>14.6</td>
<td>-0.3</td>
<td>29.2</td>
<td>-0.1</td>
<td>&lt;0.2</td>
</tr>
</tbody>
</table>

| WIND DIRECTION (*) | Linearly Check | Oriented to True North | Starting 
<table>
<thead>
<tr>
<th>Site</th>
<th>North</th>
<th>East</th>
<th>South</th>
<th>West</th>
<th>True North</th>
<th>Torque g-cm&lt;sup&gt;10&lt;/sup&gt;</th>
</tr>
</thead>
<tbody>
<tr>
<td>MET 1</td>
<td>1</td>
<td>+1</td>
<td>93</td>
<td>+2</td>
<td>273</td>
<td>+3</td>
</tr>
<tr>
<td>MET 2</td>
<td>0</td>
<td>0</td>
<td>91</td>
<td>+1</td>
<td>272</td>
<td>+2</td>
</tr>
<tr>
<td>MET 3</td>
<td>0</td>
<td>0</td>
<td>92</td>
<td>+2</td>
<td>273</td>
<td>+3</td>
</tr>
<tr>
<td>MET 4</td>
<td>367</td>
<td>+7</td>
<td>95</td>
<td>+3</td>
<td>270</td>
<td>0</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>TEMPERATURE °C (°F)</th>
<th>Low Point</th>
<th>Mid Point</th>
<th>High Point</th>
</tr>
</thead>
<tbody>
<tr>
<td>Site</td>
<td>Audit</td>
<td>Response</td>
<td>Difference</td>
</tr>
<tr>
<td>MET 1 (GM)</td>
<td>0.00 (32.0)</td>
<td>0.11 (32.2)</td>
<td>+0.11 (+0.2)</td>
</tr>
<tr>
<td>MET 1 (10M)</td>
<td>N/A</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>MET 1 (10M)</td>
<td>0.10 (32.2)</td>
<td>0.06 (32.1)</td>
<td>-0.04 (-0.1)</td>
</tr>
<tr>
<td>MET 2</td>
<td>0.10 (32.2)</td>
<td>0.00 (32.0)</td>
<td>-0.10 (-0.2)</td>
</tr>
<tr>
<td>MET 3</td>
<td>0.05 (32.1)</td>
<td>0.00 (32.0)</td>
<td>-0.05 (-0.1)</td>
</tr>
<tr>
<td>MET 4</td>
<td>0.10 (32.2)</td>
<td>0.04 (32.1)</td>
<td>-0.06 (-0.1)</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>RELATIVE HUMIDITY</th>
<th>Audit</th>
<th>Dew Point</th>
<th>Response</th>
<th>RH</th>
<th>Dew Point</th>
<th>Difference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Site</td>
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<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>MET 1</td>
<td>88.5</td>
<td>3.1°C (37.6°F)</td>
<td>97.1</td>
<td>4.4°C (40.0°F)</td>
<td>+1.3°C (+2.4°F)</td>
<td></td>
</tr>
</tbody>
</table>

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### Table 4.3-1 (Sheet 2 of 2)

**Meteorological System Audit Results Summary**

<table>
<thead>
<tr>
<th>SOLAR RADIATION (Langley Per Hour)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Site</td>
</tr>
<tr>
<td>----------</td>
</tr>
<tr>
<td>MET 2</td>
</tr>
<tr>
<td>MET 3</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>RAIN FALL (°H₂O)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Site</td>
</tr>
<tr>
<td></td>
</tr>
<tr>
<td>MET 1</td>
</tr>
<tr>
<td>MET 2</td>
</tr>
<tr>
<td>MET 3</td>
</tr>
<tr>
<td>MET 4</td>
</tr>
</tbody>
</table>

\[
\text{MPh} = \frac{[(\text{RPM} / \text{RPM}) / 6.95] + 0.5}{100}
\]

- Acceptable WIS starting Torque <0.2 g.cm.
APPENDIX I

CONTINUOUS AIR QUALITY DATA

11 Carbon Monoxide (CO)
12 Ozone (O₃)
13 Sulfur Dioxide (SO₂)
14 Nitric Oxide (NO)
15 Nitrogen Dioxide (NO₂)
16 Nitrogen Oxides (NOₓ)
Carbon Monoxide (CO)
Carbon Monoxide (CO) Daily Data in parts per million (ppm) for FY90

<table>
<thead>
<tr>
<th>Calendar Month</th>
<th>Julian Day</th>
<th>Daily Max</th>
<th>Daily Min</th>
<th>Daily Mean</th>
<th>Valid Hours</th>
</tr>
</thead>
<tbody>
<tr>
<td>10 1</td>
<td>274</td>
<td>1.000</td>
<td>0.200</td>
<td>0.371</td>
<td>24</td>
</tr>
<tr>
<td>10 2</td>
<td>275</td>
<td>1.200</td>
<td>0.300</td>
<td>0.479</td>
<td>24</td>
</tr>
<tr>
<td>10 3</td>
<td>276</td>
<td>0.600</td>
<td>0.300</td>
<td>0.367</td>
<td>24</td>
</tr>
<tr>
<td>10 4</td>
<td>277</td>
<td>1.000</td>
<td>0.300</td>
<td>0.450</td>
<td>24</td>
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<tr>
<td>10 5</td>
<td>278</td>
<td>0.500</td>
<td>0.200</td>
<td>0.298</td>
<td>24</td>
</tr>
<tr>
<td>10 6</td>
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<td>1.700</td>
<td>0.300</td>
<td>0.662</td>
<td>24</td>
</tr>
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<td>10 7</td>
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<td>1.900</td>
<td>0.300</td>
<td>0.683</td>
<td>24</td>
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<tr>
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<td>0.300</td>
<td>0.596</td>
<td>24</td>
</tr>
<tr>
<td>10 9</td>
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<td></td>
<td></td>
<td></td>
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<tr>
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<td>283</td>
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<td>0.300</td>
<td>0.746</td>
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</tr>
<tr>
<td>10 11</td>
<td>284</td>
<td>3.200</td>
<td>0.300</td>
<td>1.012</td>
<td>24</td>
</tr>
<tr>
<td>10 12</td>
<td>285</td>
<td>1.500</td>
<td>0.300</td>
<td>0.629</td>
<td>24</td>
</tr>
<tr>
<td>10 13</td>
<td>286</td>
<td>1.800</td>
<td>0.300</td>
<td>0.691</td>
<td>24</td>
</tr>
<tr>
<td>10 14</td>
<td>287</td>
<td>0.900</td>
<td>0.300</td>
<td>0.579</td>
<td>24</td>
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<tr>
<td>10 15</td>
<td>288</td>
<td>1.000</td>
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Carbon Monoxide
November 1989

Day of Month

Co2c in PPM

Daily Max

Daily Avg
Carbon Monoxide

December 1989

![Graph showing daily maximum and average concentrations of carbon monoxide over 31 days of December 1989. The graph indicates variations in concentration throughout the month, with notable peaks on the 21st and 23rd of December.]
Carbon Monoxide
January 1990

[Graph showing daily max and daily average concentrations of carbon monoxide over the days of January 1990]
Carbon Monoxide
February 1990

[Graph showing Carbon Monoxide levels over the days of February 1990, with peak values occurring on certain days.

- Daily Max
- Daily Avg]
Carbon Monoxide
March 1990

Day of Month

- Daily Max  - Daily Avg

Conc. in ppm

1 3 5 7 9 11 13 15 17 19 21 23 25 27 29 31
Carbon Monoxide
April 1990

Day of Month

Conc. in ppm

Daily Max  Daily Avg
Carbon Monoxide
May 1990

Day of Month

Conc. in PPM

Daily Max  Daily Avg
Carbon Monoxide
July 1990

Day of Month
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

Conc. in PPM
0 1 2 3 4 5 6 7 8 9

- Daily Max  - Daily Avg

Graph showing daily maximum and average concentrations of carbon monoxide over the days of July 1990.
Carbon Monoxide
August 1990

Day of Month
0 1 3 5 7 9 11 13 15 17 19 21 23 25 27 29 31

Conc. in PPM
0 1 2 3 4 5 6 7 8 9

Daily Max Daily Avg

- -
Carbon Monoxide
September 1990

Day of Month

Conc. in PPM

Daily Max

Daily Avg
12  Ozone (O₃)
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Ozone
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Day of Month

Conc. in FPM

Daily Max

Daily Avg
Ozone
November 1989

Conc. in PPM

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0.1

0.08

0.06

0.04

0.02

0

0 1 3 5 7 9 11 13 15 17 19 21 23 25 27 29
Day of Month

Daily Max  Daily Avg
Ozone

January 1990

Day of Month

Conc. in PPM

- Daily Max  - Daily Avg
Ozone
February 1990

Day of Month
Conc. in PPM

Daily Max  Daily Avg
Ozone
April 1990

Day of Month

0.02 0.04 0.06 0.08 0.1 0.12

Cone. in PPM

Daily Max  Daily Avg
Ozone
May 1990

Day of Month

Daily Max  Daily Avg
Ozone
June 1990

Conc. in PPM

Day of Month

- Daily Max  - Daily Avg
Ozone
July 1990

Day of Month

Daily Max   Daily Avg

Conc. in PPM

0.12
0.1
0.08
0.06
0.04
0.02
0

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Sulfur Dioxide

October 1989

Day of Month

Cone. in PPM

Daily Max  Daily Avg
Sulfur Dioxide
December 1989

Conc. in PPM

Day of Month

Daily Max  Daily Avg
Sulfur Dioxide
January 1990

Conc. in ppm

Day of Month

- Daily Max  - Daily Avg
Sulfur Dioxide
February 1990

Day of Month
-0.01 0 0.01 0.02 0.03 0.04 0.05 0.06

Conc. in ppm

Daily Max  Daily Avg
Sulfur Dioxide
March 1990

Conc. in PPM

-0.01  0  0.01  0.02  0.03  0.04  0.05  0.06

Day of Month

Daily Max  Daily Avg
Sulfur Dioxide
May 1990

Conc. in PPM

Day of Month

- Daily Max  - Daily Avg
Sulfur Dioxide
July 1990

Cone. in PPM

Day of Month

Daily Max  Daily Avg
Sulfur Dioxide
August 1990

![Graph showing sulfur dioxide concentrations over the course of August 1990. The x-axis represents the day of the month, and the y-axis represents concentration in parts per million (PPM). The graph shows daily maximum and average concentrations.]
Sulfur Dioxide
September 1990

- Daily Max  - Daily Avg

Day of Month

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Nitric Oxide
October 1989

Day of Month

Conc. in PPM

- Daily Max
- Daily Avg.
Nitric Oxide
November 1989

![Graph showing daily max and average concentrations of nitric oxide over the days of November 1989. The x-axis represents the day of the month, and the y-axis represents concentration in PPM. The graph shows peaks in concentration on certain days, with a general trend of increasing concentration towards the end of the month.]
Nitric Oxide
January 1990

Day of Month

- Daily Max
- Daily Avg
Nitric Oxide
April 1990

Day of Month

Daily Max  Daily Avg
Nitric Oxide

May 1990

Day of Month

Daily Max  Daily Avg
Nitric Oxide
June 1990

Day of Month

- Daily Max  - Daily Avg

Conc. in PPM

0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
-0.1

1 3 5 7 9 11 13 15 17 19 21 23 25 27 29
Nitric Oxide
July 1990

![Graph showing Nitric Oxide levels for July 1990 with daily max and average measurements.](image)
Nitric Oxide
August 1990

Day of Month

Daily Max  Daily Avg
Nitric Oxide
September 1990

Nitric Oxide
September 1990

Daily Max  Daily Avg
Nitrogen Dioxide (NO₂)
## Nitrogen Dioxide (NO₂) Daily Data in parts per million (ppm) for FY90

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Nitrogen Dioxide
October 1989

![Graph showing Nitrogen Dioxide concentration over October 1989.](Image)
Nitrogen Dioxide
November 1989

Day of Month

- Daily Max  - Daily Avg
Nitrogen Dioxide
December 1989

Conc. in PPM

Day of Month

- Daily Max  - Daily Avg
Nitrogen Dioxide
January 1990

Day of Month

Daily Max

Daily Avg
Nitrogen Dioxide
February 1990

Nitrogen Dioxide

Conc. in PPM

0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
-0.1

Day of Month

1 3 5 7 9 11 13 15 17 19 21 23 25 27

Daily Max

Daily Avg
Nitrogen Dioxide
March 1990

Day of Month

Daily Max
Daily Avg

Conc. in PPM

0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
-0.1
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0 00 0 00 0
Nitrogen Dioxide
April 1990

- Daily Max
- Daily Avg

Day of Month
Nitrogen Dioxide
May 1990

0.7

0.6

0.5

0.4

0.3

0.2

0.1

0

-0.1

Conc. in PPM

Day of Month

Daily Max

Daily Avg
Nitrogen Dioxide
June 1990

Day of Month

Daily Max Dates

Daily Avg Dates

Conc in PPM

0.7

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Nitrogen Dioxide
July 1990

[Graph showing concentrations of Nitrogen Dioxide from Day 1 to Day 31 of July 1990, with daily max and daily average indicated.]
Nitrogen Dioxide
August 1990

Conc. in PPM

Day of Month

Daily Max  Daily Avg
Nitrogen Dioxide

September 1990

[Graph showing concentration of Nitrogen Dioxide (in ppm) for each day of September 1990, with daily max and daily average lines.]
16  Nitrogen Oxides (NO$_x$)
Nitrogen Oxides (NOx) Daily Data in parts per million (ppm) for FY90

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# Nitrogen Oxides (NOx) Daily Data in parts per million (ppm) for FY90

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Nitrogen Oxides
October 1989

![Graph showing daily maximum and average concentrations of nitrogen oxides for October 1989. The x-axis represents the day of the month, and the y-axis represents concentration in PPM. The graph shows fluctuations in concentration throughout the month.](graph.png)
Nitrogen Oxides
November 1989

![Graph showing nitrogen oxide concentrations for November 1989. The x-axis represents the day of the month, and the y-axis represents concentration in PPM.]
Nitrogen Oxides
January 1990

Day of Month

Conc. in PPM

Daily Max

Daily Avg
Nitrogen Oxides
February 1990

[Graph showing concentrations of nitrogen oxides over the days of February 1990]
Nitrogen Oxides
March 1990

Conc. in PPM

Day of Month

Daily Max  Daily Avg
Nitrogen Oxides

April 1990

Daily M  Daily Avg
Nitrogen Oxides
May 1990

- Daily Max
- Daily Avg

Day of Month

Cone. in FPM
-0.1 0.1 0.2 0.3 0.4 0.5 0.6 0.7
1 3 5 7 9 11 13 15 17 19 21 23 25 27 29 31
Nitrogen Oxides
June 1990

Day of Month
- Daily Max  - Daily Avg

Cone. in PPM
Nitrogen Oxides
July 1990

Day of Month

Daily Max

Daily Avg
Nitrogen Oxides
August 1990

- - Daily Max   - - Daily Avg

Day of Month

Cone. in PPM
Nitrogen Oxides
September 1990

Day of Month

Daily Max

Daily Avg
APPENDIX K

ISC AND INPUFF2 EPA MODEL DESCRIPTION

K1  ISC EPA Model Description
K2  INPUFF2
APPENDIX J

METEOROLOGICAL DATA AND
JOINT FREQUENCY DISTRIBUTION

J1  Meteorological Data
J2  Joint Frequency Distribution
J1 Meteorological Data
(on diskette file APJ1.TXT; archived with PKZIP)
Joint Frequency Distribution
(on diskette file APPJ2.TXT)
APPENDIX K

ISC AND INPUFF2 EPA MODEL DESCRIPTION

K.1 ISC EPA Model Description
K.2 INPUFF2
K 1  ISC EPA Model Description
ISC AND INPUTF2 EPA MODEL DESCRIPTIONS

Description of Industrial Source Complex Model (ISC)


Availability: This model is available as part of UNAMAP (Version 6). The computer code is available on magnetic tape from:

Computer Products
National Technical Information Service
U.S. Department of Commerce
Springfield, Virginia 22161

Phone (703) 487-4650

Abstract: The ISC model is a steady-state Gaussian plume model which can be used to assess pollutant concentrations from a wide variety of sources associated with an industrial source complex. This model can account for settling and dry deposition of particulates, downwash area, line and volume sources, plume rise as a function of downwind distance, separation of point sources, and limited terrain adjustment. It operates in both long- and short-term modes.

a. Recommendations for Regulatory Use

ISC is appropriate for the following applications:

- industrial source complexes;
- rural or urban areas;
- flat or rolling terrain;
- transport distances less than 50 kilometers; and
- one hour to annual averaging times.

The following options should be selected for regulatory applications:

- For short term modeling, set the regulatory "default option" (ISW(28)=1), which automatically selects stack tip downwash, final plume rise, buoyancy induced dispersion (BID), the vertical potential temperature gradient, a treatment for calms,
the appropriate wind profile exponents, and the appropriate value for pollutant half-life; set rural option (ISW(20)=0) or urban option (ISW(20)=3); and set the concentration option (ISW(1)=1).

- For long term modeling, set the regulatory "default option" (ISW(22)=0), which automatically selects stack tip downwash, final plume rise, buoyancy-induced dispersion (BID), the vertical potential temperature gradient, the appropriate wind profile exponents, and the appropriate pollutant value for half-life; set rural option (ISW(9)=3) or urban option (ISW(9)=4); and set the concentration option (ISW(1)=1).

b. **Input Requirements**

Source data: location, emission rate, physical stack height, stack gas exit velocity, stack inside diameter, and stack gas temperature. Optional inputs include source elevation, building dimensions, particle size distribution with corresponding settling velocities, and surface reflection coefficients.

Meteorological data: ISCST requires hourly surface weather data from the preprocessor program RAMMET, which provides hourly stability class, wind direction, wind speed, temperature, and mixing height. For ISCLT, input includes stability wind rose (STAR deck), average afternoon mixing height, average morning mixing height, and average air temperature.

Receptor data: coordinates and optional ground elevation for each receptor.

c. **Output**

Printed output options include:

- program control parameters, source data and receptor data;

- tables of hourly meteorological data for each specified day;

- "N"-day average concentration or total deposition calculated at each receptor for any desired combinations of sources;

K = 2
concentration or deposition values calculated for any desired combinations of sources at all receptors for any specified day or time period within the day;

tables of highest and second-highest concentration or deposition values calculated at each receptor for each receptor for each specified time period during an "N"-day period for any desired combinations of sources; and

tables of the maximum 50 concentration or deposition values; calculated for any desired combinations of sources for each specified time period.

d. **Type of Model**

ISC is a Gaussian plume model.

e. **Pollutant Types**

ISC may be used to model primary pollutants. Settling and deposition are treated.

f. **Source-Receptor Relationships**

ISC applies user-specified locations for point, line, area and volume sources, and user-specified receptor locations or receptor rings. Receptors are assumed to be at ground level, and must be at elevations not exceeding stack height.

Actual separation between source-receptor pair is used.

g. **Plume Behavior**


Stack tip downwash equation from Briggs (1974) and building downwash (Huber and Snyder, 1976) are used.

For rolling terrain (terrain not above stack height), plume centerline is horizontal at height of final rise above source.

Fumigation is not treated.

K - 3
h. **Horizontal Winds**

Constant, uniform (steady-state) wind is assumed for each hour.

Straight line plume transport is assumed to all downwind distances.

Separate wind speed profile exponents (EPA, 1980) for both rural and urban cases are used.

An optional treatment for calm winds is included for short term modeling.

i. **Vertical Wind Speed**

Vertical wind speed is assumed equal to zero.

j. **Horizontal Dispersion**

Rural dispersion coefficients from Turner (1969) are used, with no adjustments for surface roughness or averaging time.

Urban dispersion coefficients from Briggs (Gifford, 1976) are used.

Buoyancy induced dispersion (Pasquill, 1976) is included.

Six stability classes are used.

k. **Vertical Dispersion**

Rural dispersion coefficients from Turner (1969) are used, with no adjustments for surface roughness.

Urban dispersion coefficients from Briggs (Gifford, 1976) are used.

Buoyancy induced dispersion (Pasquill, 1976) is included.

Six stability classes are used.
Mixing height is accounted for with multiple reflections until the vertical plume standard deviation equals 1.6 times the mixing height; uniform vertical mixing is assumed beyond that point.

Perfect reflection is assumed at the ground.

Chemical Transformation

Chemical transformations are treated using exponential decay. Time constant is input by the user.

Physical Removal

Settling and dry deposition of particulates are treated.

Evaluation Studies


Scire, J. S., and L. L. Schulman, 1981 Evaluation of the BLP and ISC Models with SF6 Tracer Data and SO2 Measurements at Aluminum Reduction Plants. Air Pollution Control Association Specialty Conference on Dispersion Modeling for Complex Sources, St. Louis, MO.
K2 INPUFF2
INTRODUCTION

INPUFF is a Gaussian integrated puff model with a wide range of applications. The implied modeling scale is capable of addressing the accidental release of a substance over several minutes, or of modeling the more typical continuous plume from a stack. [A requirement for] assistance in modeling the air quality downwind of incineration ships prompted the development of an integrated puff model. INPUFF is, therefore, capable of simulating moving point sources as well as stationary sources.

Computations in INPUFF can be made for multiple point sources at up to 100 receptor locations. In practice, however, the number of receptor locations should be kept to a minimum to avoid excessive run time. INPUFF is primarily designed to model a single event during which one meteorological transition period may occur, such as, going from afternoon to evening conditions. Up to 144 separate meteorological periods of the same length may be used to characterize the meteorology during the event; this provides a time resolution that ranges from minutes to an hour. The user has the option of specifying the wind field for each meteorological period at up to 100 grid locations or allowing the model to default to a homogeneous wind field.

Three dispersion algorithms are used within INPUFF for dispersion downwind of the source. The user may select the Pasquill-Gifford (P-G) scheme (Turner, 1970) or the on-site scheme (Irwin, 1983) for short travel time dispersion. The on-site scheme, so named because it requires specification of the variances of the vertical and lateral wind direction, is a synthesis of work performed by Draxler (1976) and Cramer (1976). The long travel time scheme is the third dispersion algorithm in which the growth of the puff becomes proportional to the square root of time. Optionally, the user can incorporate his own subroutine for estimating atmospheric dispersion.

INPUFF utilizes the deposition algorithms given by Rao (1982). In the limit when pollutant settling and dry deposition velocities are zero, these expressions reduce to the Gaussian diffusion algorithms.

Description of INPUFF2.0

FEATURES AND LIMITATIONS

The model possesses the following features which increase its flexibility and range of application:

- Optional stack-tip downwash,
- Wind speed extrapolated to release height,
- Temporally variable source characteristics,
- Temporally and spatially variable wind field,
- Up to 100 receptors,
- Some consideration of terrain effects through the wind field,
- Optional buoyancy induced dispersion,
- Optional deposition and settling,
- Optional user-supplied dispersion parameters,
- Optional user-supplied plume rise, and
- Optional graphics display.

The implied modeling scale is from tens of meters to tens of kilometers. INPUFF is capable of addressing the accidental release of a substance over a short time period, or of modeling the more typical continuous plume from a stack.

Although INPUFF has several advantages over its continuous plume counterparts, it still retains several limitations, including:

- Wind direction constant with height,
- No consideration of chemical reactions,
- No explicit treatment of complex terrain,
- No consideration of building wake or cavity effects.

BASIS FOR INPUFF

GAUSSIAN PUFF METHIODOLOGY

A graphical representation of the INPUFF model is given in Figure 1. Here the first puff (the puff with the longest trajectory) was first exposed to east-southeast winds, followed by slightly
Figure 1. Gaussian puff model.
stronger winds from the south and the south-southeast. The second puff was released at the time the winds shifted from east-southeast to south. The third puff was released when winds were from the south-southeast. The stability conditions need not be equal for the various time steps, though in the figure, stability is shown to be fairly constant with time (i.e., the rate of puff growth is constant over the time frame). INPUFF assumes $\sigma_x = \sigma_y$, thus puffs remain circular throughout their lifetime. Puffs A, B, and C represent the location of the three emitted puffs at time $t_3$.

In Gaussian-puff algorithms, source emissions are treated as a series of puffs emitted into the atmosphere. Constant conditions of wind and atmospheric stability are assumed during a time interval. The diffusion parameters are functions of travel time. During each time step, the puff centers are determined by the trajectory and the in-puff distributions are assumed to be Gaussian, thus, each puff has a center and a volume which are determined separately by the mean wind, atmospheric stability, and travel time. [An example of a PUFF Model 15-minute time-step interval used in the RMA Basin I remedial operations is shown in Figure 2.]

PLUME RISE

Plume rise is calculated using the methods of Briggs (see Section 5). Although plume rise from point sources is usually dominated by buoyancy, plume rise due to momentum is also considered. Building downwash, and gradual plume rise are not treated by INPUFF.

Stack-tip downwash (optional) can be considered using the methods of Briggs. In such an analysis, a height increment is deducted from the physical stack height before momentum or buoyancy rise is determined. Use of this option primarily affects computations from stacks having small ratios of exit velocity to wind speed.

DISPERSION ALGORITHMS

Three dispersion algorithms are used within INPUFF for dispersion downwind of the source:

- P-G scheme as discussed by Turner (1970),
- On-site scheme formulated by Irwin (1983), and
- Long travel time scheme.

The user has the option of choosing either the P-G or the on-site algorithm (for short travel time dispersion) and specifying when the long travel time dispersion parameters are to be implemented. Optionally, a user-supplied subroutine to estimate dispersion can be used.
Dispersion downwind of a source, as characterized by the P-G scheme, is a function of stability class and downwind distance. Stability categories are commonly specified in terms of wind speed and solar radiation. The on-site dispersion algorithm is a synthesis of Draxler's (1976) and Cramer's (1976) ideas and requires specification of the variances of the vertical and lateral wind directions. The third dispersion scheme is used in conjunction with the other two and is for long travel times in which the growth of the puff is proportional to the square root of time.

SETTLING AND DRY DEPOSITION

Rao (1982) gave analytical solutions of a gradient-transfer model for dry deposition of pollutants from a plume. His solutions treat gravitational settling and dry deposition of pollutants in a physically realistic manner, and are subject to the same basic assumptions and limitations associated with Gaussian plume models. His equations for deposition and settling were incorporated in several EPA air quality models including PAL-DS (Rao and Snodgrass, 1982). The equations used in INPUFF are the same as those used in PAL-DS except they are cast in terms of travel time instead of wind speed and downwind distance.

DATA-REQUIRED CHECKLIST

INPUFF requires data on user options, grid dimensions, sources, meteorology, receptors, and plotter control. The user must indicate whether the following options are to be employed:

- Stack-tip downwash,
- Source update,
- User-supplied wind field,
- Intermediate concentration output,
- Puff information output,
- Buoyancy induced dispersion,
- User-supplied dispersion algorithm, and
- User-supplied plume rise algorithm.

The dimension of the modeling grid must be specified. If the user-supplied wind field option is implemented, then the dimension of the meteorological grid along with the size of each grid rectangle must also be indicated. It is recommended that both grids be given a common origin. If a puff travels outside the modeling region, it is deleted from further consideration. If it travels outside the
meteorological grid, but is still within the modeling region, the wind at the nearest grid point to the puff is used to advect it further.

Information on the source includes the following:

- Location (km),
- Emission rate (g/sec),
- Physical stack height (m),
- Stack gas temperature (K),
- Stack diameter (m),
- Stack gas velocity (m/sec),
- Stack gas volume flow (m³/sec),
- Initial dispersion parameters (m), and
- Deposition and gravitational settling velocities (cm/sec).

Also, the direction and speed of the source, if it is moving, must be provided as input.

The meteorological data needed for the computations are as follows:

- Wind direction (deg),
- Wind speed (m/sec),
- Mixing height (m),
- Stability class (dimensionless),
- Standard deviation of elevation angle (radians),
- Standard deviation of azimuth angle (radians),
- Ambient air temperature (K), and
- Anemometer height (m).

The user has the option of updating the meteorological information after each meteorological time period. The location and height of each receptor must be indicated. If dispersion is characterized by the on-site scheme, then the standard deviations of the azimuth and elevation angles are required.
The following information is required by the plot routines:

- Type of plot desired,
- Location of concentration versus time plots, and
- Plotting grid.

The plot routines were developed on a UNIVAC 1110 and use CALCOMP plotting software.
REFERENCES


K - 14
APPENDIX L

IRA-F TOTAL SUSPENDED PARTICULATES (TSP) DATA
(on diskette file APPL.TXT)
APPENDIX M

IRA-F RESPIRABLE PARTICULATES
OF LESS THAN 10 MICRONS
(on diskette file APPK.TXT)
APPENDIX N

IRA-F ARSENIC, METALS, AND MERCURY DATA
(These data have not been finalized by PMRMA)
(on diskette file APPN1.TXT and APPN2.TXT)
APPENDIX O

IRA-F VOLATILE ORGANIC COMPOUNDS (VOC) DATA
(These data have not been finalized by PMRMA)
(on diskette file APPO1.TXT and APPO2.TXT)
APPENDIX P

IRA-F SEMI-VOLATILE ORGANIC COMPOUNDS
(SVOC) DATA
(These data have not been finalized by PMRMA)
(on diskette file APFP.TXT)
APPENDIX Q

IRA-F ORGANOCHELORINE PESTICIDES (OCP) DATA
(These data have not been finalized by PMRMA)
(on diskette file APPQ.TXT)