

AD-A225 468

Center for Night Vision and Electro-Optics

AMSEL-NV-TR-0093

Model Tank Reflectance Study at Two Wavelengths

by

Jay A. Fox
and
Cynthia R. Gautier

JUNE 1990

Approved for public release; distribution unlimited.



DTIC
ELECTE
AUG 21 1990
D

FORT BELVOIR, VIRGINIA 22060-5677

**Destroy this report when it is no longer needed.
Do not return it to the originator.**

**The citation in this report of trade names of
commercially available products does not constitute
official endorsement or approval of the use of such
products.**

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE

REPORT DOCUMENTATION PAGE				Form Approved OMB No. 0704-0188	
1a. REPORT SECURITY CLASSIFICATION Unclassified		1b. RESTRICTIVE MARKINGS None			
2a. SECURITY CLASSIFICATION AUTHORITY		3. DISTRIBUTION/AVAILABILITY OF REPORT Approved for public release; distribution unlimited.			
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE					
4. PERFORMING ORGANIZATION REPORT NUMBER(S) AMSEL-NV-TR-0093		5. MONITORING ORGANIZATION REPORT NUMBER(S)			
6a. NAME OF PERFORMING ORGANIZATION CECOM, Center for Night Vision and Electro-Optics (C ² NVEO)		6b. OFFICE SYMBOL (If applicable) AMSEL-RD-NV-LR	7a. NAME OF MONITORING ORGANIZATION		
6c. ADDRESS (City, State, and ZIP Code) Fort Belvoir, VA 22060-5677		7b. ADDRESS (City, State, and ZIP Code)			
8a. NAME OF FUNDING/SPONSORING ORGANIZATION Same	8b. OFFICE SYMBOL (If applicable) Same	9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER DAAB07-88-C-F200			
8c. ADDRESS (City, State, and ZIP Code) Same		10. SOURCE OF FUNDING NUMBERS			
		PROGRAM ELEMENT NO.	PROJECT NO.	TASK NO.	WORK UNIT ACCESSION NO.
11. TITLE (Include Security Classification) Model Tank Reflectance Study at Two Wavelengths (U)					
12. PERSONAL AUTHOR(S) Jay A. Fox and Cynthia R. Gautier					
13a. TYPE OF REPORT Final		13b. TIME COVERED FROM <u>Jan 89</u> TO <u>Apr 89</u>		14. DATE OF REPORT (Year, Month, Day) June 1990	
15. PAGE COUNT 32					
16. SUPPLEMENTARY NOTATION					
17. COSATI CODES			18. SUBJECT TERMS (Continue on reverse if necessary and identify by block number)		
FIELD	GROUP	SUB-GROUP			
			7 Reflectance, CO ₂ , Near-IR. Shortley and Fox 7/89		
19. ABSTRACT (Continue on reverse if necessary and identify by block number)					
A scale model laboratory investigation was conducted wherein lasers operating at 1.52 μ m and 10.6 μ m irradiated a painted scale model of an M60A1 tank with realistic spot sizes for varying aspect angles and the resulting retroreflections were measured. <i>Keywords</i>					
20. DISTRIBUTION/AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS REPORT <input type="checkbox"/> DTIC USERS			21. ABSTRACT SECURITY CLASSIFICATION Unclassified		
22a. NAME OF RESPONSIBLE INDIVIDUAL Cynthia R. Gautier		22b. TELEPHONE (Include Area Code) 703-664-4287		22c. Office Symbol AMSEL-RD-NV-LR	

DD Form 1473, JUN 86

Previous editions are obsolete.

SECURITY CLASSIFICATION OF THIS PAGE

UNCLASSIFIED

PREFACE

An important tool for evaluating the expected performance of laser radar systems is computer modeling. When a target is irradiated by a known amount of laser energy, it is a straightforward exercise to calculate the amount of reflected energy detected by the system and thereby compute the signal-to-noise (S/N) ratio and thus infer system performance. Typical systems that can be evaluated in this manner include laser radars for ranging, imaging, vibration sensing, obstacle avoidance, and chemical sensing.

One vital parameter in this calculation is the target reflectance which is directly proportional to the S/N ratio. How does one determine the proper value to use for a typical painted military target? At first glance, it might appear that a straightforward bidirectional reflectance measurement of a painted metal plate would yield a useful value; but realistic targets such as tanks have geometrically complex structures which could substantially modify the flat plate result in at least two ways. First, multiple reflections could have the effect of reducing the return. On the other hand, it could be contended that since the target is fairly specular at long laser wavelengths (say $10\mu\text{m}$), there will always be some aspect of the target oriented so as to give rise to a specular return (glint) which could increase the effective reflectance. Thus, there are two possibilities which affect the reflectance in opposite senses. To further complicate matters, typical laser systems can operate with wavelengths that differ by a factor of ten; e.g., $1.06\mu\text{m}$ for Nd:YAG vs. $10.6\mu\text{m}$ for CO_2 . It is not difficult to imagine that target structure and target specularity effects might be wavelength dependent and thereby affect the reflectance differently.

In order to determine the effect of these issues on target reflectance and to obtain useful values for realistic targets, it was decided to conduct a scale model laboratory investigation at two widely varying wavelengths. Lasers operating at $1.52\mu\text{m}$ and $10.6\mu\text{m}$ irradiated a painted scale model of an M60A1 tank with realistic spot sizes for varying aspect angles, and the resulting retroreflections were measured. A detailed description of the experiment follows.

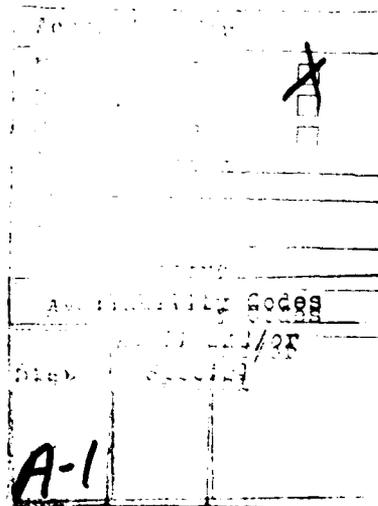


TABLE OF CONTENTS

	Page
SECTION I. EXPERIMENTAL SETUP AND PROCEDURE.....	1
Description of the 10.6 μ m Apparatus	1
Description of the 1.52 μ m Apparatus	1
Targets and Coatings	1
Measurement Procedure	2
SECTION II. EXPERIMENTAL RESULTS.....	3
Reflectance Dependence on Aspect Angle	3
Effective Tank Reflectivity	4
SECTION III. DISCUSSION AND CONCLUSIONS	5
APPENDIX OF FIGURES.....	A-1

SECTION I. EXPERIMENTAL SETUP AND PROCEDURE

DESCRIPTION OF THE 10.6 μ m APPARATUS

A diagram of the experimental setup appears in Figure 1 (page A-2). A Line Lite Model 950 CO₂ laser produced an 8W maximum CW beam. The beam was attenuated by means of a variable polarizer so as to not saturate the detectors or heat the model tank target. The beam was chopped via a Laser Precision Model CTX-534 variable speed chopper, referenced to an EG&G Princeton Applied Research Model 5301 lock-in amplifier. A 50% beamsplitter was used to allow for relative measurement of the outgoing power via an HgCdTe detector and a Scientech power meter. The remainder of the beam passed through a variable beam expander, enlarging the beam to a circular spot of approximately 15.5mm diameter at the target. This was done in order to simulate the spot size (approximately 0.5m) of a beam that would be incident upon a realistic military target at a range of 1km. The retroreflected power was focussed onto a moveable PbSnTe detector and was displayed on the lock-in amplifier. An Optical Engineering, Inc. CO₂ spectrum analyzer was available to ascertain that the laser was operating at 10.6 μ m.

DESCRIPTION OF THE 1.52 μ m APPARATUS

A diagram of the experimental setup appears in Figure 2 (page A-3). A Melles Griot Model 05-SIR-871 1.52 μ m HeNe laser produced a 5mW maximum, randomly polarized, CW beam. This beam was also attenuated by means of a variable filter to reduce power levels in order to avoid saturation and heating effects. The beam was chopped with reference to the lock-in amplifier and expanded to the appropriate size as was done in the CO₂ experiment. Since the laser was previously determined to have stable output power after a 1-hour warm-up period, only a periodic measurement of relative outgoing power was necessary. The retroreflected power was focussed onto the 2mm element of a SPEX Model 1429A IR detector and was again displayed on the lock-in amplifier. A video camera was available to view the beam via illumination by a UV lamp and thus beam position was easily displayed on a black and white video monitor.

TARGET AND COATINGS

A 1/35 scale plastic model of an M60A1 tank was used as the target in these experiments, positioned on a variable-height turntable calibrated in degree increments. This type of mount allowed the beam to be positioned at different heights on the tank target at all aspect angles. A sample of canvas with previously characterized reflectivity was mounted on cardboard and periodically placed on the turntable, as indicated in Figures 1 and 2. This was done for the purpose of normalizing the relative measurements made on the tank model to true values of reflectivity.

Two types of paint were used as coatings for the tank: a US Army Green-383 polyurethane CARC, and a commercially available polyurethane green gloss enamel (Red Devil G13 Lawn Green). The former paint is referred to as "flat" and the latter as "glossy" which describes the visible appearance of the paint. It has been reported in the past that some threat vehicles are of a glossier nature than domestic vehicles. Hence, the glossy paint was used in addition to the flat so that any differences in the specularities of the paints could be investigated. The tank model was sprayed with each paint thick enough to ensure opacity at each wavelength of interest. Figure 3 (page A-4), shows actual photographs of the tank model covered with each paint.

MEASUREMENT PROCEDURE

As indicated earlier, the tank model was irradiated at three levels: 24, 48, and 72mm heights, as shown in Figure 4 (page A-5) which correspond to 0.84, 1.68, and 2.52m heights on an actual tank. At each aim level, relative measurements of reflected power were taken, starting with a frontal aspect angle, then every 10 degrees of a 360 degree rotation. Measurements were also taken at 2-degree increments in a 10-degree region centered about the most normal aspects (front, sides, and rear of the tank) due to increased specularities in these areas. The short-term power fluctuations of the 10.6 μ m laser required that a four-sample average be taken at each position. The measurements were later corrected for any fluctuations in outgoing power using simultaneously recorded values of the reference power levels. Measurements were also normalized at a later time to those taken with the canvas sample at the beginning of each aim level sequence so that calibrated values of reflectivity could be obtained.

SECTION II. EXPERIMENTAL RESULTS

REFLECTANCE DEPENDENCE ON ASPECT ANGLE

Figures 5 and 6 (pages A-6 and A-7) show the $10.6\mu\text{m}$ retroreflectance at the three aim points as a function of aspect angle for the tank painted flat green and gloss green, respectively. Figure 7 (page A-8) provides a direct comparison of the effect of paint specularity at $10.6\mu\text{m}$. In this graph, the retroreflectance has been averaged over the three aim points. Figures 8, 9, and 10 (pages A-9, A-10, and A-11) depict the results of similar experiments performed with $1.52\mu\text{m}$ radiation impinging on the target. The following observations were made.

10.6 μm Case

1. The typical return from the flat green target was higher than that from the glossy green target.
2. Relatively few highly specular glints appeared for either paint, and even then they were confined to narrow angular cones centering about 180° for the flat paint and 90° , 180° , and 270° for the glossy paint. As expected, the glint returns were stronger for the glossy paint.
3. When there was a significant difference, the middle aim point of the target usually provided a higher glint return than either of the other two areas. This was particularly true for the gloss green case, and to a lesser extent for the flat green coating.
4. With the exception of the narrow glint areas mentioned above, the tank retroreflectance did not show a significant dependence on aspect angle.

1.52 μm Case

1. In contrast with the $10.6\mu\text{m}$ case, now the typical return from the flat green target was about equal to that reflecting from the glossy painted tank.
2. As in the $10.6\mu\text{m}$, relatively few highly specular glints appeared for either color, with those confined to narrow cones centered around 90° , 180° , and 270° . Evidently, the effects of specularity are much less for $1.52\mu\text{m}$ radiation than for the $10.6\mu\text{m}$ case.
3. As in the $10.6\mu\text{m}$ case, when there was a significant difference, the middle aim point of the target usually provided a higher glint return than either of the other two areas. However, in this situation, a difference was only noticeable for the gloss green coating.

4. The tank retroreflectance exhibited even less dependence on aspect angle than it did for the 10.6 μ m case.

EFFECTIVE TANK REFLECTIVITY

While the previous results may be instructive in a general sense, they do not directly address the issue of which value target reflectance to use when evaluating the effectiveness of a rangefinder. To some extent, the value obviously depends upon the aspect angle of the tank. Thus, in order to evaluate this quantity, the previous observations must be casted in a more analytic manner. One may account for the possibility of observing a target oriented at a random aspect angle and thereby calculate the probability $P(R)$ that any observation will result in a measured retroreflection value greater than R . These calculations were performed and Figures 11, 12, 13, and 14 (pages A-12 through A-15) are plots of this probability for the tank coated with both paints and irradiated at the three levels with both 10.6 μ m and 1.52 μ m radiation. Figures 15 and 16 (pages A-16 and A-17) are averages of those graphs. The abscissa has been expressed as absolute reflectivity by means of direct comparison with a known canvas standard. The following observations were made.

10.6 μ m Case

1. Most of the time, there was not a significant difference among the three aim points for the glossy coating.
2. For the flat green coating, aiming at the turret slightly increased the probability of a high reflectance return, but the increase probably has marginal value.
3. On the average, most of the time reflectivity values about 1% and 3% were typical for this target when coated with glossy and flat paints, respectively.

1.52 μ m Case

1. Most of the time, there was a significant advantage in aiming at the turret as opposed to the wheels for the glossy coating.
2. For the flat coating, this advantage was minimal and probably of no practical use.
3. On the average, most of the time reflectivity values of about 24% were typical for this target when coated with either type paint.

SECTION III. DISCUSSION AND CONCLUSIONS

It has been shown that the effective reflectance of an M60A1 tank model was about 3% at 10.6 μm and about 24% at 1.52 μm when the coating was flat polyurethane green paint. Using a glossy green coating, the value at 10.6 μm decreased to about 1% and did not significantly change the result for 1.52 μm . In addition, separate measurements showed that a flat plate painted with the same coatings had reflectivities of about 6 to 7% at 10.6 μm and 30% at 1.52 μm . The following conclusions were drawn from these facts.

1. A geometrically complex target has a reduced reflectance compared to a flat plate. This effect was more pronounced at 10.6 μm than at 1.52 μm . The cause of this effect was probably multiple reflections of the radiation. The wavelength dependence seemed to be reasonable since these coatings were more specular at longer wavelengths.
2. A target coated with glossy paint exhibited a considerable reflectivity loss at 10.6 μm .

Naturally, inherent possible flaws exist in modeling experiments. Not only are the textures of real surfaces different than that of the model, but environmental effects will almost surely be an important factor. For example, will a tank painted a flat color still exhibit a non-specular nature after emerging from a rainstorm? What about the effect of dirt/mud and obscurants on the surface of a tank? Clearly, full scale tests under realistic conditions are needed to completely answer these questions. However, the results presented in this report should be of value in providing practical estimates until the full scale data are available.

APPENDIX OF FIGURES

Figure	Caption	Page
1	Schematic diagram of the 10.6 μ m apparatus.....	A-2
2	Schematic diagram of the 1.52 μ m apparatus.....	A-3
3	Side aspect of the model painted with flat coating (top) and with gloss coating (bottom).....	A-4
4	Three aim points corresponding to scaled heights of 0.84, 1.68, and 2.52 meters	A-5
5	Retroreflectance at 10.6 μ m for the flat coating	A-6
6	Retroreflectance at 10.6 μ m for the gloss coating	A-7
7	Retroreflectance at 10.6 μ m for both coatings. Each reflectance value is the average over the three aim points	A-8
8	Retroreflectance at 1.52 μ m for the flat coating	A-9
9	Retroreflectance at 1.52 μ m for the gloss coating	A-10
10	Retroreflectance at 1.52 μ m for both coatings. Each reflectance value is the average over the three aim points	A-11
11	The probability that an observation of the target will result in a measured reflectivity greater than R. The irradiating wavelength is 10.6 μ m and the coating is flat green	A-12
12	The probability that an observation of the target will result in a measured reflectivity greater than R. The irradiating wavelength is 10.6 μ m and the coating is gloss green	A-13
13	The probability that an observation of the target will result in a measured reflectivity greater than R. The irradiating wavelength is 1.52 μ m and the coating is flat green	A-14
14	The probability that an observation of the target will result in a measured reflectivity greater than R. The irradiating wavelength is 1.52 μ m and the coating is gloss green	A-15
15	The probability that an observation of the target will result in a measured reflectivity greater than R. Both coatings are shown. The irradiating wavelength is 10.6 μ m and each point has been averaged over the three aim points	A-16
16	The probability that an observation of the target will result in a measured reflectivity greater than R. Both coatings are shown. The irradiating wavelength is 1.52 μ m and each point has been averaged over the three aim points	A-17

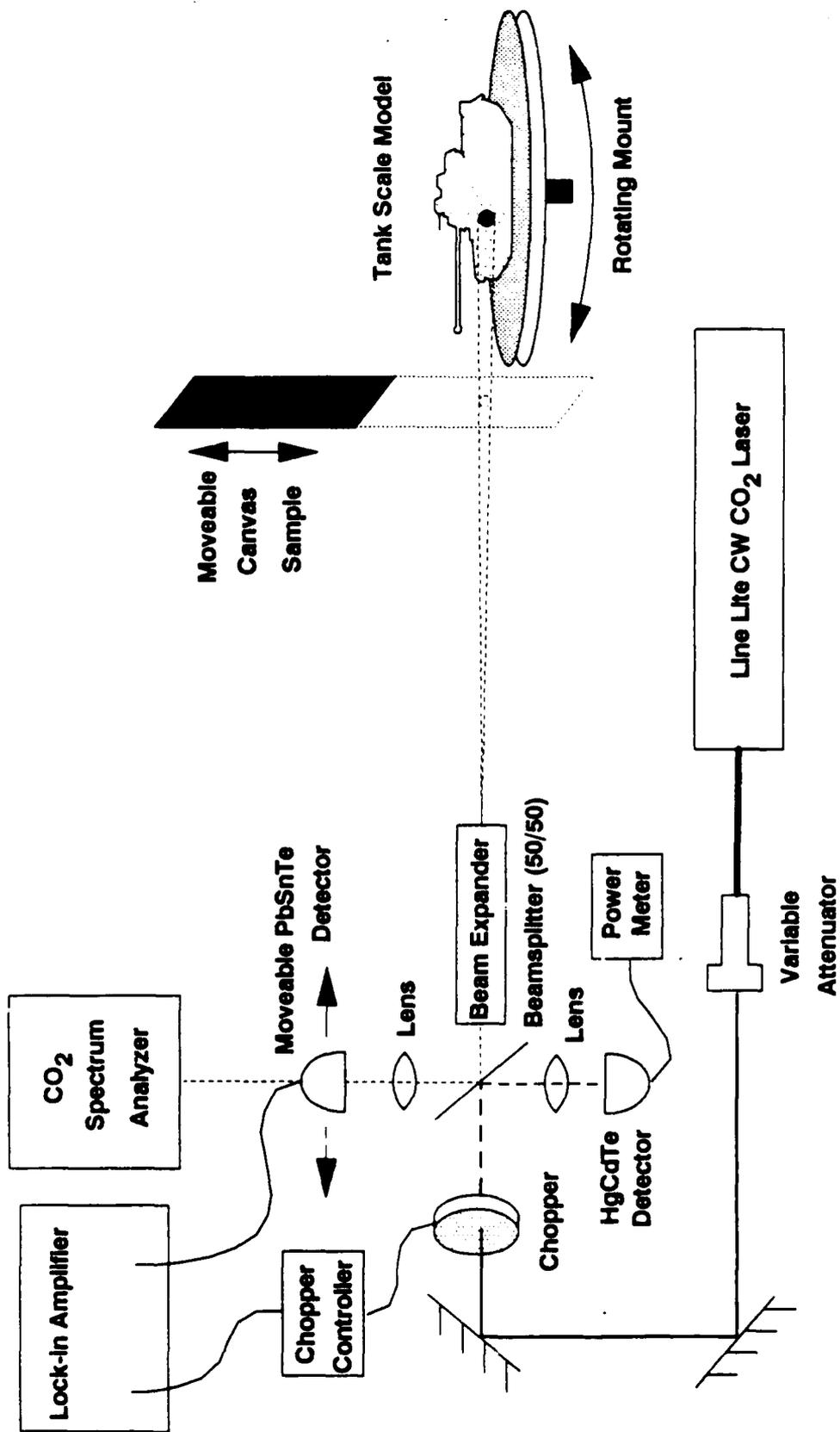


Figure 1. Schematic diagram of the 10.6 μm apparatus

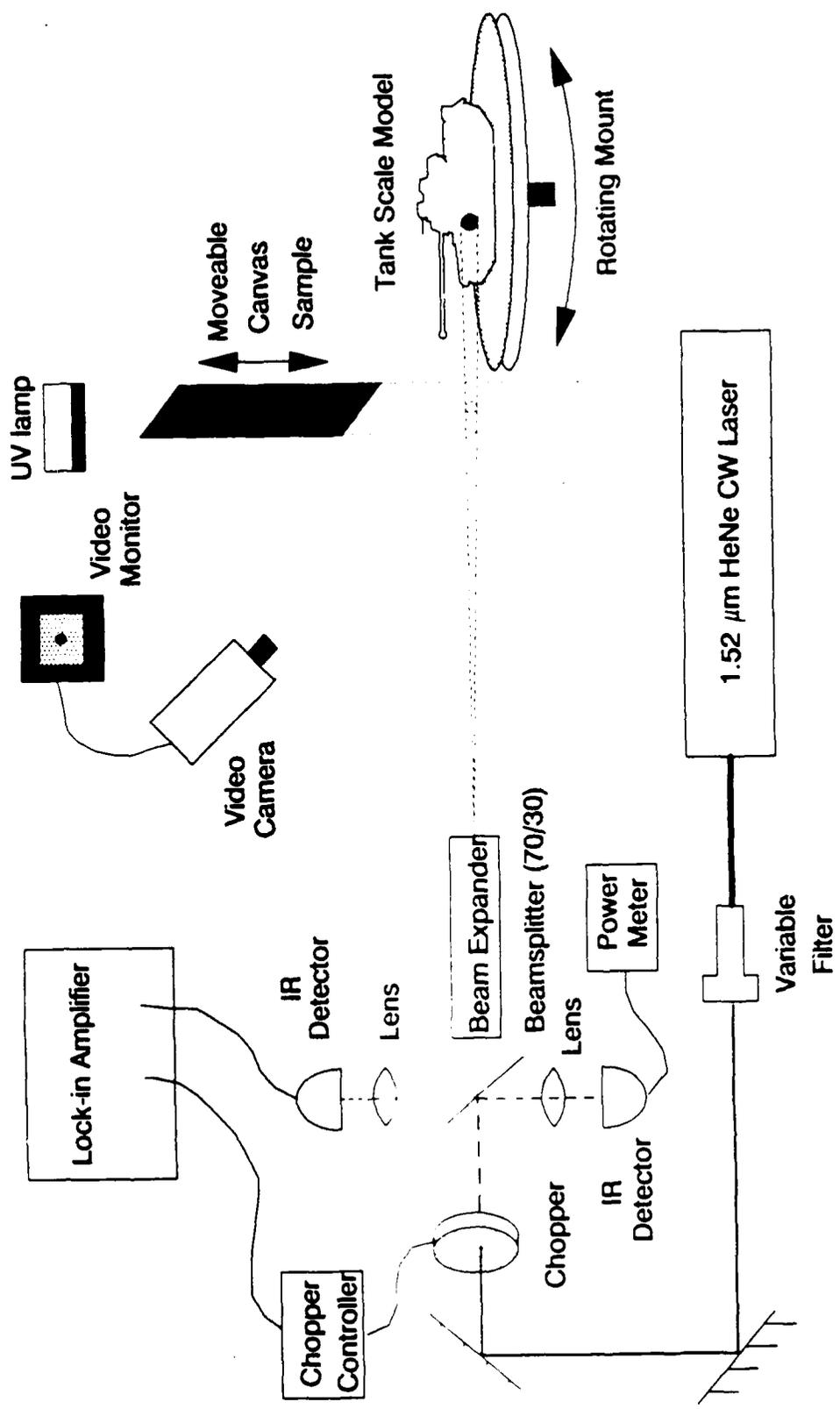


Figure 2. Schematic diagram of the 1.52 μm apparatus



Figure 3. Side aspect of the model painted with flat coating (top) and with gloss coating (bottom)



Figure 4. Three aim points corresponding to scaled heights of 0.84, 1.68, and 2.52 meters

10.6 μm - Flat Green

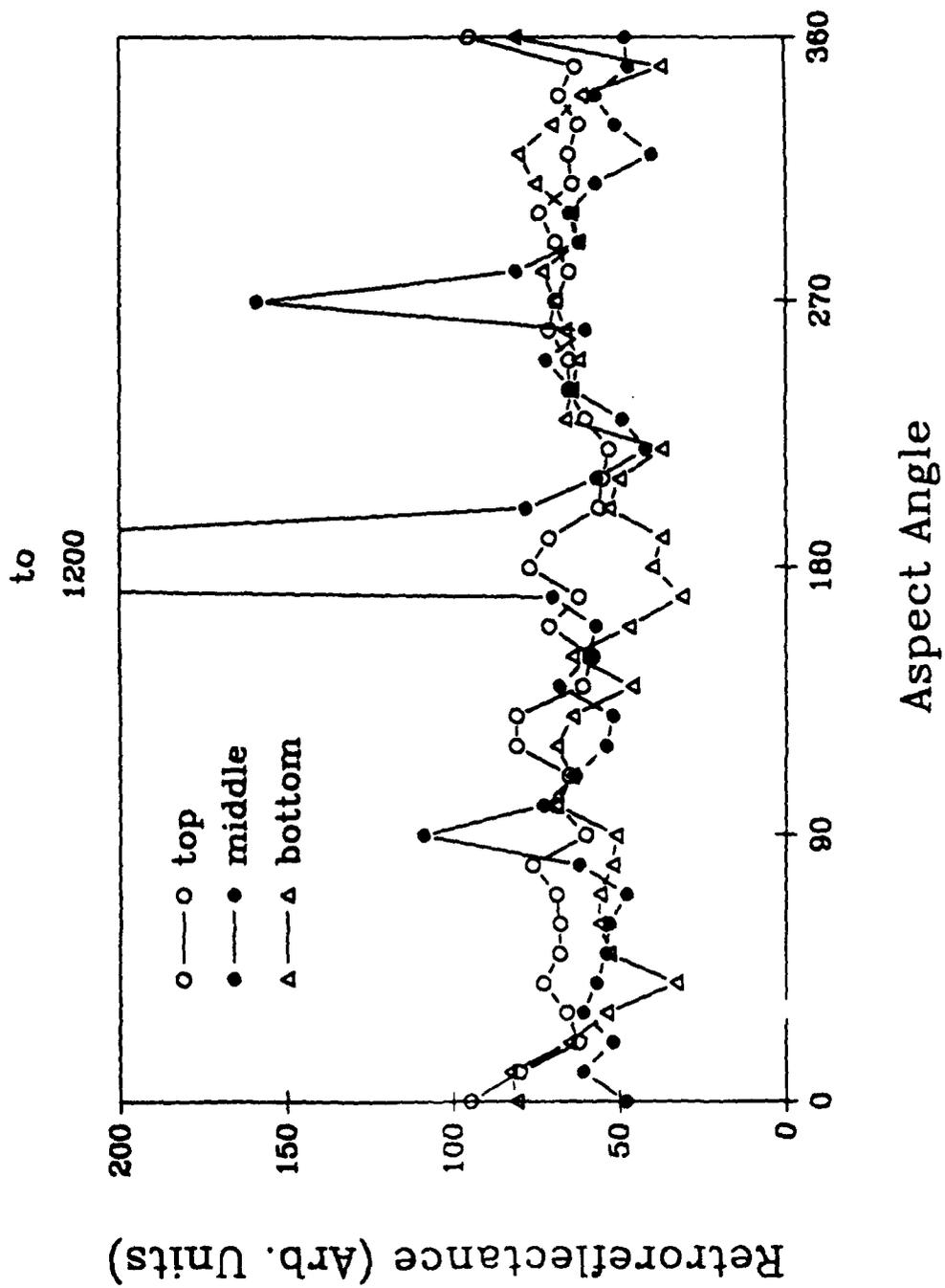


Figure 5. Retroreflectance at 10.6 μm for the flat coating

10.6 μm - Gloss Green

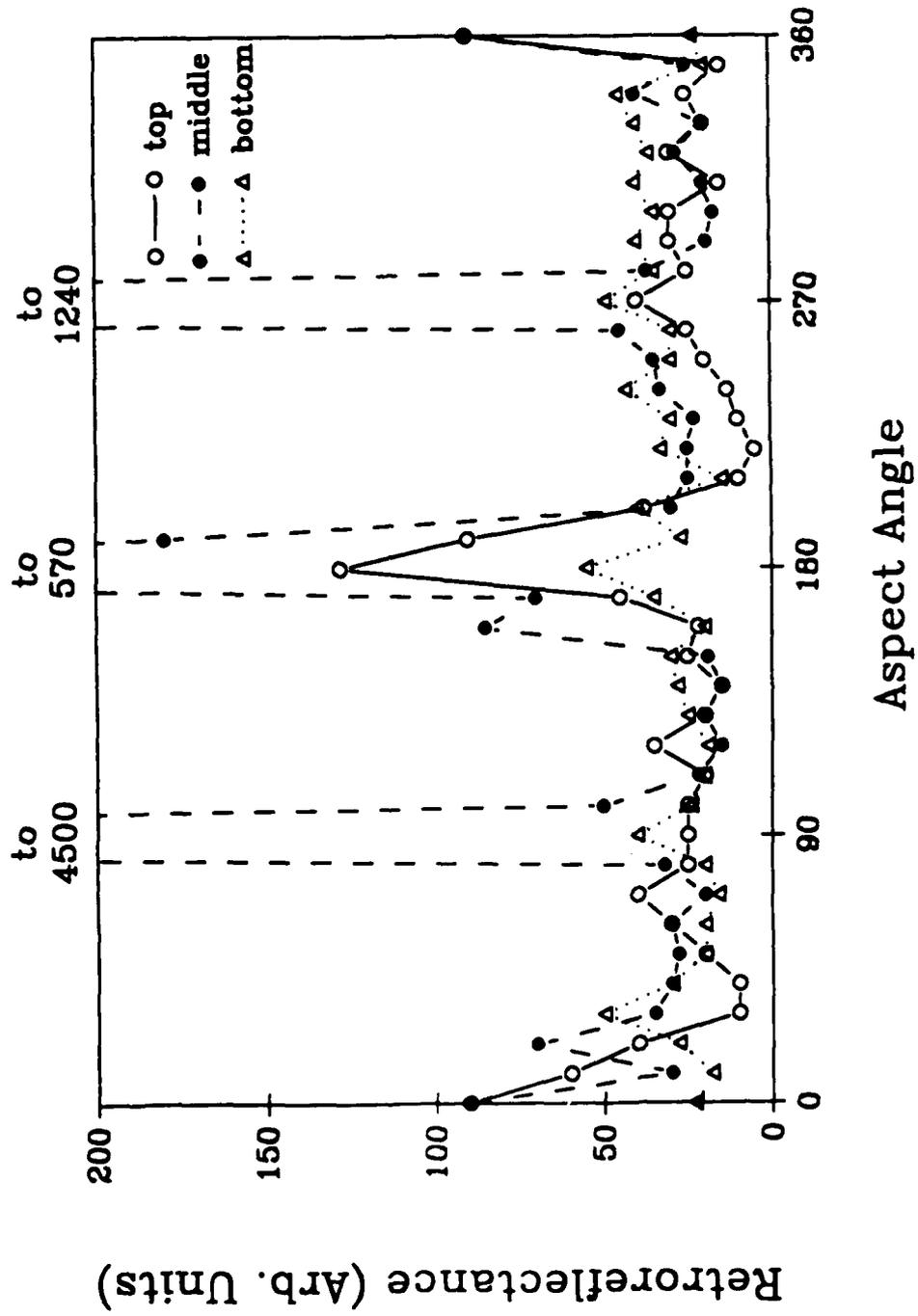


Figure 6. Retroreflectance at 10.6 μm for the gloss coating

10.6 μm - Flat and Gloss Averaged Over Tank

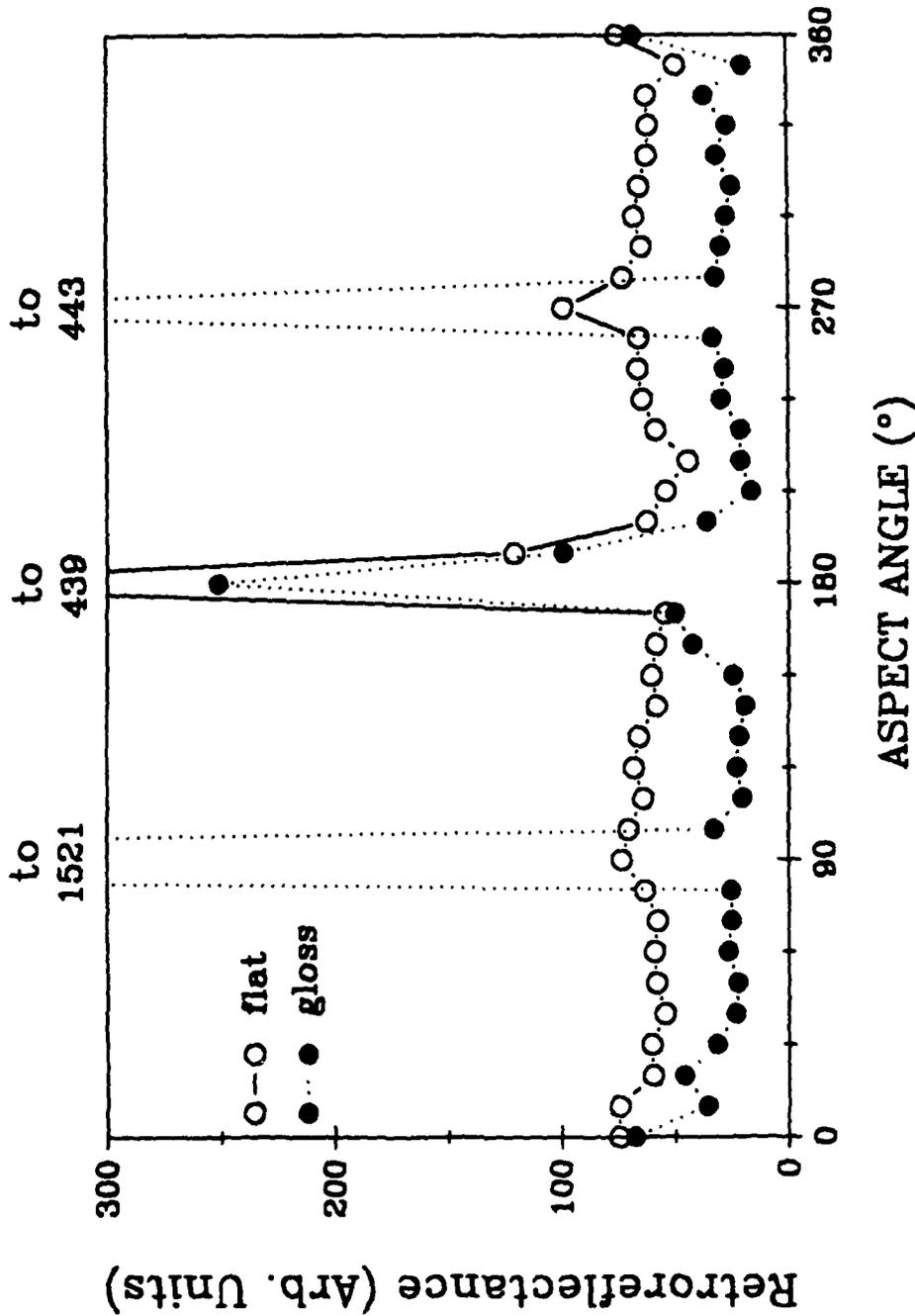


Figure 7. Retroreflectance at 10.6 μm for both coatings.
Each reflectance value is the average over the three aim points

1.52 μm - Flat Green

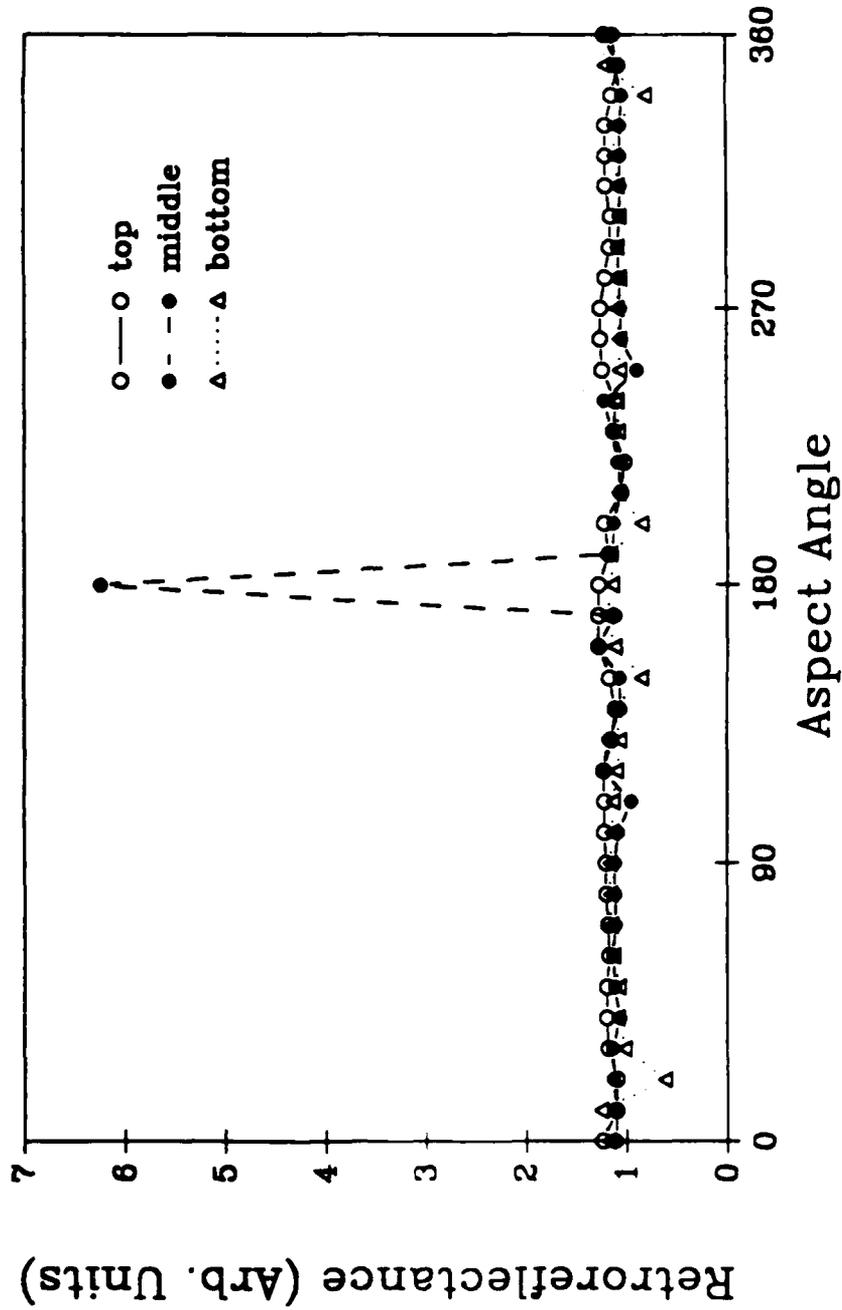


Figure 8. Retroreflectance at 1.52 μm for the flat coating

1.52 μm - Gloss Green

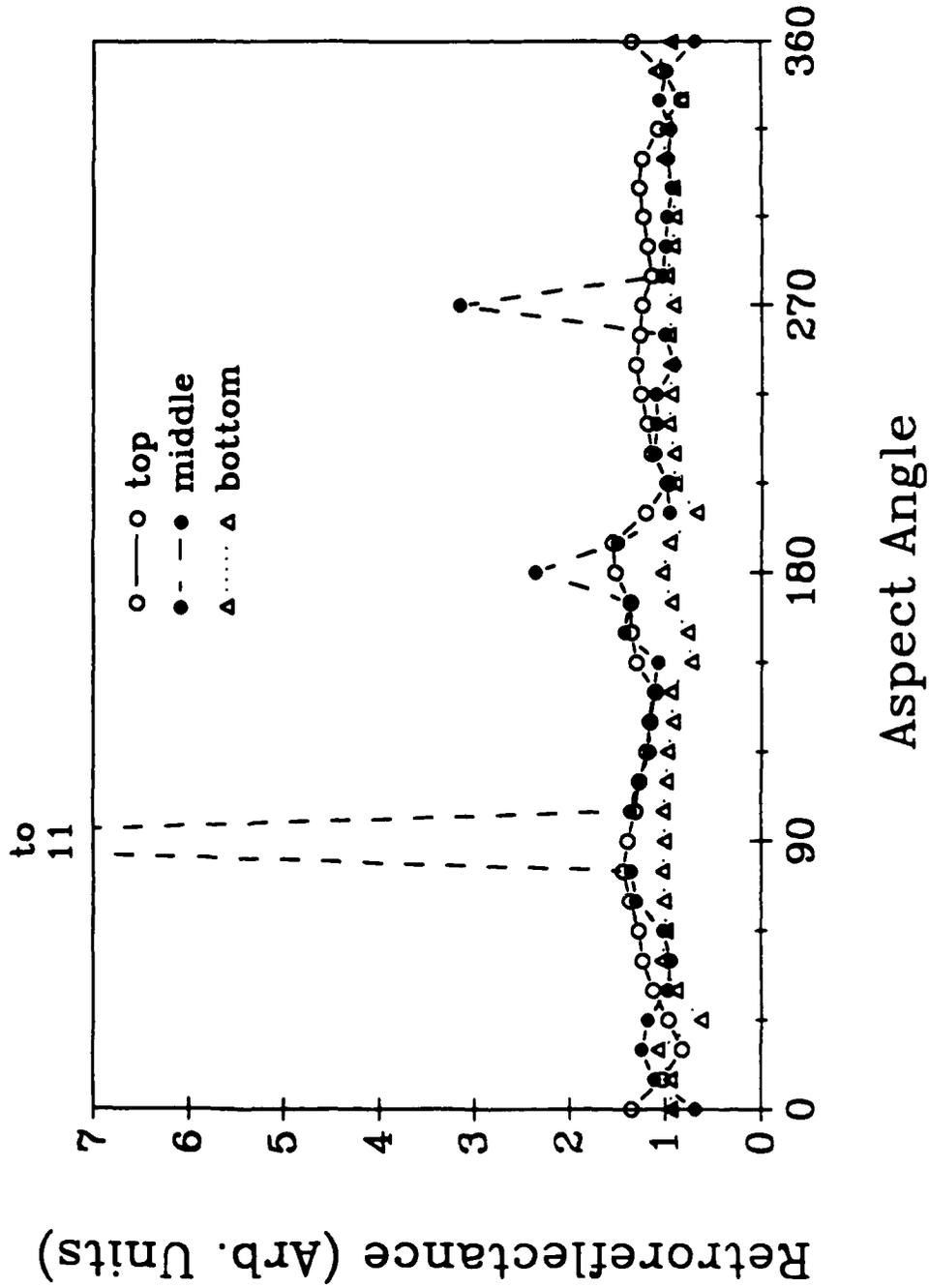


Figure 9. Retroreflectance at 1.52 μm for the gloss coating

1.52 μm - Flat and Gloss Averaged Over Tank

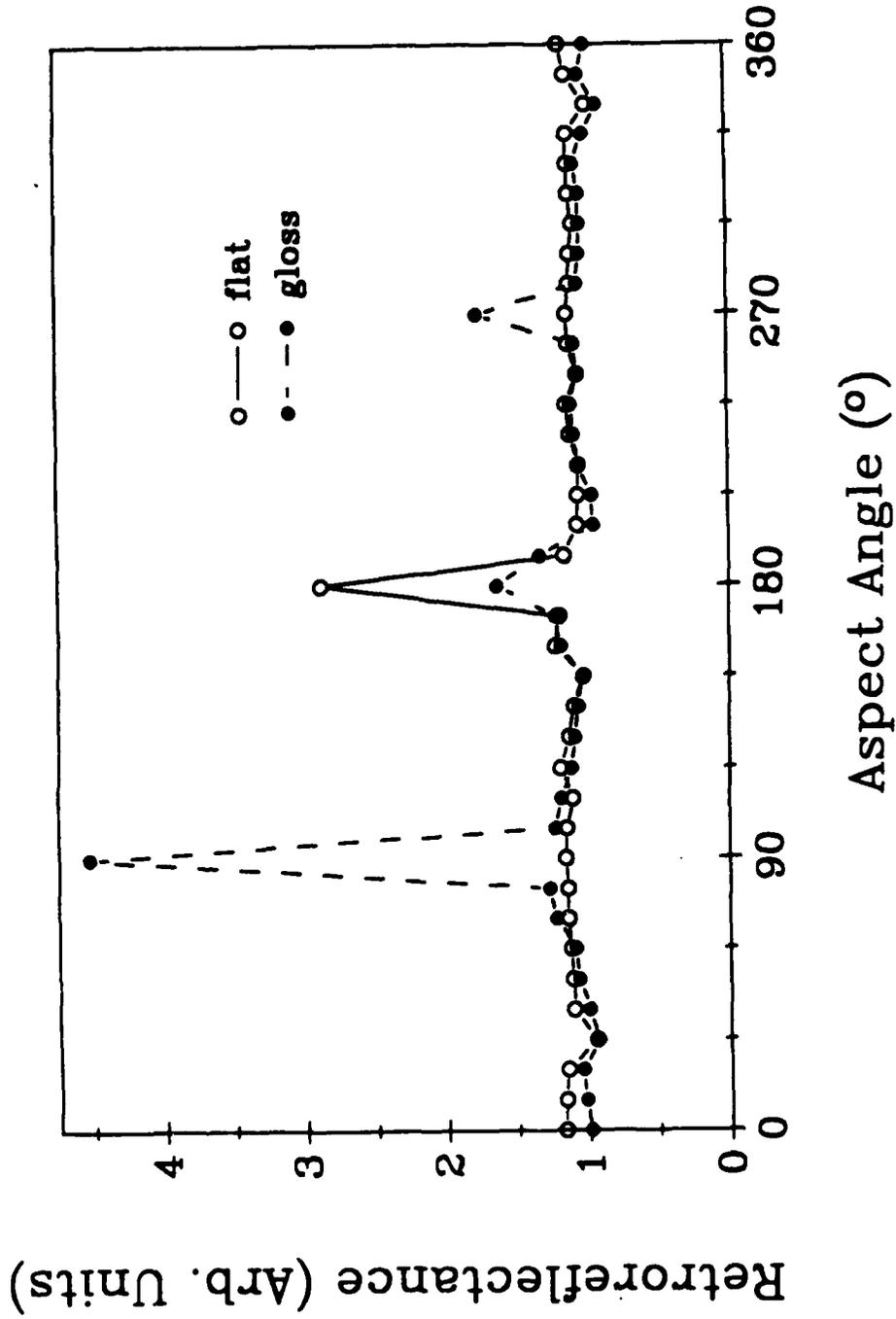


Figure 10. Retroreflectance at 1.52 μm for both coatings. Each reflectance value is the average over the three aim points

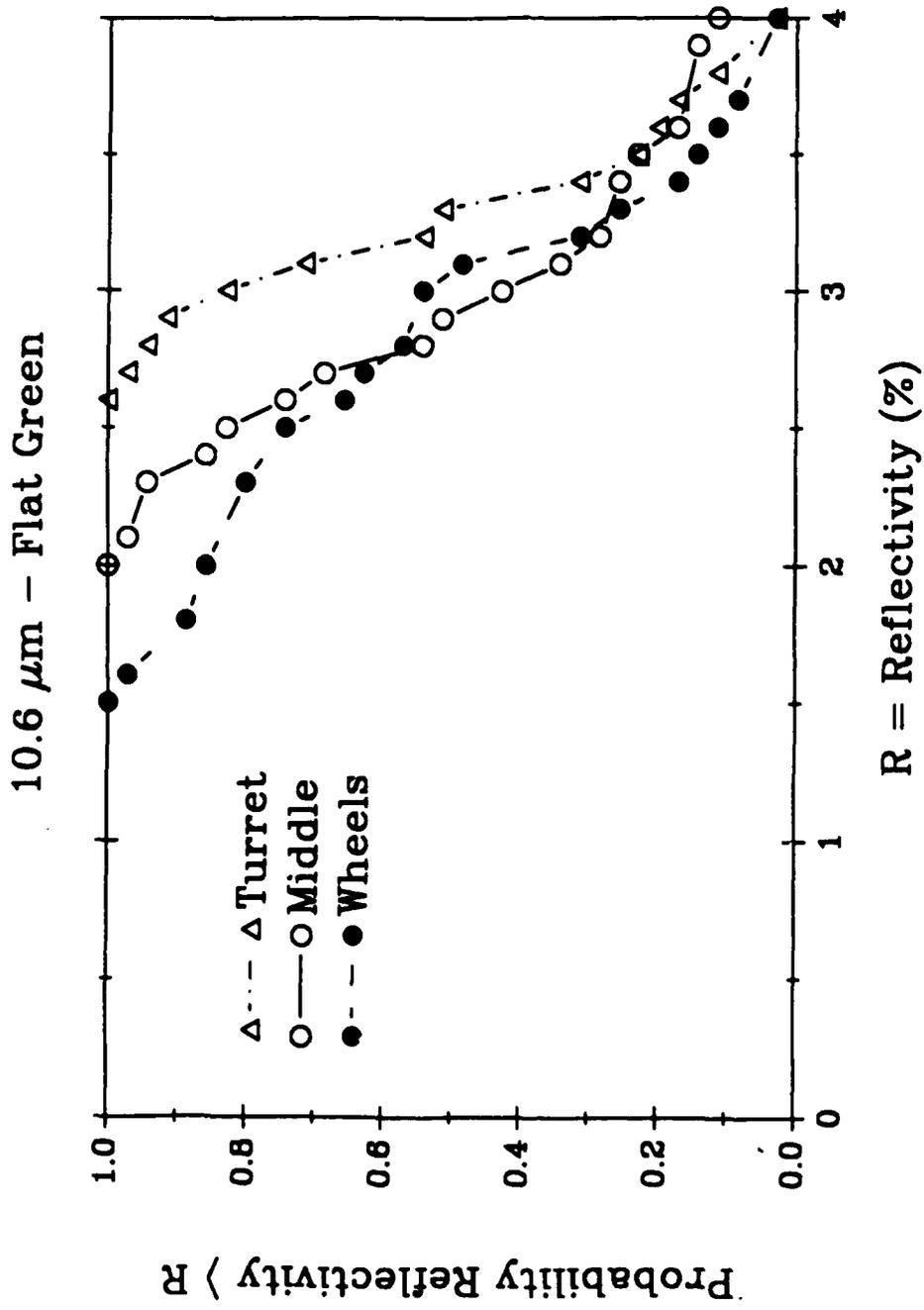


Figure 11. The probability that an observation of the target will result in a measured reflectivity greater than R. The irradiating wavelength is 10.6 μm and the coating is flat green

10.6 μm - Gloss Green

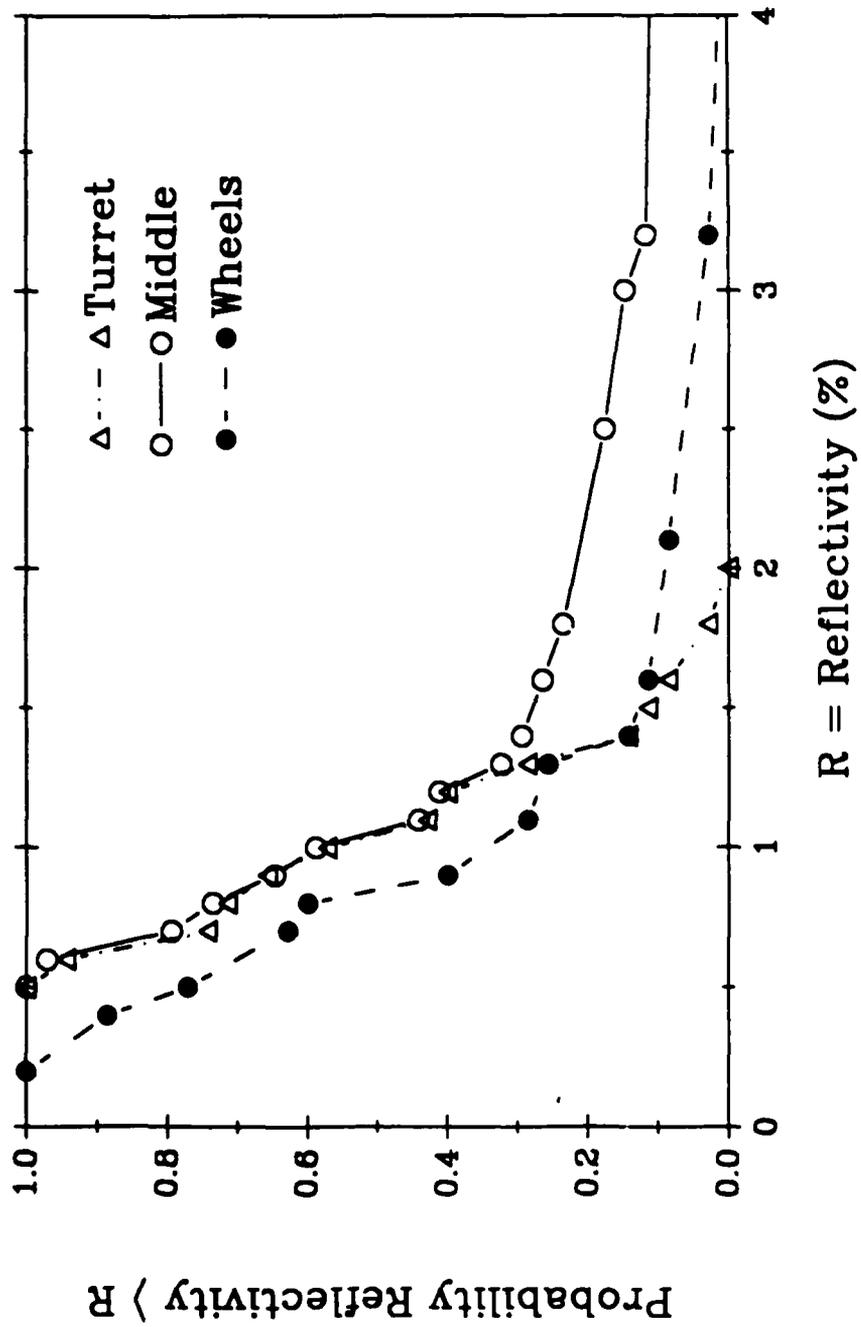


Figure 12. The probability that an observation of the target will result in a measured reflectivity greater than R. The irradiating wavelength is 10.6 μm and the coating is gloss green.

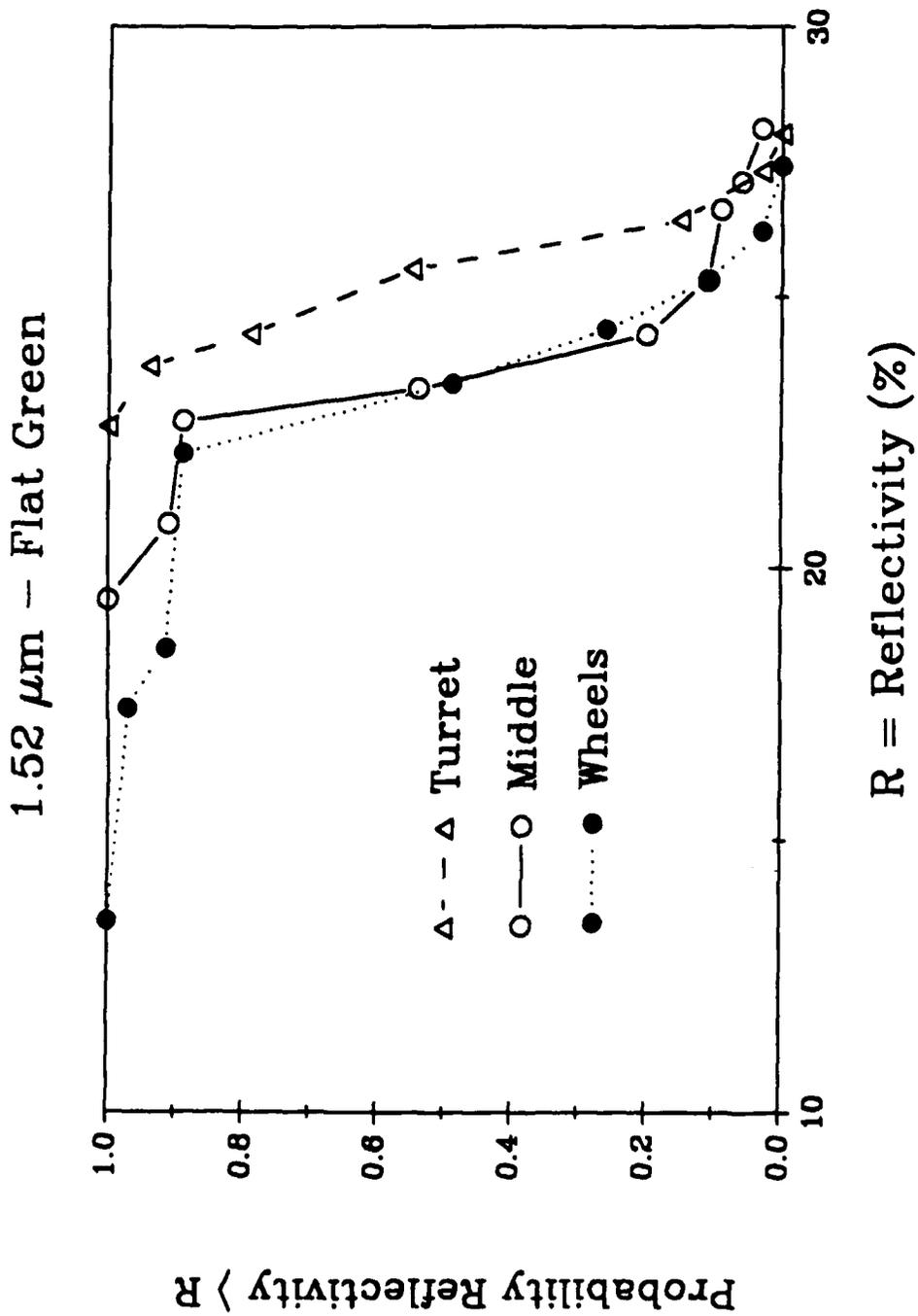


Figure 13. The probability that an observation of the target will result in a measured reflectivity greater than R. The irradiating wavelength is 1.52 μm and the coating is flat green.

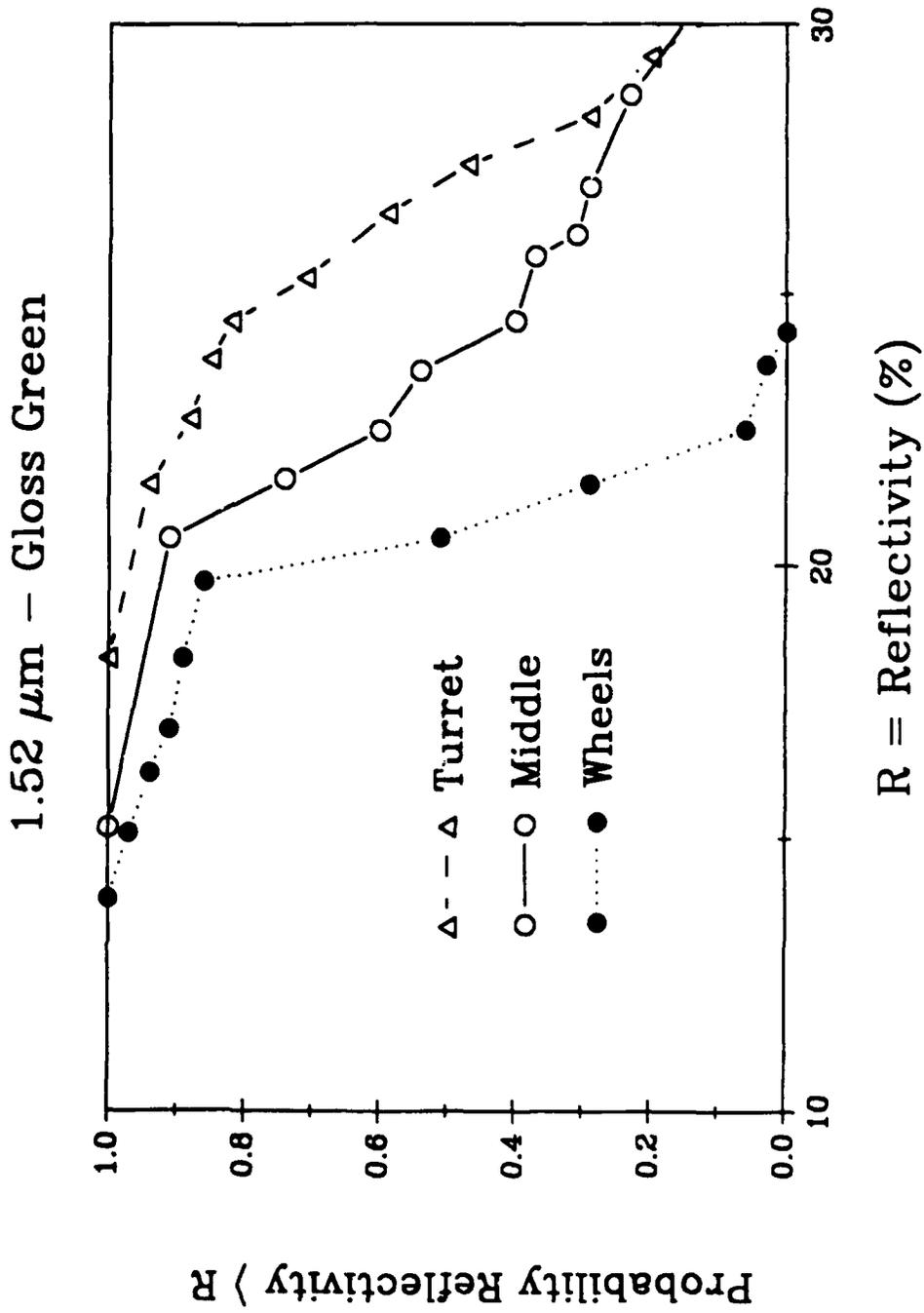


Figure 14. The probability that an observation of the target will result in a measured reflectivity greater than R. The irradiating wavelength is 1.52 μm and the coating is gloss green.

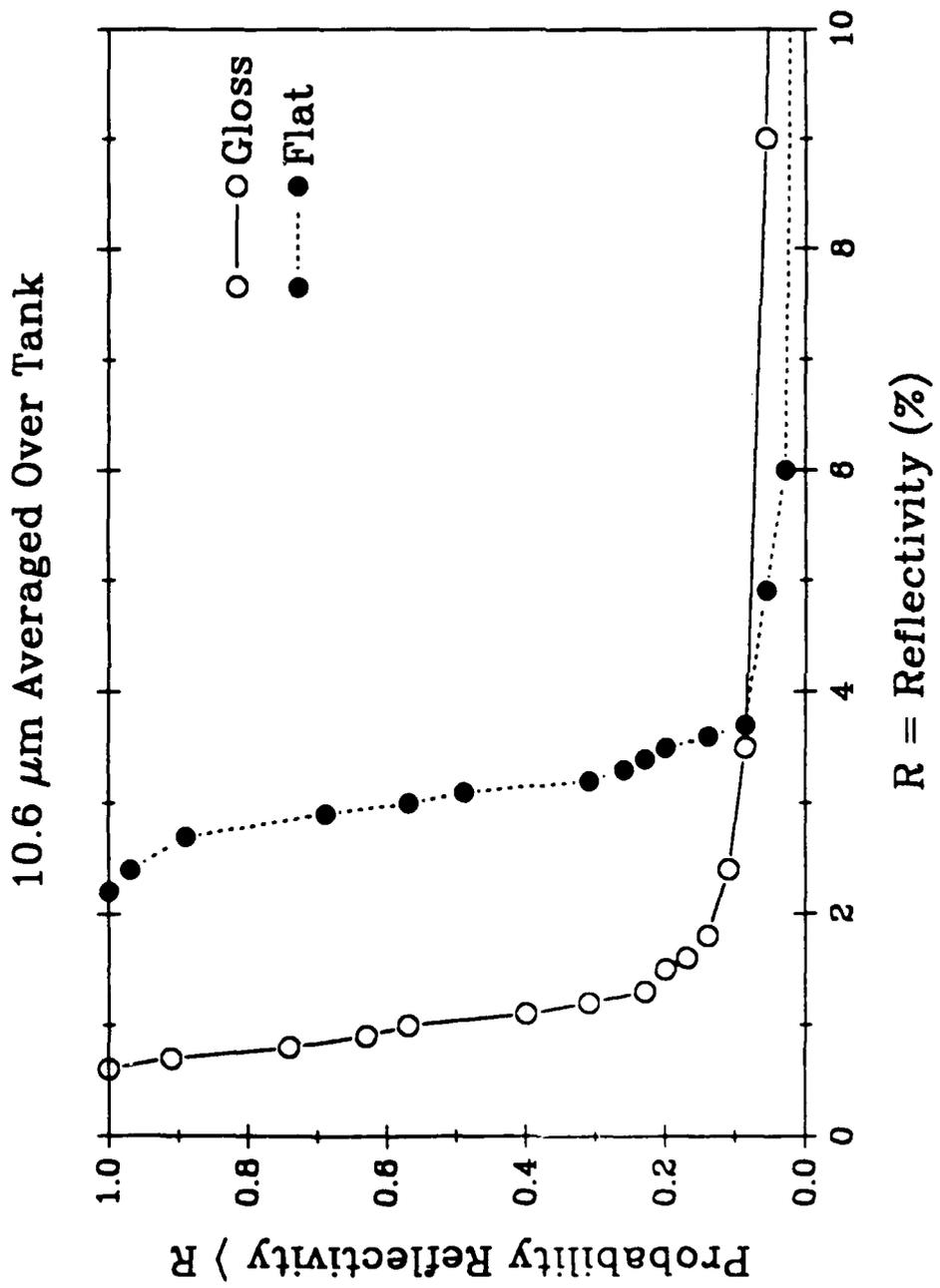


Figure 15. The probability that an observation of the target will result in a measured reflectivity greater than R. Both coatings are shown. The irradiating wavelength is 10.6 μm and each point has been averaged over the three aim points.

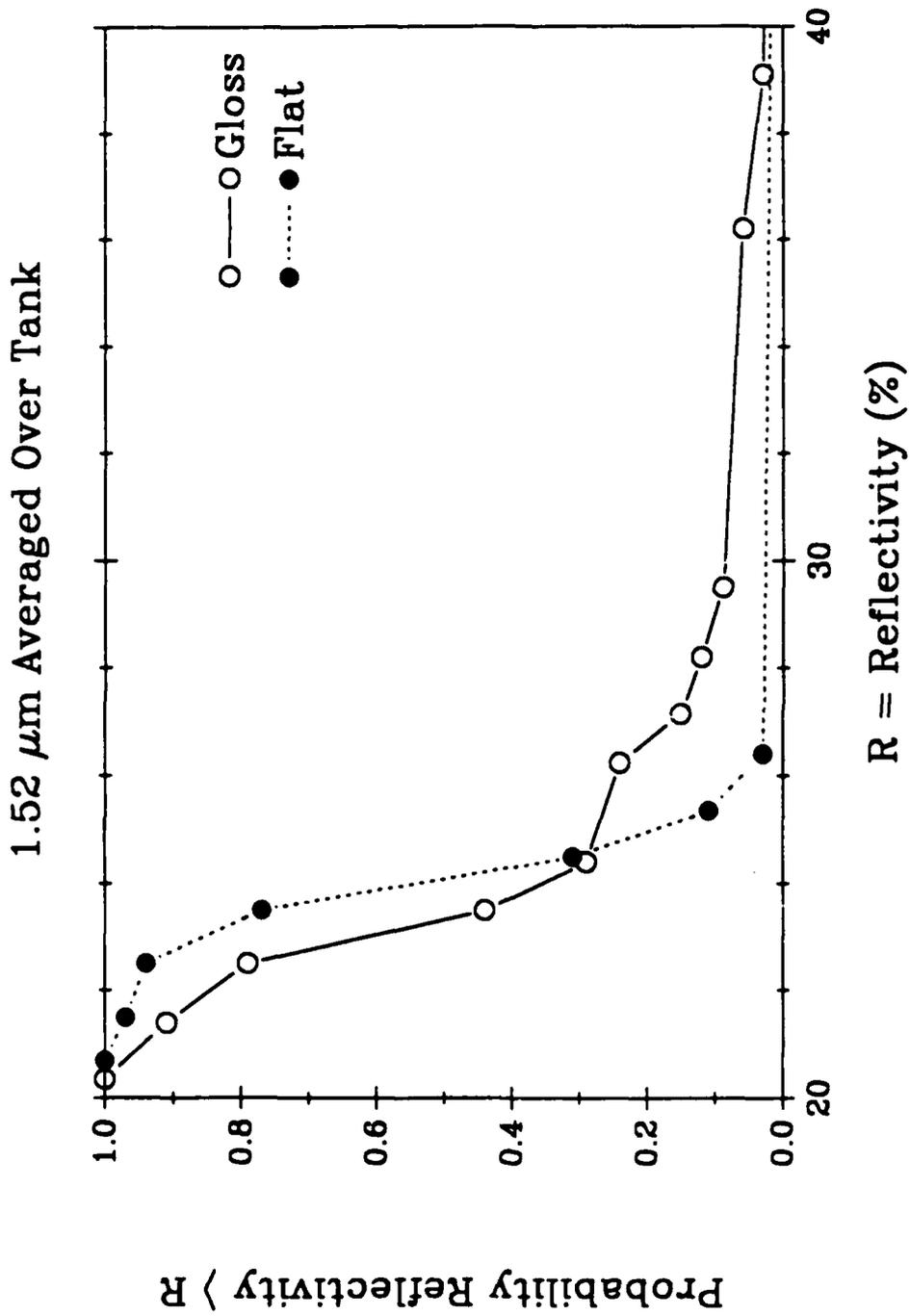


Figure 16. The probability that an observation of the target will result in a measured reflectivity greater than R. Both coatings are shown. The irradiating wavelength is 1.52 μm and each point has been averaged over the three aim points.

DISTRIBUTION FOR AMSEL-NV-TR-0093

- | | | | |
|---|--|---|---|
| 1 | Air Force Wright Aeronautical Laboratories
ATTN: AFWAL/AADO
Wright Patterson AFB, OH 45433 | 1 | MSNW, Inc.
ATTN: J. J. Ewing
2755 Northup Way
Bellevue, Washington 98004 |
| 1 | Air Force Wright Patterson Aeronautical
Laboratories
ATTN: AFWAL/AARI-1 (Mr. Gerald Shroyer)
Wright Patterson AFB, OH 45433 | 1 | Laser Science, Inc.
80 Prospect St.
ATTN: Ali Javan
Cambridge, MA 02139 |
| 1 | Naval Weapons Center
ATTN: Mr. Robert Hintz
Code 31506
China Lake, CA 93555 | 2 | Pulse Systems, Inc.
ATTN: Ed McLellan
422 Connie Avenue
Los Alamos, NM 87544 |
| | Marine Corps Development & Education
Command | 1 | Honeywell Systems & Research Center
ATTN: Dr. Hans Mocker
2600 Ridgway Pkwy
P. O. Box 312
Minneapolis, MN 55440 |
| 1 | ATTN: CWO-2 L. J. Kase | | |
| 1 | ATTN: SPWT Section
Code D091
Quantico, VA 22134-5080 | 1 | Texas Instruments, Inc.
ATTN: Mr. Carol Taylor
P. O. Box 226015
Mail Station 312B
Dallas, TX 75266 |
| 1 | Director
Los Alamos National Laboratory
Mail Stop M888
P. O. Box 1663
ATTN: Dr. Gary Salzman
Los Alamos, NM 87545 | 1 | SRI Inc.
ATTN: Dr. J. Leonelli
333 Ravenswood Avenue
Menlo Park, CA 94025 |
| 1 | Director
EW/RSTS Center
ATTN: AMSEL-EW-SS (Mr. Edward Groeber)
Ft. Monmouth, NJ 07703-5303 | | Hughes Aircraft Co.
Electro-Optical & Data System Group |
| 1 | HQAFESC/RDVS
ATTN: MAJ Kenneth Denbleyker
Tyndall AFB, FL 32403-6001 | 1 | John V. Cernius |
| 1 | GEC Avionics
P. O. Box 81999
2975 Northwoods Parkway/Norcross
Atlanta, GA 30366 | 1 | Dr. John Wang |
| | | 1 | Dr. Mike Henderson
P. O. Box 902
El Segundo, CA 90245 |
| 1 | Westinghouse R&D Center
ATTN: J. F. Lowry
Pittsburgh, PA 15235 | | USA CRDEC |
| | | 1 | ATTN: SMCCR-MUM (Walter Klimek) |
| | | 5 | ATTN: SMCCR-DDT (K. Phelps)
Aberdeen Proving Ground, MD 21010-5423 |

1 **Commander**
 US Army Test and Evaluation Command
 ATTN: AMSTE-CT-T
 Aberdeen Proving Ground, MD 21005-5055

1 **Commander**
 US Army Armament
 Munitions and Chemical Command
 ATTN: AMSMC-QAE (A)
 Aberdeen Proving Ground, MD 21010-5423

1 **Commander**
 US Army Technical Escort Unit
 ATTN: SMCTE-AD
 Aberdeen Proving Ground, MD 21010-5423

1 **Director**
 US Army Research Office
 ATTN: AMXRO-CB
 P. O. Box 1221
 Research Triangle Park, NC 27709

1 **Project Manager**
 Cannon Artillery Weapons System
 ATTN: AMCPM-CAWS-A
 Dover, NJ 07801-5001

1 **Commander/Director**
 US Army Atmospheric Sciences Laboratory
 ATTN: SLCAS-AE
 White Sands Missile Range, NM 88002-5501

1 **Commander**
 Air Force Avionics Laboratory
 ATTN: Electro-Optics Technology Branch
 (Dr. R. Paulson)
 Wright Patterson AFB, OH 45433

1 **Director**
 Central Intelligence Agency
 ATTN: AMR/ORD/DD/S&T
 Washington, DC 20505

Commander
 Air Force Systems Command
 1 ATTN: AD/YQ
 1 ATTN: AD/YQO (MAJ Owens)
 Eglin AFB, FL 32542-6008

1 **Commander**
 Tactical Air Warfare Center
 ATTN: THLO (LTC Kotouch)
 Eglin AFB, FL 32542-6008

1 **Commandant**
 US Army Infantry School
 ATTN: ATSH-CD-MLS-F (Mr. D. Dowie)
 Fort Benning, GA 31905-5400

Commander
 US Army Armament, Munitions and
 Chemical Command
 1 ATTN: AMSMC-ASN
 1 ATTN: AMSMC-IRA
 1 ATTN: AMSMC-SFS
 Rock Island, IL 61299-6000

Director
 US Army Materiel Command Field
 Safety Activity
 1 ATTN: AMXOS-C (Mr. L. Morgan)
 1 ATTN: AMXOS-SE (Mr. Yutmeyer)
 Charleston, IN 47111-9669

1 **Commander**
 US Army Combined Arms Center
 Development Activity
 ATTN: ATZL-CAM-M
 Fort Leavenworth, KS 66027-5300

Commander
 US Army Armor Center & Fort Knox
 1 ATTN: ATZK-CD-MS
 1 ATTN: ATZK-DPT-N (NBC School)
 Fort Knox, KY 40121-5000

1 **Commander**
 5th Infantry Division (Mech)
 ATTN: AFZX-CL
 Fort Polk, LA 71459

1 **Commander**
 US Air Force Geophysics Laboratory
 ATTN: Dr. R. Philbrick
 Bedford, MA 01731

1 **Commander**
 Natick RD&E Center
 1 ATTN: STRNC-IC
 Natick, MA 01760-5015

- 1 Commander
Air Force Systems Command
ATTN: SDN
ATTN: SGB
Andrews AFB, MD 20334-5000
- 1 Commander
US Army Intelligence & Security Command
ATTN: IAQM-SED-III
Fort Meade, MD 20755-5000
- 1 Commander
Foreign Technology Division
ATTN: TQTR
Wright Patterson AFB, OH 45433-6508
- 1 Commander
Naval Air Development Center
ATTN: Code 2012 (Mr. D. C. Tauros)
Warminster, PA 18974-5000
- Commander
US Army Dugway Proving Ground
Chemical Laboratory Division
1 ATTN: Dr. J. Comeford
1 ATTN: STEDP-SD-TA-F (Technical Library)
Dugway, UT 84022
- 1 Chief of Naval Research
ATTN: Code 441
800 N. Quincy Street
Arlington, VA 22217
- Defense Technical Information Center
2 ATTN: DTIC-FDAC
Cameron Station, Building 5
Alexandria, VA 22304-6145
- 1 Commander
US Army Materiel Command
ATTN: AMCCN
5001 Eisenhower Avenue
Alexandria, VA 22333-0001
- Commander
Naval Surface Weapons Center
1 ATTN: Code G51 (Mr. Brumfield)
1 ATTN: Code N54 (Mr. B. Vastag)
Dahlgren, VA 22448
- 1 Commander
US Army Foreign Science and
Technology Center
ATTN: AMXST-CW2
220 Seventh Street, NE
Charlottesville, VA 22901-5396
- 1 Commander
US Army Training & Doctrine Command
ATTN: ATCG-N
Fort Monroe, VA 23651-5000
- 1 NASA Langley Research Center
ATTN: Dr. F. Allario
Mail Stop 476
Hampton, VA 23665
- 1 Commander
US Army Logistics Center
ATTN: ATCL-MGF
Fort Lee, VA 23801-5000
- Commandant
US Army Ordnance Missile & Munitions
Center and School
1 ATTN: ATSK-CM
1 ATTN: ATSK-EI (Mr. Crawford)
1 ATTN: ATSK-TME
Redstone Arsenal, AL 35897-6700
- 2 Commander
US Army Missile Command
Redstone Scientific Information Center
ATTN: AMSMI-RPR (Documents)
Redstone Arsenal, AL 35898-5241
- 1 Commandant
US Army Chemical School
1 ATTN: ATZN-CM-CC
1 ATTN: ATZN-CM-MLB
1 ATTN: ATZN-CM-NC
Fort McClellan, AL 36205-5020
- 1 Commander
US Army Aviation Center
ATTN: ATZQ-D-MS
Fort Rucker, AL 36362-5000

- 1 Commander
HQ, Sixth US Army
ATTN: AFKC-TR-I (NBC)
Presidio of San Francisco, CA 94129-5000
- 1 Commander
North American Air Defense Command
ATTN: J31CN
Cheyenne Mountain Complex
Peterson AFB, CO 80914-5601
- HQDA
- 1 ATTN: DAMA-CSS-C
- 1 ATTN: DAMO-NCC
Washington, DC 20310
- Naval Sea Systems Command
PM-Theater Nuclear Warfare Program Office
- 1 ATTN: Code TN20A (Dr. G. Patton)
Washington, DC 20362-5101
- 1 Commander
Naval Research Lab
ATTN: Code 6182 (Dr. R. Taylor)
4555 Overlook Avenue, SW
Washington, DC 20375-5000
- 1 Director
Center for Signal Warfare Laboratory
ATTN: AMSEL-RD-SW-D
Vint Hill Station, VA 22186
- 1 Project Manager
ATTN: AMCPM-AAH
4300 Goodfellow Blvd.
St. Louis, MO 63120
- 1 Project Manager
TADS/PNVS
ATTN: AMCDM-AAH-TP
4300 Goodfellow Blvd.
St. Louis, MO 63120
- 1 Director
Defense Advanced Research Projects Agency
1400 Wilson Blvd.
Rosslyn, VA 22209
- 1 Raytheon Company
Equipment Division
Electro-Optics Laboratory
ATTN: Mr. Al Jelalian
528 Boston Post Road
Sudbury, MA 01776
- 1 United Technologies Research Center
400 Main Street
ATTN: Dr. B. Silverman
East Hartford, CT 06108
- 1 CLS Laser Systems Incorporated
5 Jeffrey Drive
ATTN: Dr. Robert DelBoca
P. O. Box 767
South Windsor, CT 06074
- 1 Richard Powell
Texas Instruments
8505 Forest Lane
P. O. Box 660246, MS 3150
Dallas, TX 75266
- Abrams Tank Systems
- 1 ATTN: AMCPM-ABMS-SW (Mr. Havrilla)
Warren, MI 48397-5000
- 1 Mark Michel
GDLS, Mail Zone 439-01-10
P. O. Box 2094
Warren, MI 48090
- Director
CECOM Center for Night Vision
& Electro-Optics
- 25 ATTN: AMSEL-RD-NV-LR
Fort Belvoir, VA 22060-5677
- 1 ASQNK-BVP-G (Editor)