Alternatives to Mie Theory

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**Alternatives to Mie Theory**

This report examines how the scattering properties of spheres can be calculated without using Mie theory. Specifically, the scheme of ray optics is used to develop software that calculates the phase matrix elements of polydisperse spheres in geometrical optics limit. (Ray optics works well for size parameters greater than 400, and becomes more accurate for particles containing significant absorption.) In addition, this report examines a collection of numerical algorithms, developed by Nussenzveig and Wiscombe, that use complex angular momentum theory to obtain the efficiency factors for Mie scattering. Although accurate for size parameters greater than 20, it is shown that these algorithms are only computationally efficient for size parameters greater than 500. Finally, this report establishes regions of validity for over... 

### ABSTRACT (Continue on reverse if necessary and identify by block number)

- This report examines how the scattering properties of spheres can be calculated without using Mie theory. Specifically, the scheme of ray optics is used to develop software that calculates the phase matrix elements of polydisperse spheres in geometrical optics limit. (Ray optics works well for size parameters greater than 400, and becomes more accurate for particles containing significant absorption.) In addition, this report examines a collection of numerical algorithms, developed by Nussenzveig and Wiscombe, that use complex angular momentum theory to obtain the efficiency factors for Mie scattering. Although accurate for size parameters greater than 20, it is shown that these algorithms are only computationally efficient for size parameters greater than 500. Finally, this report establishes regions of validity for other...
approximations to the Mie efficiency factors which exist in the scientific literature. It is shown that existing approximations can give reasonable estimates for the extinction efficiency for most size parameters and complex indices of refraction. On the other hand, the approximations for the absorption efficiency are much less accurate.
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Preface

We wish to thank Warren Wiscombe of NASA/GSFC for providing us with a copy of the FORTRAN programs that implement the complex angular momentum algorithms developed by Nussenzveig and himself, as discussed in Chapter 3 of this report.
1. INTRODUCTION

Mie theory provides a means of calculating the absorption and scattering of electromagnetic radiation by spheres of any size compared with the wavelength. Although exact, performing full Mie theory calculations is often cumbersome: it requires an excessive amount of numerical storage space and computer time, especially when the particles are large compared with the wavelength. Under certain circumstances however, it is possible to obtain a reasonable estimate of the scattering and absorption properties of spheres without resorting to detailed Mie theory calculations. These alternative approaches to exact Mie theory calculations are useful provided the user realizes their limitations.

The regions of validity for Mie approximations are usually characterized in terms of the size parameter, \( X = \frac{2\pi r}{\lambda} \), where \( r \) is the radius of the particle and \( \lambda \) is the wavelength of the impinging radiation. Unfortunately, the use of an approximation over Mie theory is not a clearcut decision; that is, the accuracy of most approximations depend not only on \( X \), but to some extent on the complex index of refraction of the particle, \( m = n + ik \). Also the user must consider the degree of accuracy required for his or her particular problem.

1.1 Organization of the Report

It is the aim of this report to explore some of the alternatives to Mie theory and to access their ranges of
applicability. Chapter 2 discusses the use of ray optics to obtain the phase matrix elements of a sphere that is large compared with the wavelength. Chapter 3 discusses the use of complex angular momentum theory to calculate the efficiency factors for extinction, absorption and radiation pressure. Chapter 4 compares various Mie approximations in the scientific literature and assesses their regions of validity. Chapter 5 summarizes the main results of this report. For reference, Appendix A gives the equations for the various Mie approximations investigated in this report.
2. THE USE OF RAY OPTICS TO OBTAIN THE SCATTERING MATRIX ELEMENTS FOR A SPHERE

2.1 Overview

The angular scattering properties of spheres can be calculated using the scheme of ray optics (van de Hulst\textsuperscript{1} and Liou and Hansen\textsuperscript{2}) provided four conditions are satisfied:

1) the size parameter is much greater than one

2) the real part of the index of refraction is greater than one

3) the user is interested in the scattering pattern for a small spread of particle sizes

4) the far field scattering pattern is desired.

In ray optics, incident radiation is treated as localized rays whose encounters with the particle are governed by the laws of reflection and refraction for geometrical optics. The localized rays can be reflected externally or can enter the particle where they are either absorbed or internally reflected a number of times before exiting. Also, light rays passing very close to the particle are affected by Fraunhofer diffraction. Thus the total intensity at a particular scattering angle is equal to the contribution from Fraunhofer diffraction, plus that for rays emerging from the particle after reflection and refraction.

---


(Strictly speaking it is not correct to simply add the intensities of the separate rays. For a single particle, emergent rays interfere with each other because of phase changes caused by external and internal reflection, and by differing optical paths. These interference effects lead to rapid oscillations in the scattered intensity as a function of scattering angle which can only be predicted by Mie theory. However if a small spread of particle sizes is considered, any phase effects are averaged out when integrating over the spread of particle sizes.)

In ray optics, the gain, $G$, is used to describe the relative scattered intensity as a function of scattering angle. It represents the ratio of scattered intensity to that which would exist if it were scattered isotropically and conservatively $^2$. Thus the gain is defined such that

$$w_o = \frac{\int G(\Omega)d\Omega}{\int d\Omega} = \frac{1}{4\pi} \int G(\Omega)d\Omega$$

(1)

where $\Omega$ is the solid angle and $w_o$, the single scattering albedo, is the ratio of the scattered energy to that scattered and absorbed by the particles.

Below the equations governing ray optics are presented. These equations are essentially the same as those found in van de Hulst$^1$ and in Liou and Hansen$^2$. Next, a Fortran subroutine called RAYOPT is described which determines the angular dependent phase matrix elements $i_1$, $i_2$, $i_3$ and $i_4$. These matrix elements relate the polarization and the amplitude of the incident field to that of the scattered field.
The results from RAYOPT are then verified against those from Liou and Hansen, and from full Mie theory.

### 2.2 Fraunhofer Diffraction

Diffraction of the incident beam occurs because the wavefront is partially obstructed as it passes very close to the particle. For spheres, the gain as a function of scattering angle resulting from diffraction is given by

\[ G^F_1(\theta, X) = G^F_2(\theta, X) = 2X^2 \left[ \frac{J_1(X \sin \theta)}{X \sin \theta} \right]^2 \]  

where the superscript $F$ denotes the gain due to Fraunhofer diffraction, $J_1$ is the first order Bessel function and the subscripts 1 and 2 refer to the gain components perpendicular and parallel, respectively, to a particular scattering plane. The diffracted pattern is radially symmetric about the forward direction and becomes more concentrated in the forward direction as the size parameter increases. For the case when $\theta = 0$, $G^F_1(0, X) = G^F_2(0, X) = 0.5X^2$.

### 2.3 Geometrical Optics

The geometry of the problem is given in Figure 1. The angle between an incident ray and the tangent of the local particle surface is denoted by $\tau$. For grazing incidence, $\tau$ equals 0 degrees; for central incidence, $\tau$ equals 90 degrees. As an incident ray encounters the particle, some of its energy is externally reflected while the rest enters the particle. The ratio of externally reflected energy to the
incident energy is equal to the squares of the Fresnel reflection coefficients, $r_1$ and $r_2$:

$$|r_1|^2 = \left| \frac{\sin r - m \sin r'}{\sin r + m \sin r'} \right|^2$$

and

$$|r_2|^2 = \left| \frac{m \sin r - \sin r'}{m \sin r + \sin r'} \right|^2$$

where $r'$ is the direction of the ray upon entering the particle. The angle $r'$ is related to the incident angle, $\gamma$, through Snell's law

$$\cos r' = \frac{\cos \gamma}{n}$$

Because energy is conserved, the energy entering the particle must either be absorbed or emerge after any number of
internal reflections. For a nonabsorbing particle, the fraction of energy emerging after refraction with no internal reflection is equal to \((1-|r_{1,2}|^2)^2\); after one internal reflection, it is \(|r_{1,2}|^2(1-|r_{1,2}|^2)^2\), etc. Here it is convenient to define

\[
e^{1,2}_{1,2} = \frac{|r_{1,2}|^2}{(1-|r_{1,2}|^2)^2(|r_{1,2}|^2)^{p-1}} \quad \text{for } p \geq 1
\]

where \(p = 0\) means external reflection and \(p \geq 1\) means refraction plus \(p-1\) internal reflections (see Fig. 1). The gain for geometrical optics, as given by Liou and Hansen, is then

\[
G(p)_{1,2}(\theta, X) = 2e^{1,2}_{1,2}D \exp(-4X k \rho \sin \tau'),
\]

where \(D\) is the divergence, defined as

\[
D = \frac{\sin \tau \cos \tau}{\sin \theta} \frac{d \theta}{d \tau}
\]

and

\[
\frac{d \theta}{d \tau} = 2 - 2p \frac{\tan \tau}{\tan \tau'}.
\]

In Eq. 7, the exponential term accounts for absorption within the particle. The total gain at a particular scattering angle is then

\[
G_{1,2}(\theta, X) = G^{F}_{1,2} + \sum_{p=0}^{N} G^{(p)}_{1,2}
\]
where in practice, a value of 3 for N is sufficient to account for most of the energy scattered by geometrical optics.

2.4 Relationship Between Gain And The Phase Matrix Elements

The angular dependent phase matrix elements relate the polarization and amplitude of the scattered field to the incident field. In the work of Blattner\(^3\), the incident and scattered fields are described by the parameters \(I_1, I_2, U\) and \(V\) which are similar to, but not the same as, the Stokes parameters. For a spherical scatterer, the scattered field (\(s\) subscript) is related to the incident field (\(o\) subscript) through the amplitude scattering matrix

\[
\begin{bmatrix}
I_{s1} \\
I_{s2} \\
I_s \\
V_s
\end{bmatrix} = \begin{bmatrix}
\lambda^2 \\
0 \\
0 \\
0
\end{bmatrix} \begin{bmatrix}
i_1 & 0 & 0 & 0 \\
i_2 & 0 & 0 & 0 \\
0 & i_3 & i_4 \\
0 & -i_4 & i_3
\end{bmatrix} \begin{bmatrix}
I_o \\
I_o \\
U_o \\
V_o
\end{bmatrix}
\]

where \(R\) is the distance from the scatterer to the observer and \(i_1, i_2, i_3\) and \(i_4\) are the angular dependent scattering matrix elements defined as

\[
\begin{align*}
i_1 &= c|S_1|^2 \\
i_2 &= c|S_2|^2 \\
i_3 &= c \Re\{S_1 S_2^*\} \\
i_4 &= -c \Im\{S_1 S_2^*\}
\end{align*}
\]

where $S_1$ and $S_2$ are the familiar complex amplitude functions and $c$ is a normalization constant such that

$$1 = \int i_1(u) du$$

(13)

Comparing Equations 1 and 13 suggests that

$$i_1 = G_1/4\pi w_o$$
$$i_2 = G_2/4\pi w_o$$
$$i_3 = (G_1 G_2)^{1/2}/4\pi w_o$$
$$i_4 = 0$$

(14)

### 2.5 Ray Optics Subroutine

A subroutine called RAYOPT has been developed to determine the phase matrix elements $i_1$, $i_2$, $i_3$, and $i_4$ at user specified scattering angles. The inputs to the subroutine are listed in Table 1. A flow diagram for RAYOPT is given in Figure 2 and a brief description of the important variables and functions is given in Table 2.

For geometrical optics, RAYOPT determines the gains at the user scattering angles in the following manner. With $p$ held fixed, the total deviation of a ray from its original path, $\theta'$, is computed for incident angles, $\tau$, between 0 and 90 degrees in steps of 0.5 degrees where

$$\theta' = 2\tau - 2p\tau'$$

(15)

Next, each user scattering angle is transformed so that it also represents the total deviation of a ray from its original path. This deviation is then compared with the devia-
Table 1. Input Parameters for RAYOPT

<table>
<thead>
<tr>
<th>VARIABLE</th>
<th>DESCRIPTION</th>
</tr>
</thead>
<tbody>
<tr>
<td>NP</td>
<td>Maximum Value for p When Performing the Ray Tracing</td>
</tr>
<tr>
<td>NTHETA</td>
<td>Number Of User Scattering Angles. The Maximum is 150</td>
</tr>
<tr>
<td>PM</td>
<td>Complex Index of Refraction of the Particle. The Imaginary Part Is Positive</td>
</tr>
<tr>
<td>THET(150)</td>
<td>Array Containing the User Scattering Angles</td>
</tr>
<tr>
<td>WO</td>
<td>Single Scattering Albedo of the Particle</td>
</tr>
<tr>
<td>X</td>
<td>Size Parameter</td>
</tr>
</tbody>
</table>

Before computing the gain, RAYOPT checks to make sure the incident angle does not lead to either a rainbow, i.e. $d\theta/dr \to 0$, or a glory, i.e. $\theta = 180$ and $\sin \theta = 0$. (The scheme of ray optics predicts infinite intensities at these angles, see Eq. 8.) If a rainbow or glory angle is found, the gain calculation is performed for an incident angle given by $\tau = \tau - 2$ degrees. The resulting gain is then used unless it is still excessively large (>100); in that case, the gain
Compute the Gain at the User Scattering Angles Due to Diffraction

\[ \Downarrow \]

Calculate the Gain at the User Scattering Angles Due to External Reflection \((P = 0)\)

\[ \Downarrow \]

Determine the Gain at the User Scattering Angles for All \(P\) That Do Not Have a Rainbow or Glory (Criterion: \(P < n'\))

\[ \Downarrow \]

Compute the Gain at the User Scattering Angles for All Remaining \(P\) Upto \(NP\)

\[ \Downarrow \]

Convert the Gains to Matrix Elements

\[ \Downarrow \]

Return

Figure 2. Flow Diagram of the Subroutine RAYOPT.
Table 2. Important Variables and Functions in RAYOPT

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>DESCRIPTION</th>
</tr>
</thead>
<tbody>
<tr>
<td>GAINP</td>
<td>Function That Returns the Gain for a Given Incident Angle and p</td>
</tr>
<tr>
<td>GAIN1(150),</td>
<td>Keeps a Running Total of the Gains at the User Scattering Angles</td>
</tr>
<tr>
<td>GAIN2(150)</td>
<td></td>
</tr>
<tr>
<td>GDIFF(150)</td>
<td>Gains at the User Scattering Angles Due To Fraunhofer Diffraction</td>
</tr>
<tr>
<td>Ji</td>
<td>Function That Returns The Bessel Function Of The First Kind</td>
</tr>
<tr>
<td>PNAUT</td>
<td>Maximum Value of p that Does Not Have a Rainbow or Glory</td>
</tr>
<tr>
<td>RENT1(150),</td>
<td>Angular Dependent Matrix Elements $i_1$, $i_2$, $i_3$ and $i_4$ Respectively</td>
</tr>
<tr>
<td>RENT2(150)</td>
<td></td>
</tr>
<tr>
<td>ENT3(150),</td>
<td></td>
</tr>
<tr>
<td>ENT4(150)</td>
<td></td>
</tr>
<tr>
<td>TAU</td>
<td>Angle of An Incident Ray With Respect To The Particle Surface</td>
</tr>
<tr>
<td>THETPR(181)</td>
<td>Array Containing the Total Deviation of Emergent Rays for Incident Rays between 0 and 90 degrees in Steps of 0.5 degrees</td>
</tr>
</tbody>
</table>
is set equal to 100. The gain calculations are simplified for \( p \leq n \) because they do not contain rainbows or glorys. These values of \( p \) are done first in RAYOPT where the amount of computer time is reduced significantly. Finally for central incidence, where \( \tau \) is 90 degrees and \( \theta \) is 0 degrees, the gain equals \( g_{1,2}^p = 0.5(e_{1,2}^2/(1-p/n)^2)\exp(-4X k p) \).

2.6 Sample Calculations Using RAYOPT

To ensure that RAYOPT is working properly, a series of calculations have been performed and compared with those from other researchers. Figures 3 and 4 duplicate Figures 1

![Graph](image)

Figure 3. Recalculation of Figure 1 of Liou and Hansen\(^2\), Angular Gain for Geometrical Optics using RAYOPT. The Vertical Scale Applies to the Lowermost Curves (\( n = 1.45 \) and 2.00) while the Other Curves Are Displaced Upwards by Factors of 10\(^2\).
Figure 4. Recalculation of Figure 2 of Liou and Hansen\textsuperscript{2}, Degree of Polarization for Geometrical Optics using RAYOPT. The Vertical Scale Applies to the Lowermost Curves ($n = 1.45$ and $2.00$) while the Other Curves Are Displaced Upwards by 0.8.
and 2 of Liou and Hansen. There is complete agreement except in some instances at the rainbow and glory angles: Liou and Hansen did not say how they dealt with these angles.

Figures 5 and 6 give comparisons between ray optics and Mie theory for the matrix elements $i_1$, $i_2$ and $i_3$. Figure 5 represents the scattering by a particle with an index of refraction of $1.33 + 0.0i$ while in Figure 6, an index of refraction of $1.54 + 0.01i$ has been used. In both figures, the matrix elements for ray optics represent a size parameter of 400. When performing the Mie calculations, it was necessary to use a particle number density distribution, $N(r)$, described by a log-normal distribution because interference effects lead to rapid oscillations in the angular scattering pattern of a single sphere. This analytical formulation is given by

$$\frac{dN(r)}{d\log(r)} = \frac{N_0}{(2\pi)^{1/2}\log\sigma} \exp\left[-\left(\frac{\log(r/r_0)}{2\log\sigma}\right)^2\right]$$

where $r_0$, $\sigma$ and $N_0$ are the geometric mean radius, geometric standard deviation and total number of particles respectively. In Figures 5 and 6, an $r_0$ of 63.66 micrometers, $\sigma$ of 0.1, and $N_0$ of 1 particle cm$^{-1}$ have been used. The value for $r_0$ was chosen because it converts to a size parameter of 400 for 1 micrometer radiation. The range of the Mie calculations was from 50 to 100 micrometers.

Figure 5(a) shows good agreement between the values of $i_1$ for ray optics and Mie theory except for the rainbow region from 130 to 140 degrees and at 180 degrees. The peak
Figure 5. Values of (a) $i_1$, (b) $i_2$ for Ray Optics and Mie Theory Where There Is No Absorption Within the Particle
Figure 5. (continued) Values of (c) $i_3$ for Ray Optics and Mie Theory Where There Is No Absorption Within the Particle. In (c) the Values Beyond About 80 Degrees Are Not Plotted Because $i_3$ for Mie Theory Is Negative.
Figure 6. Values of (a) $i_1$, (b) $i_2$ for Ray Optics and Mie Theory where there is absorption within the particle.
Figure 6. (continued) Values of (c) $i_3$ for Ray Optics and Mie Theory Where There Is Absorption Within the Particle. In (c) the Values Beyond About 70 Degrees Are Not Plotted Because $i_3$ for Mie Theory Is Negative.
at 180 degrees for Mie theory is related to the familiar glory phenomenon. Ray optics does not predict the glory and here lies one of its major weaknesses. Figure 5(b) suggests only fair agreement between the values of $i_2$ for ray optics and Mie theory. In Figure 5(c), the values of $i_3$ for ray optics are close to those for Mie theory provided the scattering angle is less than 80 degrees. Beyond this angle however, ray optics cannot be used in place of Mie theory because $i_3$ for Mie theory is negative. This limitation of ray optics is not as severe as it may appear since $|i_3|$ is small beyond 80 degrees.

Figures 6(a) and 6(b) show better general agreement between Mie theory and ray optics except near the diffraction peak. The improved accuracy of ray optics can be attributed to the absorption within the particle which eliminates the less accurate contributions from $p > 1$. However discrepancies still exist in the values of $i_2$ for scattering angles between 60 and 80 degrees. Here, ray optics predicts values for $i_2$ that are 10 to 100 times greater than Mie theory. In Figure 6(c), the values of $i_3$ for ray optics are close to those for Mie theory provided the scattering angle is less than 60 degrees. Beyond 60 degrees, Mie theory predicts negative values for $i_3$. 
3. Calculating Mie Efficiency Factors with Complex Angular Momentum Theory

3.1 Overview

Three parameters often obtained from Mie theory calculations are the efficiency factors for extinction, absorption and radiation pressure which are referred to as \( Q_{\text{ext}} \), \( Q_{\text{abs}} \) and \( Q_{\text{pr}} \) respectively. \( Q_{\text{ext}} \) and \( Q_{\text{abs}} \) are related to the extinction and absorption cross sections, \( C_{\text{ext}} \) and \( C_{\text{abs}} \), by

\[
Q_{\text{ext}} = \frac{C_{\text{ext}}}{A} \quad \text{(17)}
\]

and

\[
Q_{\text{abs}} = \frac{C_{\text{abs}}}{A} \quad \text{(18)}
\]

where \( A \) is the cross-sectional area of the sphere and the scattering efficiency follows as \( Q_{\text{sct}} = Q_{\text{ext}} - Q_{\text{abs}} \). The radiation pressure efficiency, which measures the total rate of momentum transfer to the particle, can be converted to the asymmetry parameter, \( g \), by

\[
g = \frac{(Q_{\text{ext}} - Q_{\text{pr}})}{Q_{\text{sct}}} \quad \text{(19)}
\]

Complex angular momentum theory can be used to determine the Mie efficiency factors of a sphere that is large compared with the wavelength. The governing equations have been developed by Nussenzveig and Wiscombe\(^4\). (These equations have been replicated in Appendix A due to their ex-

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Nussenzveig and Wiscombe have shown that when compared with exact Mie values, complex angular momentum theory gives relative errors of \(-(1-10)\)% for \(X = 10\) and \(-(0.01-0.001)\)% for \(X = 1000\). The theory does not predict the rapid changes in the values of \(Q_{\text{ext}}\) and \(Q_{\text{abs}}\) as a function of size parameter, but this high-frequency "ripple structure" can be ignored in many applications.

### 3.2 Software

Source code has been obtained from Warren Wiscombe\(^5\) which calculates \(Q_{\text{ext}}, Q_{\text{abs}}\) and \(Q_{\text{pr}}\) using complex angular momentum theory. The code was written in standard Fortran 77 and therefore, required very few modifications to operate on the AFGL CYBER system. Specifically, to avoid underflow errors, checks have been inserted before calls to the Fortran CEXP function. In addition the ACCUR parameter in the code, which establishes a convergence criterion for numerical integrations, has been changed from \(10^{-6}\) to \(10^{-3}\). This change was recommended by Warren Wiscombe and acts to speed up the program without a significant loss of accuracy.

### 3.3 Timing Comparisons with Mie Theory

It is well known that the computation time for Mie calculations is directly proportional to the size parameter. Figure 7 illustrates this clearly where the contours represent CPU times for various size parameters and imaginary indices of refraction. The CPU times were determined using

\(^{5}\) Wiscombe, W. J., private communication.
Figure 7. Computation Time for Mie Theory (in CPU seconds) as a Function of Size Parameter and the Imaginary Part of the Index of Refraction
the Fortran SECOND function, available on the AFGL Cyber computer.

For complex angular momentum theory, the expression for $Q_{\text{ext}}$ is a "one line" expression that requires very little computer time. On the other hand, the expressions for $Q_{\text{abs}}$ and $Q_{\text{pr}}$ involve numerical integrations that require more CPU time. Therefore, a series of timing runs have been performed for a wide range of size parameters and indices of refraction to determine where complex angular momentum theory is faster than Mie theory. In the comparisons, the CPU time for complex angular momentum theory represents the total time required to compute $Q_{\text{ext}}$, $Q_{\text{abs}}$ and $Q_{\text{pr}}$. ($Q_{\text{ext}}$, $Q_{\text{abs}}$ and $Q_{\text{pr}}$ are computed simultaneously during a single Mie run.)

Figure 8 gives CPU times for complex angular momentum theory as a function of size parameter and imaginary index of refraction. The figure suggests that there is broad minima in the CPU time for imaginary indices of -1 - (0.01 - 1). Other timing runs indicated that the CPU times were not influenced by the real index of refraction.

Figure 9 compares the CPU times for complex angular momentum theory against those for Mie theory where the comparison is expressed as

$$\log \left( \frac{T_{\text{APX}}}{T_{\text{MIE}}} \right).$$

(20)

In Figure 9, it can be seen that complex angular momentum theory is faster than Mie theory for size parameters greater
Figure 8. Computation Time for Complex Angular Momentum Theory (in CPU seconds) as a Function of Size Parameter and the Imaginary Part of the Index of Refraction. The Shaded Region Denotes Where the Computation Time Is Less Than 0.03 Seconds
Figure 9. Comparison of the Computation Times for Complex Angular Momentum Theory Against Those for Mie Theory. The Shaded Region Indicates Where Complex Angular Momentum Theory Is Faster Than Mie Theory.
than 200 to 500, depending on the imaginary index of refraction. Furthermore, percent errors are generally less than 1% for size parameters greater than 500 so Mie theory can be replaced by complex angular momentum theory without sacrificing accuracy.

3.4 A Singularity in the Expression for $Q_{\text{ext}}$

In the course of testing the source code provided by Warren Wiscombe, it was discovered that a singularity exists for $Q_{\text{ext}}$ whenever the imaginary index was less than about $10^{-3}$ and the real index equals 3, 5, 7... Specifically, this ill-behavior arises from a division by zero in the summation term of Eq. 1 of Nussenzveig and Wiscombe$^4$. The extent of the ill-behavior can be seen in Figures 10(a) and 10(b) where percent errors, when compared with Mie theory values, are given for real parts of 2.5 and 3.0. Subsequent testing showed that the expression for $Q_{\text{ext}}$ can be used confidently provided

$$|n - n^*| > 0.05$$

(21)

where $n^* = 3, 5, 7...$
Figure 10. Percent Errors in $Q_{\text{ext}}$ for Complex Angular Momentum Theory for (a) $n = 2.50$
Figure 10. (continued) Percent Errors in $Q_{ext}$ for Complex Angular Momentum Theory for (b) $n = 3.00$. In (b), the shaded region illustrates the singularity.
4. OTHER APPROXIMATIONS FOR $Q_{\text{ext}}$ AND $Q_{\text{abs}}$

This chapter examines various approximations for $Q_{\text{ext}}$ and $Q_{\text{abs}}$ that are available in the scientific literature. Specifically, regions of validity are established for each approximation by comparing exact Mie value against the corresponding approximate value. A wide range of size parameters and indices of refraction were considered in the analysis. In addition, the regions of validity are represented in a way that permits the various approximations to be intercompared. The purpose of this latter test is to see where better approximations are needed.

4.1 Approximations That Were Investigated

Five approximations for $Q_{\text{ext}}$ have been investigated in this report: two for small particles$^{6,7}$ and three for large particles$^{4,8,9}$. For $Q_{\text{abs}}$, a total of seven approximations were looked at: those given by $^{4,6-9}$, plus two other approximations for large particles$^{10,11}$. A brief description of

how each approximation works is given in Table 3. For reference, the equations governing the various approximations have been reproduced in Appendix A of this report.

4.2 Comparison Scheme

4.2.1 Realm of Comparison

Table 4 summarizes the size parameters and complex indices of refraction that are investigated in the current analysis. These values encompass the realm of particles normally encountered in atmospheric aerosol modeling. For each approximation, \( n \) is held fixed and the exact Mie and approximate values are calculated at incremental steps of the size parameter, \( X \), and the imaginary index of refraction, \( k \). The steps are equally spaced in the logarithms of \( X \) and \( k \) where the spacing consists of fifty steps per decade of \( X \) and twenty five steps per decade of \( k \). Similar sets of data are also computed for other fixed values of \( n \).

4.2.2 Smoothing Function

Before constructing error plots, data for Mie theory and the approximations have been convolved with an eleven point smoothing function, \( S \). Specifically, the smoothing function is passed over the data for \( X \geq 1 \) while \( k \) is held

---

### Table 3. Summary of the Approximations That Were Investigated

<table>
<thead>
<tr>
<th>RESEARCHER</th>
<th>PARTICLE SIZE</th>
<th>$Q_{\text{ext}}$</th>
<th>$Q_{\text{abs}}$</th>
<th>BRIEF DESCRIPTION</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rayleigh$^6$</td>
<td>Small</td>
<td>Yes</td>
<td>Yes</td>
<td>Radiation emitted by an oscillating dipole</td>
</tr>
<tr>
<td>Wiscombe$^7$</td>
<td>Small</td>
<td>Yes</td>
<td>Yes</td>
<td>Retention of first-order terms in the Mie expansion</td>
</tr>
<tr>
<td>Deirmendjian$^8$</td>
<td>Large</td>
<td>Yes</td>
<td>Yes</td>
<td>Applies an empirical correction to the anomalous diffraction theory of van de Hulst$^1$</td>
</tr>
<tr>
<td>Ackerman and Stephens$^9$</td>
<td>Large</td>
<td>Yes</td>
<td>Yes</td>
<td>Uses the anomalous diffraction theory of van de Hulst$^1$ plus first order corrections for refraction and edge effects</td>
</tr>
<tr>
<td>Nussenzveig and Wiscombe$^4$</td>
<td>Large</td>
<td>Yes</td>
<td>Yes</td>
<td>Complex angular momentum theory</td>
</tr>
<tr>
<td>Bohren and Nevitt$^{10}$</td>
<td>Large</td>
<td>No</td>
<td>Yes</td>
<td>Expression is developed from the laws governing geometrical optics</td>
</tr>
<tr>
<td>Levine$^{11}$</td>
<td>Large</td>
<td>No</td>
<td>Yes</td>
<td>Uses the van de Hulst$^1$ expression in the large particle limit plus a correction term for front surface reflections</td>
</tr>
</tbody>
</table>
Table 4. Particle Characteristics That Were Investigated

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>RANGE</th>
</tr>
</thead>
<tbody>
<tr>
<td>Real Part of the Index of Refraction, n</td>
<td>1.1 - 3.0</td>
</tr>
<tr>
<td>Imaginary Part of the Index of Refraction, k</td>
<td>10^{-6} - 10</td>
</tr>
<tr>
<td>Size Parameter, X</td>
<td>10^{-2} - 10^{3}</td>
</tr>
</tbody>
</table>

fixed so that

\[
\bar{F}_{X_i} = \sum_{L=0}^{10} S_L F_{X_i+L-5}
\]  

(22)

where \( F_{X_i} \) represents the Mie or approximate value at consecutive steps of the size parameter, \( X_i \). The weighting factors for the smoothing function are given by

\[
S_L = \frac{\binom{10}{L}}{1024}, \quad L = 0, 1, \ldots, 10
\]  

(23)

where \( \binom{10}{L} \) is the binomial coefficient,

\[
\binom{10}{L} = \frac{10!}{(\{L\})(10-L)!}.
\]  

(24)

The smoothing function acts to eliminate the high-frequency ripple structure that occurs in the exact Mie values.
for the efficiency factors as a function of $X$ for fixed $k$. For reference, the ripple structure in $Q_{sct}$ is illustrated in Figure 11 for fixed values of $k$. The reason for eliminating the ripple structure is twofold:

1) it allows for a fairer assessment of the various approximations because the ripple structure can only be calculated with Mie theory

2) since many aerosol modeling applications involve a polydispersion of particles, the effects of the ripples are "washed out" when integrating over particle size.

The width of the smoothing function has been chosen to preserve the large scale oscillations, known as interference structure.

4.2.3 Percent Error Contour Plots

For each approximation, two-dimensional percent error diagrams have been developed for fixed values of $n$. The percent errors are computed by

$$E_{X_i,k_j} = \frac{100(A_{X_i,k_j} - M_{X_i,k_j})}{M_{X_i,k_j}}$$

where $A$ and $M$ are the (smoothed) approximate and Mie values, respectively, evaluated at size parameter $X_i$ and imaginary index of refraction $k_j$. Contour lines have been drawn for percent errors of 8, 20 and 50%.

4.3 Results

4.3.1 Regions of Validity for the Extinction Approximations

Figures 12(a) - 12(e) give representative percent error diagrams for each of the extinction approximations. Each plot is for $n = 1.54$, and the regions where percent errors
Figure 11. Mie Theory Calculations of $Q_{\text{scat}}$ Showing the Interference and Ripple Structure as a Function of Size Parameter and $k$ for Fixed $n$ (\(= 1.33\))
Figure 12. Percent Errors in $Q_{\text{ext}}$ for the Approximation of (a) Rayleigh, for $n = 1.54$
Figure 12. (continued) Percent Errors in $Q_{ext}$ for the Approximation of (b) Wiscombe, for $n = 1.54$
Figure 12. (continued) Percent Errors in $Q_{\text{ext}}$ for the Approximation of (c) Deirmendjian, for $n = 1.54$
Figure 12. (continued) Percent Errors in $Q_{ext}$ for the Approximation of (d) Ackerman and Stephens, for $n = 1.54$
Figure 12. (continued) Percent Errors in $\varphi_{\text{ext}}$ for the Approximation of (e) Nussenzveig and Wiscombe, for $n = 1.54$
are less than 8% have been shaded. For brevity, plots for other values of n have not been included here.

Figures 12(a) - 12(e), and similar plots for other n, have been used to determine the regions of validity of the various approximations for $Q_{\text{ext}}$. These results are given in Figure 13. The dashed line for the Nussenzveig and Wiscombe approximation indicates the useful range if the singularity that arises for odd integer values of n is avoided (see Section 3.4).

In general, existing approximations for $Q_{\text{ext}}$ do reasonably well for both large and small size parameters. Of the large particle approximations, the Ackerman and Stephens approximation extends to the lowest size parameter. If higher accuracies are needed (i.e. 0.1 to 1% or better), the Nussenzveig and Wiscombe approximation has a wider useful range than the other large particle approximations because it reproduces the higher-order ripple structure better. Most approximations however, have trouble predicting the magnitude and location of the first interference peak which occurs between size parameters of 1 and 10 (see Figure 11). On the other hand, percent errors within this narrow band are generally less than 20% for many of the approximations.

4.3.2 Regions of Validity for the Absorption Approximations

Figures 14(a) - 14(g) give representative percent error diagrams for each of the absorption approximations. Each plot is for $n = 1.54$, and the regions where percent errors
Figure 13. Regions of Validity for the Mie Approximations for $Q_{\text{ext}}$. The Shaded Regions Indicates Where All of the Approximations Give Percent Errors $> 8\%$. The Dashed Line for the Nussenzveig and Wiscombe Approximation Indicates the Useful Range If the Singularity That Arises for Odd Integer Values of $n$ Is Avoided.
Figure 14. Percent Errors in $Q_{abs}$ for the Approximation of (a) Rayleigh, for $n = 1.54$
Figure 14. (continued) Percent Errors in $Q_{abs}$ for the Approximation of (b) Wiscombe, for $n = 1.54$.
Figure 14. (continued) Percent Errors in $Q_{abs}$ for the Approximation of (c) Deirmendjian, for $n = 1.54$
Figure 14. (continued) Percent Errors in $Q_{abs}$ for the Approximation of (d) Ackerman and Stephens, for $n = 1.54$
Figure 14. (continued) Percent Errors in $Q_{\text{abs}}$ for the Approximation of (e) Nussenzveig and Wiscombe, for $n = 1.54$
Figure 14. (continued) Percent Errors in $Q_{abs}$ for the Approximation of ($f$) Bohren and Nevitt, for $n = 1.54$
Figure 14. (continued) Percent Errors in $Q_{abs}$ for the Approximation of (g) Levine, for $n = 1.54$
are less than 20% have been shaded. For brevity, plots for other \( n \) have not been included here.

Figures 14(a) - 14(g), and similar plots for other \( n \), have been used to determine the regions of validity of the various approximations for \( Q_{\text{abs}} \). These results are given in Figure 15. The region of validity of the Nussenzveig and Wiscombe approximation is drawn with a dashed line because it is only computationally efficient for size parameters greater than about 200, relative to exact Mie theory (see Section 3.3), where it is accurate to about 0.1%. Also, to avoid clutter, the region of validity of the Ackerman and Stephens approximation has not been shown; however, its omission does not alter the shape of the shaded region in Figure 15 because the Ackerman and Stephens approximation for \( Q_{\text{abs}} \) is similar to the Bohren and Nevitt approximation.

Figure 15 suggests that existing approximations for \( Q_{\text{abs}} \) are less accurate than those for \( Q_{\text{ext}} \). For example, the tolerable error has been relaxed to 20% because significant errors extend to rather large size parameters. Of the large particle approximations, the Bohren and Nevitt approximation appears to have the largest region of applicability. In contrast to Figure 13, the percent errors within the shaded region of Figure 15 often exceed 50%.
Figure 15. Regions of Validity for the Mie Approximations for $Q_{abs}$. The Shaded Regions Indicates Where All of the Approximations Give Percent Errors $> 20\%$. The Ackerman and Stephens Approximation Is Omitted for Clarity, But Is Similar to That of Bohren and Nevitt. The Nussenzveig and Wiscombe Approximation Is Shown with a Dashed Line Because It Is Only Computationally Efficient for $X > 200$. 
5. SUMMARY AND CONCLUSIONS

This report has explored alternative algorithms to Mie theory. Specifically, Chapter 2 discussed the use of ray optics to calculate the phase matrix elements of polydisperse spheres in geometrical optics limit. Generally speaking, ray optics should be used for size parameters greater than 400, and becomes more accurate for particles containing significant absorption. Chapter 3 explored the use of complex angular momentum theory to determine $Q_{\text{ext}}$, $Q_{\text{abs}}$ and $Q_{\text{pr}}$ (or $g$). It was shown that although accurate for size parameters greater than 20, this technique is only computationally efficient for size parameters greater than 500. In Chapter 4, approximations for $Q_{\text{ext}}$ and $Q_{\text{abs}}$ in the scientific literature were investigated and their regions of validity were established. It was shown that existing approximations can give reasonable estimates of $Q_{\text{ext}}$ for most size parameters and complex indices of refraction. On the other hand, the approximations for $Q_{\text{abs}}$ are much less accurate.


5. Wiscombe, W. J., private communication.


Appendix A

Equations for the Various Mie Approximations Investigated in this Report

This appendix gives the equations used to calculate the extinction efficiency, $Q_{\text{ext}}$, and the absorption efficiency, $Q_{\text{abs}}$, for the Mie approximations discussed in this report. For some of the approximations, the scattering efficiency, $Q_{\text{sca}}$, is calculated in place of either $Q_{\text{ext}}$ or $Q_{\text{abs}}$ where the three terms are then related by $Q_{\text{ext}} = Q_{\text{sca}} + Q_{\text{abs}}$. The list of equations serves only as an overview and the reader should consult the original references for more detailed information. Also, some of notation from the original references has been changed such that it is consistent with the terminology used in this report. In the equations below, $\chi$ represents the particle size parameter and $\chi = n + ik$ represents the complex index of refraction of the particle.

Equations for the Rayleigh Approximation

The Rayleigh approximation for $Q_{\text{abs}}$ is computed as

$$Q_{\text{abs}} = 4\pi \text{Im} \left\{ \frac{m^2 - 1}{m^2 + 2} \right\} \quad (A-1)$$

and $Q_{\text{sca}}$ is given by

$$Q_{\text{sca}} = \frac{8}{3} \chi^4 \left| \frac{m^2 - 1}{m^2 + 2} \right|^2 \quad (A-2)$$

where $Q_{\text{ext}} = Q_{\text{sca}} + Q_{\text{abs}}$. 
Equations for the Wiscombe Approximation

The Wiscombe approximation for $Q_{\text{ext}}$ is computed as

$$Q_{\text{ext}} = 6 \Re \left( \hat{a}_1 + \hat{b}_1 + \frac{5}{3} \hat{a}_2 \right)$$  \hspace{1cm} (A-3)

and $Q_{\text{sca}}$ is given by

$$Q_{\text{sca}} = 6 \xi^4 T \hspace{1cm} (A-4)$$

where $Q_{\text{abs}} = Q_{\text{ext}} - Q_{\text{sca}}$ and

$$\hat{a}_1 = 2i \frac{m^2 - 1}{3} \frac{1 - \frac{1}{10} X^2 + \frac{4 m^4 + 5}{1400} X^4}{D}$$ \hspace{1cm} (A-5)

$$\hat{b}_1 = i X^2 \frac{m^2 - 1}{45} \frac{1 + \frac{2 m^2 - 5}{70} X^2}{1 - \frac{2 m^2 - 5}{30} X^2}$$ \hspace{1cm} (A-6)

$$\hat{a}_2 = i X^2 \frac{m^2 - 1}{15} \frac{1 - \frac{1}{14} X^2}{2 m^2 + 3 - \frac{2 m^2 - 7}{14} X^2}$$ \hspace{1cm} (A-7)

$$D = m^2 + 2 + \left( 1 - \frac{7}{10} m^2 \right) X^2 - \frac{8 m^4 - 385 m^2 + 350}{1400} X^4 \hspace{1cm} (A-8)$$

$$+ 2i \frac{m^2 - 1}{3} X^3 \left( 1 - \frac{1}{10} X^2 \right)$$

and

$$T = |\hat{a}_1|^2 + |\hat{b}_1|^2 + \frac{5}{3} |\hat{a}_2|^2 \hspace{1cm} (A-9)$$
Equations for the Deirmendjian Approximation

The Deirmendjian approximation for $Q_{ext}$ is computed as

$$Q_{ext} = Q_{VHext} (1 + D) \quad (A-10)$$

and $Q_{abs}$ is given by

$$Q_{abs} = Q_{VHabs} (1 + D) \quad (A-11)$$

where $Q_{VHext}$ is the extinction efficiency from van de Hulst,  

$$Q_{VHext} = 2 - \frac{4 \cos \beta}{\rho} \exp(-\rho \tan \beta) \sin(\rho - \beta)$$

$$+ 4\left(\frac{\cos \beta}{\rho}\right)^2 \left[ \cos 2\beta - \exp(-\rho \tan \beta) \cos(\rho - 2\beta) \right] \quad (A-12)$$

and $Q_{VHabs}$ is the absorption efficiency from van de Hulst,  

$$Q_{VHabs} = 1 + \frac{\exp(-2\rho \tan \beta)}{\rho \tan \beta} + \frac{\exp(-2\rho \tan \beta) - 1}{2(\rho \tan \beta)} \quad (A-13)$$

where

$$\beta = \tan^{-1}\left(\frac{k}{n-1}\right) \quad (A-14)$$

and

$$\rho = 2\pi(n-1) \quad . \quad (A-15)$$
In Eqs. A-10 and A-11, the correction term, \( D \), is given by

\[
D = \begin{cases} 
\frac{(n-1)^2}{1.632n} [f(\beta) + 1] + \frac{0.2n - n + 1}{(n-1)\beta(\beta)} & \text{for } \rho \leq 5(n-1) \\
\frac{n-1}{8.16n} [\beta(\beta) + 1] \rho & \text{for } 5(n-1) \leq \rho \leq \frac{4.08}{1 + 3\tan \beta} \\
\frac{(n-1)[\beta(\beta) + 1]}{2n(1 + 3\tan \beta)} & \text{for } \frac{4.08}{1 + 3\tan \beta} \leq \rho \leq \frac{4.08}{1 + \tan \beta} \\
\frac{2.04(n-1)[\beta(\beta) + 1]}{n\beta(\beta) \rho} & \text{for } \rho > \frac{4.08}{1 + \tan \beta}
\end{cases}
\]  

(A-16)

where

\[
f(\beta) = 1 + 4\tan \beta + 3\tan^2 \beta
\]  

(A-17)
Equations for the Ackerman and Stephens Approximation

The Ackerman and Stephens approximation for $Q_{\text{ext}}$ is computed as

$$Q_{\text{ext}} = 2 - \frac{4m^2}{\rho} e^{-\rho \tan \beta} \left[ \cos \beta \sin (\rho - \beta) + \frac{\cos^2 \beta}{\rho} \cos (\rho - 2\beta) \right]$$

$$+ \frac{4m^2}{\rho} e^{-\rho \tan \beta \sqrt{1 - m^{-2}}} \left[ \sqrt{1 - m^{-2}} \cos \beta \right.$$ \nonumber

$$\left. \times \sin (\rho \sqrt{1 - m^{-2}} - \beta) + \frac{\cos^2 \beta}{\rho} \cos (\rho \sqrt{1 - m^{-2}} - 2\beta) \right] \quad (A-18)$$

and $Q_{\text{abs}}$ is given by

$$Q_{\text{abs}} = 2 + \frac{m^2}{2\chi k} e^{-4\chi k} \left[ 1 + (4\chi k)^{-1} \right]$$

$$- \frac{m}{2\chi k} e^{-4\chi k \sqrt{1 - m^{-2}}} \left( \sqrt{m^2 - 1} + \frac{m}{4\chi k} \right) \quad (A-19)$$

where

$$\beta = \tan^{-1} \left( \frac{k}{n-1} \right) \quad (A-20)$$

and

$$\rho = 2\chi (n-1) \quad (A-21)$$
Equations for the Nussenzveig and Wiscombe Approximation

The Nussenzveig and Wiscombe approximation for $Q_{\text{ext}}$ is computed as

$$Q_{\text{ext}} = 2 + 1.9923861X^{-\frac{2}{3}} + 8 \text{Im} \left\{ \frac{\pi}{4} (m^2 + 1) (m^2 - 1)^{-\frac{1}{2}} x^{-1} \right\}$$

$$- m^2 (m + 1)^{-1} (m^2 - 1)^{-1} \left[ 1 + \frac{i}{2X} \left( \frac{1}{m - 1} - \frac{m - 1}{m} \right) \right] x^{-1}$$

$$\times \exp[2i(m - 1)x] - \frac{1}{2}(m - 1) \sum_{j=1}^{m-1} \left[ j - \left( \frac{m - 1}{2} \right) \right]^{-1} \left( \frac{m - 1}{m + 1} \right)^{2j}$$

$$\times \exp \left\{ 2i (m - 1 + 2jm)x \right\} \right\} - 0.7153537X^{-\frac{4}{3}}$$

$$- 0.3320643 \text{Im} \left\{ e^{\frac{3}{2} (m^2 - 1)} (m^2 + 1) (2m^4 - 6m^2 + 3) \right\}^{-\frac{5}{3}}$$

$$+ O(x^{-2}) + \text{ripple} \quad \text{. (A-22)}$$

$Q_{\text{abs}}$ is given by

$$Q_{\text{abs}} = \langle Q_{\text{abs}} \rangle_{\ast_{\ast}} + \langle Q_{\text{abs}} \rangle_{\ast_{\ast}} + \langle Q_{\text{abs}} \rangle_{\ast_{\ast}} \quad \text{(A-23)}$$

where

$$\langle Q_{\text{abs}} \rangle_{\ast_{\ast}} = \sum_{\lambda=1}^{2} \int_{0}^{\pi} \phi \left( r_{\lambda} \right) \sin \theta \cos \theta \, d\theta \quad \text{(A-24)}$$

$$\langle Q_{\text{abs}} \rangle_{\ast_{\ast}} = 2^{-\frac{1}{3}} X^{-\frac{2}{3}} \sum_{\lambda=1}^{2} \int_{0}^{\infty} \phi \left( r_{\lambda} \right) \, dx \quad \text{(A-25)}$$

and

$$\langle Q_{\text{abs}} \rangle_{\ast_{\ast}} = 2^{-\frac{1}{3}} X^{-\frac{2}{3}} \sum_{\lambda=1}^{2} \int_{0}^{\infty} \left[ \phi \left( r_{\lambda} \right) - \phi \left( \bar{r}_{\lambda} \right) \right] \, dx \quad \text{. (A-26)}$$
In Eqs. A-24 through A-26,\n\[
\phi(r_{j+1}) = (1 - e^{-b})(1 - r_{2j+1}) / (1 - r_{2j+1}e^{-b})
\] (A-27)

where \( r_{j+1} = |R_{j+1}|^2 \), \( j, \lambda = 1, 2 \); \( R_{j+1} = (-1)^j (z_{j+1} - u e_{\lambda}) / (z + u e_{\lambda}) \) (A-28)

\[
z = \cos \theta, \quad u = m \cos \theta', \quad \sin \theta = m \sin \theta',
\] (A-29)

\[
e_1 = 1, \quad e_2 = m^{-2}, \quad z_1 = z, \quad z_2 = \begin{cases} z & \text{for Eq. A-24} \\ z^* & \text{for Eqs. A-25 and A-26} \end{cases}
\] (A-30)

and finally,
\[
b = 4\pi \text{Im}(m \cos \theta' + \theta' \sin \theta)
\] (A-31)

**Equations for the Bohren and Nevitt Approximation**

The Bohren and Nevitt approximation for \( Q_{\text{abs}} \) is computed as

\[
Q_{\text{abs}} = \frac{4n^3}{(n + 1)^2 - (n - 1)^2 \exp(-\tau)} \left\{ \frac{1}{n^2} - \frac{2}{\tau^2} \left[ \exp\left( -\frac{\tau\sqrt{n^2 - 1}}{n} \right) \right] \right\}
\times \left\{ \frac{1 + \tau\sqrt{n^2 - 1}}{n} - \exp(-\tau)(1 + \tau) \right\}
\] (A-32)

where \( \tau = 4kX \) (A-33)
Equations for the Levine Approximation

The Levine approximation for $Q_{abs}$ is computed as

$$Q_{abs} = 2(1 - A)\{H(4kX) + H(B) - H(4kX + B)\}$$  \hspace{1cm} (A-34)

where the function $H(u)$ is given by

$$H(u) = \frac{1}{2} + \frac{e^{-u}}{u} + \frac{e^{-u} - 1}{u^2}$$  \hspace{1cm} (A-35)

and

$$B = \frac{2n\left[1 + \frac{2}{(n^2 + k^2)}\right]}{1 - A}.$$  \hspace{1cm} (A-36)

The value for $A$ in Eqs. A-34 and A-36 is determined using an iterative scheme given by

$$A = R + (A - 1) \exp \left[\frac{-2n\left(1 + \frac{2}{n^2 + k^2}\right)}{1 - A}\right]$$  \hspace{1cm} (A-37)

where the iteration is begun with $A^{(0)} = R$ and

$$R = \left[\frac{(n - 1)^2 + k^2}{(n + 1)^2 + k^2}\right].$$  \hspace{1cm} (A-38)