REPORT NO. EVT 33-90-1

OPERATION DESERT STORM

SOLAR RADIATION SHIELDING MATERIALS FOR AMMUNITION STORAGE

DTIC ELECTED FEB 21 1992

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VALIDATION ENGINEERING DIVISION
SAVANNA, ILLINOIS 61074-9639
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The U.S. Army Defense Ammunition Center and School (USADACS), Validation Engineering Division (SMCAC-DEV), conducted engineering tests on thermal insulating materials which could be used to protect ammunition in Saudi Arabia (SA). This report contains the test results of several materials which provide excellent shielding of ammunition from direct solar radiation.
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</table>
PART 1

INTRODUCTION

A. BACKGROUND. Absorption of heat through high ambient temperatures and solar radiation has proven to have an adverse/detrimental effect on ammunition in open storage. As such, USADACS, during early deployment of ammunition to Saudi Arabia (SA), conducted screening tests on solar radiation materials that could be used to protect ammunition stored under desert conditions. As a result of this testing, several thermal insulating materials were identified that could be used as solar radiation protective covers in SA.

B. AUTHORITY. These tests were conducted in accordance with mission responsibilities delegated by the U.S. Army Armament, Munitions and Chemical Command (AMCCOM), Rock Island, IL.

C. OBJECTIVE. The objectives of this evaluation were to determine what effect direct solar radiation had on ammunition in open storage, in individual shipping containers, in pallets, and loaded Military Vans (MILVANS). Other objectives included the screening of synthetic materials to determine which were most suitable for thermal shields to protect the ammunition.
PART 2

OPERATION DESERT STORM

SOLAR RADIATION SHIELDING MATERIALS FOR
AMMUNITION STORAGE

TEST ATTENDEES

<table>
<thead>
<tr>
<th>NAME AND TELEPHONE NUMBER</th>
<th>ORGANIZATION</th>
</tr>
</thead>
<tbody>
<tr>
<td>William R. Meyer</td>
<td>Director</td>
</tr>
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<td>Test Engineer</td>
<td>U.S. Army Defense Ammunition Center and School</td>
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<tr>
<td>DSN 585-8090</td>
<td>ATTN: SMCAC-DEV</td>
</tr>
<tr>
<td>Comm 815-273-8090</td>
<td>Savanna, IL 61074-9639</td>
</tr>
</tbody>
</table>

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| Test Engineer             | U.S. Army Defense Ammunition Center and School |
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| Comm 815-273-8992         | Savanna, IL 61074-9639 |

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| Comm 815-273-8988         | Savanna, IL 61074-9639 |

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| Technical Illustrator     | U.S. Army Defense Ammunition Center and School |
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PART 3

TEST PROCEDURES

A. THERMAL SHIELDING TESTS. A total of 15 thermal shielding materials were evaluated. Each material was tested with inertly-loaded 155mm propellant charge containers, with interior and exterior temperature probes placed at critical points. Temperature data were taken every 5 minutes for a period of not less than 24 hours per each test, including ambient and control (unprotected) temperature measurements. After testing, all materials were evaluated to determine which materials provided the greatest protection against solar radiation. Drawing no. 1 (see page 3-2) depicts the typical test setup used during these tests.
SOLAR RADIATION PROTECTIVE COVERING

DATA ACQUISITION PACKAGE

AMBIENT THERMISTOR PROBE

SOLAR RADIATION INTENSITY PER SQUARE METER

PRESSURE PROBE

INTERIOR TEMPERATURE

CONTROL NO PROTECTION THERMOSHIELD FOIL BACK NO INSULATION ORCOFILM AN-21A INSULATION ORCOFILM AN-33 INSULATION ASAT INSULATION

NOTES:
1. 155mm PROP CHARGES INERT FILL.
B. PALLET TESTING. Pallets containing inertly-loaded PA116 containers were instrumented with external probes both on top and between layers of the pallet. Instrumentation included at least one ambient temperature probe and a control pallet which had no protective covering. Test pallets were covered with different protective coverings both with and without air space between the covering. Additional tests were conducted with sandbag-covered pallets with no air space provided. All test pallets were compared to the control pallet to determine what level of protection was being afforded by the protective coverings. Drawing no. 2 (see page 3-4) depicts the typical test setup used during this series of tests.
C. MILVAN TESTING. A MILVAN containing inertly-loaded 105mm boxed ammunition was instrumented at the following locations:

1. On the outside of the roof of the MILVAN.
2. At the top of the MILVAN load.
3. At the center of the load.
4. Ambient temperatures at the test site.

Tests were conducted with the MILVAN doors open and closed. Test data were taken every 5 minutes for a period of not less than 24 hours. Interior, roof, and ambient temperatures were compared to determine internal temperature gain within the MILVAN. Drawing no. 3 (see page 3-6) depicts the typical test setup during MILVAN testing.
1. TEST CONTAINERS.
   a. Item: 155mm Hol. M119 Containers (OD color)
   b. FSN: 1320-143-6847-D533
   c. Type: SPM109 A1
   d. Weight: 41 pounds
   e. Cube: 1.7 cubic feet

2. TEST PALLET.
   a. Item: PA116 Containers W/Metal Pallets (OD color)
   b. Drawing: AC200000501
   c. Width: 40 inches
   d. Length: 44-1/2 inches
   e. Height: 52-5/8 inches
   f. Weight: 2,400 pounds

3. DATA RECORDER.
   a. Manufacturer: Omega Engineering
   b. Model No.: OM-220
   c. Channels: 8
   d. Memory: 32,000 Reading
A. MATERIAL SCREENING TESTS:

1. Tests were conducted 17 August - 26 September 1990 on 15 thermal shielding materials. To assist in evaluation of these materials, test data has been broken down into the following four categories:

   (a) Exterior temperature of control samples.

   (b) Interior temperature of control samples.

   (c) Exterior temperature of protected (shielded) samples.

   (d) Interior temperature of protected (shielded) samples.

This approach will help assess temperature buildup on both unprotected and protected containers.

2. Table no. 1 depicts the effects of solar radiation on unprotected 155mm propellant charge containers exposed directly to sunlight. During this test, surface temperature probes were attached to the exterior skin of each container. During the nine tests, ambient temperature averaged 89 degrees Fahrenheit while the average skin temperature of unprotected containers averaged 133.2 degrees Fahrenheit, or 44.2 degrees Fahrenheit above ambient.
155mm Propellant Charge Container
Exterior Skin Temperatures
No Exterior Protection

Table 1

<table>
<thead>
<tr>
<th>Test Number</th>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Skin Temperature</th>
<th>Temperature Differential</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>8-23</td>
<td>85</td>
<td>120</td>
<td>+35</td>
</tr>
<tr>
<td>2</td>
<td>9-25</td>
<td>85</td>
<td>132</td>
<td>+47</td>
</tr>
<tr>
<td>3</td>
<td>8-30</td>
<td>85</td>
<td>135</td>
<td>+50</td>
</tr>
<tr>
<td>4</td>
<td>9-26</td>
<td>85</td>
<td>140</td>
<td>+56</td>
</tr>
<tr>
<td>5</td>
<td>8-24</td>
<td>89</td>
<td>125</td>
<td>+36</td>
</tr>
<tr>
<td>6</td>
<td>8-29</td>
<td>90</td>
<td>140</td>
<td>+50</td>
</tr>
<tr>
<td>7</td>
<td>8-27</td>
<td>93</td>
<td>140</td>
<td>+47</td>
</tr>
<tr>
<td>8</td>
<td>9-4</td>
<td>94</td>
<td>132</td>
<td>+38</td>
</tr>
<tr>
<td>9</td>
<td>8-17</td>
<td>95</td>
<td>135</td>
<td>+40</td>
</tr>
</tbody>
</table>

3. Of notable interest during this series of tests was the effect of solar radiation on test samples when ambient temperature remained constant. Note: test numbers 1-4 had an ambient temperature of 85 degrees Fahrenheit; however, surface skin temperatures ranged from 120 degrees to 140 degrees Fahrenheit. This 41 percent to 64 percent elevation over ambient was due to the intensity of the sun, duration of the solar radiation, cloud cover, particulate in the air, wind, etc. This is significant when determining adverse effects of solar radiation in SA; i.e., ambient temperatures of 120 degrees Fahrenheit could result in surface skin temperatures as high as 180 degrees Fahrenheit or higher.

4. A second series of tests conducted used internal proximity probes within the 155mm propellant charge metal containers to determine what thermal conductivity was taking place inside the containers. These probes were in direct contact with the inert propellant bags. During
this test average ambient temperature was 88.3 degrees Fahrenheit, while the average interior temperature was 119.0 degrees Fahrenheit, or a temperature elevation of 30.7 degrees Fahrenheit (35 percent increase). Thermal lag during this test was approximately 14 degrees lower than the outside skin temperature.

155mm Propellant Charge Metal Container
Interior Propellant Charge Temperatures
No Exterior Protection

Table 2

<table>
<thead>
<tr>
<th>Test Number</th>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Skin Temperature</th>
<th>Temperature Differential</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>1-23</td>
<td>85</td>
<td>105</td>
<td>+20</td>
</tr>
<tr>
<td>2</td>
<td>8-30</td>
<td>85</td>
<td>118</td>
<td>+33</td>
</tr>
<tr>
<td>3</td>
<td>9-25</td>
<td>85</td>
<td>120</td>
<td>+35</td>
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<tr>
<td>4</td>
<td>9-25</td>
<td>85</td>
<td>128</td>
<td>+43</td>
</tr>
<tr>
<td>5</td>
<td>8-24</td>
<td>89</td>
<td>110</td>
<td>+21</td>
</tr>
<tr>
<td>6</td>
<td>8-29</td>
<td>90</td>
<td>124</td>
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<td>7</td>
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<tr>
<td>8</td>
<td>9-4</td>
<td>94</td>
<td>122</td>
<td>+28</td>
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<tr>
<td>9</td>
<td>9-26</td>
<td>84</td>
<td>129</td>
<td>+45</td>
</tr>
</tbody>
</table>

5. As noted above, internal air temperatures varied within the sealed containers while ambient temperature remained constant (as shown in tests 1 - 4, ambient temperature was 85 degrees). While interior temperatures ranged from 105 degrees Fahrenheit to 128 degrees Fahrenheit, this suggests that with ambient temperature approaching 120 degrees Fahrenheit in SA, internal temperatures could reach in excess of 165 degrees Fahrenheit.

6. Other tests were conducted on materials used for thermal shielding. All shielding materials were placed directly in contact with the surface of the container (with no air space or
1/2-inches above as noted), this provided a "worst case" condition for materials being tested. Due to different ambient temperatures during these tests, effectiveness of materials was determined by the temperature rise over ambient temperature. For example, shielding materials that allowed for very little temperature elevation over ambient were determined to be most effective. Table 3 summarizes the test results.

**Table 3**

<table>
<thead>
<tr>
<th>Sample Type</th>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Exterior Temperature</th>
<th>Temperature Differential</th>
</tr>
</thead>
<tbody>
<tr>
<td>R13 Insulated White/Foil</td>
<td>8-17</td>
<td>89</td>
<td>88</td>
<td>-1</td>
</tr>
<tr>
<td>White/Foil W/O Insulation</td>
<td>8-17</td>
<td>89</td>
<td>95</td>
<td>+6</td>
</tr>
<tr>
<td>Camouflage W/F 3.5&quot; Space</td>
<td>8-24</td>
<td>89</td>
<td>95</td>
<td>+6</td>
</tr>
<tr>
<td>Ludlow</td>
<td>9-4</td>
<td>94</td>
<td>100</td>
<td>+6</td>
</tr>
<tr>
<td>Chase Ext</td>
<td>9-4</td>
<td>94</td>
<td>100</td>
<td>+6</td>
</tr>
<tr>
<td>ASATI</td>
<td>8-29</td>
<td>92</td>
<td>99</td>
<td>+7</td>
</tr>
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<td>AN19</td>
<td>9-25</td>
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<td>AN35-40</td>
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<td>+8</td>
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<td>12589 Ext</td>
<td>8-30</td>
<td>85</td>
<td>95</td>
<td>+10</td>
</tr>
<tr>
<td>Canvas (3.5&quot; space ext)</td>
<td>8-24</td>
<td>91</td>
<td>103</td>
<td>+12</td>
</tr>
<tr>
<td>Champion</td>
<td>9-26</td>
<td>85</td>
<td>99</td>
<td>+14</td>
</tr>
<tr>
<td>ER-3834</td>
<td>8-29</td>
<td>90</td>
<td>105</td>
<td>+15</td>
</tr>
<tr>
<td>Camouflage White/Foil</td>
<td>8-23</td>
<td>85</td>
<td>105</td>
<td>+20</td>
</tr>
<tr>
<td>Canvas (no space ext)</td>
<td>8-23</td>
<td>85</td>
<td>112</td>
<td>+27</td>
</tr>
<tr>
<td>DeWitt Ext</td>
<td>9-26</td>
<td>85</td>
<td>120</td>
<td>+35</td>
</tr>
</tbody>
</table>

7. As noted above, canvas with no air space was one of the poorest solar radiation materials (this would hold true for any dark, opaque materials). When the canvas was elevated...
(3.5 inches) above the container, a marked improvement in the cooling effect was noted (+12 versus +27 temperature differential). Of the 15 materials tested, 8 materials were successful at maintaining temperature elevations of less than 10 degrees Fahrenheit above ambient, with all being classified as satisfactory thermal shielding materials. Eight materials appeared to be equivalent with the exception of a product containing 3.5 inches of insulation, (Ref: R13 Insulated White/Foil). Although this material was far superior at keeping temperatures closer to ambient, it appeared to be not practical for field applications.

8. During additional tests, interior temperature probes were placed within 120mm propellant charge metal containers to determine what heat was thermally conducted through the skin of the container.

120mm Propellant Charge Metal Container
Interior Temperatures
Exterior Protection

Table 4

<table>
<thead>
<tr>
<th>Sample Type</th>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Interior Temperature</th>
<th>Temperature Differential</th>
</tr>
</thead>
<tbody>
<tr>
<td>Canvas (3.5&quot; Space Int)</td>
<td>8-27</td>
<td>93</td>
<td>105</td>
<td>+12</td>
</tr>
<tr>
<td>DeWitt Int</td>
<td>9-25</td>
<td>85</td>
<td>100</td>
<td>+15</td>
</tr>
<tr>
<td>DeWitt Int</td>
<td>9-26</td>
<td>85</td>
<td>109</td>
<td>+24</td>
</tr>
<tr>
<td>Chase Int</td>
<td>9-4</td>
<td>94</td>
<td>98</td>
<td>+4</td>
</tr>
</tbody>
</table>

9. As noted in Table 4, temperature elevations within the containers ranged from 4 degrees Fahrenheit to 24 degrees Fahrenheit above ambient, and dependent on the type of cover being used. As was apparent during this test, the interior temperature is not directly related to the ambient temperature, but indirectly related to the amount and duration of solar exposure. For example, on two separate test dates ambient temperatures were at 85 degrees, while the interior
temperatures of DeWitt Company samples ranged from 15 degrees Fahrenheit to 24 degrees Fahrenheit above ambient.
B. **PALLET TESTS:**

1. During this test, temperature probes were placed on top as well as on intermittent layers within the pallets (second and fourth layers). Two pallets were used during this test: control pallet with no protection, and a covered (protected) pallet with 18 inches of air space.

Pallet Solar Radiation Test
Exterior Skin Temperatures
Canvas Covered, 18-Inches Above

Table 5

<table>
<thead>
<tr>
<th>Test Number</th>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Control Pallet</th>
<th>Test Pallet (Covered)</th>
<th>Temperature Differential</th>
</tr>
</thead>
<tbody>
<tr>
<td>Top Containers</td>
<td>Top Containers</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1</td>
<td>9-5</td>
<td>90</td>
<td>130</td>
<td>105</td>
<td>25</td>
</tr>
<tr>
<td>2</td>
<td>9-6</td>
<td>91</td>
<td>125</td>
<td>96</td>
<td>29</td>
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<tr>
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<td>9-10</td>
<td>82</td>
<td>125</td>
<td>92</td>
<td>33</td>
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<tr>
<td>4</td>
<td>9-11</td>
<td>85</td>
<td>130</td>
<td>96</td>
<td>34</td>
</tr>
<tr>
<td>5</td>
<td>9-12</td>
<td>85</td>
<td>122</td>
<td>92</td>
<td>30</td>
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</table>

Middle Layers

<table>
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<tr>
<th>Test Number</th>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Control Pallet</th>
<th>Test Pallet (Covered)</th>
<th>Temperature Differential</th>
</tr>
</thead>
<tbody>
<tr>
<td>Top Containers</td>
<td>Top Containers</td>
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<td></td>
<td></td>
<td></td>
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<tr>
<td>2</td>
<td>9-6</td>
<td>91</td>
<td>95</td>
<td>95</td>
<td>0</td>
</tr>
<tr>
<td>3</td>
<td>9-10</td>
<td>82</td>
<td>84</td>
<td>82</td>
<td>2</td>
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<tr>
<td>4</td>
<td>9-11</td>
<td>85</td>
<td>86</td>
<td>85</td>
<td>1</td>
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<tr>
<td>5</td>
<td>9-12</td>
<td>85</td>
<td>86</td>
<td>84</td>
<td>2</td>
</tr>
</tbody>
</table>

2. During the five tests conducted, the average temperature rise of the unprotected container was 39.6 degrees over ambient, or a 45.6 percent temperature increase on the exposed top container layer. The protected (canvas-covered) pallet, on the other hand, showed a 9.6 degree increase, or an 11.1 percent increase over ambient. For both pallets, temperature
increases in the middle container layers were 1-4 degrees over ambient. This clearly demonstrated that the outer containers of the pallet shielded the inner layers whether the pallet was protected or not.

3. Additional tests were conducted substituting canvas elevated above the pallet for sandbags placed directly on top of the ammunition. This test was to determine if materials readily available in SA could serve as solar radiation shields.

**Exterior Skin Temperatures**

**Sandbag-Covered**

<table>
<thead>
<tr>
<th>Test Number</th>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Control Pallet Temperature</th>
<th>Test Pallet Covered Temperature</th>
<th>Temperature Differential</th>
</tr>
</thead>
<tbody>
<tr>
<td>Top Containers</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1</td>
<td>9-13</td>
<td>85</td>
<td>115</td>
<td>88</td>
<td>27</td>
</tr>
<tr>
<td>2</td>
<td>9-15</td>
<td>78</td>
<td>105</td>
<td>78</td>
<td>28</td>
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<tr>
<td>2</td>
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</tr>
<tr>
<td>Fourth Layer Containers</td>
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<td></td>
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<td>9-15</td>
<td>78</td>
<td>79</td>
<td>78</td>
<td>1</td>
</tr>
</tbody>
</table>

4. During this test the top container layer of the unprotected pallet showed an average temperature increase of 27.5 degrees, or 34 percent over ambient (See Table 6). The sandbag-covered pallet, on the other hand, showed a 1.5 degree average temperature increase, or 2 percent over ambient. At different layers (within both pallets) there was very little difference in temperature, as noted previously.
5. Another pallet test evaluated a commercially available greenhouse shading material manufactured by DeWitt Company, Incorporated.

Pallet Solar Radiation Test
Exterior Skin Temperatures
DeWitt-Covered, 18-Inches Air Space

Table 7

<table>
<thead>
<tr>
<th>Probe Location</th>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Control Pallet</th>
<th>Test Pallet Covered</th>
<th>Temperature Differential</th>
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</thead>
<tbody>
<tr>
<td>Top Layer</td>
<td>9-21</td>
<td>63</td>
<td>90</td>
<td>63</td>
<td>27</td>
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<tr>
<td>Second Row</td>
<td>9-21</td>
<td>63</td>
<td>63</td>
<td>63</td>
<td>-0</td>
</tr>
</tbody>
</table>

6. The unprotected pallet showed a 27 degree rise (42.8 percent increase) over ambient, while the covered pallet remained at ambient temperature, indicating a very effective thermal shield. The effectiveness was undoubtedly enhanced by the 18-inch air space between the cover and the pallet.
C. MILVAN TESTING.

1. In the final series of tests, a MILVAN loaded with inert 105mm howitzer cartridges was instrumented. Temperature probes were located in the following locations: the MILVAN roof, internal top of the load, internal center of the load, and test site ambient temperature. Tests were conducted with the doors open and closed.

Milvan Solar Radiation Test
Exterior/Interior Temperatures

Table 8

<table>
<thead>
<tr>
<th>Test Number</th>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Milvan Roof</th>
<th>Milvan Top</th>
<th>Milvan Middle</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>9-5</td>
<td>91</td>
<td>135</td>
<td>120</td>
<td>99</td>
</tr>
<tr>
<td>2</td>
<td>9-6</td>
<td>92</td>
<td>130</td>
<td>115</td>
<td>96</td>
</tr>
<tr>
<td>3</td>
<td>9-7</td>
<td>81</td>
<td>116</td>
<td>108</td>
<td>94</td>
</tr>
<tr>
<td>4</td>
<td>9-8</td>
<td>81</td>
<td>127</td>
<td>109</td>
<td>91</td>
</tr>
<tr>
<td>5</td>
<td>9-9</td>
<td>82</td>
<td>129</td>
<td>114</td>
<td>95</td>
</tr>
<tr>
<td>6</td>
<td>9-10</td>
<td>85</td>
<td>135</td>
<td>120</td>
<td>97</td>
</tr>
<tr>
<td>Average</td>
<td></td>
<td>85</td>
<td>129</td>
<td>114</td>
<td>95</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Test Date</th>
<th>Ambient Temperature</th>
<th>Milvan Roof</th>
<th>Milvan Top</th>
<th>Milvan Middle</th>
</tr>
</thead>
<tbody>
<tr>
<td>9-11</td>
<td>80</td>
<td>122</td>
<td>101</td>
<td>84</td>
</tr>
<tr>
<td>9-12</td>
<td>82</td>
<td>118</td>
<td>102</td>
<td>85</td>
</tr>
<tr>
<td>9-13</td>
<td>84</td>
<td>129</td>
<td>108</td>
<td>87</td>
</tr>
<tr>
<td>Average</td>
<td>82</td>
<td>123</td>
<td>104</td>
<td>85</td>
</tr>
</tbody>
</table>

2. During this test solar radiation generated an average roof temperature of 129 degrees Fahrenheit (closed door) and 123 degrees Fahrenheit (open door). Of particular interest during this test was an average 10 degree temperature drop within the MILVAN when the doors were
open versus the doors being closed and the middle probe being within 3 degrees Fahrenheit of ambient on the open door MILVAN. This test demonstrated thermal convection (cooling effect) on the open-door MILVAN with hot air leaving the top and cooler air entering the bottom of the MILVAN.
PART 6

DISCUSSION

a. In lieu of protective covering, empty containers/boxes should be used as shielding materials both on the top and sides of the pallets to avoid solar radiation (reference inner layers remained close to ambient temperature with little heat transfer) with or without protective covering.

b. There is no direct correlation between ammunition skin temperature and ambient temperature, it is dependent on such variables as wind speed/direction, length of exposure, cloud cover, amount of particulate in the air, color, and thermal mass of the ammunition. All of these factors have an effect on the amount of solar radiation received by the ammunition.

c. Heat damage to ammunition cannot be determined by skin temperature probes alone, due to the thermal lag and heat transfer into the rounds. Therefore, internal thermal couples should be used on inert ammunition in the future to determine what temperature the ammunition is experiencing.

d. Sandbags covering ammunition appear to be a very suitable solar radiation cover for ammunition. Due to the mass of sandbags, wind would have little effect on the covering. This is an inherent problem with other thermal shields on how to keep them in place during high winds.

e. If MILVANs are used for ammunition storage, the doors should remain open with the door opening directed away from the sunlight.
PART 7

PHOTOGRAPHS
This photo is a typical example of a solar material screening test. Note, four different materials are being evaluated during this test.
Photo No. AO317-SPN-90-367-6386. This photo is a typical application of a thermal couple to 120mm metal container during solar radiation testing.
U.S. ARMY DEFENSE AMMUNITION CENTER AND SCHOOL - SAVANNA, IL

Photo No. AO317-SPN-90-367-6394. This photo is a typical test setup for pallet testing using 120mm tank rounds. Note, sandbags being evaluated during this test.
This photo is a typical example of MILVAN testing using inert 105mm cartridge HE. Note, ambient temperature and humidity probe on top of MILVAN during this test.
PART 8

GRAPHS
Solar Shield Test
Test Date: 08/17-20/90

1. Ambient
2. UnShielded
3. Insulated
4. Shielded

Container Temp (°F)

Time of Sample

Graph No. 1
Solar Shield Test
Test Date: 08/24-27/90

Cont. Temp. Deg. F


Time of Sample

1 14:30:39 2 8:17:19 3

1 65.00 2 85.00 3 95.00 4 105.00 5 115.00 6 125.00

1 Ambient
2 Int. Cntrl
3 Ext. Cntrl
4 Ins. Shld
5 Uns. Shld
6 Elv Canvas
7 Elv Camo

GRAPH NO. 2
Solar Shield Test
Test Date: 08/27-29/90

GRAPH NO. 4

1. Ambient
2. Control I
3. Control S
4. Elv Camo S
Solar Shield Test

Test Date: 08/30-31/90

Graph No. 7

Sample Time vs Temp. Deg. F

Legend:
1. Ambient
2. Control I
3. Control 5
4. 12589 I
5. 12589 S
Solar Shield Test
Test Date: 09/04-05/90

GRAPH NO. 8
Solar Shield Test
Test Date: 09/26-28/90

Temperature Deg. F

0 23:07:26  1 13:00:46  2 2:54:06  2 16:47:26
Time of Sample

1. Ambient
2. DEWITT Ext
3. Champn Int
4. Cntrl Int
5. Cntrl Ext
6. Shield Ext
7. DEWITT Int
8. AN35-40 Ex

GRAPH NO. 9
Solar Shield Test
Test Date: 09/05-06/90

Temperature Deg. F

Sample Time


1. Ambient
2. COV PLT T
3. UNC PLT T

GRAPH NO. 10
Solar Shield Test
Test Date: 09/05-06/90

1. Ambient
2. COV PLT M
3. UNC PLT M

Temperature

Sample Time

GRAPH NO. 11
Solar Shield Test
Test Date: 09/06-07/90

Graph No. 12
Solar Shield Test
Test Date: 09/07-10/90

1. Ambient
2. COV PLT T
3. UNC PLT T

Temperature Deg. F

Sample Time

GRAPH NO. 13
Solar Shield Test
Test Date: 09/07-10/90

- Ambient
- COV PLT M
- UNC PLT M

Temperature (Deg.)

Sample Time
0 14:26:28 1 14:19:48 2 8:06:28 3 11:53:08

GRAPH NO. 14
Solar Shield Test
Test Date: 09/14-17/90

Temperature (F)

Ambient
2LD EX PL
2LD SBPL

Time of Sample:
1 11:53:53
2 15:40:38
3 19:27:18

Graph No. 17
Solar Shield Test
Test Date: 09/06-07/90

① Ambient
② Milv Roof
③ Milv M. I
④ Milv I, I

Temperature Deg. F

Sample Time
Solar Shield Test
Test Date: 09/12-13/90

1. Ambient
2. Milv Roof
3. Milv M. I
4. Milv T. I

Sample Time

GRAPH NO. 21
Solar Shield Test
Test Date: 08/24-27/90
Solar Shield Test

Test Date: 08/27-29/90

Solar Rad W/M Sq.
Solar Shield Test

Test Date: 08/29-30/90

Solar Rad. kW/M Sq.

Sample Time

Graph No. 25
Solar Shield Test
Test Date: 08/30-31/90

Solar Rad KW/M Sq.

Sample Time
Solar Shield Test

Test Date: 09/04-05/90

Graph No. 27
Solar Shield Test
Test Date: 09/05-06/90

Solar Rad KW/M Sq.

Sample Time

GRAPH NO. 28
Solar Shield Test

Test Date: 09/06-07/90

Solar Rad K/M Sq.

Sample Time


Graph No. 29
Solar Shield Test
Test Date: 09/07/90

Solar Rad KW/M Sq.

0.00 0.20 0.40 0.60 0.80 1.00
0 9:33:10 0 10:56:30 0 12:19:50 0 13:43:10 0 15:06:30
Sample Time

Graph No. 30
Solar Shield Test
Test Date: 09/07-10/90

Sample Time

Solar Rad KW/M Sq.
Solar Shield Test
Test Date: 09/11/90

Sample Time

Graph No. 33
Solar Shield Test

Date: 09/11/12/90

Sample Time

Graph No. 34
Solar Shield Test
Test Date: 09/12-13/90

Solar Rad KWM Sq.

0.80

0.60

0.40

0.20

0.00

Sample Time

0 8:30:30

0 14:03:50

0 19:37:10

1 11:10:30

1 12:17:10

GRAPH NO. 35
Solar Shield Test
Test Date: 09/14-17/90

Sample Time

0 8:07:18
1 11:53:50
2 15:40:38
3 19:27:18

0.00
0.25
0.50
0.75
1.00
1.25
Solar Rad KW/M Sq.