

An analytical solution for benchmark problem 1: The "ideal" wedge

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Results from an exact analytical solution for the field in a wedge with pressure-release boundaries (benchmark problem 1) are presented in the form of transmission loss as a function of horizontal range from the source. These computed curves contain no significant error, and thus may be used as a primary benchmark for establishing the accuracy of range-dependent, numerical propagation models.

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INTRODUCTION

Over the past decade or so, several computer codes have been developed for calculating the sound field in complex underwater environments. These algorithms are based on numerical solutions of the wave equation (or related equations) and are very complicated, generally requiring long run times to arrive at a final estimate of the field. Most, if not all, of these codes are based on some more or less subtle form of approximation. After many hours of CPU time, when the estimate for the field is finally produced, the question inevitably arises: How accurate is the result?

There is no simple answer to this enquiry because, for most range-dependent ocean channels, no reference solution exists. This problem has been recognized by the ocean acoustics community for some time, and was addressed recently in two "benchmark" sessions at consecutive meetings of the Acoustical Society of America. At the first of these meetings, three range-dependent problems were specified, benchmarks 1, 2, and 3, to be used as test cases for comparing the various propagation models, one with another. The details of these three problems are given by Jensen and Ferla¹ in this issue of the *Journal of the Acoustical Society of America*.

The purpose of this paper is to present an analytical solution for benchmark problem 1, which is the two-dimensional, "ideal" wedge problem: The acoustic field is required in a wedge, with pressure-release boundaries, which contains a line source parallel to the apex. This is one of the few range-dependent problems with an exact analytical solution. The form of this solution is outlined below, and transmission loss results evaluated from it are given graphically. Comments are included about the evaluation procedure and the care that was exercised to eliminate errors.

I. THE ANALYTICAL SOLUTION

Figure 1 shows the geometry of the wedge and the cylindrical coordinates used in the analysis. The medium supporting the field is a homogeneous fluid, the line source is parallel to the apex, and the boundaries are plane, pressure-release surfaces.

The procedure used to obtain an expression for the field is to apply two integral transforms to the inhomogeneous Helmholtz equation, a finite Fourier sine transform, and a Hankel transform. On taking the inverse transforms, the velocity potential is found to be the following sum of uncoupled normal modes:

$$\Psi = \frac{2}{\theta_0} \sum_{m=1}^{\infty} I_m(r, r') \sin(v\theta) \sin(v\theta'), \quad (1)$$

where θ_0 is the wedge angle, r and r' are the ranges of the receiver and source from the apex of the wedge, θ and θ' are the angular depths of the receiver and source measured about the apex, and

$$v = m\pi/\theta_0. \quad (2)$$

The mode coefficients in Eq. (1) are

$$I_m(r, r') = \int_0^{\infty} \frac{p}{p^2 - k^2} J_m(pr) J_m(pr') dp, \quad (3)$$

where k is the wavenumber of the source radiation and $J_m(\cdot)$ is a Bessel function of the first kind of order m . The integral in Eq. (3) is Hankel's discontinuous integral, which is equal to the product of a Bessel function and a Hankel function.² When this result is substituted into Eq. (1), the final expression for the field is found to be

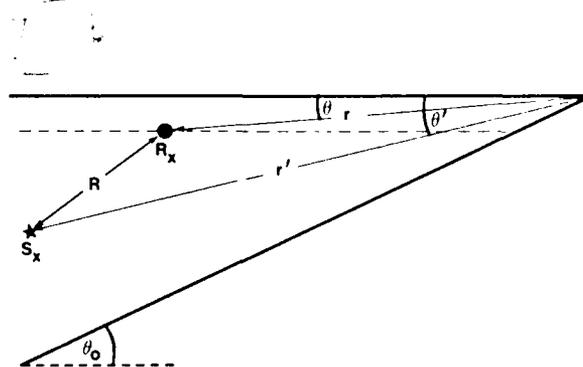


FIG. 1. Coordinates of the source, S_x , and receiver, R_x , in the ideal wedge. The wedge angle is θ_0 , and the radial distance between the source and receiver is R .

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$$\Psi(r,r',\theta,\theta') = \frac{i\pi}{\theta_0} \sum_{m=1}^{\infty} J_{\nu}(kr_0) H_{\nu}^{(1)}(kr_0) \times \sin(\nu\theta)\sin(\nu\theta'), \quad (4)$$

where $r_0 = \min(r,r')$, $r_1 = \max(r,r')$, $i = (-1)^{1/2}$, and $H_{\nu}^{(1)}(\cdot)$ is the Hankel function of the first kind of order ν .

The expression for the velocity potential in Eq. (4) is exact and valid for all wedge angles (i.e., it is not restricted to wedge angles that are submultiples of π). Thus it includes the effect of diffraction by the apex of the wedge, as well as the image component of the field.

For comparison with other solutions for the field in the wedge, the expression in Eq. (4) is to be normalized to the field at 1 m from a line source in an unbounded homogeneous medium. Now, the velocity potential of the field generated by a line source in an infinite medium is

$$\Phi(R) = (i/4)H_0^{(1)}(kR), \quad (5)$$

where R is the radial distance from the source to the field point and $H_0^{(1)}(\cdot)$ is the Hankel function of the first kind of order zero. This result, which depends on just one spatial coordinate R , is well known.³ One method of deriving it is to apply a Hankel transform to the Helmholtz equation, followed by the inverse transformation. Equation (5) represents cylindrical spreading and shows a logarithmic singularity at the origin, $R = 0$.

With R set equal to 1 m, the normalized field in the wedge is

$$\Lambda = |\Psi(r,r',\theta,\theta')|/|\Phi(1)|, \quad (6)$$

and the transmission loss in dB is

$$TL = 20 \log_{10}(\Lambda). \quad (7)$$

This expression was evaluated for a fixed receiver depth as a function of horizontal range from the source to the apex.

II. THE COMPUTATIONS

Full details of the parameter values for benchmark problem 1 are listed in Table I of Ref. 1, and the source/receiver configuration in the wedge is illustrated in Fig. 1 of Ref. 1. Note that the sound speed of interest is $c = 1500$ m/s, the frequency is 25 Hz, and the wedge angle is $\theta_0 = \arctan(1/20) = 2.862405^\circ$. The source is at a horizontal range of 4 km from the apex of the wedge, at a depth of 100 m. This is midway down the water column, which is 200 m deep at the source position.

Equation (7) was evaluated with these parameter values on a VAX 11/750 computer, using double precision throughout, for 1000 evenly spaced horizontal range points at a depth of 30 m. A standard Bessel function package known as VAXMATH⁴ (also known as SLATEC) and asymptotics were used to evaluate the Hankel and Bessel functions. With 100 modes in the summation for the field in the wedge, the calculation of TL took less than 2 min. of CPU time.

Computational difficulties can arise with the imaginary part of the Hankel function [i.e., the Neumann function $Y_{\nu}(x)$] when the order ν becomes large relative to the argument x : for a fixed value of x , $Y_{\nu}(x) \rightarrow -\infty$ as $\nu \rightarrow \infty$. We tested the VAXMATH calculations against tabulated results published by Abramowitz and Stegun⁵ for a wide range

of values, including $(x,\nu) = (1,20), (2,30), (5,50), (10,50), (40,50), (50,50), (50,100),$ and $(100,100)$, and found exact agreement. We also tested the Debye asymptotic expansions for large ν (Eqs. 9.3.7 and 9.3.8 in Abramowitz and Stegun⁵), using only the first two terms, and found very good agreement (to three significant figures) with the corresponding tabulated values in Ref. 5. The latter checks were performed because, when the value of Y_{ν} dropped below -10^{10} , we switched from VAXMATH to Debye asymptotics.

In the benchmark problem, only odd-order modes are excited, since the source is symmetrically placed in the channel at middepth. Moreover, since $kr \approx 400$ and $\nu = (62.9 \times \text{mode number})$, we see that only modes 1, 3, and 5 will propagate through the wedge. However, in the immediate vicinity of the source, many more terms must be included in the mode sum to achieve acceptable accuracy, that is, to give the correct nearfield behavior. We considered as many as 1000 modes for field computations at the source depth, in an attempt to examine nearfield and normalization effects, but there was no perceptible difference between transmission loss (TL) curves, plotted on a scale of 4 dB/cm, based on sums containing 100 modes and 1000 modes. Moreover, for $R > 120$ m (i.e., two wavelengths at 25 Hz), where R is the range from the source, these plots were no different from a plot derived from a summation of only five modes. Thus we feel confident that our results based on sums of 100 modes contain no significant truncation errors.

III. RESULTS

Figure 2 shows the transmission loss calculated from Eq. (7) for benchmark problem 1. TL is shown as a function of horizontal range measured from the source of increments of 4 m, at a depth of 30 m. The field shows rapid spatial fluctuations at ranges up to 3.4 km, which is the cutoff range (measured from the source) of the first mode. The structure of these fluctuations changes at a range of 2.2 km, which is the cutoff range of the third mode. Thus at ranges between 2.2 and 3.4 km, only the first mode contributes to the field, which shows a more regular structure than at shorter ranges, where two or more modes interfere.

In the region where only the first mode is present, the

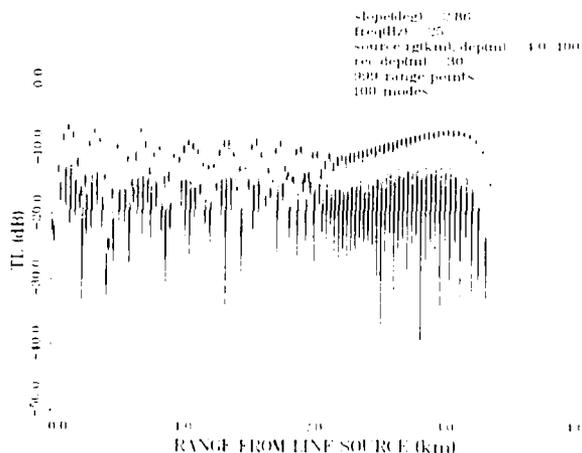


FIG. 2. Transmission loss as a function of horizontal range from the source, calculated from Eq. (7) for a receiver depth of 30 m a frequency of 25 Hz, and a wedge angle of 2.86 deg.

Wide-angle parabolic equation solutions to two range-dependent benchmark problems

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Numerical solutions are presented to two benchmark problems involving acoustic propagation in range-dependent media. The two problems deal with: (1) upslope propagation in a wedge-shaped channel with a penetrable bottom, and (2) propagation in a plane-parallel waveguide with a range-varying sound-speed profile. The solutions are based on a pair of wide-angle, variable-density, parabolic equations, one of which is solved using a finite-difference algorithm while the other is solved using a split-step algorithm.

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INTRODUCTION

Two benchmark problems involving acoustic propagation in range-dependent media were recently proposed for numerical consideration.¹ Numerical solutions to these problems were subsequently presented at a special session of the 113th Meeting of the Acoustical Society of America. Problem I dealt with upslope propagation in a wedge-shaped channel for: (a) a rigid and (b) a penetrable sloping-bottom boundary. Problem II dealt with propagation in a plane-parallel waveguide with a range-dependent sound-speed profile. This paper presents numerical solutions to problems I(b) and II using a computer code based on a pair of wide-angle, variable-density parabolic equations.

The development and use of the parabolic equation (PE) approximation in ocean acoustics is reviewed elsewhere.³⁻⁵ Unlike the (elliptic) wave equation, parabolic equations contain only first derivatives in the range variable, and so allow efficient numerical solution by noniterative marching techniques. This numerical advantage is achieved by (a) neglecting backscatter, and (b) limiting the angular aperture of the forward-scattered waves. Because of (a), the outgoing waves in a range-independent waveguide formally satisfy a single first-order equation containing a square-root operator. As a result of (b), different approximations to this operator give rise to different parabolic equations.

The first numerical solutions to the standard parabolic equation of ocean acoustics appeared during 1973-1974 and were obtained using the split-step algorithm.⁶⁻⁸ Based on a presentation by F. D. Tappert,⁹ a split-step version was implemented at DREP by 1975 where it was used to assess some bottom-limited propagation data provided by NUSC.^{10,11} When acoustic waves interact significantly with the ocean bottom, however, the rapid variations in sound speed and density can be accommodated more easily using finite-difference methods.¹²⁻¹⁴ For this reason, a finite-difference version was developed at DREP to accommodate the test cases examined at a PE workshop held in 1981.¹⁵

In recent years, wide-angle approximations to the square-root operator have been proposed that result in para-

bolic equations that are more accurate than the standard PE.¹⁶⁻²¹ At the same time, advances in computer technology have produced smaller and faster machines with which to compute the acoustic field. By 1984, the merging of PE software with dedicated hardware for generating and displaying numerical PE solutions had been effected.²²⁻²⁴ As a result of these software and hardware improvements, DREP has proceeded with the development of a high-speed, stand-alone, computer and display system based on the PE model for making sonar performance predictions at sea.²⁵ The numerical solutions presented in this paper were obtained using a pair of variable-density, wide-angle, parabolic equations that form the basis for this shipboard system.

The rest of the paper is organized in the following way. In the next section, a brief review of the approximations that underlie the pair of DREP parabolic equation codes is given. This is followed by a simple error analysis that compares the inherent accuracy of the two wide-angle approximations. Section III contains the detailed split-step and finite-difference numerical solutions to problems I(b) and II. Finally, the paper concludes with a summary of the numerical results.

I. BASIC THEORY

Let the region $z > 0$ (z positive down) of a cylindrical coordinate system (r, θ, z) contain an inhomogeneous oceanic waveguide, and let $p(r, z) \exp(-i\omega t)$ represent the azimuthally symmetric, time-harmonic acoustic field due to a point source located at $r = 0, z = z_0$. For $r > 0$, the pressure $p(r, z)$ satisfies the variable-density acoustic wave equation

$$\nabla^2 p + k_0^2 (n^2 + 2i\alpha/k_0) p - (\nabla_r^2 / \rho) \cdot \nabla p = 0, \quad (1)$$

where $n(r, z) = c_0/c(r, z)$ is the refractive index, $c(r, z)$ is the sound speed, $\rho(r, z)$ is the density, and $\alpha(r, z) \ll k_0$ is the absorption. Here $k_0 = \omega/c_0$ is an arbitrary reference wavenumber.

In regions where ρ is constant, the farfield ($k_0 r \gg 1$) pressure can be determined by solving the "one-way" operator equation for the outgoing field ψ :^{3,4}