

AD-A248 077



2

AD

TECHNICAL REPORT ARCCB-TR-92006

MINIMAX LINEAR SPLINES

DTIC
ELECTE
MAR 31 1992
S D D

ROYCE W. SOANES

FEBRUARY 1992



US ARMY ARMAMENT RESEARCH,
DEVELOPMENT AND ENGINEERING CENTER
CLOSE COMBAT ARMAMENTS CENTER
BENÉT LABORATORIES
WATERVLIET, N.Y. 12189-4050



APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED

92-08071



92 3 31 029

DISCLAIMER

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

The use of trade name(s) and/or manufacturer(s) does not constitute an official indorsement or approval.

DESTRUCTION NOTICE

For classified documents, follow the procedures in DoD 5200.22-M, Industrial Security Manual, Section II-19 or DoD 5200.1-R, Information Security Program Regulation, Chapter IX.

For unclassified, limited documents, destroy by any method that will prevent disclosure of contents or reconstruction of the document.

For unclassified, unlimited documents, destroy when the report is no longer needed. Do not return it to the originator.

REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503

1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE February 1992	3. REPORT TYPE AND DATES COVERED Final	
4. TITLE AND SUBTITLE MINIMAX LINEAR SPLINES			5. FUNDING NUMBERS AMCMS: 6111.01.91A1.1 PRON: 1A1AZ11BNMBJ	
6. AUTHOR(S) Royce W. Soanes				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Benet Laboratories, SMCAR-CCB-TL Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-TR-92006	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000			10. SPONSORING / MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES Presented at the 9th Army Conference on Applied Mathematics and Computing, Minneapolis, MN, 19-21 June 1991 Published in Proceedings of the Conference				
12a. DISTRIBUTION / AVAILABILITY STATEMENT Approved for public release; distribution unlimited			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) An algorithm is derived for obtaining a mesh that minimizes the maximum local interpolatory error for a linear spline, where the error is measured in any classical Banach norm. This algorithm is based on the standard method of approximate error equidistribution advocated by C. de Boor.				
14. SUBJECT TERMS Splines, Interpolation, Error Analysis, Banach Space, Variable Knots, Error Equidistribution, de Boor			15. NUMBER OF PAGES 16	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED	18. SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED	19. SECURITY CLASSIFICATION OF ABSTRACT UNCLASSIFIED	20. LIMITATION OF ABSTRACT UL	

TABLE OF CONTENTS

	<u>Page</u>
INTRODUCTION	1
INTERPOLATORY ERROR	1
INTERPOLATORY ERROR NORM	2
NORM OF ARBITRARY FUNCTION	5
STANDARD APPROXIMATION TO $\ e\ _{n,h}$	6
STANDARD ERROR EQUIDISTRIBUTION FOR ANY BANACH NORM	7
CONVERGENCE OF STANDARD METHOD	8
IMPROVED APPROXIMATION TO $\ e\ _{n,h}$	9
COMPUTATION	11
ALGORITHM	13
REFERENCES	15

Accession For	
NTIS CR&I	J
DTIC TAB	
Unannounced	
J. Publication	
By	
J. Publication	
Availability Codes	
Dist	Availability Codes
A-1	

INTRODUCTION

In order to enable an industrial machine with primitive computational ability to use complicated or difficult to compute functional relationships repeatedly, efficiently, and accurately, it is necessary to supply the machine with these functional relationships as sets of data in tabular form. It is assumed that the machine can deal with continuous, piecewise linear functions (linear splines). A graphics tube is a good example. Such a tube can draw only straight lines, but drawing many short, connected line segments can represent an arbitrary curve well. In order to represent these functions most accurately, a nonuniform mesh must be used. Finding such a mesh is, in principle, a very difficult nonlinear optimization problem, but C. de Boor (refs 1-3) advocated a general method by which the mesh can be found quickly, easily, robustly (and approximately) without any recourse to optimization methods! We present herein a robust addition to de Boor's standard method which improves its accuracy without increasing the essential complexity of his algorithm.

INTERPOLATORY ERROR

Let l be the linear interpolant of function f on a subinterval of length h . The error is given by

$$f(t) = l(t) + e(t) \quad (\mu - \frac{h}{2} \leq t \leq \mu + \frac{h}{2})$$

Expand e in a Taylor series around the midpoint (μ) of the subinterval

$$e(t) = \sum_{i=0}^{\infty} \frac{e^{(i)}(\mu)}{i!} (t-\mu)^i$$

Applying the two boundary conditions

$$e(\mu - \frac{h}{2}) = 0 = e(\mu + \frac{h}{2})$$

ultimately yields

$$e\left(\frac{ht}{2} + \mu\right) = \sum_{i=1}^{\infty} \frac{f^{(2i)}(\mu)}{(2i)!} \left(\frac{h}{2}\right)^{2i} (t^{2i}-1) \\ + \sum_{i=1}^{\infty} \frac{f^{(2i+1)}(\mu)}{(2i+1)!} \left(\frac{h}{2}\right)^{2i+1} t(t^{2i}-1)$$

Taking the first two terms of each sum

$$e\left(\frac{ht}{2} + \mu\right) = \frac{f''(\mu)}{2^3} h^2 (t^2-1) \\ + \frac{f^{(3)}(\mu)}{2^4 \cdot 3} h^3 t (t^2-1) \\ + \frac{f^{(4)}(\mu)}{2^7 \cdot 3} h^4 (t^4-1) \\ + \frac{f^{(5)}(\mu)}{2^8 \cdot 3 \cdot 5} h^5 t (t^4-1) + O(h^6)$$

Letting

$$\rho_i = \frac{f^{(2+i)}(\mu)}{f''(\mu)}$$

one has

$$e\left(\frac{ht}{2} + \mu\right) = \frac{f''(\mu)}{2^3} h^2 (t^2-1) \left\{ 1 + \frac{\rho_1}{2 \cdot 3} ht + \frac{\rho_2}{2^4 \cdot 3} h^2 (t^2+1) \right. \\ \left. + \frac{\rho_3}{2^8 \cdot 3 \cdot 5} h^3 t (t^2+1) + O(h^4) \right\} = \frac{f''(\mu)}{2^3} h^2 (t^2-1) (1+S)$$

where

$$S = a_1 ht + a_2 h^2 (t^2+1) + a_3 h^3 t (t^2+1) + O(h^4)$$

and

$$a_1 = \frac{\rho_1}{2 \cdot 3}, \quad a_2 = \frac{\rho_2}{2^4 \cdot 3}, \quad a_3 = \frac{\rho_3}{2^8 \cdot 3 \cdot 5}$$

INTERPOLATORY ERROR NORM

The local L^n norm of the error on a subinterval of length h is defined by

$$\|e\|_{n,h} = \left(\int_{\mu-h/2}^{\mu+h/2} |e(t)|^n dt \right)^{1/n}$$

where $1 \leq n < \infty$ and n is an integer. For $n = \infty$, we have the maximum error.

Now,

$$\|e\|_{n,h}^n = \frac{h}{2} \int_{-1}^1 |e(\frac{ht}{2} + \mu)|^n dt$$

but

$$e(\frac{ht}{2} + \mu) = \frac{f''(\mu)}{2^3} h^2 (t^2 - 1)(1+S)$$

So if we let h be sufficiently small so that $|S| < 1$ on $(-1,1)$, we have

$$\|e\|_{n,h}^n = \frac{|f''(\mu)|}{2^{3n+1}} \frac{n^{2n+1}}{2^{3n+1}} \int_{-1}^1 (1-t^2)^n (1+S)^n dt$$

Since only the even terms of $(1+S)^n$ contribute to the integral, we have

$$\|e\|_{n,h}^n = \frac{|f''(\mu)|}{2^{3n}} \frac{n^{2n+1}}{2^{3n}} \int_0^1 (1-t^2)^n \text{Ev}(1+S)^n dt$$

where $\text{Ev}(1+S)^n$ denotes the even terms of $(1+S)^n$.

Hence,

$$\text{Ev}(1+S)^n = 1 + \binom{n}{1} a_2 h^2 (1+t^2) + \binom{n}{2} a_1^2 h^2 t^2 + O(h^4)$$

Letting

$$I_{n,i} = \int_0^1 (1-t^2)^n t^{2i} dt$$

we therefore have

$$\begin{aligned} & \int_0^1 (1-t^2)^n \text{Ev}(1+S)^n dt \\ &= \int_0^1 (1-t^2)^n (1+h^2(na_2(1+t^2) + \frac{n(n-1)}{2} a_1^2 t^2) + O(h^4)) dt \\ &= I_{n,0} + nh^2(a_2(I_{n,0}+I_{n,1}) + \frac{n-1}{2} a_1^2 I_{n,1}) + O(h^4) \\ &= I_{n,0}(1+nh^2(a_2(1 + \frac{I_{n,1}}{I_{n,0}}) + \frac{n-1}{2} a_1^2 \frac{I_{n,1}}{I_{n,0}}) + O(h^4)) \end{aligned}$$

Using integration-by-parts on $I_{n,i}$ and solving the resulting recursion ultimately yields

$$I_{n,i} = \frac{2^{2n} n! (2i)! (i+n)!}{i! (2i+2n+1)!}$$

from which we conclude that

$$I_{n,0} = \frac{2^{2n} (n!)^2}{(2n+1)!}$$

$$I_{n,1} = \frac{2^{2n+1} n! (n+1)!}{(2n+3)!}$$

and

$$\frac{I_{n,1}}{I_{n,0}} = \frac{1}{2n+3}$$

Hence,

$$\int_0^1 (1-t^2)^n \text{Ev}(1+S)^n dt$$

$$= \frac{2^{2n} (n!)^2}{(2n+1)!} \left(1 + nh^2 \left(\frac{2(n+1)}{2n+3} a_2 + \frac{n-1}{2(2n+3)} a_1^2 \right) + O(h^4) \right)$$

and

$$\| \text{ell}_{n,h}^n = \frac{|f''(\mu)| \frac{1}{2^n (2n+1)!} (n!)^2}{2^n (2n+1)!} \left(1 + nh^2 \left(\frac{2(n+2)}{2n+3} a_2 + \frac{n-1}{2(2n+3)} a_1^2 \right) + O(h^4) \right)$$

or

$$\| \text{ell}_{n,h} = k |f''(\mu)| h^{2+1/n} \left(1 + h^2 \left(\frac{2(n+2)}{2n+3} a_2 + \frac{n-1}{2(2n+3)} a_1^2 \right) + O(h^4) \right)$$

where

$$k = \frac{1}{2} \left(\frac{(n!)^2}{(2n+1)!} \right)^{1/n}$$

Using Stirling's approximation to the factorial, it is easy to show that

$$\lim_{n \rightarrow \infty} k = \frac{1}{8}$$

Recalling that

$$a_1 = \frac{\rho_1}{2 \cdot 3} \quad \text{and} \quad a_2 = \frac{\rho_2}{2^2 \cdot 3}$$

we finally have

$$\| \text{ell}_{n,h} = k |f''(\mu)| h^{2+1/n} \left(1 + \frac{h^2}{24} \left(\frac{n+2}{2n+3} \rho_2 + \frac{n-1}{3(2n+3)} \rho_1^2 \right) + O(h^4) \right)$$

as $h \rightarrow 0$, where

$$k = \frac{1}{2} \left(\frac{(n!)^2}{(2n+1)!} \right)^{1/n}$$

and

$$\rho_i = f^{(2+i)}(\mu) / f''(\mu)$$

NORM OF ARBITRARY FUNCTION

The local L^p norm of arbitrary function ϕ over a subinterval of length h is defined as

$$\|\phi\|_{p,h} = \left(\int_{\mu-h/2}^{\mu+h/2} |\phi(t)|^p dt \right)^{1/p}$$

where $p > 0$, finite and real. In this context, we allow $p < 1$ even though Minkowski's triangle inequality holds only for $p \geq 1$.

Expand ϕ in a Taylor series around the midpoint of the subinterval

$$\phi(t) = \phi(\mu) \sum_{i=0}^{\infty} \frac{\rho_i}{i!} (t-\mu)^i$$

where

$$\rho_i = \phi^{(i)}(\mu) / i!$$

Now,

$$\|\phi\|_{p,h}^p = \frac{h}{2} \int_{-1}^1 \left| \phi\left(\frac{ht}{2} + \mu\right) \right|^p dt$$

but

$$\phi\left(\frac{ht}{2} + \mu\right) = \phi(\mu)(1+S)$$

where

$$S = \sum_{i=1}^{\infty} a_i t^i$$

and

$$a_i = \frac{\rho_i}{i!} \left(\frac{h}{2}\right)^i$$

Hence, letting h be sufficiently small so that $|S| < 1$ on $(-1,1)$, we have

$$\|\phi\|_{p,h}^p = \frac{h}{2} |\phi(\mu)|^p \int_{-1}^1 (1+S)^p dt = \frac{h}{2} |\phi(\mu)|^p \int_{-1}^1 E_V(1+S)^p dt$$

but

$$S = a_1 t + a_2 t^2 + a_3 t^3 + O(h^4)$$

hence

$$E v(1+S)^P = 1 + \binom{P}{1} a_2 t^2 + \binom{P}{2} a_1^2 t^2 + O(h^4)$$

We therefore have

$$\begin{aligned} \|\phi\|_{p,h}^P &= h |\phi(\mu)|^P \int_0^1 1 + p t^2 (a_2 + \frac{p-1}{2} a_1^2) + O(h^4) dt \\ &= h |\phi(\mu)|^P (1 + \frac{p h^2}{24} (\rho_2 + (p-1)\rho_1^2) + O(h^4)) \end{aligned}$$

or

$$\|\phi\|_{p,h} = h^{1/p} |\phi(\mu)| (1 + \frac{h^2}{24} (\rho_2 + (p-1)\rho_1^2) + O(h^4))$$

as $h \rightarrow 0$.

STANDARD APPROXIMATION TO $\|e\|_{n,h}$

Recalling that

$$h^{-1/p} \|f''\|_{p,h} = |f''(\mu)| (1 + \frac{h^2}{24} (\rho_2 + (p-1)\rho_1^2) + O(h^4))$$

and

$$\|e\|_{n,h} = k h^{2+1/n} |f''(\mu)| (1 + \frac{h^2}{24} (\frac{n+2}{2n+3} \rho_2 + \frac{n-1}{3(2n+3)} \rho_1^2) + O(h^4))$$

we multiply the first equation by $k h^{2+1/n}$ and subtract from the second, getting

$$\begin{aligned} \|e\|_{n,h} &= k h^{2+1/n-1/p} \|f''\|_{p,h} \\ &+ k h^{2+1/n} |f''(\mu)| (\frac{h^2}{24} (-\frac{n+1}{2n+3} \rho_2 + (\frac{7n+8}{6n+9} - p)\rho_1^2) + O(h^4)) \end{aligned}$$

If we now let $p = \frac{n}{2n+1}$, we have

$$\begin{aligned} \|e\|_{n,h} &= k \|f''\|_{n/(2n+1),h} \\ &+ k h^{4+1/n} |f''(\mu)| (\frac{1}{24} (-\frac{n+1}{2n+3} \rho_2 + \frac{5n^2+14n+8}{12n^2+24n+9} \rho_1^2) + O(h^2)) \\ &= k \|f''\|_{p,h} + k h^{4+1/n} |f''(\mu)| (\frac{1}{24} (-a\rho_2 + b\rho_1^2) + O(h^2)) \\ &= k \|f''\|_{n/(2n+1),h} + O(h^{4+1/n}) \end{aligned}$$

For $n = 1, 2$, and ∞ , respectively, we have

$$\|e\|_{1,h} = \frac{1}{12} \|f''\|_{1/3,h} + O(h^4)$$

$$\|e\|_{2,h} = \frac{1}{2\sqrt{30}} \|f''\|_{2/5,h} + O(h^{9/2})$$

$$\|e\|_{\infty,h} = \frac{1}{8} \|f''\|_{1/2,h} + O(h^4)$$

STANDARD ERROR EQUIDISTRIBUTION FOR ANY BANACH NORM

In this section, we justify the standard method of error equidistribution with respect to any Banach norm. The global L^n norm of the error over interval (a,b) is

$$\|e\|_n = \left(\int_a^b |e(t)|^n dt \right)^{1/n}$$

Hence, for a mesh $a = x_1 < x_2 < \dots < x_N = b$

$$\|e\|_n^n = \sum_{i=1}^{N-1} \int_{x_i}^{x_{i+1}} |e_i(t)|^n dt = \sum_{i=1}^{N-1} \|e\|_{n,h_i}^n$$

Let single bars around the error denote the standard approximation to the error norm and analogously define

$$|e|_n^n = \sum_{j=1}^{N-1} |e|_{n,h_j}^n$$

but

$$|e|_{n,h_j} = k \|f''\|_{p,h_j} = k \left(\int_{x_j}^{x_{j+1}} |f''(t)|^p dt \right)^{1/p}$$

where

$$p = \frac{n}{2n+1}$$

Hence, letting

$$I_{p,h_j} = \int_{x_j}^{x_{j+1}} |f''(t)|^p dt$$

we have

$$|e|_n^n = k^n \sum_{j=1}^{N-1} I_{p,h_j}^{2n+1}$$

We will refer to the integrals $I_{p,h}$ as the standard or de Boor integrals.

It follows trivially, using Leibnitz's rule, that

$$\frac{\partial}{\partial x_i} |e|_n = 0 \quad 1 < i < N$$

implies that

$$I_{p,h_{i-1}} = I_{p,h_i} \quad 1 < i < N$$

Hence, the condition $I_{p,h} = \text{constant}$ determines the mesh which minimizes the standard global approximation to $\|e\|_n$.

For a linear spline approximation to f'' , it is a fairly simple (see COMPUTATION) matter to find the mesh for which the de Boor integrals are constant.

CONVERGENCE OF STANDARD METHOD

Recall that

$$\|e\|_{n,h} = k \|f''\|_{p,h} + \frac{k}{24} h^{4+1/n} |f''(\mu)| (-ap_2 + bp_1^2) + O(h^{6+1/n})$$

Letting

$$F = -af''(\mu)f^{(4)}(\mu) + bf^{(3)}(\mu)^2$$

we have the following one term approximation to the difference between $\|e\|_{n,h}$ and $|e|_{n,h}$:

$$\|e\|_{n,h} - |e|_{n,h} \approx \frac{kFh^{4+1/n}}{24|f''(\mu)|^2}$$

but

$$\|e\|_{n,h} \approx kh^{2+1/n} |f''(\mu)|$$

Therefore, we also have

$$\frac{\|e\|_{n,h} - |e|_{n,h}}{\|e\|_{n,h}} \approx \frac{Fh^2}{24|f''(\mu)|^2}$$

but also

$$\|f''\|_{p,h} \approx h^{1/p} |f''(\mu)|$$

hence,

$$h \approx \left(\frac{\|f''\|_{n,h}}{|f''(\mu)|} \right)^p = \left(\frac{I_{p,h}^{1/p}}{|f''(\mu)|} \right)^p = \frac{I_{p,h}}{|f''(\mu)|^p}$$

In addition, for the correct mesh

$$I_{p,h} = \frac{I_p}{N-1}$$

hence,

$$h \approx \frac{I_p}{(N-1)|f''(\mu)|^p}$$

and therefore,

$$\frac{\|e\|_{n,h} - |e|_{n,h}}{\|e\|_{n,h}} \approx \frac{FI_p^2}{24|f''(\mu)|^{2+2p}(N-1)^2}$$

This tells us that the relative difference between $\|e\|_{n,h}$ and $|e|_{n,h}$ is $O(\frac{1}{N^2})$ as $N \rightarrow \infty$, which means that the standard method works better and better

($\|e\|_{n,h}$ will be more nearly constant) as N gets larger and larger. This is all true, however, with the proviso that

$$\frac{F}{|f''(\mu)|^{2+2p}}$$

is bounded throughout the region of interest. It stands to reason, therefore, that the standard method will perform worst where f'' is not bounded away from zero.

IMPROVED APPROXIMATION TO $\|e\|_{n,h}$

Recall that

$$\|e\|_{n,h} = k|f''(\mu)|h^{2+1/n} \left(1 + \frac{h^2}{24} \left(\frac{n+2}{2n+3} \rho_2 + \frac{n-1}{3(2n+3)} \rho_1^2 \right) + O(h^4) \right)$$

and

$$\|f''\|_{q,h} = h^{1/q} |f''(\mu)| \left(1 + \frac{h^2}{24} (\rho_2 + (q-1)\rho_1^2) + O(h^4) \right)$$

Multiplying h by r in the second equation, we have

$$r^{-1/q} \|f''\|_{q,rh} = h^{1/q} |f''(\mu)| \left(1 + \frac{h^2}{24} (r^2 \rho_2 + r^2 (q-1)\rho_1^2) + O(h^4) \right)$$

Multiplying this equation by kh^Q gives us

$$kr^{-1/q}h^Q \|f''\|_{q,rh} = kh^{Q+1/q} |f''(\mu)| \left(1 + \frac{h^2}{24}(r^2\rho_2 + r^2(q-1)\rho_1^2) + O(h^4)\right)$$

Now, in order to make this equation look as much like the very first one as possible, we set

$$r^2 = \frac{n+2}{2n+3}, \quad r^2(q-1) = \frac{n-1}{3(2n+3)}$$

and

$$Q + \frac{1}{q} = 2 + \frac{1}{n}$$

Solving for r , q , and Q , we have

$$r = \left(\frac{n+2}{2n+3}\right)^{1/2}$$

$$q = \frac{4n+5}{3n+6}$$

and

$$Q = \frac{5n^2+8n+5}{4n^2+5n}$$

A simple subtraction then gives us an improved approximation to $\|e\|_{n,h}$

$$\|e\|_{n,h} = kr^{-1/q}h^Q \|f''\|_{q,rh} + O(h^{6+1/n})$$

where before, we had

$$\|e\|_{n,h} = k\|f''\|_{p,h} + O(h^{4+1/n}) = |e|_{n,h} + O(h^{4+1/n})$$

It must be mentioned however, that although this improved approximation is asymptotically more efficient, no such approximation can be uniformly superior in all cases. Bearing this in mind, we dispense with approximations on all subintervals not having f'' bounded away from zero and instead use the exact error

$$e_i(x) = \int_{x_i}^x \int_{x_i}^t f''(u)du dt - \frac{x-x_i}{x_{i+1}-x_i} \int_{x_i}^{x_{i+1}} \int_{x_i}^t f''(u)du dt$$

COMPUTATION

In actual computation, we assume the existence of a piecewise linear approximation to $|f''|$. The mesh over which this function is defined is referred to as the "original" mesh. In order to deal with the standard and improved asymptotic integral approximations to the local error norm, we will need to deal with integrals of the form

$$L = \int_c^{c+l} \lambda(t)^{m/n} dt$$

where λ is a nonnegative linear function with slope s

$$\lambda(t) = \lambda(c) + s(t-c)$$

with

$$\lambda(t) \geq 0 \quad \text{for} \quad c \leq t \leq c + l$$

and where m and n are arbitrary positive integers.

In the following, let

$$\alpha = \lambda(c)^{1/n}$$

and

$$S_k = \sum_{i=0}^k \alpha^i \beta^{k-i} = \frac{\beta^{k+1} - \alpha^{k+1}}{\beta - \alpha}$$

First, we need to compute L as a function of l

$$L = \frac{l n S_{m+n-1}}{(m+n) S_{n-1}} = A(l)$$

where

$$\beta = (\lambda(c) + sl)^{1/n}$$

Second, we need to compute l as a function of L

$$l = \frac{L(m+n) S_{n-1}}{n S_{m+n-1}} = B(L)$$

where

$$\beta = (\lambda(c)^{m/n+1} + (\frac{m}{n} + 1) s L)^{1/(m+n)}$$

A and B are therefore inverse functions, i.e.,

$$A(B(x)) = x = B(A(x))$$

or

$$A^{-1} = B \quad \text{and} \quad B^{-1} = A$$

Now let values of u denote the original mesh and let g be the piecewise linear interpolant to the $(u_i, |f_i''|)$ data.

Define the integral

$$G(x) = \int_{u_1}^x g(t)^{m/n} dt$$

Now if $u_i \leq x \leq u_{i+1}$,

$$\begin{aligned} G(x) &= \int_{u_1}^{u_i} g(t)^{m/n} dt + \int_{u_i}^{u_i+x-u_i} g_i(t)^{m/n} dt \\ &= G(u_i) + L \end{aligned}$$

where $\lambda = g_i$, $c = u_i$, and $l = x - u_i$. Hence,

$$G(x) = G(u_i) + A(x - u_i)$$

explicitly defines G for all x in the domain of interest.

In order to get the standard mesh, we will also have to compute the inverse of G (only for $m/n = p$).

$$B(G(x) - G(u_i)) = B(A(x - u_i)) = x - u_i$$

Hence,

$$x = u_i + B(G(x) - G(u_i))$$

but if $G(x) = \gamma$, then $x = G^{-1}(\gamma)$. Therefore,

$$G^{-1}(\gamma) = u_i + B(\gamma - G(u_i))$$

for

$$G(u_i) \leq \gamma \leq G(u_{i+1})$$

and provided

$$G(u_i) \neq G(u_{i+1})$$

Define

$$I_i = G(x_{i+1}) - G(x_i) = \int_{x_i}^{x_{i+1}} g(t)^p dt$$

where x is the standard or improved mesh, obtained by prescribing values for the I 's. The standard method prescribes

$$I_i = \text{const} = \frac{G(x_N)}{N-1} \quad (1 \leq i \leq N)$$

For the improved mesh, the I 's will vary, but the mesh is still obtained in the standard way. Since

$$G(x_{i+1}) = G(x_i) + I_i$$

we have immediately that

$$x_{i+1} = G^{-1}(G(x_i) + I_i) \quad i = 1, 2, \dots, N-2$$

ALGORITHM

Let $*$ denote a standard or improved mesh and $**$ denote the succeeding improved mesh. We have seen that the main contributor to the ratios $\|e\|_{n,h^{**}}/\|e\|_{n,h^*}$ and $|e|_{n,h^{**}}/|e|_{n,h^*}$ is

$$\left(\frac{h^{**}}{h^*} \right)^{2+1/n} \left| \frac{f''(\mu^{**})}{f''(\mu^*)} \right|$$

We therefore have the approximate asymptotic relation

$$\frac{|e|_{n,h^{**}}}{|e|_{n,h^*}} \approx \frac{\|e\|_{n,h^{**}}}{\|e\|_{n,h^*}}$$

But we would like $\|e\|_{n,h^{**}}$ to be constant, hence we have the proportionality

$$|e|_{n,h^{**}} \propto \frac{|e|_{n,h^*}}{\|e\|_{n,h^*}}$$

or

$$I_{p,h^{**}} \propto \left(\frac{|e|_{n,h^*}}{\|e\|_{n,h^*}} \right)^p$$

We calculate the I's accordingly and multiply them by the appropriate constant to get

$$\sum_{i=1}^{N-1} I_{p,h_i^{**}} = \frac{G(x_N)}{N-1}$$

The quantities $\|e\|_{n,h_i^*}$ are computed either from the improved asymptotic approximation or exactly (relative to the original data) depending on whether or not f'' is bounded away from zero on the subinterval in question. It is important to note that this approximate relation between the * and ** meshes can lead to exact convergence (rapidly) to the minimax mesh. If the * mesh is the minimax mesh ($\|e\|_{n,h_i^*} = \text{constant}$), then the de Boor integrals ($I_{p,h}$) on the ** mesh will be no different from those on the * mesh.

The practical convergence properties of this algorithm are as follows. If f'' is well bounded away from zero, the standard de Boor method gives impeccable results without any iteration. If f'' is not bounded away from zero, convergence to a virtually perfect minimax mesh can easily occur in only two iterations. A few iterations may be needed in the presence of multiple inflection points.

In any case, even the very first iteration improves the mesh markedly.

REFERENCES

1. C. de Boor, "Good Approximation by Splines With Variable Knots," in:
Spline Functions and Approximation Theory (A. Meir and A. Sharma, eds.),
Birkhäuser Verlag, Basel, 1973, pp. 57-72.
2. C. de Boor, "Good Approximation by Splines With Variable Knots, II," in:
Numerical Solution of Differential Equations (G.A. Watson, ed.), Lecture
Notes in Math, No. 363, Springer Verlag, 1974, pp. 12-20.
3. C. de Boor, A Practical Guide to Splines, Springer-Verlag, New York, 1978.

TECHNICAL REPORT INTERNAL DISTRIBUTION LIST

	<u>NO. OF COPIES</u>
CHIEF, DEVELOPMENT ENGINEERING DIVISION	
ATTN: SMCAR-CCB-DA	1
-DC	1
-DI	1
-DR	1
-DS (SYSTEMS)	1
CHIEF, ENGINEERING SUPPORT DIVISION	
ATTN: SMCAR-CCB-S	1
-SD	1
-SE	1
CHIEF, RESEARCH DIVISION	
ATTN: SMCAR-CCB-R	2
-RA	1
-RE	1
-RM	1
-RP	1
-RT	1
TECHNICAL LIBRARY	5
ATTN: SMCAR-CCB-TL	
TECHNICAL PUBLICATIONS & EDITING SECTION	3
ATTN: SMCAR-CCB-TL	
OPERATIONS DIRECTORATE	1
ATTN: SMCWV-ODP-P	
DIRECTOR, PROCUREMENT DIRECTORATE	1
ATTN: SMCWV-PP	
DIRECTOR, PRODUCT ASSURANCE DIRECTORATE	1
ATTN: SMCWV-QA	

NOTE: PLEASE NOTIFY DIRECTOR, BENET LABORATORIES, ATTN: SMCAR-CCB-TL, OF ANY ADDRESS CHANGES.

TECHNICAL REPORT EXTERNAL DISTRIBUTION LIST

	<u>NO. OF COPIES</u>		<u>NO. OF COPIES</u>
ASST SEC OF THE ARMY RESEARCH AND DEVELOPMENT ATTN: DEPT FOR SCI AND TECH THE PENTAGON WASHINGTON, D.C. 20310-0103	1	COMMANDER ROCK ISLAND ARSENAL ATTN: SMCRI-ENM ROCK ISLAND, IL 61299-5000	1
ADMINISTRATOR DEFENSE TECHNICAL INFO CENTER ATTN: DTIC-FDAC CAMERON STATION ALEXANDRIA, VA 22304-6145	12	DIRECTOR US ARMY INDUSTRIAL BASE ENGR ACTV ATTN: AMXIB-P ROCK ISLAND, IL 61299-7260	1
COMMANDER US ARMY ARDEC ATTN: SMCAR-AEE	1	COMMANDER US ARMY TANK-AUTMV R&D COMMAND ATTN: AMSTA-DDL (TECH LIB) WARREN, MI 48397-5000	1
SMCAR-AES, BLDG. 321	1	COMMANDER US MILITARY ACADEMY	1
SMCAR-AET-O, BLDG. 351N	1	ATTN: DEPARTMENT OF MECHANICS WEST POINT, NY 10996-1792	
SMCAR-CC	1		
SMCAR-CCP-A	1	US ARMY MISSILE COMMAND	
SMCAR-FSA	1	REDSTONE SCIENTIFIC INFO CTR	2
SMCAR-FSM-E	1	ATTN: DOCUMENTS SECT, BLDG. 4484 REDSTONE ARSENAL, AL 35898-5241	
SMCAR-FSS-D, BLDG. 94	1		
SMCAR-IMI-I (STINFO) BLDG. 59	2		
PICATINNY ARSENAL, NJ 07806-5000			
DIRECTOR US ARMY BALLISTIC RESEARCH LABORATORY ATTN: SLCBR-DD-T, BLDG. 305	1	COMMANDER US ARMY FGN SCIENCE AND TECH CTR ATTN: DRXST-SD 220 7TH STREET, N.E. CHARLOTTESVILLE, VA 22901	1
ABERDEEN PROVING GROUND, MD 21005-5066			
DIRECTOR US ARMY MATERIEL SYSTEMS ANALYSIS ACTV ATTN: AMXSY-MP	1	COMMANDER US ARMY LABCOM MATERIALS TECHNOLOGY LAB ATTN: SLCMT-IML (TECH LIB)	2
ABERDEEN PROVING GROUND, MD 21005-5071		WATERTOWN, MA 02172-0001	
COMMANDER HQ, AMCCOM ATTN: AMSMC-IMP-L	1		
ROCK ISLAND, IL 61299-6000			

NOTE: PLEASE NOTIFY COMMANDER, ARMAMENT RESEARCH, DEVELOPMENT, AND ENGINEERING CENTER, US ARMY AMCCOM, ATTN: BENET LABORATORIES, SMCAR-CCB-TL, WATERVLIET, NY 12189-4050, OF ANY ADDRESS CHANGES.

TECHNICAL REPORT EXTERNAL DISTRIBUTION LIST (CONT'D)

	<u>NO. OF COPIES</u>		<u>NO. OF COPIES</u>
COMMANDER US ARMY LABCOM, ISA ATTN: SLCIS-IM-TL 2800 POWDER MILL ROAD ADELPHI, MD 20783-1145	1	COMMANDER AIR FORCE ARMAMENT LABORATORY ATTN: AFATL/MN EGLIN AFB, FL 32542-5434	1
COMMANDER US ARMY RESEARCH OFFICE ATTN: CHIEF, IPO P.O. BOX 12211 RESEARCH TRIANGLE PARK, NC 27709-2211	1	COMMANDER AIR FORCE ARMAMENT LABORATORY ATTN: AFATL/MNF EGLIN AFB, FL 32542-5434	1
DIRECTOR US NAVAL RESEARCH LAB ATTN: MATERIALS SCI & TECH DIVISION CODE 26-27 (DOC LIB) WASHINGTON, D.C. 20375	1 1	MIAC/CINDAS PURDUE UNIVERSITY 2595 YEAGER ROAD WEST LAFAYETTE, IN 47905	1
DIRECTOR US ARMY BALLISTIC RESEARCH LABORATORY ATTN: SLCBR-IB-M (DR. BRUCE BURNS) ABERDEEN PROVING GROUND, MD 21005-5066	1		

NOTE: PLEASE NOTIFY COMMANDER, ARMAMENT RESEARCH, DEVELOPMENT, AND ENGINEERING CENTER, US ARMY AMCCOM, ATTN: BENET LABORATORIES, SMCAR-CCB-TL, WATERVLIET, NY 12189-4050, OF ANY ADDRESS CHANGES.