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DEEP-OCEAN BOTTOM PRESSURE AND TEMPERATURE SENSORS
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NARRAGANSETT GRADUATE SCHOOL OF OCEANOGRAPHY

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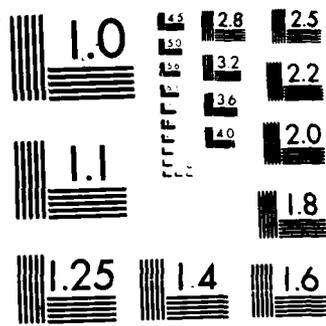
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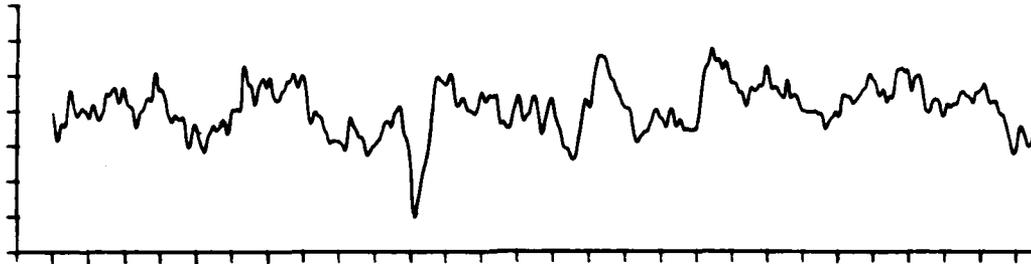
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DEEP-OCEAN BOTTOM PRESSURE
AND TEMPERATURE SENSORS REPORT:
METHODS AND DATA



by

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GRADUATE SCHOOL OF OCEANOGRAPHY
UNIVERSITY OF RHODE ISLAND
NARRAGANSETT, RHODE ISLAND

DEEP-OCEAN BOTTOM PRESSURE AND TEMPERATURE SENSORS

REPORT: METHODS AND DATA

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D. R. Watts and H. Kontoyiannis

December, 1986

GSO Technical Report No. 86-8

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ABSTRACT

This report documents ocean bottom pressure data collected from September 1983 to May 1985 in eleven deployments of pressure sensors under the Gulf Stream northeast of Cape Hatteras in depths of 3300 to 3900 m, as part of the Gulf Stream Dynamics Experiment.

In past experiments, pressure sensors suitable for ocean depths have typically exhibited systematic drifts in calibration that seriously contaminate any observed periodicities longer than a few days. We used Digiquartz sensors (manufactured by Paroscientific, Inc.), because these sensors offered potentially much lower drift than other commercially available sensors. In these sensors, either a bellows or a Bourdon tube applies stress to an oscillating quartz-crystal beam, causing its oscillation frequency to vary.

Several factors influence the amount of drift: bellows vs. Bourdon-tube construction, the applied pressure, the duration of deployment, and, for some sensors, high-pressure preconditioning in the lab. For the sensors deployed in the Gulf Stream, the total drift during deployments lasting from 3 to 12 months ranged from undetectable (≤ 0.01 dbar) to 0.20 to 0.50 dbar. About half of the total drift typically occurred within the first 6 days of deployment.

We estimate the residual error in the final pressure records, after the "dedrifting" calculations, to be typically 0.02 dbar r.m.s. (or 0.06 dbar r.m.s.) if the first 6 days of the record are excluded (or included, respectively). This low drift-error opens many possibilities for studies that require knowledge of the low-frequency dynamic pressure signal in the deep ocean.

Part I on Methods contains a short review of bottom pressure measurement in the deep ocean, a description of the sensors that we used, a discussion of their performance and drift relative to type of construction and prior pressurization history ("preconditioning"), and estimates of the accuracy of the dedrifted pressure records.

In Part II of this report, the full data processing is described, including calibration parameters, corrections for the influence of temperature variations on the pressure sensor, and parameterization to remove sensor drift errors by least-squares regression onto an exponentially decaying time-dependence. Time series are plotted which illustrate several steps in the processing: the edited half-hourly pressure records, the detided pressures with drift-model curves superimposed, and the low-pass filtered, "dedrifted" pressure records (i.e., after subtracting the estimated drift curve).



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PART I. METHODS

1. BOTTOM PRESSURE MEASUREMENT IN THE DEEP OCEAN

Physical oceanographers have long desired to have instrumentation capable of accurately monitoring the small variations in bottom pressures in the deep ocean (Baker, 1981) in order to observe the oceanic pressure field in analogy with the use of barometers by meteorologists. The measurement problem has been challenging because the dynamic pressure fluctuations are only ~ 0.10 to 0.01 dbar in an ambient pressure of 4000 dbar, requiring resolution and stability of ~ 1 ppm.

In the last fifteen years, deep-ocean bottom pressure measurements have been conducted in several studies on ocean tides (Filloux, 1971; Zetler et al., 1975), the ocean eddy pressure field (Brown et al., 1975), weather-induced bottom pressure fluctuations (Beardsley et al., 1977), and the performance of the pressure instruments themselves (Snodgrass et al., 1975). The most common pressure instruments used in the above studies have been strain gauges (Wunsch and Wimbush, 1977), Vibrotron sensors (Wimbush, 1977), metal Bourdon tubes (Filloux, 1971; Mofjeld and Wimbush, 1977), and quartz-crystal transducers (Snodgrass et al., 1975).

Although the requirement of adequate sensitivity and short-term stability is of great importance, the chief difficulty in dealing with pressure instruments is the instrumental noise of low frequency, i.e., drift, whose magnitude typically increases with applied pressure. Consequently, it has been most difficult to measure bottom pressures of the deep ocean. The drift contaminates the observed spectrum most at low frequencies. (A simple example is that a linear drift would add a red noise spectrum of slope f^{-2} .) Consequently, earlier studies with

deep pressure gauges have tended to focus on the higher frequency (less contaminated) aspects of the data.

In Part I, we present the experimental setting and measurements (Section 2), and we describe the pressure and temperature sensors (Section 3). We next discuss the observed pressure drifts in relation to sensor construction and to prior history of pressurization (Section 4). Next, we describe our techniques to model and remove the drift (Section 5), and finally we attempt to estimate the uncertainties in the drift removal, i.e., the accuracy of the final records (Section 6). All the time series plots of the data are shown in Part II.

2. EXPERIMENTAL SETTING AND MEASUREMENTS

2.1 Experiment Description and Overview

As part of the Gulf Stream Dynamics Experiment, data were collected using deep-ocean bottom pressure and temperature sensors in the Gulf Stream northeast of Cape Hatteras from September 1983 to May 1985. The measurements were made under the combined support of an NSF project entitled "The Dynamics of Gulf Stream Meanders" and an ONR project entitled "Observations on the Current Structure and Energetics of Gulf Stream Fluctuations Downstream of Cape Hatteras". Other data collected as part of this program are documented in separate reports (Tracey et al., 1985; Tracey and Watts, 1986b; Friedlander et al., 1986).

The deployment sites and the overall study area are shown in Figure 2.1. Inverted echo sounders were deployed at all the sites, whereas pressure sensors, along with temperature sensors, were deployed only at the sites indicated by the solid circles. The data records in this report are labelled by (a) the letters "PIES", indicating that a pressure sensor,

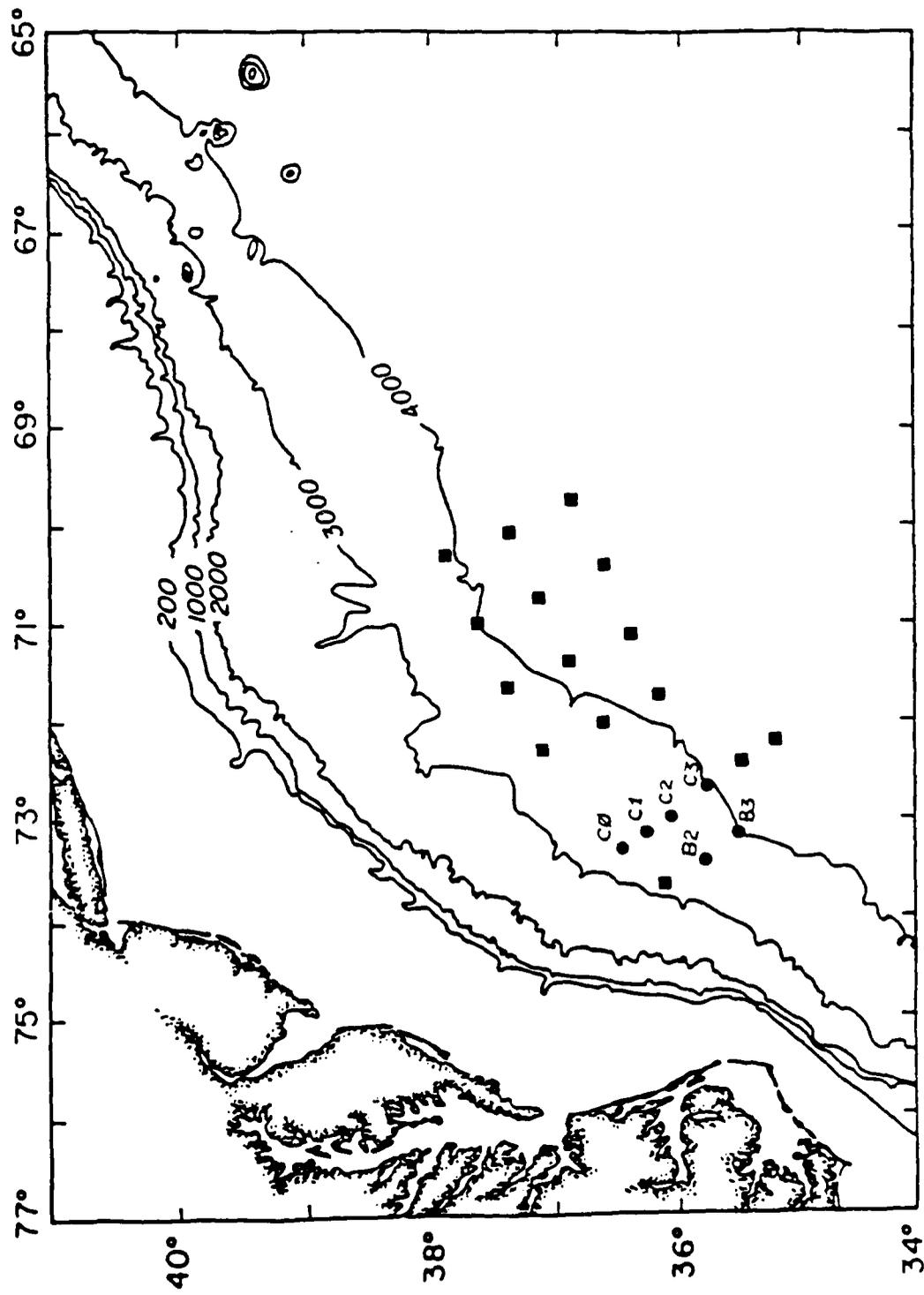


Figure 2.1 Study area and deployment sites. Inverted echo sounders were deployed at all 21 sites. Pressure sensors and temperature sensors were deployed at sites indicated by solid circles.

a temperature sensor, and an inverted echo sounder were deployed at the site, (b) the last two digits of the year (84 or 85) in which the instrument was recovered, (c) the site designation indicated in Figure 2.1, and (d) the letters "CM" between the line letter and the site number if a current meter mooring was also at the site. For example, PIES84BCM2 means the data record collected in 1984 at site B2 where a current meter mooring had also been deployed.

The time series plots of the raw, half-hourly bottom pressure and temperature measurements are given. Processing of the bottom pressure records included removal of the tides and, in particular, the long-term drift; these records are also shown. This report details the methods used to estimate and remove the drift, and to estimate the residual uncertainty. Subsequently, both the bottom pressure and temperature measurements were low-pass filtered, subsampled at six-hour intervals, and plotted. First order statistics (minimum, maximum, mean, and standard deviation) are listed for all data shown.

2.2 Data Recovery

In the 20-month period from September 1983 to May 1985, seven different pressure instruments (Table 2.1) were used for a total of eleven deployments at six sites (Table 2.2). These instruments were launched, recovered, and redeployed on five cruises aboard the R/V ENDEAVOR (EN106, 22-30 September 1983; EN107, 1-3 November 1983; EN118, 1-18 June 1984; EN124, 11-20 January 1985; EN130, 7-21 May 1985) and one cruise aboard the R/V OCEANUS (OC144, 9-19 January 1984).

In the eleven deployments of the deep-ocean pressure and temperature sensors, all instruments were recovered, giving an instrument recovery rate of 100%. Due to a malfunction of the electronic board controlling one pressure sensor, no pressure measurements were obtained for that

TABLE 2.1 Pressure sensors used

Sensor	Serial Number	Model	Working Range (dbar)	Type
1	8181	75K-002	0-3450	bellows
2	8180	75000	0-3450	bellows
3	17848	76KB-032	0-4100	Bourdon-tube
4	17849	76KB-032	0-4100	Bourdon-tube
5	17911	76KB-032	0-4100	Bourdon-tube
6	18426	76KB-032	0-4100	Bourdon-tube
7	19327	46K-032	0-4100	Bourdon-tube

TABLE 2.2 Deployment period (represented by the length of each rectangle) and pressure sensor used for each record.

Sites	Deployment Period																			
	1983				1984				1985											
	S	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D	J	F	M	A
B2	Sensor:1 PIES84B2		Sensor:1 PIES85BCM2																	
B3	Sensor:6 PIES85BCM3 (unreliable record)																			
C0											Sensor:5 PIES85C0									
C1	Sensor:3 PIES84C1		Sensor:3 PIES85CCM1 (sensor did not work)						Sensor:4 PIES85C1											
C2	Sensor:4 PIES84CCM2				Sensor:2 PIES85CCM2															
C3	Sensor:5 PIES84CCM3				Sensor:7 PIES85CCM3															

instrument during one deployment period (record PIES85CCM1). During the same deployment period, another pressure sensor malfunctioned; large steps (both positive and negative) were observed in the measured pressures (record PIES85BCM3). All nine remaining instruments performed successfully, giving an 82% data return for the pressure measurements. Complete records were obtained for all eleven deployments of the temperature sensors; thus the return rate was 100% for those data.

3. DESCRIPTION OF SENSORS

3.1 Pressure sensor and mounting

All the sensors we used have been manufactured by Paroscientific, Inc. A detailed description of the digital pressure transducers we used is given by Paros (1976) and by Wearn and Larson (1982). Briefly, the key sensing element in the pressure transducer is an oscillating, beam-shaped quartz crystal, which is piezoelectrically induced to vibrate in its lowest resonant flexural mode by an oscillator circuit. The oscillation frequency of the crystal varies with the stress load applied to it through a lever arm attached to either a bellows or Bourdon tube (Figure 3.1). The bellows or Bourdon tube is pressurized at the full ambient pressure of the ocean via a long, thin capillary tube filled with mineral oil. The measurement of fluid pressure is made by counting the output frequency of the oscillator circuit.

The pressure sensors were powered and controlled by Sea Data Corp. model XP35 electronics cards installed in inverted echo sounders (IESs). The IES circuitry and mooring configuration are described by Chaplin and Watts (1984). These instruments were tethered less than 1 m above the ocean floor, in order to have minimal vertical motion of the instrument in

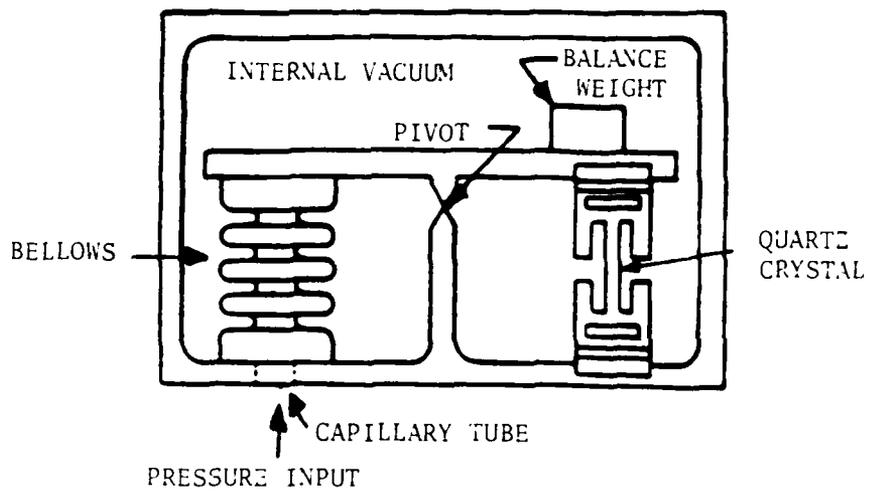


Figure 3.1 Schematic of the bellows-type Digi-quartz pressure sensor (Paroscientific, Inc.). In the Bourdon-tube type of sensor, the bellows is replaced by a Bourdon tube. The sensor is connected to the environment through a small capillary tube filled with mineral oil.

response to bottom currents; we estimate less than 0.5 cm vertical excursion in the peak observed deep current speeds (~30 cm/s) in this area.

Another potential concern for bottom pressure measurements is the stability of the mounting on the sea floor. Most evidence indicates no tendency in these deployments for the anchors to sink into the mud or for the bottom to slump downslope: all but one of the observed pressure drifts discussed in the following section are toward lower (rather than higher) pressures. Moreover, the acoustic travel times (τ) measured simultaneously on these IESs show no indication of depth change, although only large or sudden depth changes would be likely to show up in the τ records.

3.2 Temperature sensor

Because temperature also affects the oscillation frequency of the quartz crystal in the pressure sensor, it is essential to independently measure the temperature of the crystal. A thermistor (Yellow Springs International Corp., model 44032) was placed as close as possible to each sensor.

The thermistor was powered and controlled by Sea Data Corp. model DC37 electronics cards installed in the IESs. This circuitry produces an output frequency that varies with the temperature-dependent resistance of the thermistor.

3.3 Time base and recording

The frequency-counting periods for the above measurements were controlled by a quartz-crystal clock in the IES; the circuitry is described by Chaplin and Watts (1984). The stability of the crystal (JAN Crystals, model HC33/U AT cut 4.194304 MHz) and timing circuitry used in these deployments was reported by the company to be 25 ppm/ $^{\circ}$ C and

20 ppm in the first year. However, these stability specifications are not as good as they need to be; the JAN crystals were mistakenly used as a less expensive replacement for an earlier, better crystal. The JAN crystals had all been baked at elevated temperatures and aged before deployment; however, clock-frequency drift could still be responsible for most of the observed drifts in the measured pressures. (After these deployments, we discovered our error and upgraded the time bases.)

All the data were recorded digitally on the IES data cassettes using a Sea Data model 610 recorder.

4. OBSERVED DRIFTS OF PRESSURE SENSORS

4.1 General description of performance

In many records a long-term drift is apparent when we remove the mean and the tides. Some characteristics of this drift are summarized in Table 4.1, and plots of the detided pressures are shown in Part II (Figures 11.1 to 11.10).

Several features are common to these records: 1) During the first few hours (≤ 12 h) there is a rapid slewing toward higher pressure readings as the sensors come to thermal equilibrium at the ocean bottom. 2) During the next 3 to 12 months of deployment, several (five of the ten) pressure records drift by several tenths of a decibar, with the rate of drift decreasing greatly with increasing time. 3) Superimposed on the drift is the "ocean pressure signal", with obvious 5- to 30-day periodicities and 0.1- to 0.2-dbar pressure changes; these are the dynamic pressure signals of central scientific interest that we wish to study uncontaminated by drift. 4) There is high-frequency variability of roughly ± 0.02 dbar.

TABLE 4.1 Drift characteristics for each deployment.

Record	Sensor		Preconditioning			Deployment		Drift		
	Number	Type	Serial Number	Duration (months)	Pressure (dbar)	Dates	Duration (months)	Pressure (dbar)	Initial 6 days (dbar)	Entire record (dbar)
PIES84B2	1	bellows	8181	24	3200	Oct 83 - Jan 84	3	3625	-0.15	-0.21
PIES85BCM2	1	bellows	8181	3	3625	Jan 84 - Jan 85	12	3645	-0.17	-0.37
PIES85CCM2	2	bellows	8180	4	3900	Jun 84 - May 85	11	3730	+0.15	+0.48
PIES84C1	3	Bourdon-tube	17848	3	1400	Nov 83 - Jan 84	2	3514	*	none
PIES85CCM1	3	Bourdon-tube	17848	2	3514	Jan 84 - Jan 85	12	*	*	*
PIES84CCM2	4	Bourdon-tube	17849	-	-	Nov 83 - Jun 84	8	3730	0.12	-0.45
PIES85C1	4	Bourdon-tube	17849	-	-	Jan 85 - May 85	5	3530		none
PIES84CCM3	5	Bourdon-tube	17911	-	-	Jan 84 - Jun 84	6	3990		none
PIES85C0	5	Bourdon-tube	17911	-	-	Jan 85 - May 85	5	3340		none
PIES85BCM3	6	Bourdon-tube	18426	-	-	Jan 84 - Jan 85	12	†	†	†
PIES85CCM3	7	Bourdon-tube	19327	-	-	Jun 84 - May 85	11	3990	-0.08	-0.21

* Electronics failed.

† Record jumpy and unusable.

which exceeds measurement noise or our estimates of instrument depth variation.

Table 4.1 also summarizes the drift characteristics found for all the deployments; for simplicity, only the total change during the first 6 days and the total change from start to end of the record are listed. Several other factors are also listed that could be expected to influence the amount of drift. These include the ambient pressure (fairly similar at 3340 to 3990 dbar for all these deployments), the sensor construction (bellows vs. Bourdon tube), and whether the sensor was "preconditioned" to high pressure for some period before deployment. The following subsections discuss the amount of drift in relation to these factors, although we must caution that we have very few replicate cases for comparison.

4.2 Bellows vs. Bourdon-tube construction

We first categorize the drift performance by bellows vs. Bourdon-tube construction (Table 4.1). There were two bellows sensors with three deployment records, all of which showed significant drift (~0.20 to 0.50 dbar). Five Bourdon-tube sensors used in eight deployments produced seven records; in the second deployment of sensor 3 (record PIES85CCM1), the electronics did not work. In four of the seven recovered records, there was no detectable drift, but in the other three records, the sensors unfortunately performed unpredictably: One sensor (4; record PIES84CCM2) had one of the worst drifts of all (0.45 dbar) in its first deployment but none in its next (record PIES85C1). (This sensor was used in two different IESs. Clock-frequency drift could be responsible for this difference.) Another sensor (7; record PIES85CCM3) had -0.20 dbar drift. A third sensor (6; record PIES85BCM3) recorded numerous discontinuous jumps (-0.20 dbar) of varying size and sign (again, possibly

attributable to the time base crystal), as shown in Figure 11.3. Only one Bourdon-tube sensor (5) did not drift in both of its deployments.

4.3 Effect of prior pressurization ("preconditioning")

Secondly, we categorize performance according to whether the sensors were "preconditioned" at high pressure. Both bellows sensors were preconditioned. One bellows sensor (1), which was pressurized at 3200 dbar for 24 months prior to its deployment (at 3625 dbar), drifted only about half as much as the other bellows sensor (2). That sensor was pressurized at 3900 dbar for 4 months prior to deployment (at 3730 dbar) and drifted with opposite sign. (This is surprising, because Wearn and Larson (1982) suggest that all internally pressurized bellows sensors ought to drift in the same direction.) The opposite direction of drift may possibly be explained by the fact that the preconditioning was at a slightly higher pressure than that of the deployment.

The only Bourdon-tube sensor (3) that was preconditioned showed no drift, but other Bourdon-tube sensors had no drift without preconditioning.

5. METHOD OF DRIFT ESTIMATION AND REMOVAL

5.1 Introduction to drift modeling

Historically, investigators have modeled the drift of various pressure sensors by either a power-law [$-(t - t_0)^\beta$, $0 < \beta < 1$], logarithmic ["log-law", $-\ln(t - t_0)$] or exponential [$-\exp[-a(t - t_0)]$] dependence on time, t , after initial pressurization at $t = t_0$. Although the exact cause of the drift is unknown, it is believed to result from mechanical creep of materials subjected to high stress. The above three

dependencies have been used to describe creep in laboratory and geophysical studies, as has been reviewed by Wunsch and Wimbush (1977) and Wearn and Larson (1982).

It had been hoped and asserted (Wearn and Larson, 1980) that by careful measurement of drift characteristics of a sensor in the laboratory, the drift curve for it in an open ocean deployment might be accurately predicted. Skepticism has probably always been appropriate about applying such predictions, because the drift processes may not be reversible or reproducible. Moreover, for the deep-ocean pressure sensors it has not yet been practical to monitor the drift in the lab at the required ~ 1 -ppm accuracy for long time periods. In one of the best attempts (Wearn and Larson, 1980), the required level of absolute pressure and temperature stability was not achieved even by their high-quality calibration instruments.

In these deployments, the approach to drift removal has been to make least-squares fits of the above mathematical models to the records themselves. We used the non-linear least-squares regression routine, P3R, in the BMDP-79 package of computer programs (Dixon and Brown, 1979). Since the records are long compared to the time scales of the deep-ocean pressure variability, the "ocean pressure signal" will tend to average out in estimating the drift. We tried fitting our data to all three of the above drift dependencies and to an exponential-linear dependency; the results are compared in this section. The accuracy of the best-fit drift-curve models is discussed in Section 6.

5.2 Log-law vs. power-law least-squares fit

We first made a comparison between the power-law and the log-law types of drift, described by the following formulas, respectively:

$$P_{\text{drift}} = P_1 (t - t_0)^{P_2} + P_3$$

and

$$P_{\text{drift}} = P_1 \ln(t - t_0) + P_2$$

where t is the time in hours, t_0 is the time when the drift starts (13 hours before the first data point used, as explained in Section 8.3 in Part II), and P_1 , P_2 , and P_3 are free parameters whose values are individually determined for each record by the nonlinear regression subroutine.

The residual deviations of the measurements from the fitted curves are essentially the same for both laws and are shown in Table 5.1. The two types of curves, when plotted, are virtually indistinguishable within the measurement interval. The log law is preferred because of its computational simplicity and its rapid convergence to unique parameters. (By contrast, the regression for the power law converges slowly and the final parameters are affected by the starting values in the iteration process.) Values of P_1 and P_2 for the logarithmic drift curve model are listed in Table 5.2, with the r.m.s. deviations repeated for each record.

The logarithmic curves superimposed on our drift data are shown in the left-hand column of Figure 5.1. The fitted log-curves lie within the scatter of the data and approximate the existing drift remarkably well. However, in the first part (~30 days) of the records PIES84CCM2 and PIES85BCM2, the predicted drift rates are probably unreal (overestimated for PIES84CCM2 and underestimated for PIES85BCM2).

TABLE 5.1 The r.m.s. deviations of drift curves from the detided pressures. The r.m.s. $\Delta P_i = [\sum(\Delta P_i)^2 N^{-1}]^{1/2}$, where ΔP_i is the difference between P_{drift} and the detided pressure. The summation extends over all N points of the time series. The r.m.s. ΔP_i represents the r.m.s. ocean pressure signal.

Time is in hours; t_0 is the time when the drift starts.

$$\text{Power law: } P_{\text{drift}} = P_1 (t - t_0)^{P_2} + P_3$$

$$\text{Logarithmic law: } P_{\text{drift}} = P_1 \ln(t - t_0) + P_2$$

$$\text{Exponential law: } P_{\text{drift}} = P_1 [1 - \exp(P_2 t)] + P_3$$

$$\text{Exponential-linear law: } P_{\text{drift}} = P_1 [1 - \exp(P_2 t)] + P_3 + P_4 t$$

		r.m.s. ΔP_i (dbar)			
		Power	Logarithmic	Exponential	Exponential- Linear
Record	Sensor	Law	Law	Law	Law
PIES84B2	1	0.0372	0.0428	0.0372	0.0370
PIES85BCM2	1	0.0491	0.0474	0.0368	0.0368
PIES85CCM2	2	0.0361	0.0363	0.0421	0.0349
PIES84CCM2	4	0.0543	0.0542	0.0448	0.0449
PIES85CCM3	7	0.0412	0.0416	0.0370	0.0370

TABLE 5.2 Drift parameters for log-law least-squares fit:

$$P_{\text{drift}} = P_1 \ln [(t - t_0)] + P_2$$

or, in the case of no drift, P_{drift} is zero.

Parameters as in Table 5.1.

Record	Sensor	P_1 (dbar)	P_2 (dbar)	r.m.s. ΔP_1 (dbar)
PIES84B2	1	-0.037278	0.231444	0.043
PIES85BCM2	1	-0.048840	0.394873	0.047
PIES85CCM2	2	0.088609	-0.709164	0.036
PIES84C1	3	--	--	0.041
PIES84CCM2	4	-0.112501	0.852820	0.054
PIES85C1	4	--	--	0.030
PIES84CCM3	5	--	--	0.053
PIES85C0	5	--	--	0.042
PIES85CCM3	7	-0.035110	0.281740	0.042

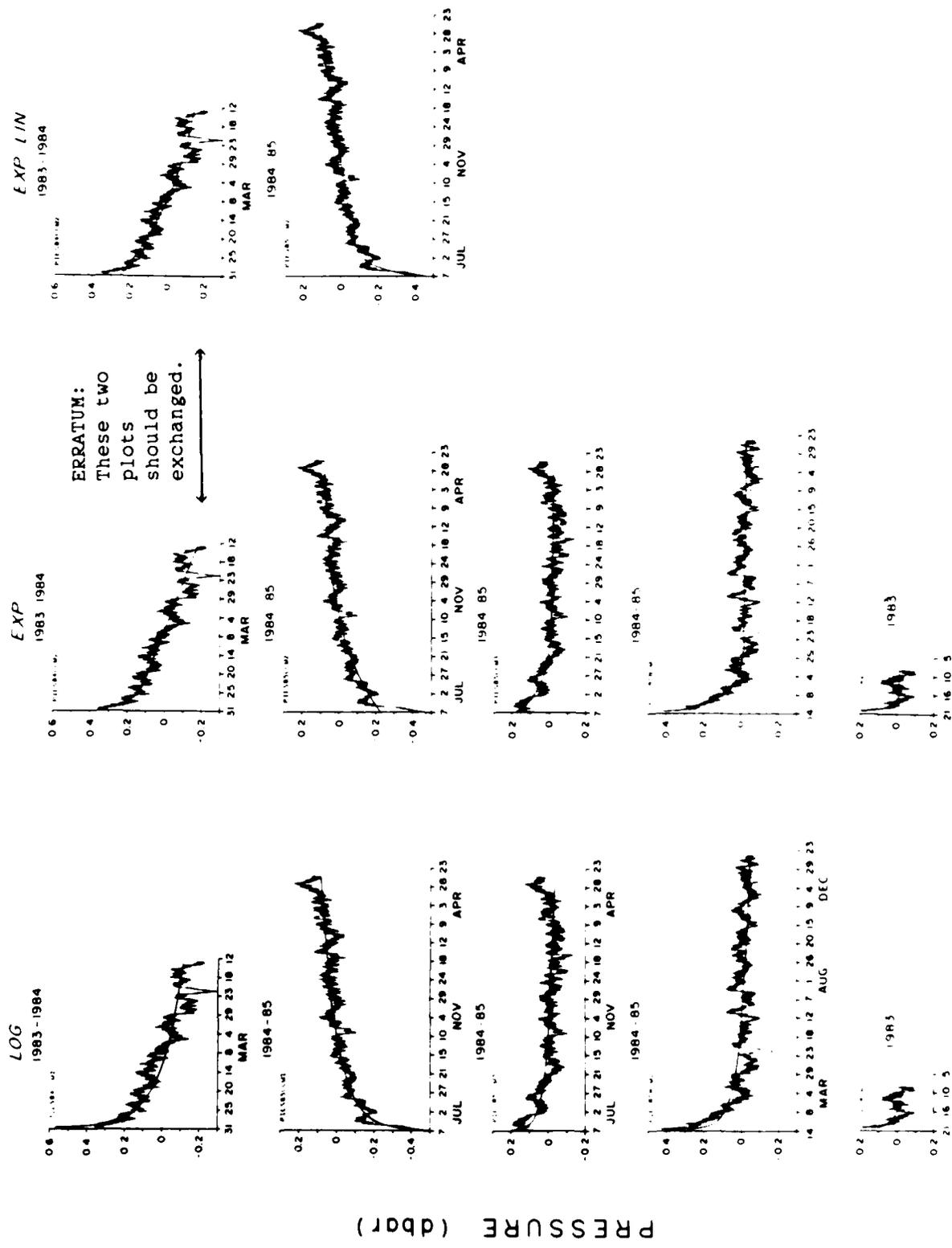


Figure 5.1 Plots of pressure drift vs. time with log-law, exponential, and exponential-linear curves superimposed.

5.3 Exponential and exponential-linear vs. log-law least-squares fit

We next made least-squares fits of exponential and exponential-linear curves to our data. The mathematical formulas we used were:

$$P_{\text{drift}} = P_1 [1 - \exp(P_2 t)] + P_3$$

for the exponential curve and

$$P_{\text{drift}} = P_1 [1 - \exp(P_2 t)] + P_3 + P_4 t$$

for the exponential-linear curve. Here P_1 , P_2 , P_3 , and P_4 are again free parameters determined by the non-linear regression subroutine and t is time in hours, relative to 13 hours before the first data point used (as explained in Section 8.3 of Part II). (N.B.: Both models could use any other chosen start time, t_0 , since any time shift, $t - t_0$, could be adjusted by corresponding changes in P_1 and P_3 .)

The above models converge rapidly and the parameters are independent of initial values in the iteration process. Values of P_1 , P_2 , P_3 , and P_4 for the exponential and exponential-linear drift curve models are listed in Table 5.3, with r.m.s. deviations repeated for each record. The predicted exponential and exponential-linear drift curves have in general smaller r.m.s. deviations from the original data than the logarithmic curves (Table 5.1). This was expected since they have more free parameters (four). However, curves for all the laws have similar shapes, and the r.m.s. residual is mainly from the oscillatory "ocean pressure signal". Plots of exponential and exponential-linear curves superimposed on the drift data are shown in the center and right-hand columns of Figure 5.1, respectively.

The regression subroutine detects no linear trends in records PIES85BCM2, PIES84B2 and PIES85CCM3. It gives $P_4 = 0$ and converges to the same values for P_1 , P_2 , and P_3 with the purely exponential type of drift. For these three records the exponential curves seem very satisfactory in

TABLE 5.3 Drift parameters for exponential $\{P_{\text{drift}} = P_1 [1 - \exp(P_2 t)] + P_3\}$ and exponential-linear $\{P_{\text{drift}} = P_1 [1 - \exp(P_2 t)] + P_3 + P_4 t\}$ least-squares fits. Parameters as in Table 5.1.

Record	Sensor	Drift law	P_1 (dbar)	P_2 (h^{-1})	P_3 (dbar)	P_4 (dbar/h)	r.m.s. ΔP_1 (dbar)
PIES84B2	1	exp.	-0.226419	-0.0110545	0.210320	--	0.037
PIES85BCM2	1	exp.	-0.369187	-0.00222225	0.350771	--	0.037
PIES85CCM2	2	exp.-lin.	0.296492	-0.0036410	-0.395883	0.000027	0.034
PIES84C1	3	-	--	--	--	--	0.040
PIES84CCM2	4	exp.	-0.511474	-0.0002825	0.244648	--	0.045
PIES85C1	4	-	--	--	--	--	0.030
PIES84CCM3	5	-	--	--	--	--	0.052
PIES85C0	5	-	--	--	--	--	0.041
PIES85CCM3	7	exp.	-0.193927	-0.0012165	0.174750	--	0.037

tracking the drift and were preferred over the logarithmic ones. In records PIES84CCM2 and PIES85CCM2 we observe a probable tendency for the exponential law to underestimate the drift rates at the beginning of the records and for the exponential-linear law to overestimate the drift rates at the end of the records. In the case of PIES84CCM2 we preferred the exponential curve: with its fewer parameters, the r.m.s. deviation was the best; we chose to accept the risk of retaining a small additional drift error in the first ~10 days of the record. In the case of PIES85CCM2 we preferred the exponential-linear curve; the r.m.s. deviation was significantly smaller with this law and we chose to accept the risk of introducing a linear drift trend of unknown origin (perhaps due to the JAN crystals).

5.4 The final ("residual") pressure records

The "residual" pressure records (detided and dedrifted), which are our best estimate of the true deep-ocean pressure signal, were calculated by subtracting the fitted P_{drift} curve, represented by the fit described above (Table 5.3), from its respective detided set of measurements at each half-hourly data point.

A low-pass filtered version of the pressure records is given in Figures 12.4 to 12.6 of Part II. All coincident records are plotted on the same time axes and with consistent pressure scales. (January-May 1984 is plotted twice to show the coincidence with earlier and later deployment periods.) Visually, the coherence between pressure records at neighboring sites is quite high. We have identified some of the major pressure-events with the passage of Gulf Stream rings offshore and their coalescence into the Gulf Stream (Bane and Watts, 1985).

6. ESTIMATED ACCURACY OF FINAL PRESSURE RECORDS

6.1 General remarks

The final record described in the previous section is a pressure record from which a drift curve has been subtracted; the best estimated drift curve is the exponential or exponential-linear least-squares fit whose parameters are listed in Table 5.3. We now attempt to estimate the uncertainty in the drift-removal procedure or, equivalently, to estimate the long-term accuracy of the dedrifted records. (N.B.: This is a separate question from that of the absolute accuracy of the mean pressure, which is about ± 1.5 dbar. The absolute accuracy has not been important thus far, because the absolute depth of the instrument site relative to the geoid is not known either.)

It is difficult to estimate the accuracy of the drift curves for these records. Each has a mixture of two unknown signals that differ for each site: the ocean pressure signal plus the drift. Some records are from different time periods, and others coincide in time but are from different sites (~15 to 50 km apart) with coherent, but different ocean pressure signals. We have no independent way to determine either the ocean pressure signal or the drift signal exactly, but the methods we have used to separate them essentially assume that they have different spectral characteristics.

Since the rate of drift decreases greatly with increasing time, another distinction is that the longer duration records (especially their later months) have a smaller proportion of their total variance associated with drift errors. Hence, they become more dominated by the ocean pressure signal.

6.2 Two methods to estimate uncertainties

We take advantage of these differences to estimate the errors in two ways. In the first method, we use records from two sites at which an instrument that had been deployed for several months was recovered and replaced almost immediately with another instrument at the same site. Figure 12.5 in Part II shows these cases (records PIES84CCM2 and PIES85CCM2 at site C2; records PIES84CCM3 and PIES85CCM3 at site C3), with the recovery and redeployment time in June 1984. The drift-removal error at the end of one record is probably small compared to that at the beginning of the subsequent record, since it seems reasonable to expect that the magnitude of error is roughly proportional to the amount of drift being removed. Hence, any pressure "jump" occurring between the records gives an estimate of the size of drift-removal error that characterizes the beginning of a record. The "jump" magnitudes are about 0.02 dbar at site C2 and 0.06 dbar at site C3 (also listed in Table 6.1A).

The second method to estimate the error was to regress the law selected for dedrifted on segments of the records. These segments have the same (true) drift curve, but our estimate of it will differ for different segments due to the contribution of the ocean pressure signal. An inference of how much the ocean pressure signal "contaminates" or causes the regressed drift curve to differ from the true drift can be taken from the difference between the regressed drift curves obtained from different segments of the record.

We used the second method only on the four longest records (7 to 12 months), because it was felt that dividing the records into segments shorter than 3 months was inadvisable, given the obviously energetic ocean pressure signals at shorter periodicities. Each of the four records was divided into two segments at a point which had a pressure near the overall

TABLE 6.1 Pressure offsets between drift curves estimated on different, sequential records (6.1A) and on segments of the same record (6.1B); estimated accuracy of final, "dedrifted" pressure records. The detection threshold (due to "noise" of the ocean pressure signal) of the exponential and exponential-linear least-squares fit is

$$< 0.01 \text{ dbar in 1 year. } \Delta P = \Delta P_b - \Delta P_a.$$

- t_a : Length of first segment or record
 t_b : Length of second segment or record
 ΔP : Pressure offset between drift curves of two segments at join-point or of two full records
 ΔP_a : Pressure offset between drift curve of first segment and drift curve of the full record at the end of first segment
 ΔP_b : Pressure offset between drift curve of second segment and drift curve of the full record at the beginning of second segment

6.1A Pressure offsets between different, sequential records

Records	t_a (months)	t_b (months)	ΔP (dbar)
PIES84CCM2 and PIES85CCM2	8	11	0.02
PIES84CCM3 and PIES85CCM3	6	11	0.06

6.1B Pressure offsets between segments of the same record

Record	t_a (months)	t_b (months)	ΔP (dbar)	ΔP_a (dbar)	ΔP_b (dbar)
PIES85BCM2	4.4	8	-0.015	0.013	-0.002
PIES85BCM2	7.4	5	0.000	0.001	0.001
PIES84CCM2	3	4.3	-0.016	-0.052	-0.036
PIES84CCM2	4.6	2.6	0.042	-0.020	0.022
PIES85CCM2	2.6	8.6	-0.007	-0.004	-0.011
PIES85CCM2	5.6	5.6	0.037	-0.028	0.009
PIES85CCM2	8.3	2.9	0.053	-0.004	0.049
PIES85CCM3	2.6	8.6	0.003	0.014	0.017
PIES85CCM3	5.6	5.6	-0.006	0.006	0.000
r.m.s. ΔP for segments:			0.027	0.021	0.022
r.m.s. ΔP for full 12-month record*:			0.019	0.015	0.016

* Obtained by dividing by $(2)^{1/2}$, because the degrees of freedom are doubled.

drift curve, to avoid introducing new "end effects". A curve was fitted to model the drift for each segment. Then we computed the offsets between these fitted curves at the point where one joins or overlaps another. At the same point, we also computed the differences between the curves fitted on the segments and the curve originally fitted on the whole record. The results of these calculations are summarized in Table 6.1B. The magnitudes of the offsets range from 0.000 to 0.053 dbar, with a r.m.s. offset of 0.023 dbar.

6.3 Discussion of drift uncertainty estimates

We now argue that the offsets between the above exponential-law regressions on segments of each given record are probably overestimates of the uncertainty of the drift regression on the full record. Two reasons support this contention: (1) The offsets occur at the beginning of each segment, where the regressed curve has its maximum amplitude and probably maximum error. However, in the regression curve for the full record, the corresponding time is not at the beginning, but farther out in the tail of the true drift curve, where the drift rate is slower and the error should be smaller. (2) The full-record regression curve is 2 or 4 times as long as the independent segments, with consequently greater degrees of freedom and more confidence in "averaging out" the ocean pressure signal; invoking a "central-limit theorem" that the ocean signal ought to be normally distributed given sufficient degrees of freedom, would suggest that doubling (or quadrupling) a record length would improve the removal of ocean pressure signal from the drift by a factor of $2^{1/2}$ (or 2, respectively). These arguments are applied in the footnote to Table 6.1B.

7. SUMMARY OF PART I

Ten records from seven Digiquartz deep-ocean bottom pressure sensors (Paroscientific, Inc.) have been obtained in eleven deployments of 3 to 12 months between September 1983 and May 1985. The deployments were under the Gulf Stream northeast of Cape Hatteras in depths of 3300 to 3900 m, as part of the Gulf Stream Dynamics Experiment. Two of the pressure sensors had bellows; five had Bourdon tubes. The records were examined with particular attention to estimating and removing any observed drift in calibration. (For this set of deployments, much of the drift may unfortunately be due to drift of the control crystals for the time base. Using better clock crystals in future deployments should result in less drift.)

All three records from the two bellows-type sensors exhibited significant drift. (Surprisingly, one sensor drifted in the opposite sense of the other sensor.)

Seven records were obtained with the five Bourdon-tube sensors. Two of these sensors were deployed twice; of these four records, three records had no detectable drift and one record (a first deployment) had a large drift. Three sensors were deployed once; of these three records, one had no detectable drift, one had significant drift, and one was jumpy and unreliable.

The drift was removed from five pressure records as follows: Least-squares fits of the power-law, logarithmic, exponential, and exponential-linear dependencies on time were made to each detided pressure record. The best-fit drift curve was subtracted from the record at each data point, yielding the "residual" pressure record. For four records,

the exponential drift curve had the best fit; for one record, the exponential-linear drift curve had the best fit.

We estimate that the errors in our drift-removal procedure are as much as 0.06 dbar (range ± 0.02 to ± 0.06 dbar; Table 6.1A) if the entire record is considered. However, the pressure error is estimated to be about 0.02 dbar r.m.s. (range ± 0.01 to ± 0.05 dbar; Table 6.1B) if the first week of a record is not included.

The residual uncertainties in the final "dedrifted" pressure records are small compared to the r.m.s. ocean pressure signal observed, and will tend to contaminate only the relatively long periodicities (≥ 60 to 90 d) in these records. This opens many possibilities for studies requiring knowledge of the deep-ocean dynamic pressures. Moreover, bottom pressure gauges in combination with inverted echo sounders can provide highly accurate definition of variations in the sea-surface height.

PART II. DATA

8. DATA PROCESSING

8.1 Program Flow Chart and Description

The data processing for all the IES, pressure, and temperature records was done on a PRIME 750 computer, using FORTRAN 77 with some extensions for bit manipulation. The basic procedural steps on the pressure data are illustrated by the flow chart in Figure 8.1 and are accomplished by a series of routines developed specifically for the IES (Tracey and Watts, 1987). The raw data are recorded within the IES on Sea Data model 610 recorders. The cassette tape contains the counts associated with sequential record number, acoustic travel time, pressure, and temperature measurements as a series of integer words of varying lengths. The subsequent processing steps are outlined below.

CARP: Transfers the data from cassettes to 9-track magnetic tape for subsequent processing.

BUNS: Converts the series of integer words of varying lengths into standard length 32-bit integer words.

MEMOD: Establishes the time base from the sequence number. Converts all travel time, pressure and temperature counts into scientific units of seconds, decibars, and degrees Celsius, respectively.

FILL: Checks for proper increment of the time base. Missing data points are filled by inserting interpolated values.

DESPIKE: Identifies and replaces travel time, pressure and temperature spikes with interpolated values.

RESPO: Determines the mean and the tidal constituents by using tidal response analysis (Munk and Cartwright, 1977). The mean and

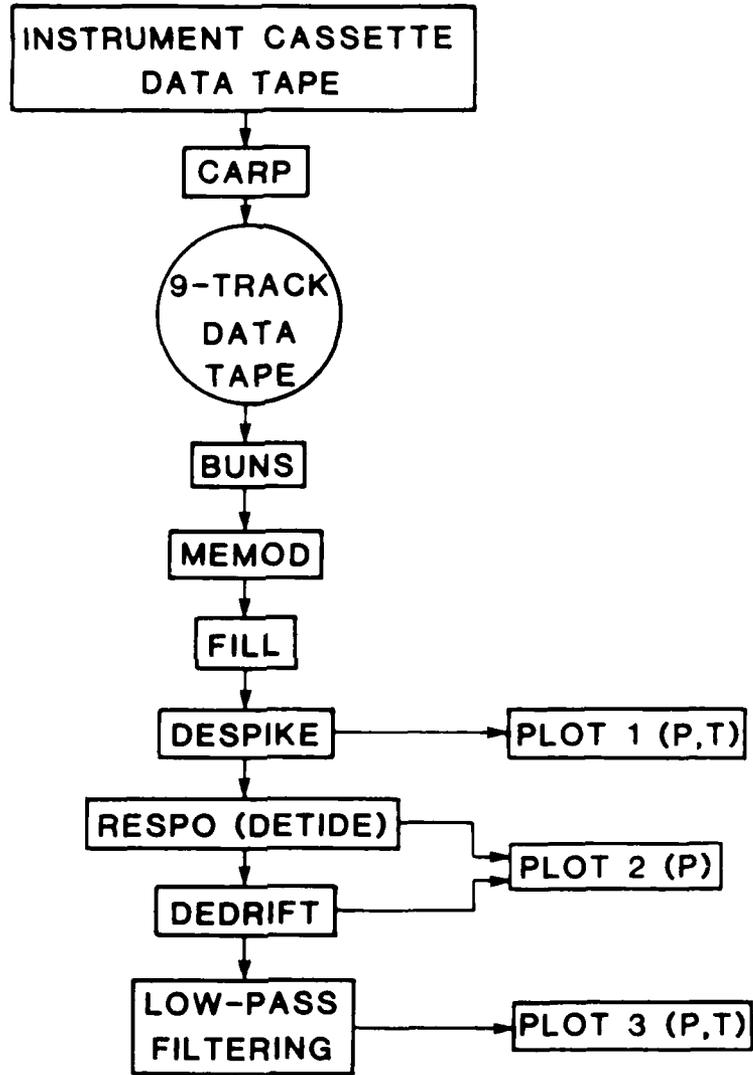


Figure 8.1 Pressure data processing flowchart

the calculated tides are then removed from the pressure values.

DEDRIFT: Identifies and removes the long-term drift of the detided pressures. The drift is tracked through the non-linear regression subroutine P3R of BMDP-79, a package of computer programs developed at UCLA (Dixon and Brown, 1979).

LOW-PASS FILTERING: Convolves the residual (detided and dedrifted) pressures with a 40-hour low-pass Lanczos filter. The FESTSA time series analysis package (Brooks, 1976), modified for the PRIME 750, was used to remove the higher frequency (tidal and inertial) motions from those with periods of several days or longer. The symmetric filter, with a Lanczos taper, was designed with the half power (-6 db) at 0.025 cph and -60 db attenuation at tidal frequencies (0.0833 cph). The smoothed output time series ("40HRLP") for pressure and temperature were subsampled at six-hour intervals.

8.2 Conversion to Scientific Units

Both the temperatures (T) and the pressures (P) are determined by counting frequencies that vary in accord with individually calibrated relationships for T and P. These are described below and the individual parameters for each instrument are given in the tables in Section 9.

8.2.1 Temperature

The T measurement is independent of P; that is, the thermistor does not vary with pressure. Thus, only the temperature-dependent resistance, $R(T)$, of the thermistor controls a variable-frequency oscillator on the DC37 electronics card (Sea Data Corp.). This circuitry is designed such that it linearizes the output frequency, f_T , as a function of T within the range 0°C to 25°C . (This linearization is

set for a standard $R(T)$ curve for this model YSI thermistor and is supposed to be accurate to 0.1°C .) The frequency, f_T , is counted for a measurement interval, Z , and divided by a scale factor, S ($= 1$ in this case), to fit into a 16-bit integer word prior to recording on the cassette tape. Therefore, the recorded count is $N_T = Zf_T/S$. From N_T one can find T ($^{\circ}\text{C}$), which is the true average temperature over the sampling interval, Z . For these deployments, the sampling interval was 30 min (1800 s).

The conversion from counts to temperature is

$$(N_T - N_a)/(N_b - N_a) = (T - T_a)/(T_b - T_a),$$

where the constants (N_a, N_b) and (T_a, T_b) , listed in Table 8.1 for each sensor, are determined from laboratory calibrations. The accuracy of the temperature measurements is about 0.1°C and the resolution is 0.0002°C . The half-hourly temperature records are shown in Section 10 (Figures 10.1-10). The temperatures were low-pass filtered and are shown in Section 12 (Figures 12.1-3).

8.2.2 Pressure

The pressure sensor, suited for deep-ocean applications, has an output frequency, f_p , that not only depends strongly on P , but also depends significantly on T . The full-range change in frequency is typically from 36 to 40 kHz, depending on the applied pressure and type of construction. It is common practice to deal with the period, $\tau = 1/f_p$, rather than the frequency; the period ranges from 25 to 28 μsec . Accompanying each sensor, we purchased individual calibrations from Paroscientific, Inc. along with polynomial expressions to determine $P(\tau, T)$.

An XP35 electronics card (Sea Data Corp.) counts the pressure sensor oscillations for the measurement interval, Z , and divides the

TABLE 8.1 Constants T_a , N_a , T_b , and N_b used for conversion of temperature counts, N_T , to temperature in $^{\circ}\text{C}$.

Record	Sensor	T_a ($^{\circ}\text{C}$)	N_a	T_b ($^{\circ}\text{C}$)	N_b
PIES84B2	1	1	4554	10	46260
PIES85BCM2	1	1	4554	10	46260
PIES85CCM2	2	1	4518	10	46080
PIES84C1	3	1	4518	10	45900
PIES85CCM1	3	1	4518	10	45900
PIES84CCM2	4	1	4428	10	45720
PIES85C1	4	0	0	12.5	57600
PIES84CCM3	5	0	0	12.5	57600
PIES85C0*	5	0	0	12.5	57600
PIES85BCM3	6	0	0	12.5	57600
PIES85CCM3	7	1	4428	10	46080

* Note added in proofreading: For record PIES85C0, the constants listed in this table were used in processing the data; however, a more accurate set of constants ($T_a = 1$, $N_a = 4428$, $T_b = 10$, and $N_b = 45720$) would give temperatures 0.045°C warmer with the same range of temperatures observed (near 2.4°C). This offset is smaller than the uncertainty in the thermistor calibration and has been ignored in subsequent processing. The effect of this warmer temperature would shift the absolute pressure calculations 0.008 dbar lower, which is also insignificant.

counts by the scale factor, S , to fit into a 24-bit integer word for recording on the cassette tape. The sampling interval was 30 min (1800 s) and the scale factor was 4 for these deployments. Therefore, the recorded count is $N_p = Zf_p/S = 450/\tau$.

The polynomial relationships $P(\tau, T)$ from Paroscientific, Inc. are listed in Table 8.2 for each sensor. τ_0 is the vibrational period at zero applied pressure, with polynomial temperature dependence. The older sensors come with "A,B, τ_0 " coefficients, each of which has its own polynomial equation in temperature, T ($^{\circ}\text{F}$). The newer sensors preferably have "C,D, τ_0 " coefficients, again each with a polynomial T dependence (again in $^{\circ}\text{F}$, except sensor 7, which is in $^{\circ}\text{C}$).

The half-hourly measured pressure records are shown in Figures 10.11 to 10.20. The absolute accuracy of the long-term average pressure measurements is within 1.5 dbar, but the resolution is much better. The pressure change corresponding to a change in N_p of one count, under typical conditions of applied pressures (~ 3500 dbar) and deep temperatures ($\sim 2^{\circ}\text{C}$), ranges from 0.0010 to 0.0025 dbar for these deployments with a measurement interval of $Z = 1800$ s. The stability of these pressures is discussed in Section 8.3.

8.2.3 Time Base

The date and time were assigned to each sampling period. The tables in Section 9 report the hour, minutes, and seconds associated with the first and last sampling period as a six-digit number. All times are given as Greenwich Mean Time (GMT). For processing convenience, the times were converted into yearhours. Table 8.3 lists the yearhour that corresponds to 0000 GMT of each day for non-leap years. (For leap years, the yearhours can be determined by adding 24 to each day after February 28.) There are a total of 8760 hours in a

TABLE 8.2 Pressure sensor calibration equations, $P(\tau, T)$, to convert sensor oscillation period, τ (s), into pressure, P (psi), with functional dependence on temperature, T (either $^{\circ}\text{F}$ or $^{\circ}\text{C}$), and on the output period at zero pressure, τ_0 (s).

Set 1: (for sensors 1 and 2) $P = A(1 - \tau_0/\tau) - B(1 - \tau_0/\tau)^2$

$A = A_0 + A_1 T + A_2 T^2$ $\tau = 450/N_p$
 $B = B_0 + B_1 T + B_2 T^2$
 $\tau_0 = \tau_{00} + \tau_1 T + \tau_2 T^2$, $T : (^{\circ}\text{F})$ (Fahrenheit)

	<u>Sensor: 1. Serial #: 8181</u>	
$A_0: 5.18004 \cdot 10^4$	$B_0: 3.17505 \cdot 10^{-4}$	$\tau_{00}: 25.97996 \cdot 10^{-6}$
$A_1: -9.70308 \cdot 10^{-1}$	$B_1: -7.80773 \cdot 10^{-1}$	$\tau_1: -1.99543 \cdot 10^{-11}$
$A_2: 1.71739 \cdot 10^{-3}$	$B_2: 1.04970 \cdot 10^{-2}$	$\tau_2: 1.70393 \cdot 10^{-13}$
	<u>Sensor: 2. Serial #: 8180</u>	
$A_0: 4.87536 \cdot 10^4$	$B_0: 2.81395 \cdot 10^{-4}$	$\tau_{00}: 25.95124 \cdot 10^{-6}$
$A_1: -9.17509 \cdot 10^{-2}$	$B_1: 8.01378$	$\tau_1: -6.38494 \cdot 10^{-11}$
$A_2: -5.94345 \cdot 10^{-4}$	$B_2: -9.13550 \cdot 10^{-3}$	$\tau_2: 2.28777 \cdot 10^{-13}$

Set 2: (for sensors 3, 4, 5, 6) $P = C[(1 - (\tau_0/\tau)^2) - D(1 - (\tau_0/\tau)^2)^2]$

$C = C_0 + C_1 T + C_2 T^2$ $\tau = 450/N_p$
 $D = D_0 + D_1 T + D_2 T^2$
 $\tau_0 = \tau_{00} + \tau_1 T + \tau_2 T^2$, $T : (^{\circ}\text{F})$ (Fahrenheit)

	<u>Sensor: 3. Serial #: 17848</u>	
$C_0: -2.95074 \cdot 10^4$	$D_0: 5.00619 \cdot 10^{-5}$	$\tau_{00}: 28.05943 \cdot 10^{-6}$
$C_1: -1.40724 \cdot 10^{-1}$	$D_1: 4.19904 \cdot 10^{-5}$	$\tau_1: -1.72125 \cdot 10^{-10}$
$C_2: 6.61457 \cdot 10^{-4}$	$D_2: -1.20873 \cdot 10^{-7}$	$\tau_2: 6.73124 \cdot 10^{-13}$
	<u>Sensor: 4. Serial #: 17849</u>	
$C_0: -2.48035 \cdot 10^4$	$D_0: 4.55063 \cdot 10^{-2}$	$\tau_{00}: 28.92787 \cdot 10^{-6}$
$C_1: 5.17487 \cdot 10^{-1}$	$D_1: 1.06118 \cdot 10^{-4}$	$\tau_1: -1.45426 \cdot 10^{-10}$
$C_2: -4.92268 \cdot 10^{-4}$	$D_2: -2.66707 \cdot 10^{-7}$	$\tau_2: 7.89478 \cdot 10^{-13}$
	<u>Sensor: 5. Serial #: 17911</u>	
$C_0: -2.27081 \cdot 10^4$	$D_0: 5.62671 \cdot 10^{-2}$	$\tau_{00}: 29.75394 \cdot 10^{-6}$
$C_1: -5.35951 \cdot 10^{-1}$	$D_1: -3.31430 \cdot 10^{-5}$	$\tau_1: -1.95993 \cdot 10^{-10}$
$C_2: 2.09832 \cdot 10^{-3}$	$D_2: 1.16763 \cdot 10^{-7}$	$\tau_2: 7.66406 \cdot 10^{-13}$
	<u>Sensor: 6. Serial #: 18426</u>	
$C_0: -2.64209 \cdot 10^4$	$D_0: 6.22649 \cdot 10^{-2}$	$\tau_{00}: 29.16313 \cdot 10^{-6}$
$C_1: -2.91091 \cdot 10^{-1}$	$D_1: -2.16853 \cdot 10^{-5}$	$\tau_1: -1.94124 \cdot 10^{-10}$
$C_2: 1.09997 \cdot 10^{-3}$	$D_2: 7.50013 \cdot 10^{-8}$	$\tau_2: 5.35286 \cdot 10^{-13}$

Set 3: (for sensor 7) $P = C[(1 - (\tau_0/\tau)^2) - D(1 - (\tau_0/\tau)^2)^2]$

$C = C_0 + C_1 T + C_2 T^2$ $\tau = 450/N_p$
 $D = D_0$
 $\tau_0 = \tau_{00} + \tau_1 T + \tau_2 T^2 + \tau_3 T^3$, $T : (^{\circ}\text{C})$ (Centigrade)

	<u>Sensor: 7. Serial #: 19327</u>	
$C_0: -2.505732 \cdot 10^4$	$D_0: 3.720884 \cdot 10^{-2}$	$\tau_{00}: 29.613417 \cdot 10^{-6}$
$C_1: -6.270068 \cdot 10^{-1}$		$\tau_1: -5.454051 \cdot 10^{-10}$
$C_2: 5.399068 \cdot 10^{-3}$		$\tau_2: 3.093264 \cdot 10^{-12}$
		$\tau_3: 8.444666 \cdot 10^{-16}$

TABLE 8.3 Yearhour calendar for non-leap years. Only the yearhour corresponding to 0000 GMT is listed for each day.

JAN			FEB			MAR			APR			MAY			JUNE		
DATE	YEAR	HOUR															
DAY	(0000Z)		DAY	(0000Z)		DAY	(0000Z)		DAY	(0000Z)		DAY	(0000Z)		DAY	(0000Z)	
1	1	0	1	321	744	1	601	1416	1	911	2160	1	1211	2880	1	1521	3624
2	21	24	2	331	768	2	611	1440	2	921	2184	2	1221	2904	2	1531	3648
3	31	48	3	341	792	3	621	1464	3	931	2208	3	1231	2928	3	1541	3672
4	41	72	4	351	816	4	631	1488	4	941	2232	4	1241	2952	4	1551	3696
5	51	96	5	361	840	5	641	1512	5	951	2256	5	1251	2976	5	1561	3720
6	61	120	6	371	864	6	651	1536	6	961	2280	6	1261	3000	6	1571	3744
7	71	144	7	381	888	7	661	1560	7	971	2304	7	1271	3024	7	1581	3768
8	81	168	8	391	912	8	671	1584	8	981	2328	8	1281	3048	8	1591	3792
9	91	192	9	401	936	9	681	1608	9	991	2352	9	1291	3072	9	1601	3816
10	101	216	10	411	960	10	691	1632	10	1001	2376	10	1301	3096	10	1611	3840
11	111	240	11	421	984	11	701	1656	11	1011	2400	11	1311	3120	11	1621	3864
12	121	264	12	431	1008	12	711	1680	12	1021	2424	12	1321	3144	12	1631	3888
13	131	288	13	441	1032	13	721	1704	13	1031	2448	13	1331	3168	13	1641	3912
14	141	312	14	451	1056	14	731	1728	14	1041	2472	14	1341	3192	14	1651	3936
15	151	336	15	461	1080	15	741	1752	15	1051	2496	15	1351	3216	15	1661	3960
16	161	360	16	471	1104	16	751	1776	16	1061	2520	16	1361	3240	16	1671	3984
17	171	384	17	481	1128	17	761	1800	17	1071	2544	17	1371	3264	17	1681	4008
18	181	408	18	491	1152	18	771	1824	18	1081	2568	18	1381	3288	18	1691	4032
19	191	432	19	501	1176	19	781	1848	19	1091	2592	19	1391	3312	19	1701	4056
20	201	456	20	511	1200	20	791	1872	20	1101	2616	20	1401	3336	20	1711	4080
21	211	480	21	521	1224	21	801	1896	21	1111	2640	21	1411	3360	21	1721	4104
22	221	504	22	531	1248	22	811	1920	22	1121	2664	22	1421	3384	22	1731	4128
23	231	528	23	541	1272	23	821	1944	23	1131	2688	23	1431	3408	23	1741	4152
24	241	552	24	551	1296	24	831	1968	24	1141	2712	24	1441	3432	24	1751	4176
25	251	576	25	561	1320	25	841	1992	25	1151	2736	25	1451	3456	25	1761	4200
26	261	600	26	571	1344	26	851	2016	26	1161	2760	26	1461	3480	26	1771	4224
27	271	624	27	581	1368	27	861	2040	27	1171	2784	27	1471	3504	27	1781	4248
28	281	648	28	591	1392	28	871	2064	28	1181	2808	28	1481	3528	28	1791	4272
29	291	672	29	301	2088	29	381	2088	29	1191	2832	29	1491	3552	29	1801	4296
30	301	696	30	891	2112	30	891	2112	30	1201	2856	30	1501	3576	30	1811	4320
31	311	720				31	901	2136				31	1511	3600			

JULY			AUG			SEPT			OCT			NOV			DEC		
DATE	YEAR	HOUR															
DAY	(0000Z)		DAY	(0000Z)		DAY	(0000Z)		DAY	(0000Z)		DAY	(0000Z)		DAY	(0000Z)	
1	1821	4344	1	2131	5088	1	2441	5832	1	2741	6576	1	3051	7320	1	3351	8064
2	1831	4368	2	2141	5112	2	2451	5856	2	2751	6600	2	3061	7344	2	3361	8088
3	1841	4392	3	2151	5136	3	2461	5880	3	2761	6624	3	3071	7368	3	3371	8112
4	1851	4416	4	2161	5160	4	2471	5904	4	2771	6648	4	3081	7392	4	3381	8136
5	1861	4440	5	2171	5184	5	2481	5928	5	2781	6672	5	3091	7416	5	3391	8160
6	1871	4464	6	2181	5208	6	2491	5952	6	2791	6696	6	3101	7440	6	3401	8184
7	1881	4488	7	2191	5232	7	2501	5976	7	2801	6720	7	3111	7464	7	3411	8208
8	1891	4512	8	2201	5256	8	2511	6000	8	2811	6744	8	3121	7488	8	3421	8232
9	1901	4536	9	2211	5280	9	2521	6024	9	2821	6768	9	3131	7512	9	3431	8256
10	1911	4560	10	2221	5304	10	2531	6048	10	2831	6792	10	3141	7536	10	3441	8280
11	1921	4584	11	2231	5328	11	2541	6072	11	2841	6816	11	3151	7560	11	3451	8304
12	1931	4608	12	2241	5352	12	2551	6096	12	2851	6840	12	3161	7584	12	3461	8328
13	1941	4632	13	2251	5376	13	2561	6120	13	2861	6864	13	3171	7608	13	3471	8352
14	1951	4656	14	2261	5400	14	2571	6144	14	2871	6888	14	3181	7632	14	3481	8376
15	1961	4680	15	2271	5424	15	2581	6168	15	2881	6912	15	3191	7656	15	3491	8400
16	1971	4704	16	2281	5448	16	2591	6192	16	2891	6936	16	3201	7680	16	3501	8424
17	1981	4728	17	2291	5472	17	2601	6216	17	2901	6960	17	3211	7704	17	3511	8448
18	1991	4752	18	2301	5496	18	2611	6240	18	2911	6984	18	3221	7728	18	3521	8472
19	2001	4776	19	2311	5520	19	2621	6264	19	2921	7008	19	3231	7752	19	3531	8496
20	2011	4800	20	2321	5544	20	2631	6288	20	2931	7032	20	3241	7776	20	3541	8520
21	2021	4824	21	2331	5568	21	2641	6312	21	2941	7056	21	3251	7800	21	3551	8544
22	2031	4848	22	2341	5592	22	2651	6336	22	2951	7080	22	3261	7824	22	3561	8568
23	2041	4872	23	2351	5616	23	2661	6360	23	2961	7104	23	3271	7848	23	3571	8592
24	2051	4896	24	2361	5640	24	2671	6384	24	2971	7128	24	3281	7872	24	3581	8616
25	2061	4920	25	2371	5664	25	2681	6408	25	2981	7152	25	3291	7896	25	3591	8640
26	2071	4944	26	2381	5688	26	2691	6432	26	2991	7176	26	3301	7920	26	3601	8664
27	2081	4968	27	2391	5712	27	2701	6456	27	3001	7200	27	3311	7944	27	3611	8688
28	2091	4992	28	2401	5736	28	2711	6480	28	3011	7224	28	3321	7968	28	3621	8712
29	2101	5016	29	2411	5760	29	2721	6504	29	3021	7248	29	3331	7992	29	3631	8736
30	2111	5040	30	2421	5784	30	2731	6528	30	3031	7272	30	3341	8016	30	3641	8760
31	2121	5064	31	2431	5808				31	3041	7296				31	3651	8784

standard year and 8784 hours in a leap year. The yearhours given in this report are referenced to 0000 GMT on either January 1, 1984 or January 1, 1985, depending on the year in which the instrument was recovered; the two-digit number of the instrument name indicates which date is the reference. Positive yearhours correspond to sampling periods which occur during the same calendar year as the reference date; negative yearhours correspond to those which occur in the calendar year prior to the reference date.

8.3 Pressure Sensor Drift Estimation and Removal

Prior to determining the long-term drift of our measurements, the mean and the tides were removed from the original pressure measurements. The time origin (when the drift started; t_0) was assumed to be the time when the instrument was about halfway to the sea floor, or 1 hour before the first sample on the bottom. We also removed the first 12 hours of data (24 points) after the instrument landed on the sea floor because during this time the sensors inside the glass instrument housing were still coming to thermal equilibrium, causing these initial measurements to change rapidly. Hence, the time origin was 13 hours before the first data point used. For computational ease and speed in estimating the drift curve, we temporarily subsample the time series every two hours; however, the drift curve was later removed from the half-hourly time series.

The method of estimating and removing the long-term drift from the pressure records was described in Section 5, and the fitted drift parameters were listed in Table 5.3. The regressed drift curves are superimposed on the detided pressures in Figures 11.1 to 11.10.

The residual pressure records (detided and dedrifted), representing our best estimate of the true deep-ocean pressure signal, were calculated as the result of subtracting the fitted P_{drift} curve from the detided sets of measurements at each half-hourly data point. These dedrifted pressures were then low-pass filtered, and are shown in Figures 12.4 to 12.6.

9. PARAMETERS AND STATISTICS OF INDIVIDUAL SITES AND RECORDS

The location, dates, and basic statistics of the eleven instrument records are given in Tables 9.1 to 9.11. Each table documents a single instrument deployment. The useful data records are plotted in Sections 10, 11, and 12. General site information, such as position, bottom depth, and launch and recovery times, are given first, followed by details about the bottom pressure and temperature data sets. The times associated with the first and last data points are supplied. The time origin (t_0) is 13 hours before the first data point used. Yearhours are referenced to 0000 GMT on January 1 of the year indicated by the two-digit number in the instrument name. Positive yearhours occur during the same calendar year as the two-digit number; negative yearhours occur during the previous one.

The first order statistics (minimum, maximum, mean, and standard deviation) were calculated for the half-hourly and the 40HRLP records for each variable. These are also presented in the following tables. In Section 10 are plots of the measured (half-hourly) temperature and pressure data. The plots in Section 11 illustrate the detided pressure records, P_{detide} , before subtracting the drift, with the drift curve superimposed. The P_{residual} records, plotted in Section 12, were obtained by subtracting the mean pressure, the drift curve (if nonzero), and the tide record from the half-hourly measured pressures. The statistics for P_{residual} are included in the following tables.

40HRLP PRESSURE RECORDS

(Fig. 12.4)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Sep 26, 1983	060000	-2322.0000
LAST DATA POINT:	Nov 17, 1983	000000	-1080.0000

Number of points: 208
 Sampling Interval: 6.00 hrs

Minimum = -0.0790 dbar
 Maximum = 0.0814 dbar
 Mean = 0.0000 dbar
 Standard deviation = 0.0330 dbar

TEMPERATURE RECORDS

(Fig. 10.1)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Sep 24, 1983	232952	-2352.5025
LAST DATA POINT:	Nov 18, 1983	052952	-1050.5025

Number of points: 2605
 Sampling Interval: 0.50 hrs

Minimum = 2.173 °C
 Maximum = 2.272 °C
 Mean = 2.218 °C
 Standard deviation = 0.035 °C

40HRLP TEMPERATURE RECORDS

(Fig. 12.1)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Sep 26, 1983	060000	-2322.0000
LAST DATA POINT:	Nov 17, 1983	000000	-1080.0000

Number of points: 208
 Sampling Interval: 6.00 hrs

Minimum = 2.173 °C
 Maximum = 2.264 °C
 Mean = 2.219 °C
 Standard deviation = 0.026 °C

TABLE 9.2
PIES85BCM2

IES Serial Number: 055
Pressure Sensor Serial Number: 8181

Position: 35°48.09 N Depth: 3560 m
73°25.88 W

	<u>DATE</u>	<u>GMT</u>	<u>CRUISE</u>
LAUNCH:	Jan 16, 1984	2344	OC144
RECOVERY:	Jan 17, 1985	0104	EN124

MEASURED PRESSURE RECORDS
(Fig. 10.12)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 17, 1984	005927	-8399.009
LAST DATA POINT:	Jan 16, 1985	235927	383.9915

Number of points: 17567
Sampling Interval: 0.50 hrs

Minimum = 3645.84 dbar Mean = 3646.57 dbar
Maximum = 3647.71 dbar Standard deviation = 0.338 dbar

RESIDUAL PRESSURE RECORDS

$$P_{\text{residual}} = P_{\text{meas}} - \text{MEAN} - \text{DRIFT} - \text{TIDE}$$

$$\text{DRIFT} = P_1 [1 - \exp(P_2 t)] + P_3$$

where t = Time of sample in hours, starting with
 $t = 13.0$ for the first data point

$$P_1 = -0.378324 \text{ dbar}$$

$$P_2 = -0.0022225 \text{ h}^{-1}$$

$$P_3 = 0.359908 \text{ dbar}$$

TIDE calculated from the following constituents:

	<u>M2</u>	<u>N2</u>	<u>S2</u>	<u>K2</u>	<u>K1</u>	<u>O1</u>	<u>P1</u>	<u>O1</u>
H (dbar):	.43233	.10587	.08715	.02063	.09064	.06984	.02990	.01485
G°:	352.84	333.99	19.68	20.286	181.05	186.12	181.76	184.73

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 17, 1984	125927	-8387.009
LAST DATA POINT:	Jan 16, 1985	235927	383.991

Number of points: 17543
Sampling Interval: 0.50 hrs

Minimum = -0.1680 dbar Mean = 0.0000 dbar
Maximum = 0.1190 dbar Standard deviation = 0.0369 dbar

40HRLP PRESSURE RECORDS
(Fig. 12.5)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 19, 1984	000000	-8352.0000
LAST DATA POINT:	Jan 15, 1985	180000	354.0000

Number of points: 1452
Sampling Interval: 6.00 hrs

Minimum = -0.150 dbar
Maximum = 0.087 dbar
Mean = 0.0000 dbar
Standard deviation = 0.0334 dbar

TEMPERATURE RECORDS
(Figs. 10.2a and 10.2b)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 17 1984	125927	-8387.009
LAST DATA POINT:	Jan 16, 1985	235927	383.991

Number of points: 17543
Sampling Interval: 0.50 hrs

Minimum = 2.166 °C
Maximum = 2.435 °C
Mean = 2.232 °C
Standard deviation = 0.080 °C

40HRLP TEMPERATURE RECORDS
(Fig. 12.2)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 19, 1984	000000	-8352.0000
LAST DATA POINT:	Jan 15, 1985	180000	354.0000

Number of points: 1452
Sampling Interval: 6.00 hrs

Minimum = 2.168 °C
Maximum = 2.432 °C
Mean = 2.234 °C
Standard deviation = 0.054 °C

TABLE 9.3
PIES85BCH3

IES Serial Number: 034
Pressure Sensor Serial Number: 18426

Position: 35°31.00 N Depth: 3930 m
73°08.02 W

	<u>DATE</u>	<u>GMT</u>	<u>CRUISE</u>
LAUNCH:	Jan. 15, 1984	0352	OC144
RECOVERY:	Washed up on beach in Bermuda		

MEASURED PRESSURE RECORDS
(Figs. 10.13a and 10.13b)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan. 15, 1984	04 51 25	- 8443.143
LAST DATA POINT:	Jan. 3, 1985	02 51 25	52.356

Number of points: 16991
Sampling Interval: 0.50 hrs

(Pressure record is jumpy.)

TEMPERATURE RECORDS
(Figs. 10.3a and 10.3b)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan. 15, 1984	045125	- 8443.143
LAST DATA POINT:	Jan. 3, 1985	035125	52.356

Number of points: 16991
Sampling Interval: 0.50 hrs

Minimum = 2.440 °C
Maximum = 10.719 °C

Mean = 2.467 °C
Standard deviation = 0.107 °C

40HRLP PRESSURE RECORDS

(Fig. 12.6)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 20, 1985	180000	474.0000
LAST DATA POINT:	May 11, 1985	060000	3126.0000

Number of points: 443
 Sampling Interval: 6.00 hrs

Minimum = -0.0802 dbar
 Maximum = 0.0831 dbar
 Mean = 0.0000 dbar
 Standard deviation = 0.0369 dbar

TEMPERATURE RECORDS

(Fig. 10.4)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 18, 1985	210004	429.0011
LAST DATA POINT:	May 12, 1985	143004	3158.5011

Number of points: 5460
 Sampling Interval: 0.50 hrs

Minimum = 2.300 °C
 Maximum = 10.436 °C
 Mean = 2.373 °C
 Standard deviation = 0.140 °C

40HRLP TEMPERATURE RECORDS

(Fig. 12.3)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 20, 1985	180000	474.0000
LAST DATA POINT:	May 11, 1985	060000	3126.0000

Number of points: 443
 Sampling Interval: 6.00 hrs

Minimum = 2.312 °C
 Maximum = 2.461 °C
 Mean = 2.369 °C
 Standard deviation = 0.032 °C

TABLE 9.5
PIES84C1

IES Serial Number: 056
Pressure Sensor Serial Number: 17848

Position: 36°17.20 N Depth: 3450 m
73°11.40 W

	<u>DATE</u>	<u>GMT</u>	<u>CRUISE</u>
LAUNCH:	Nov 01, 1983	1903	EN107
RECOVERY:	Jan 11, 1984	1459	OC144

MEASURED PRESSURE RECORDS
(Fig. 10.15)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Nov 01, 1983	200406	-1443.9316
LAST DATA POINT:	Jan 11, 1984	143406	254.5683

Number of points: 3398
Sampling Interval: 0.50 hrs

Minimum = 3513.51 dbar Mean = 3514.20 dbar
Maximum = 3515.04 dbar Standard deviation = 0.331 dbar

RESIDUAL PRESSURE RECORDS

$$P_{\text{residual}} = P_{\text{measured}} - \text{MEAN} - \text{TIDE}$$

TIDE calculated from the following constituents:

	<u>M2</u>	<u>N2</u>	<u>S2</u>	<u>K2</u>	<u>K1</u>	<u>O1</u>	<u>P1</u>	<u>O1</u>
H (dbar):	.42659	.09910	.08669	.02037	.09116	.06876	.03045	.01264
G°:	353.61	335.45	21.82	23.81	181.16	188.76	182.42	185.16

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Nov 02, 1983	080406	-1431.9316
LAST DATA POINT:	Jan 11, 1984	143406	254.5683

Number of points: 3374
Sampling Interval: 0.50 hrs

Minimum = -0.1433 dbar Mean = 0.0000 dbar
Maximum = 0.1374 dbar Standard deviation = 0.0405 dbar

TABLE 9.6
PIES85CCM1

IES Serial Number: 056
Pressure Sensor Serial Number: 17848

Position: 36°15.23 N Depth: 3475 m
 73°09.89 W

	<u>DATE</u>	<u>GMT</u>	<u>CRUISE</u>
LAUNCH:	Jan. 17, 1984	0505	OC144
RECOVERY:	Jan. 14, 1985	0120	EN124

(Pressure sensor did not work.)

40HRLP PRESSURE RECORDS
(Fig. 12.6)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 16, 1985	000000	360.0000
LAST DATA POINT:	May 11, 1985	060000	3126.0000

Number of points: 462
Sampling Interval: 6.00 hrs

Minimum = -0.0632 dbar
Maximum = 0.0763 dbar
Mean = 0.0000 dbar
Standard deviation = 0.0271 dbar

TEMPERATURE RECORDS
(Fig. 10.6)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 14, 1985	032453	315.4147
LAST DATA POINT:	May 12, 1985	122453	3156.4147

Number of points: 5683
Sampling Interval: 0.50 hrs

Minimum = 2.188 °C
Maximum = 8.291 °C
Mean = 2.280 °C
Standard deviation = 0.111 °C

40HRLP TEMPERATURE RECORDS
(Fig. 12.3)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 16, 1985	000000	360.0000
LAST DATA POINT:	May 11, 1985	060000	3126.0000

Number of points: 462
Sampling Interval: 6.00 hrs

Minimum = 2.190 °C
Maximum = 2.387 °C
Mean = 2.277 °C
Standard deviation = 0.042 °C

TABLE 9.8
PIES84CCM2

IES Serial Number: 057
Pressure Sensor Serial Number: 17849

Position: 36°05.02 N Depth: 3660 m
72°59.94 W

	<u>DATE</u>	<u>GMT</u>	<u>CRUISE</u>
LAUNCH:	Nov 1, 1983	2158	EN107
RECOVERY:	June 7, 1984	1514	EN118

MEASURED PRESSURE RECORDS

(Fig. 10.17)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Nov 1, 1983	230740	-1440.8723
LAST DATA POINT:	Jun 7, 1984	150740	3807.1277

Number of points: 10497
Sampling Interval: 0.50 hrs

Minimum = 3732.73 dbar
Maximum = 3734.59 dbar

Mean = 3733.56 dbar
Standard deviation = 0.354 dbar

RESIDUAL PRESSURE RECORDS

$$P_{\text{residual}} = P_{\text{meas}} - \text{MEAN} - \text{DRIFT} - \text{TIDE}$$

$$\text{DRIFT} = P_1 [1 - \exp(P_2 t)] + P_3$$

where t = Time of sample in hours, starting with
t = 13.0 for the first data point

$$P_1 = -0.513066 \text{ dbar}$$

$$P_2 = -0.0002825 \text{ h}^{-1}$$

$$P_3 = 0.246240 \text{ dbar}$$

TIDE calculated from the following constituents:

	<u>M2</u>	<u>N2</u>	<u>S2</u>	<u>K2</u>	<u>K1</u>	<u>O1</u>	<u>P1</u>	<u>O1</u>
H (dbar):	.43285	.10601	.08994	.02138	.09200	.06898	.03032	.01438
G°:	352.23	332.50	19.29	19.71	180.70	185.78	181.45	183.89

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Nov 2, 1983	110740	-1428.8723
LAST DATA POINT:	Jun 7, 1984	150740	3807.1277

Number of points: 10473
Sampling Interval: 0.50 hrs

Minimum = -0.190 dbar
Maximum = 0.118 dbar

Mean = 0.0000 dbar
Standard deviation = 0.0449 dbar

40HRLP PRESSURE RECORDS

(Fig. 12.4 and 12.5)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Nov 3, 1983	180000	-1398.0000
LAST DATA POINT:	Jun 6, 1984	060000	3774.0000

Number of points: 863
 Sampling Interval: 6.00 hrs

Minimum = -0.1658 dbar
 Maximum = 0.0916 dbar

Mean = 0.0000 dbar
 Standard deviation = 0.0416 dbar

TEMPERATURE RECORDS

(Fig. 10.7)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Nov 2, 1983	110740	-1428.8723
LAST DATA POINT:	June 7, 1984	150740	3807.1277

Number of points: 10473
 Sampling Interval: 0.50 hrs

Minimum = 2.244 °C
 Maximum = 2.482 °C

Mean = 2.317 °C
 Standard deviation = 0.076 °C

40HRLP TEMPERATURE RECORDS

(Fig. 12.1 and 12.2)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Nov 3, 1983	180000	-1398.0000
LAST DATA POINT:	Jun 6, 1984	060000	3774.0000

Number of points: 863
 Sampling Interval: 6.00 hrs

Minimum = 2.246 °C
 Maximum = 2.475 °C

Mean = 2.319 °C
 Standard deviation = 0.058 °C

40HRLP PRESSURE RECORDS

(Fig. 12.5 and 12.6)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	June 9, 1984	120000	-4932.0000
LAST DATA POINT:	May 11, 1985	000000	3120.0000

Number of points: 1343
 Sampling Interval: 6.00 hrs

Minimum = -0.082 dbar
 Maximum = 0.099 dbar

Mean = 0.0000 dbar
 Standard deviation = 0.0315 dbar

TEMPERATURE RECORDS

(Fig. 10.8)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	June 7, 1984	181007	-4973.8314
LAST DATA POINT:	May 12, 1985	094007	3153.6686

Number of points: 16256
 Sampling Interval: 0.50 hrs

Minimum = 2.204 °C
 Maximum = 4.619 °C

Mean = 2.256 °C
 Standard deviation = 0.071 °C

40HRLP TEMPERATURE RECORDS

(Fig. 12.2 and 12.3)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	June 9, 1984	120000	-4932.0000
LAST DATA POINT:	May 11, 1985	000000	3120.0000

Number of points: 1343
 Sampling Interval: 6.00 hrs

Minimum = 2.205 °C
 Maximum = 2.334 °C

Mean = 2.257 °C
 Standard deviation = 0.036 °C

40HRLP PRESSURE RECORDS

(Fig. 12.4 and 12.5)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 17, 1984	060000	390.0000
LAST DATA POINT:	Jun 6, 1984	120000	3780.0000

Number of points: 566
 Sampling Interval: 6.00 hrs

Minimum = -0.1363 dbar
 Maximum = 0.0881 dbar

Mean = 0.0000 dbar
 Standard deviation = 0.0511 dbar

TEMPERATURE RECORDS

(Fig. 10.9)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 15, 1984	212953	357.4981
LAST DATA POINT:	Jun 7, 1984	205953	3812.9981

Number of points: 6912
 Sampling Interval: 0.50 hrs

Minimum = 2.365 °C
 Maximum = 2.494 °C

Mean = 2.396 °C
 Standard deviation = 0.039 °C

40HRLP TEMPERATURE RECORDS

(Fig. 12.1 and 12.2)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	Jan 17, 1984	060000	390.0000
LAST DATA POINT:	Jun 6, 1984	120000	3780.0000

Number of points: 566
 Sampling Interval: 6.00 hrs

Minimum = 2.367 °C
 Maximum = 2.486 °C

Mean = 2.397 °C
 Standard deviation = 0.019 °C

40HRLP PRESSURE RECORDS

(Fig. 12.5 and 12.6)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	June 9, 1984	180000	-4926.0000
LAST DATA POINT:	May 11, 1985	000000	3120.0000

Number of points: 1342
 Sampling Interval: 6.00 hrs

Minimum = -0.100 dbar
 Maximum = 0.120 dbar
 Mean = 0.0000 dbar
 Standard deviation = 0.0334 dbar

TEMPERATURE RECORDS

(Fig. 10.10)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	June 7, 1984	235920	-4968.0111
LAST DATA POINT:	May 12, 1985	062920	3150.4889

Number of points: 16238
 Sampling Interval: 0.50 hrs

Minimum = 2.375 °C
 Maximum = 5.983 °C
 Mean = 2.414 °C
 Standard deviation = 0.077 °C

40HRLP TEMPERATURE RECORDS

(Fig. 12.2 and 12.3)

	<u>DATE</u>	<u>GMT</u>	<u>YEARHOUR</u>
1st DATA POINT:	June 9, 1984	180000	-4926.0000
LAST DATA POINT:	May 11, 1985	000000	3120.0000

Number of points: 1342
 Sampling Interval: 6.00 hrs

Minimum = 2.377 °C
 Maximum = 2.512 °C
 Mean = 2.415 °C
 Standard deviation = 0.024 °C

10. HALF-HOURLY DATA FOR EACH INSTRUMENT

Plots of the measured bottom pressure and temperature are presented. The time scale is the same for all plots, with each increment corresponding to 5 days. The axis begins on 0000 GMT of the first date labelled.

The vertical scale for each variable is consistent between instruments. Each increment corresponds to 0.5 dbar for the bottom pressure data and to 0.02°C for the temperatures.

The sampling interval is 0.5 hours for all instruments. The length and start and end times of the data records are tabulated in the previous section.

10.1 Temperature Data

The raw temperature records are shown in Figures 10.1 to 10.10. All the temperatures are in the range 2.2 to 2.5°C , with a tendency for the offshore (deeper) records to be warmer. We have observed this pattern in previous investigations in this region, where the colder core of the Western Boundary Undercurrent (WBUC) is somewhat onshore of (shallower than) the array. The temperature records are characterized by "square-pulse-like" warming events; i.e., they have many plateaus of relatively constant temperature ($\pm 0.02^{\circ}\text{C}$) separated by very rapid changes (-0.05 to 0.15°C within a few hours) to a different plateau that may last typically for 1 to 10 days. We tentatively associate this behavior with lateral shifts of the offshore temperature front of the WBUC, although it may also be caused by advective pulses of warmer or colder water.

10.2 Pressure Data

The raw pressure records are shown in Figures 10.11 to 10.20. The semidiurnal tidal oscillations of roughly 1 dbar range are prominent in these records, and the 29-day repeat-cycle of spring and neap tides is readily observed. Other features of these pressure records, which are only slightly noticeable on this coarse plotting scale, are discussed in Section 12, after the tides and the drift have been removed from them.

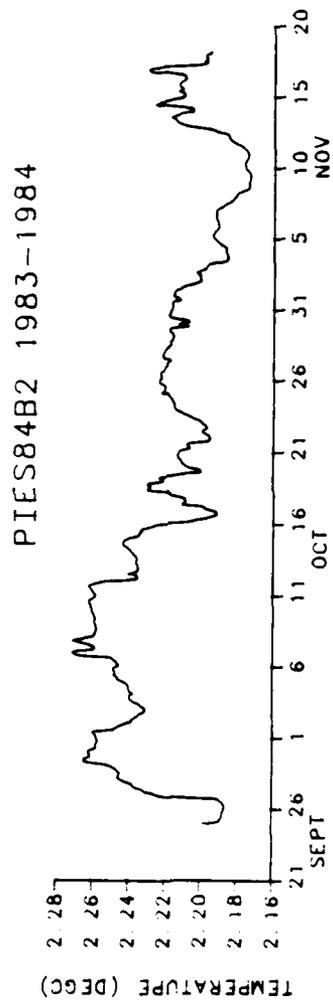


Figure 10.1 Raw temperature record of PIES84B2

PIES85BCM2 1984-1985

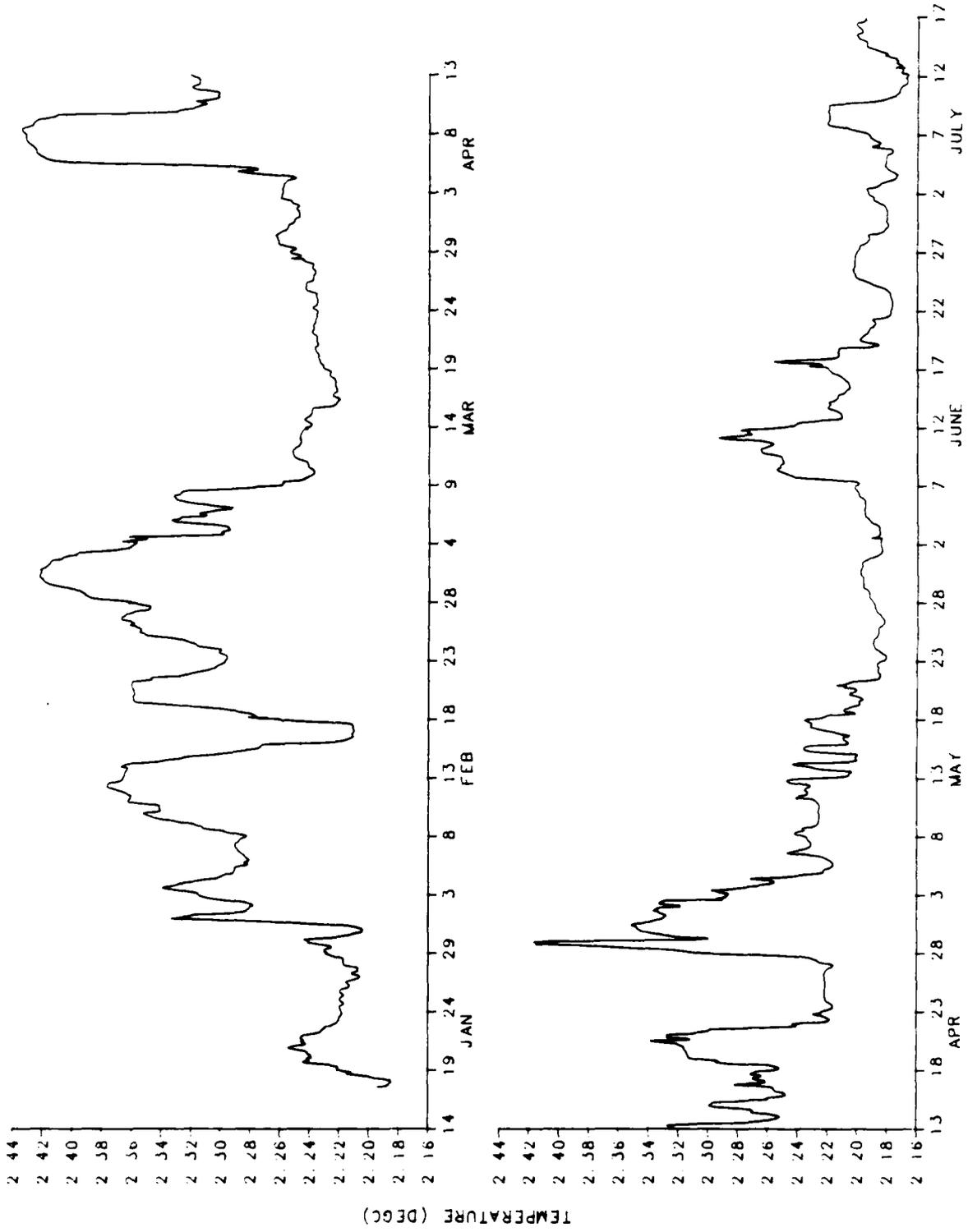


Figure 10.2a Raw temperature record of PIES85BCM2

PIES85BCM2 1984-1985

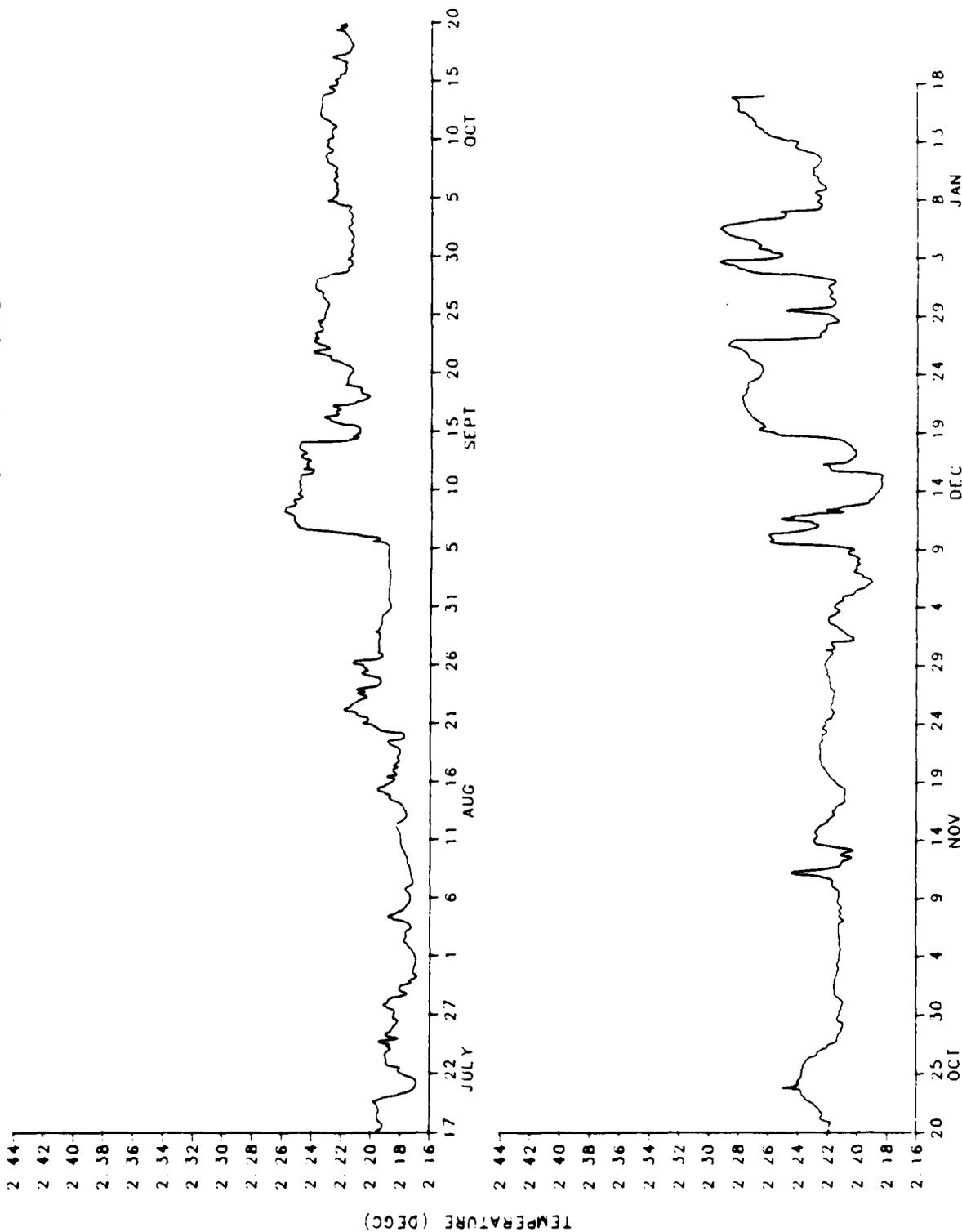


Figure 10.2b Raw temperature record of PIES85BCM2, continued

PIES85BCM3 1984-1985

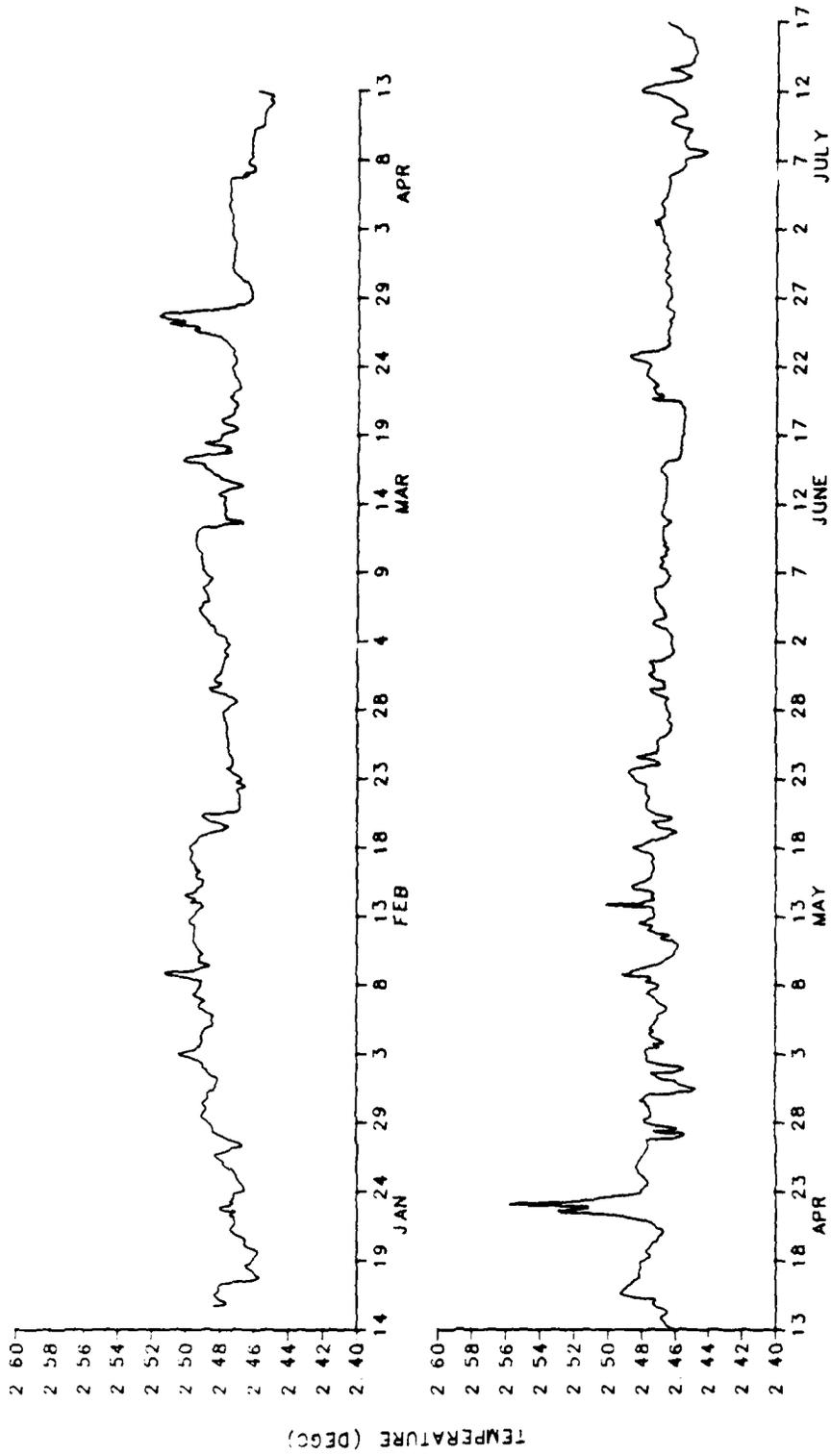


Figure 10.3a Raw temperature record of PIES85BCM3

PIES85BCM3 1984-1985

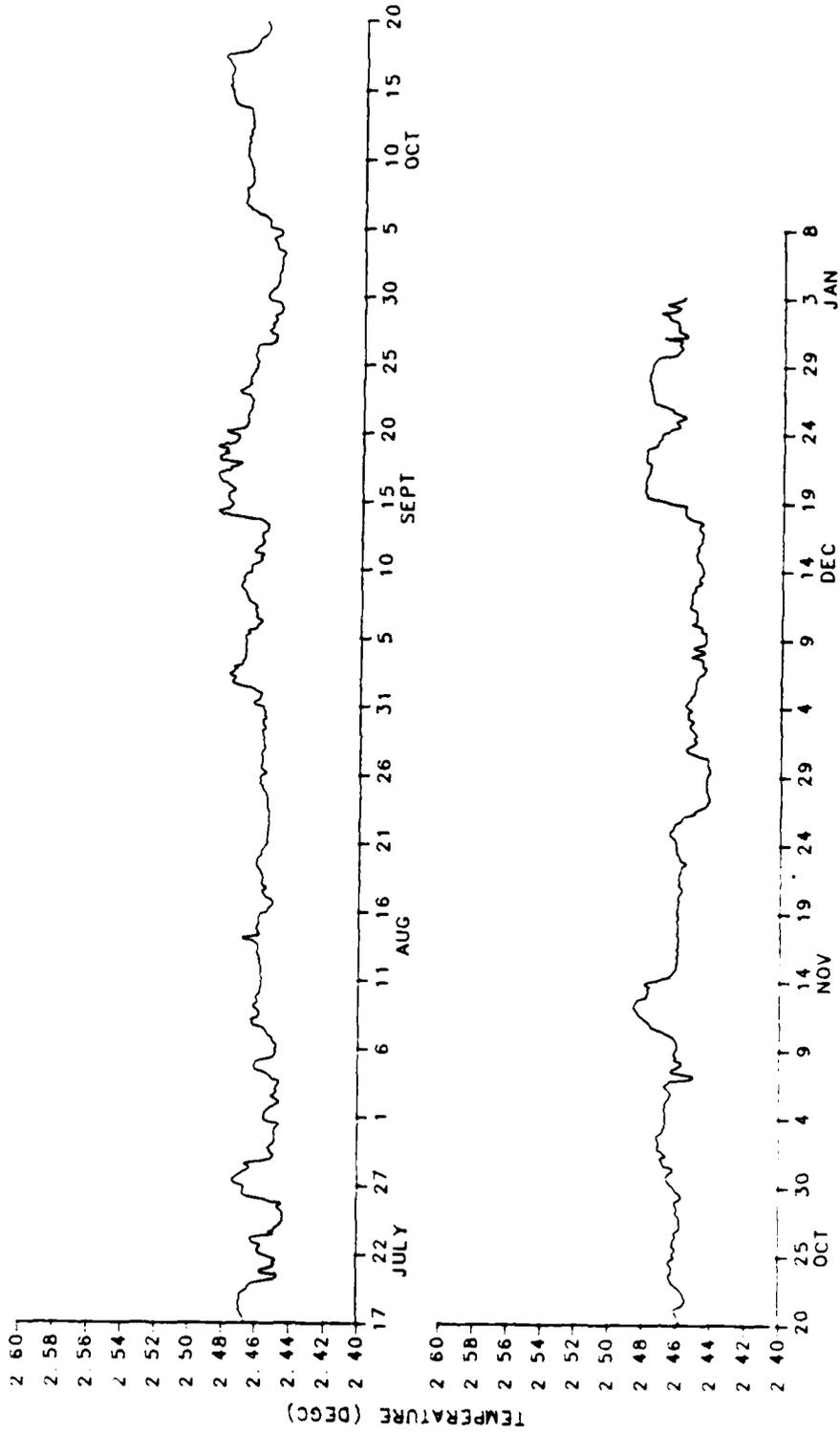


Figure 10.3b Raw temperature record of PIES85BCM3, continued

PIES85CO 1985

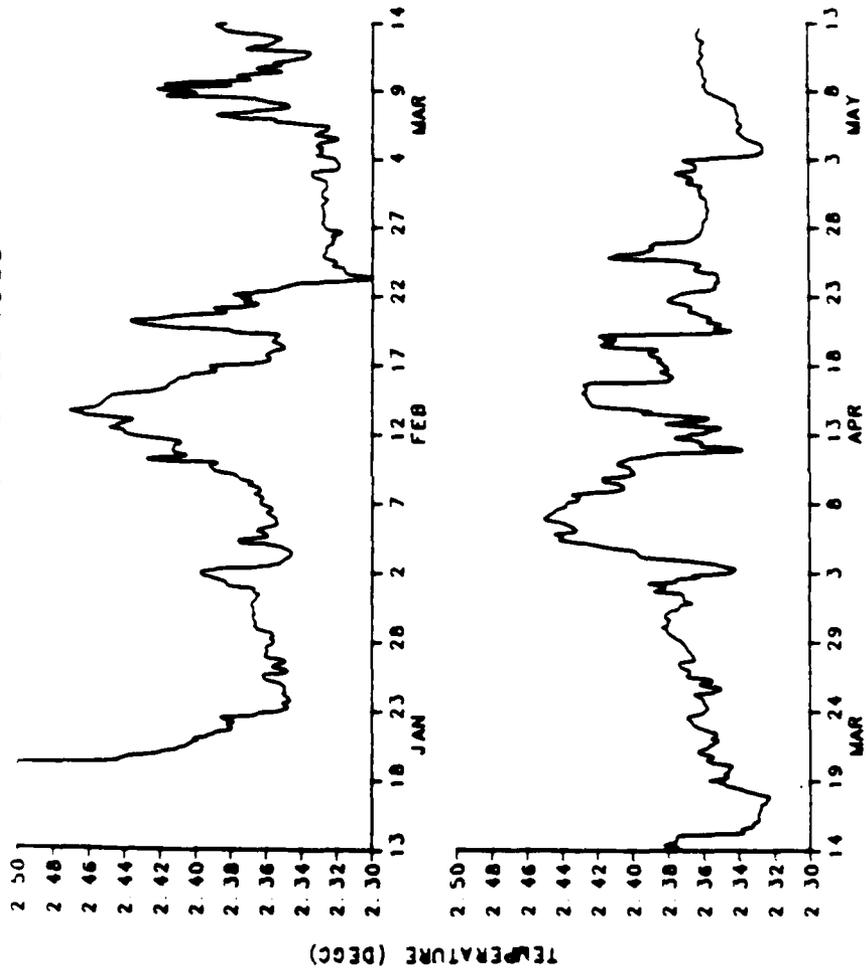


Figure 10.4 Raw temperature record of PIES85CO

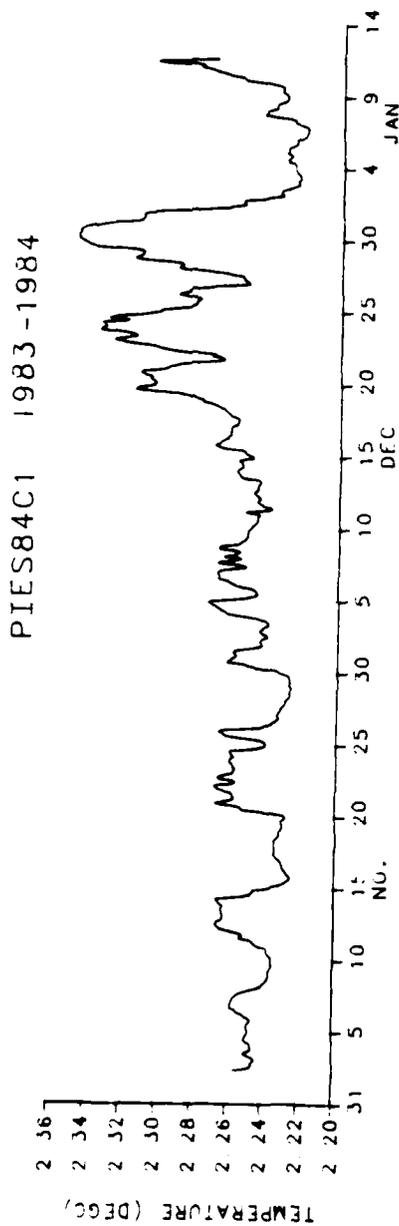


Figure 10.5 Raw temperature record of PIES84C1

PIES85C1 1985

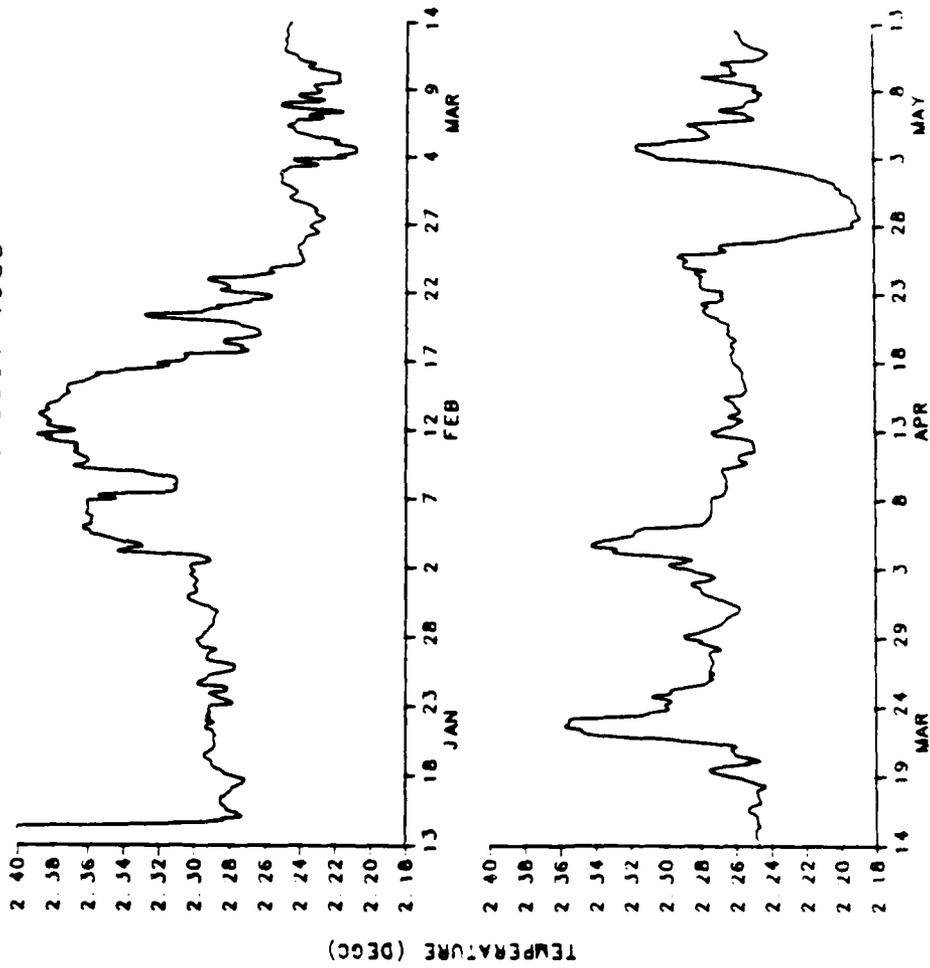


Figure 10.6 Raw temperature record of PIES85C1

PIES84CCM2 1983-1984

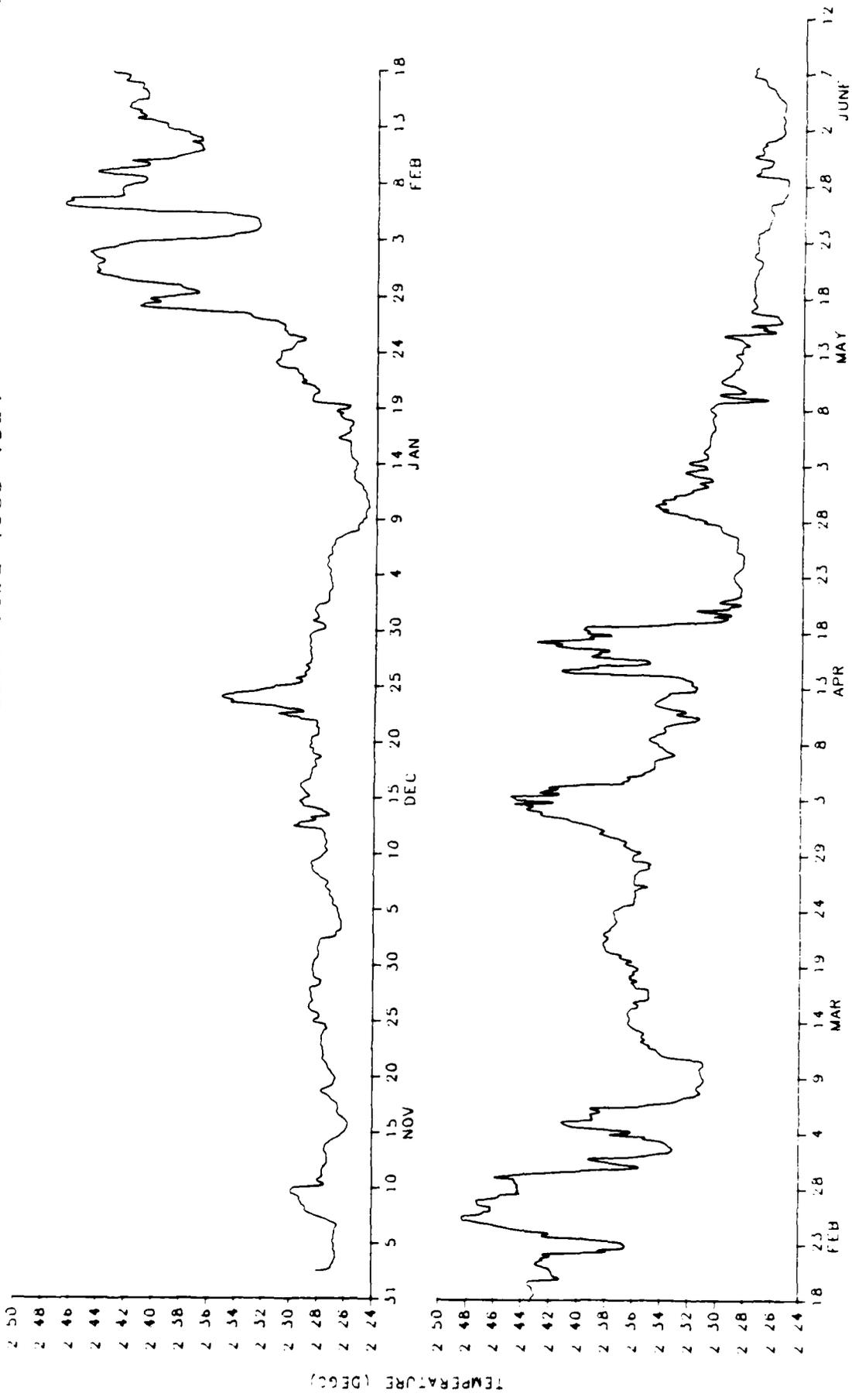


Figure 10.7 Raw temperature record of PIES84CCM2

PIES85CCM2 1984-1985

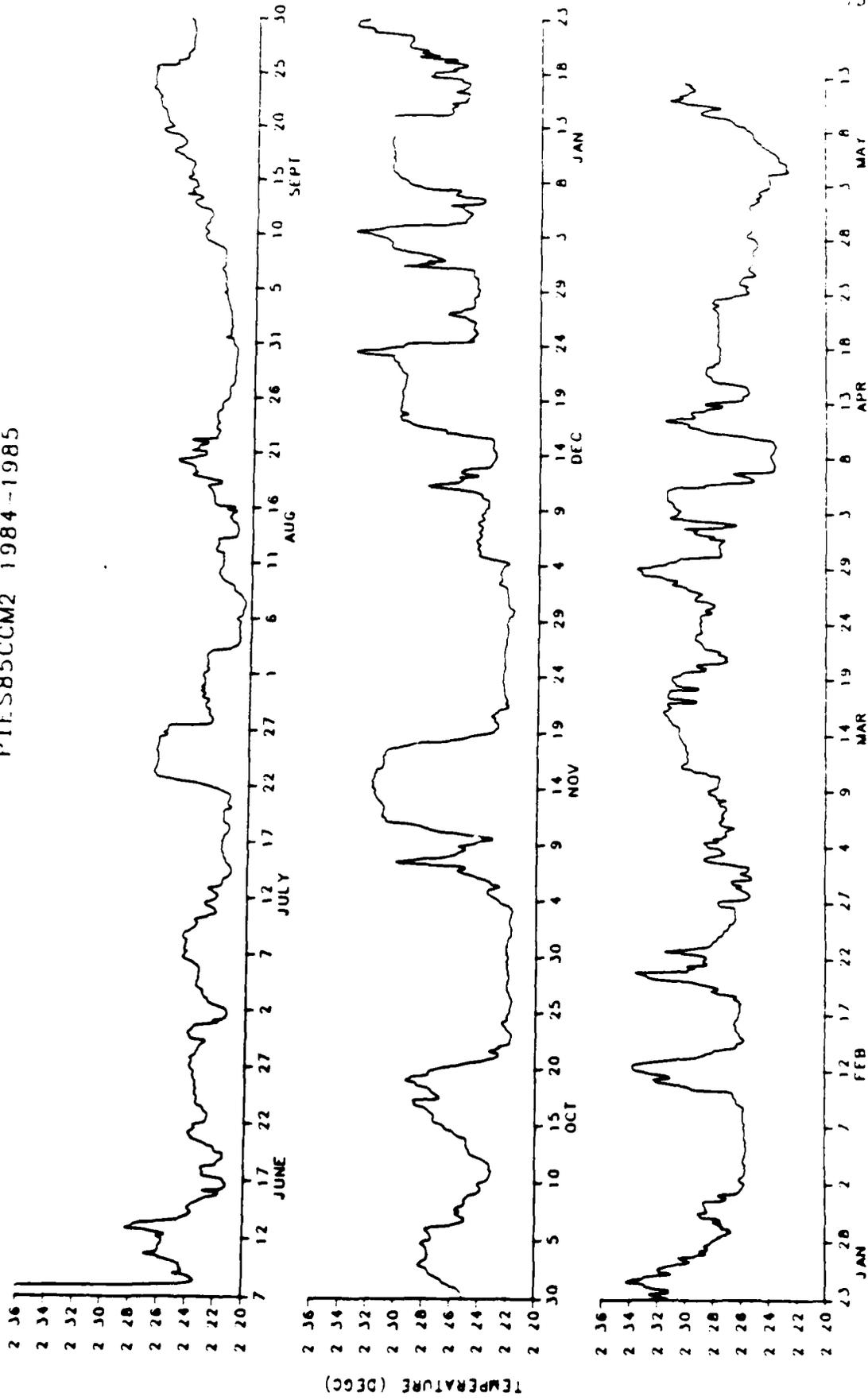


Figure 10.8 Raw temperature record of PIES85CCM2

PIES84CCM3 1984

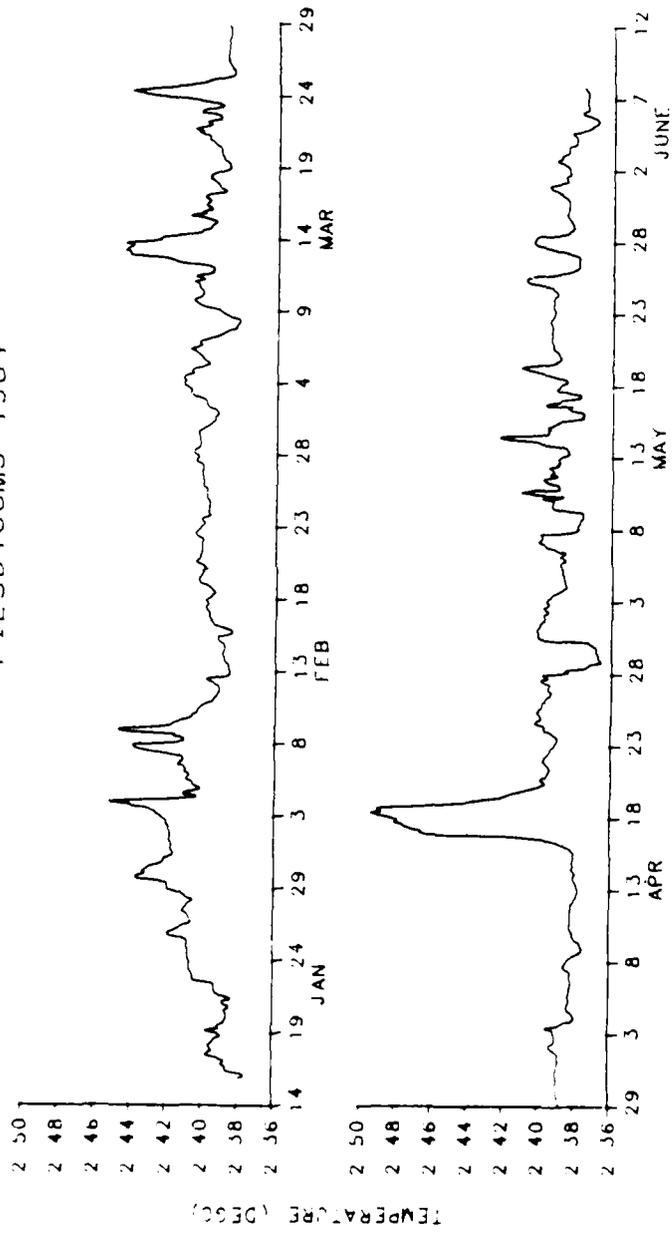


Figure 10.9 Raw temperature record of PIES84CCM3

PIES85CCMJ 1984-1985

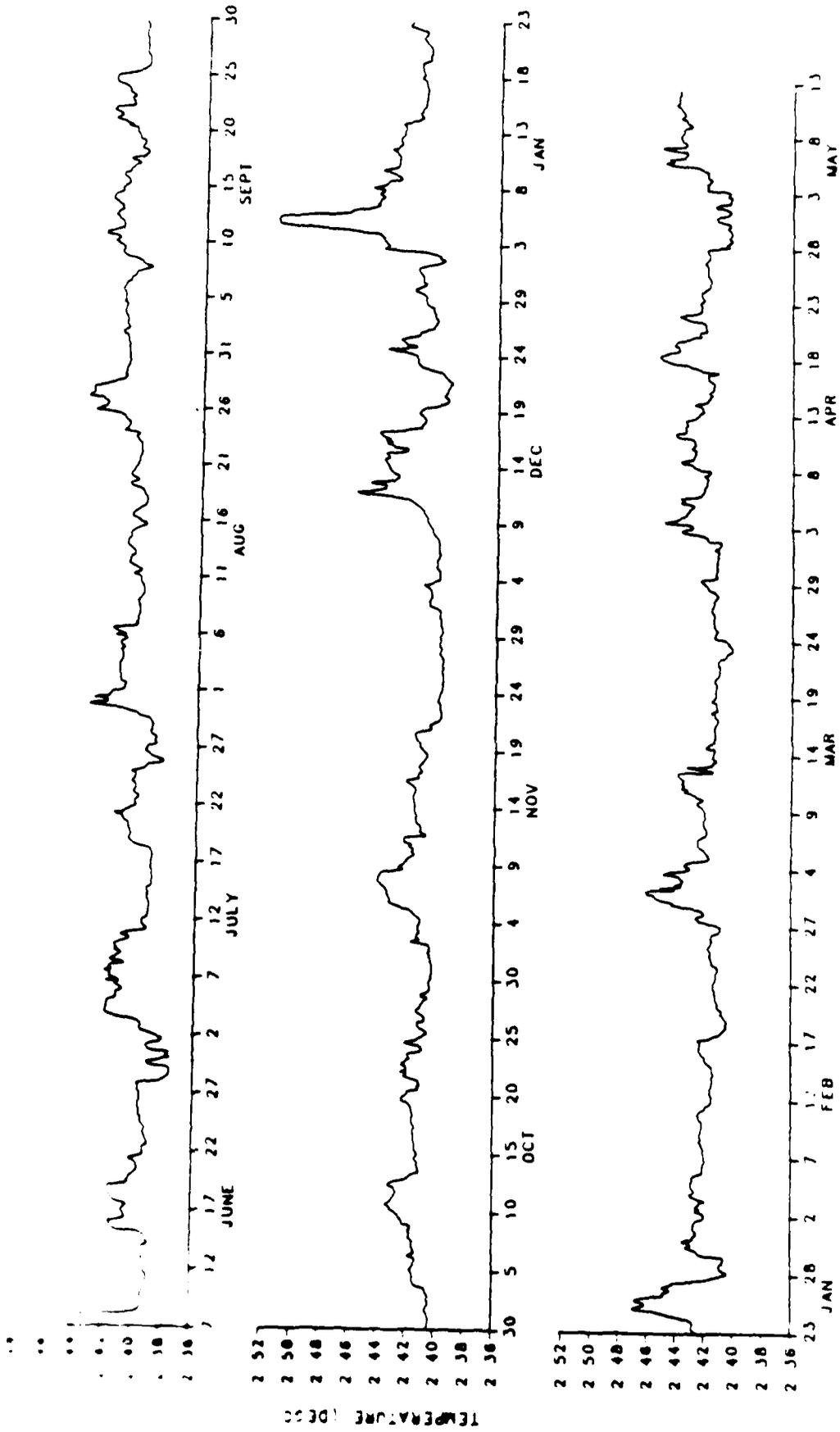


Figure 10.10 Raw temperature record of PIES85CCM3

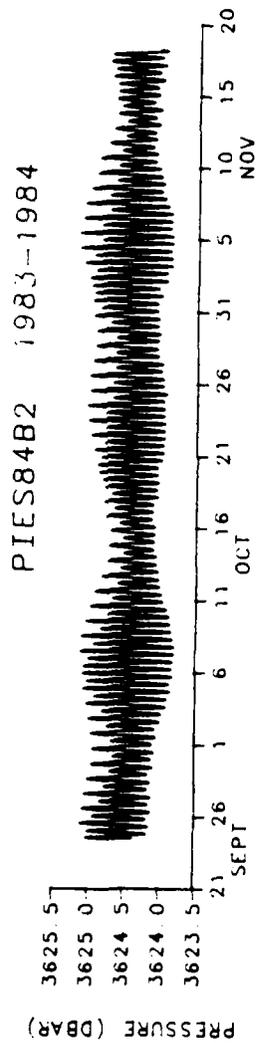


Figure 10.11 Raw pressure record of PIES84B2

PIES85BCM2 1984-1985

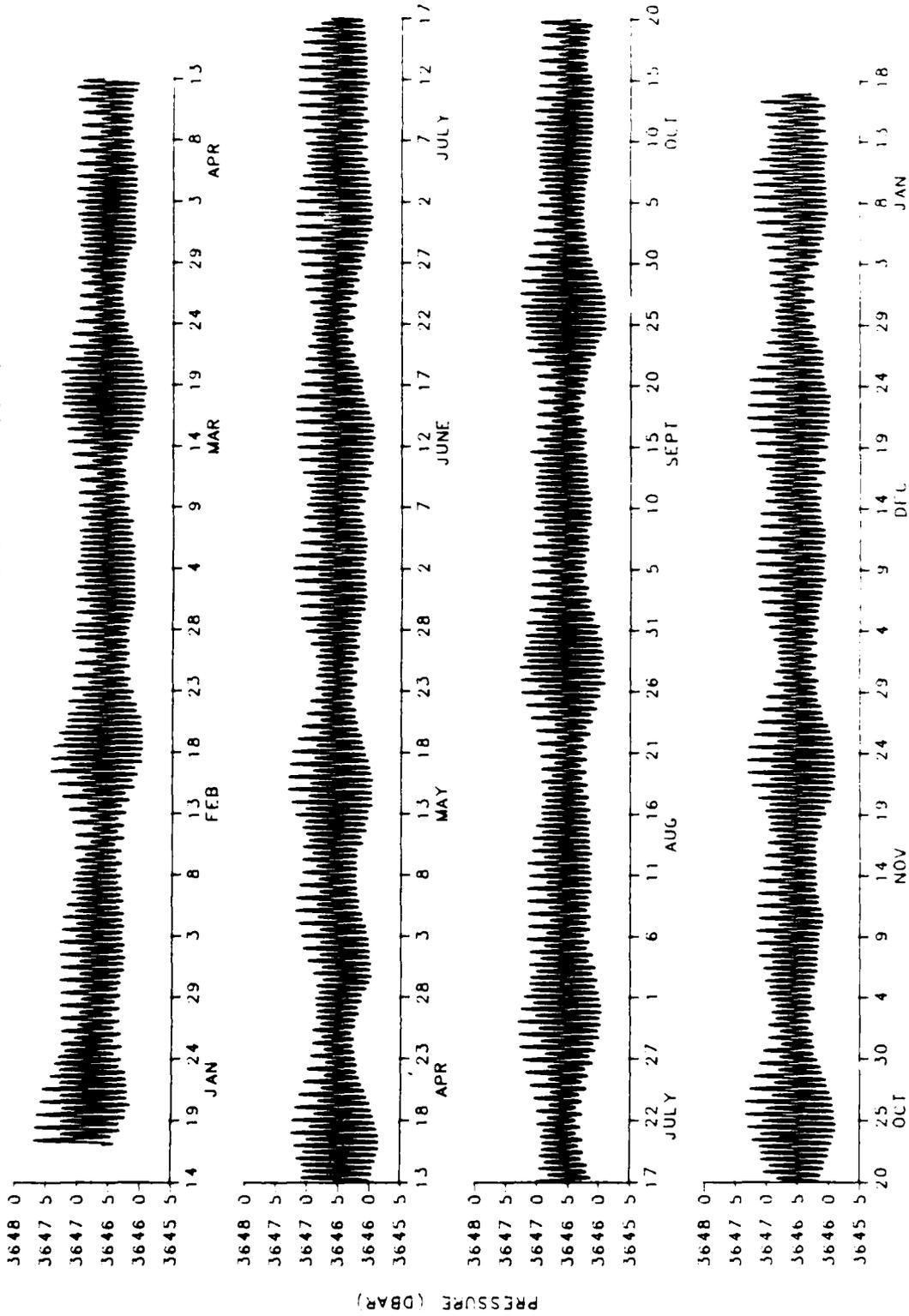


Figure 10.12 Raw pressure record of PIES85BCM2

PIES85BCM3 1984-1985

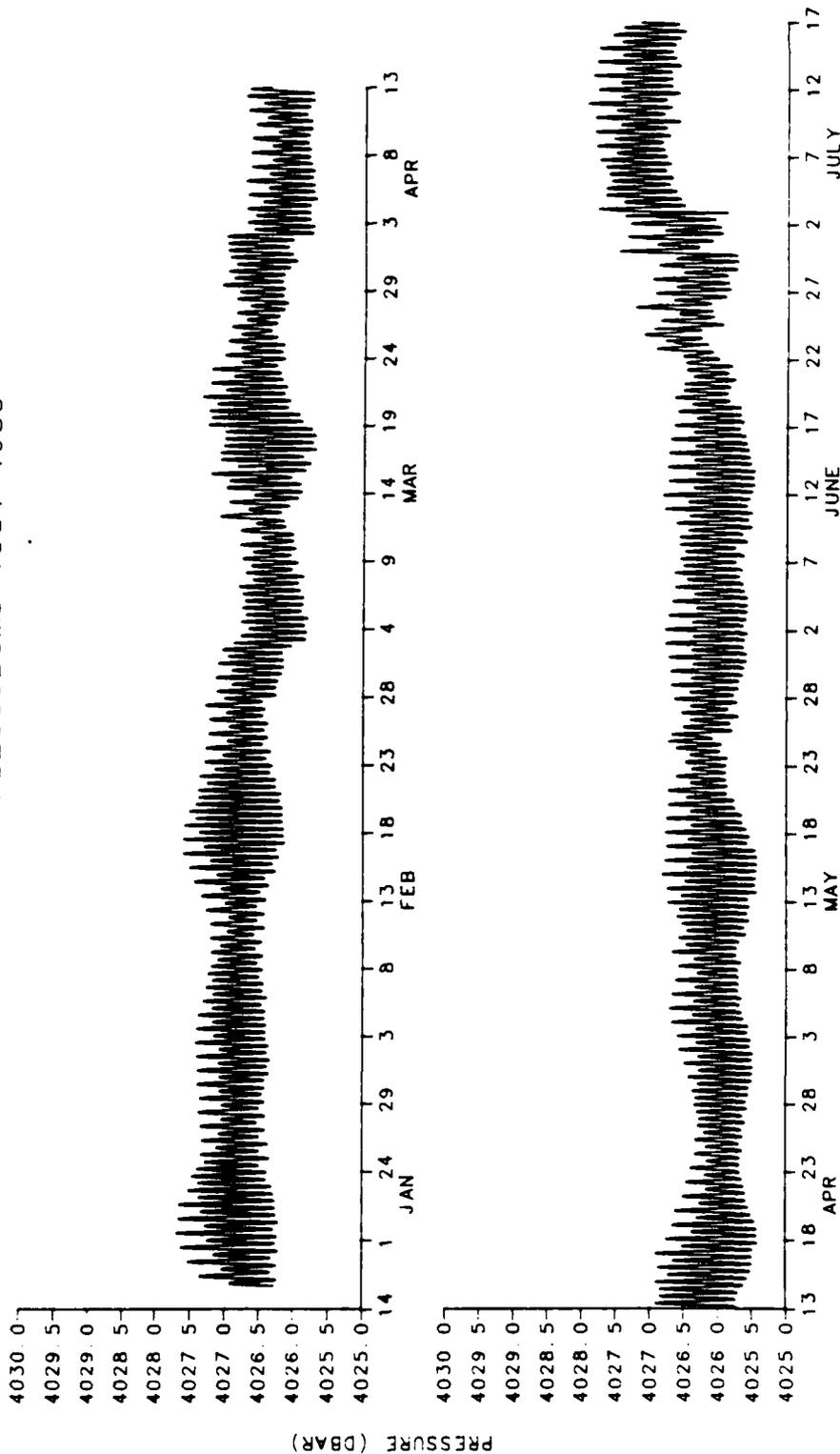


Figure 10.13a Raw pressure record of PIES85BCM3, an unreliable, "jumpy" record.

PIES85BCM3 1984-1985

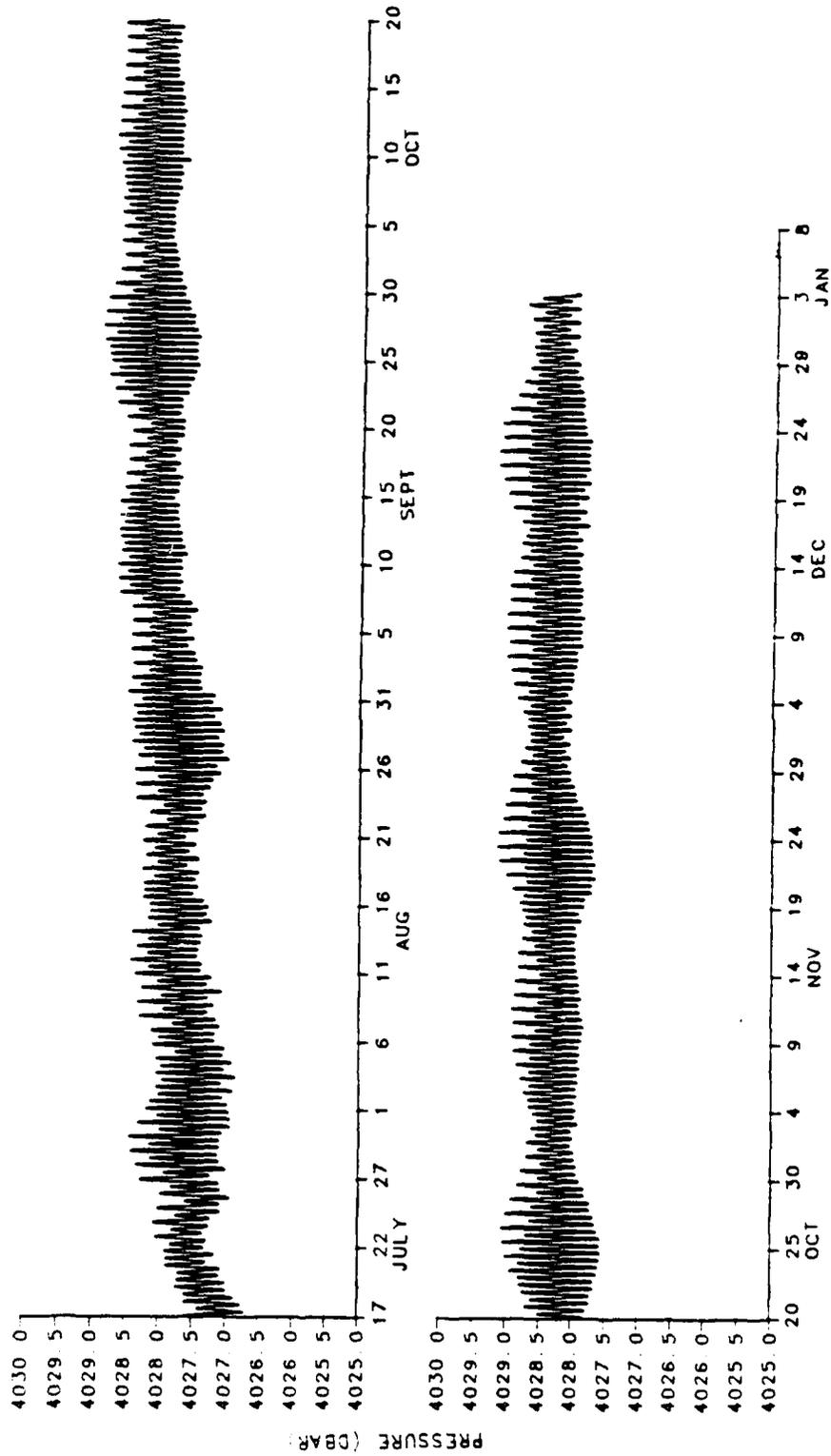


Figure 10.13b Raw pressure record of PIES85BCM3, an unreliable, "jumpy" record, continued.

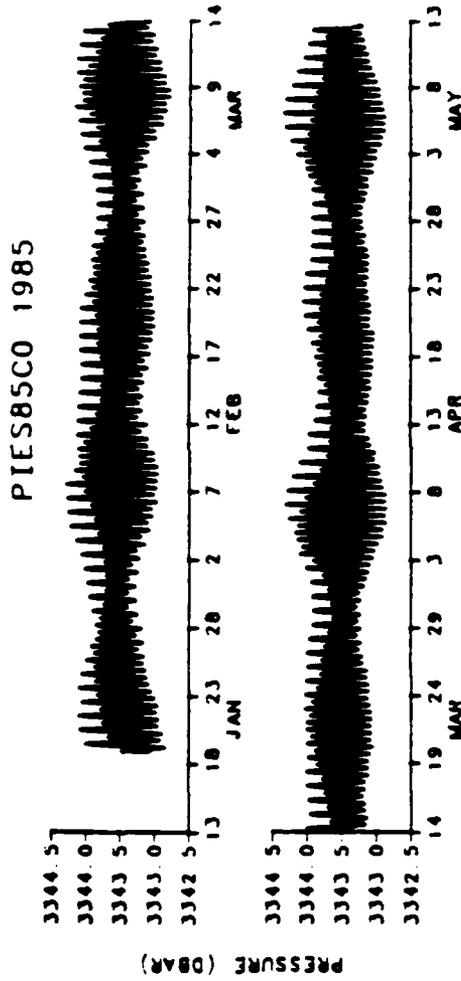


Figure 10.14 Raw pressure record of PIES85C0

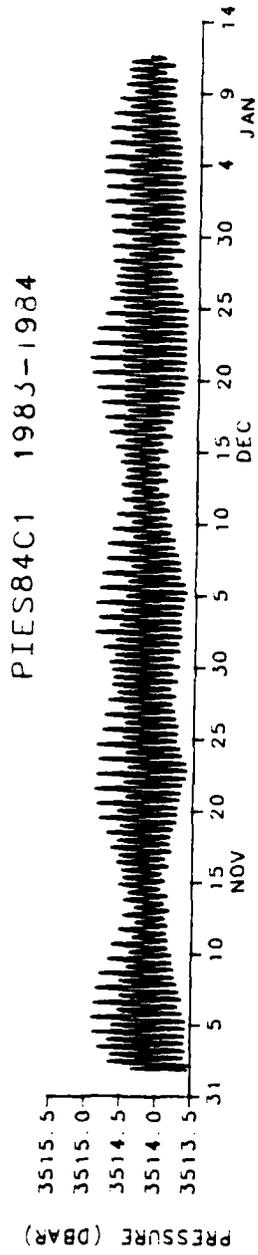


Figure 10.15 Raw pressure record of PIES84C1

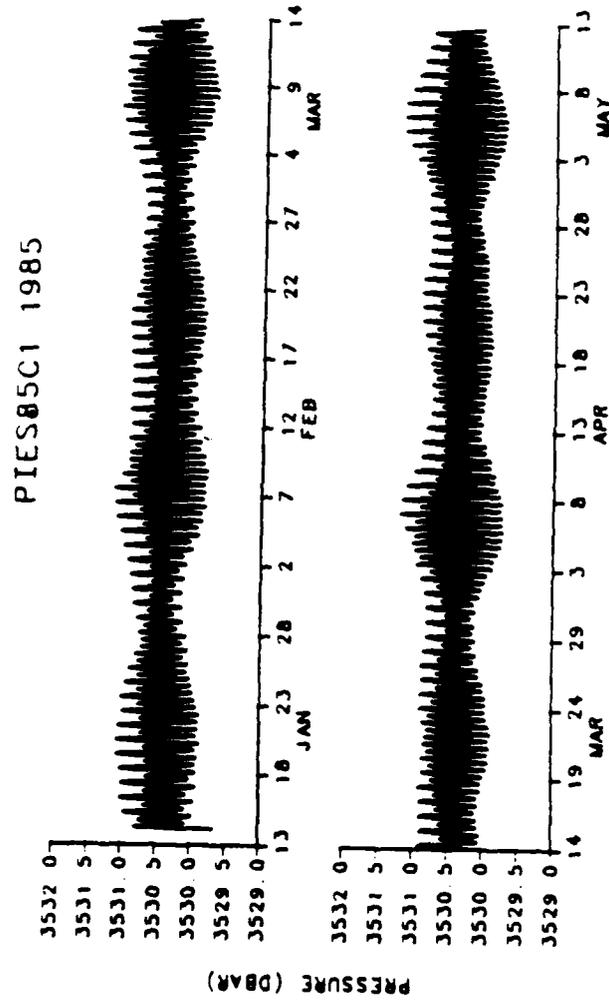


Figure 10.16 Raw pressure record of PIES85C1

PIES84CCM2 1983-1984

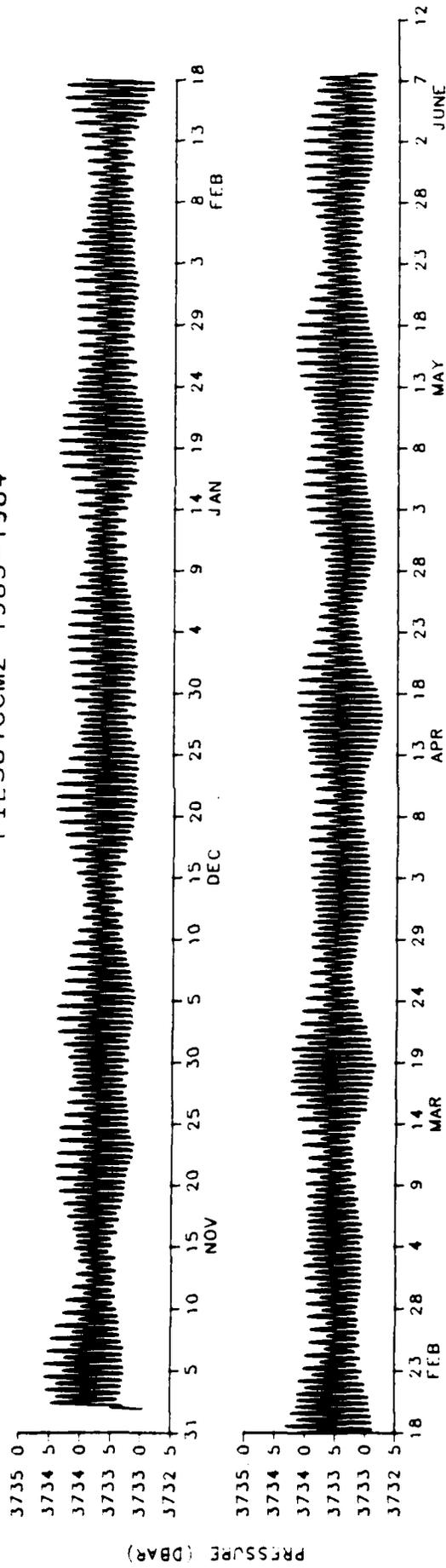


Figure 10.17 Raw pressure record of PIES84CCM2

PIES85CCM2 1984-1985

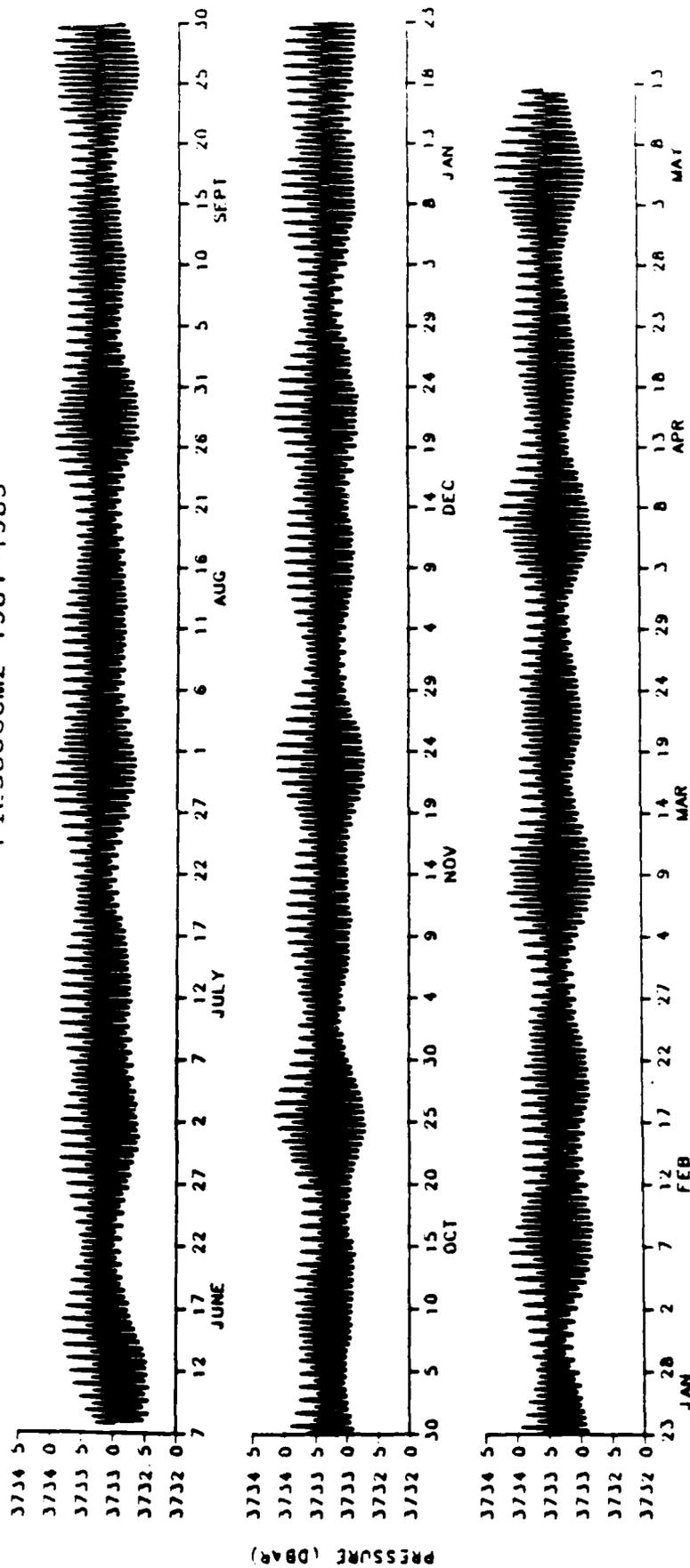


Figure 10.18 Raw pressure record of PIES85CCM2

PIES84CCM3 1984

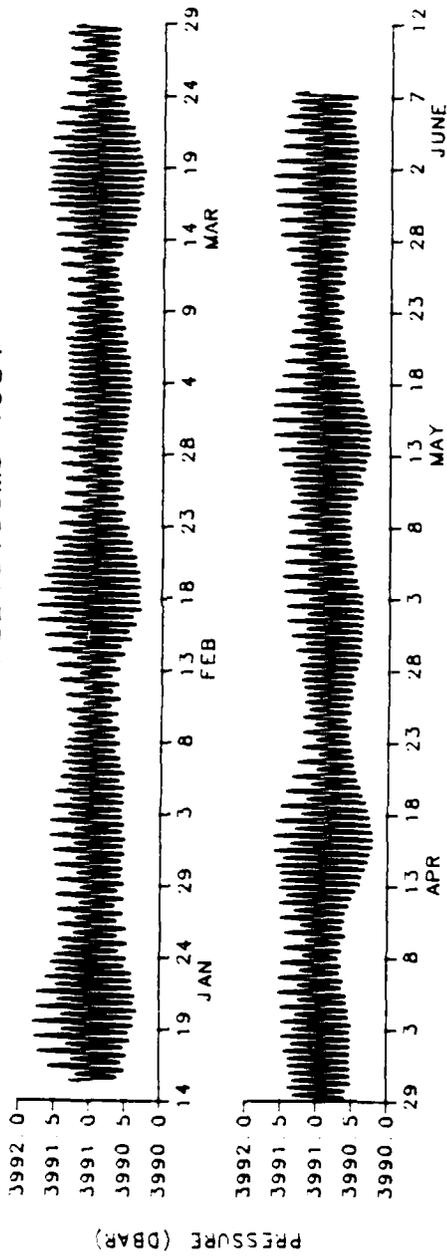


Figure 10.19 Raw pressure record of PIES84CCM3

PIES85CCM3 1984-1985

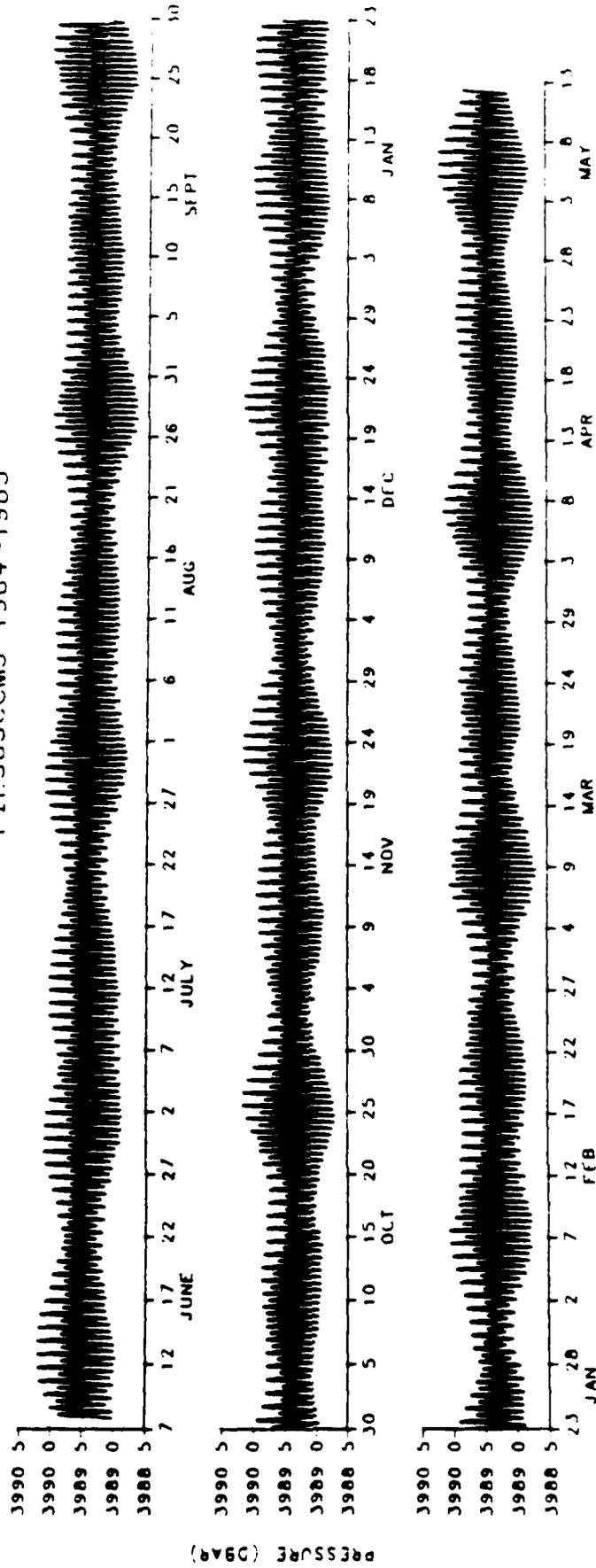


Figure 10.20 Raw pressure record of PIES85CCM3

11. DETIDED PRESSURE RECORDS AND DRIFT CURVES

The detided pressure (P_{detide}) records, which have had the mean and the tides removed, are presented in Figures 11.1 to 11.10. For the records which had a measurable long-term drift, the regressed drift curves are superimposed on the pressure curves.

The vertical scale of 0.1 dbar per increment is consistent between all records, except for PIES85BCM3 (Figure 11.3), which had large unexplained jumps. For that instrument, the vertical scale has been doubled to 0.2 dbar per increment.

The time scale is the same for all plots with each increment corresponding to 25 days. The axis begins on 0000 GMT of the first date labelled.

The sampling interval is 0.5 hours for all instruments. The length and start and end times of the data are tabulated in Section 9.

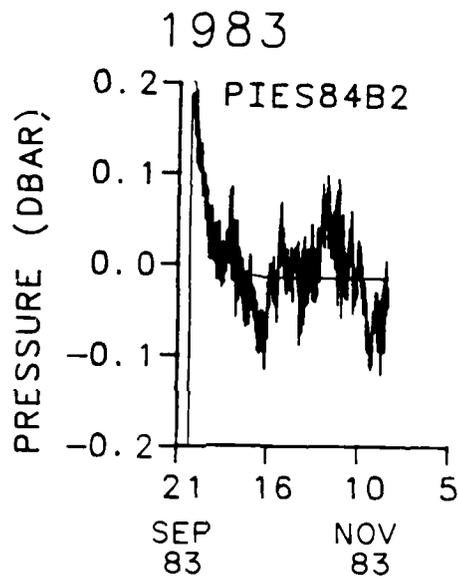


Figure 11.1 Detided pressure record of PIES84B2

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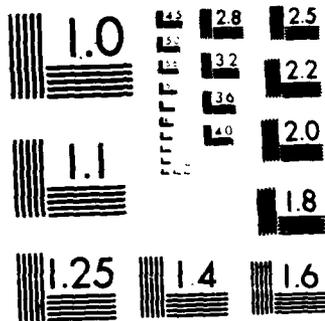
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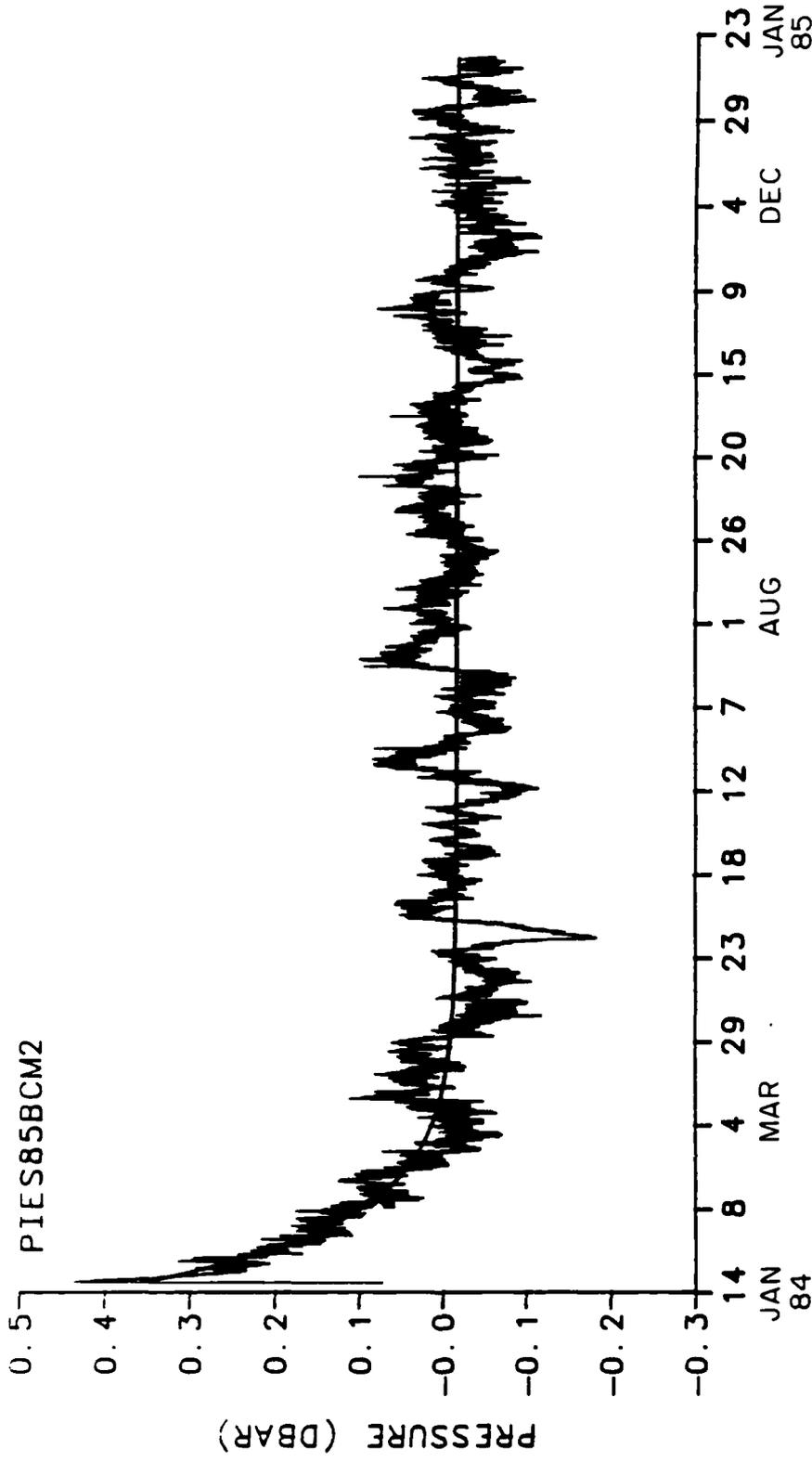


Figure 11.2 Detided pressure record of PIES85BCM2

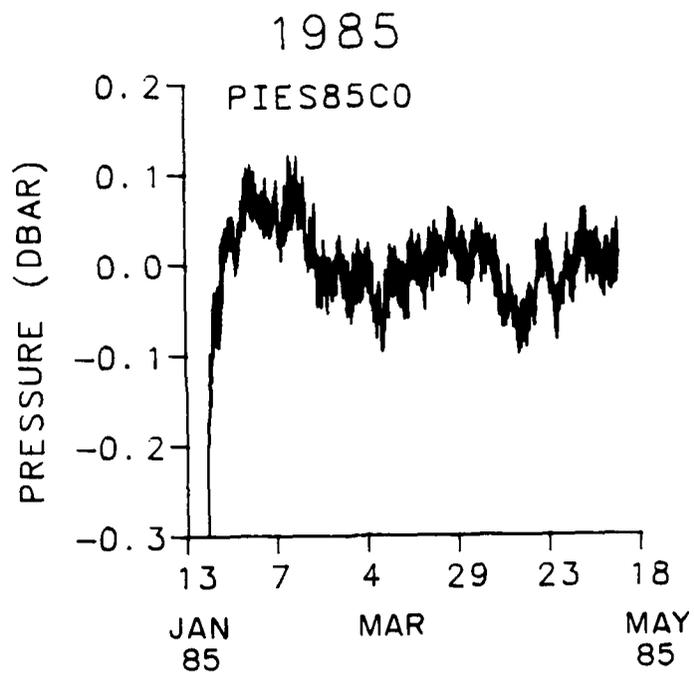


Figure 11.4 Detided pressure record of PIES85C0

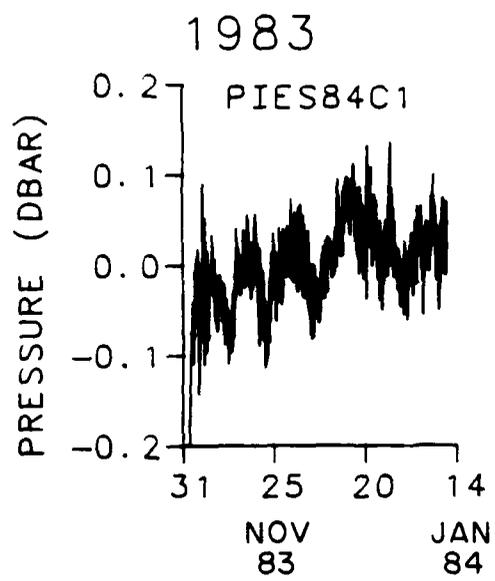


Figure 11.5 Detided pressure record of PIES84C1

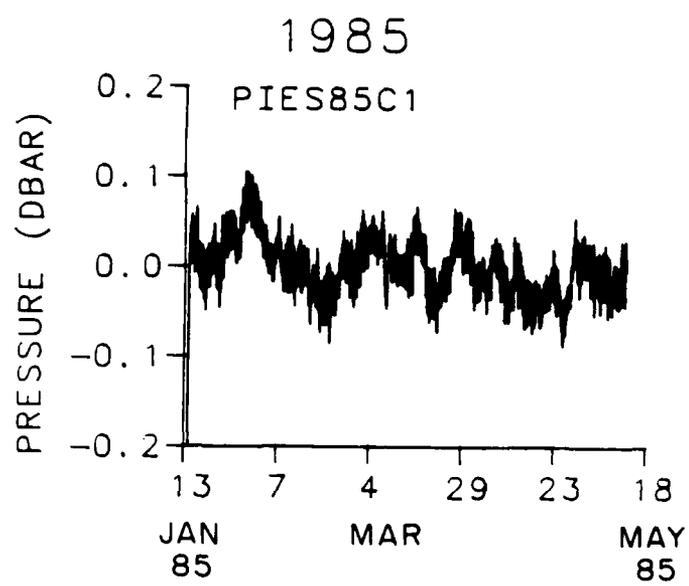


Figure 11.6 Detided pressure record of PIES85C1

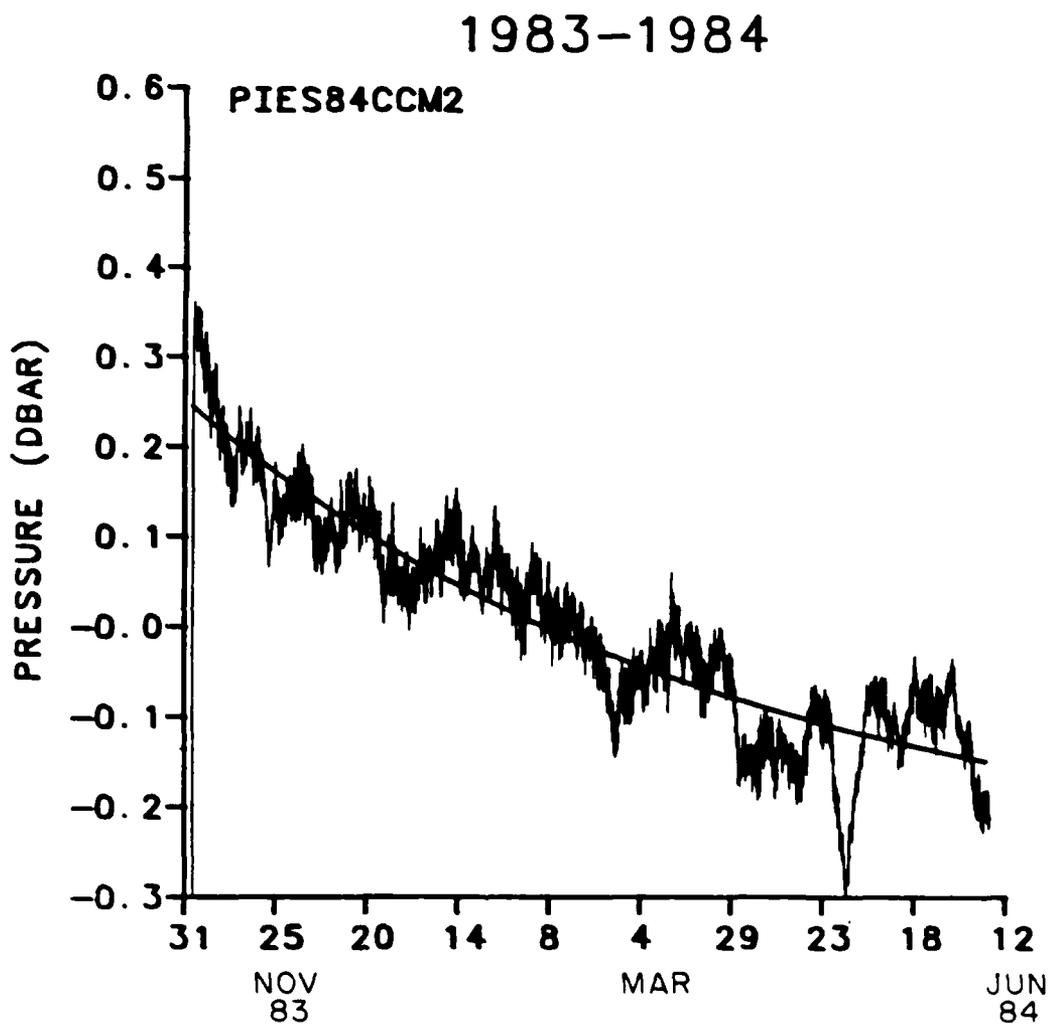


Figure 11.7 Detided pressure record of PIES84CCM2

1984-1985

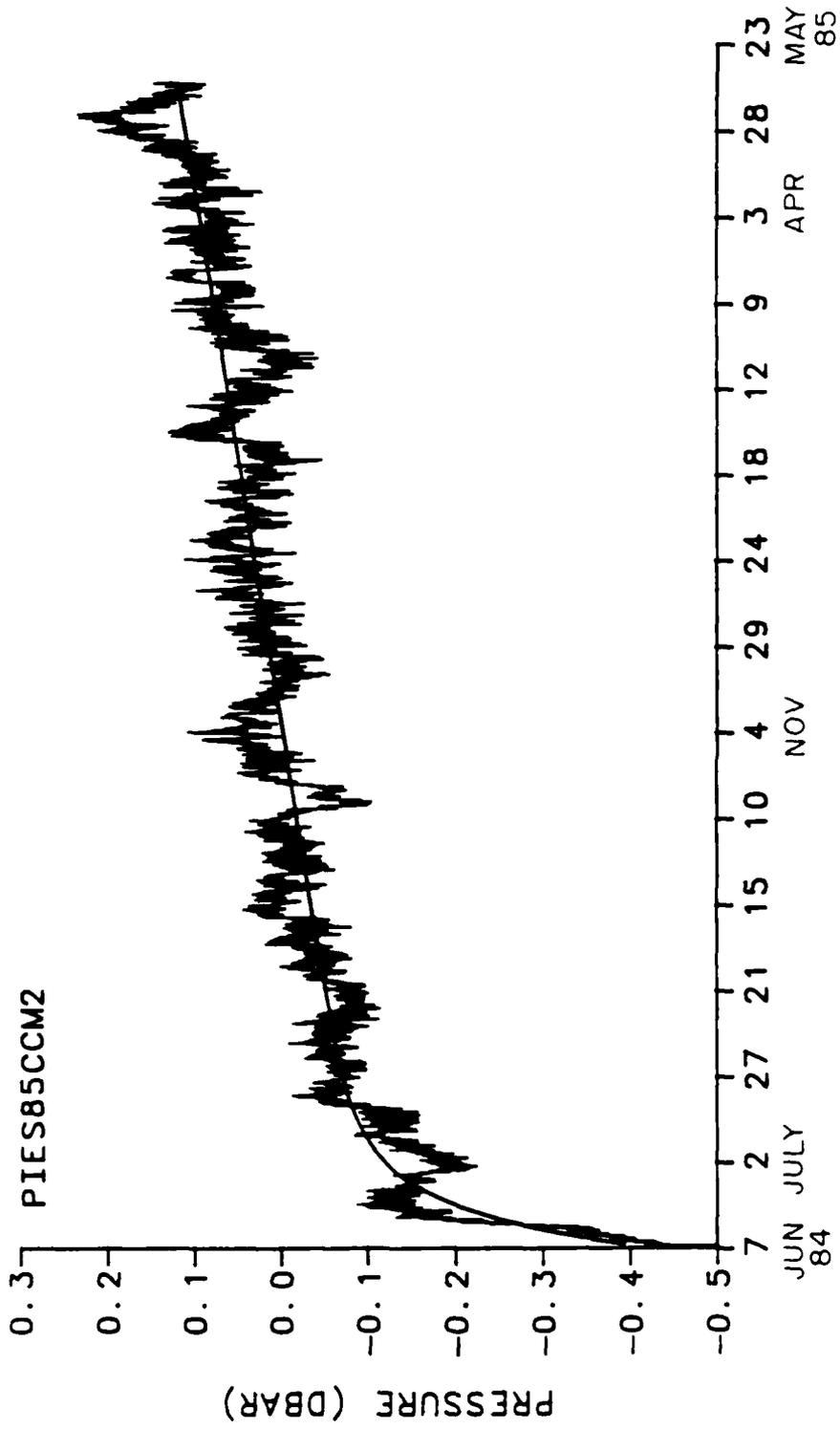


Figure 11.8 Dedided pressure record of PIES85CCM2

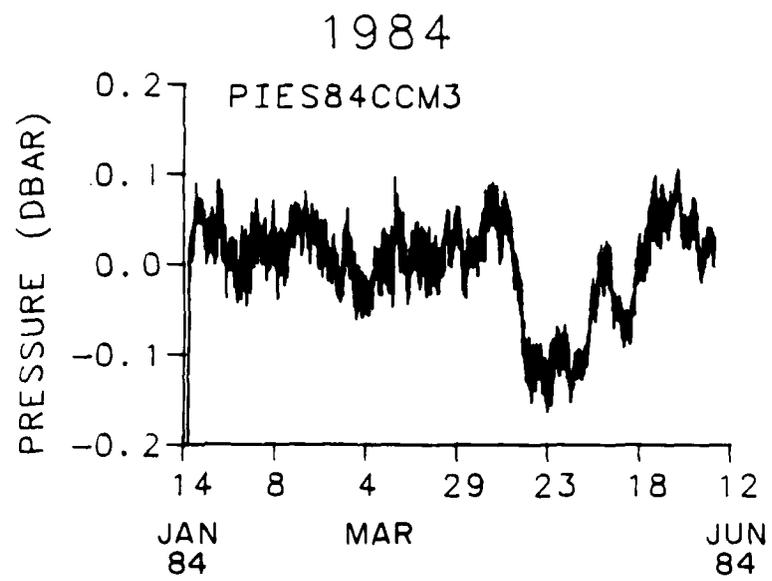


Figure 11.9 Detided pressure record of PIES84CCM3

1984-1985

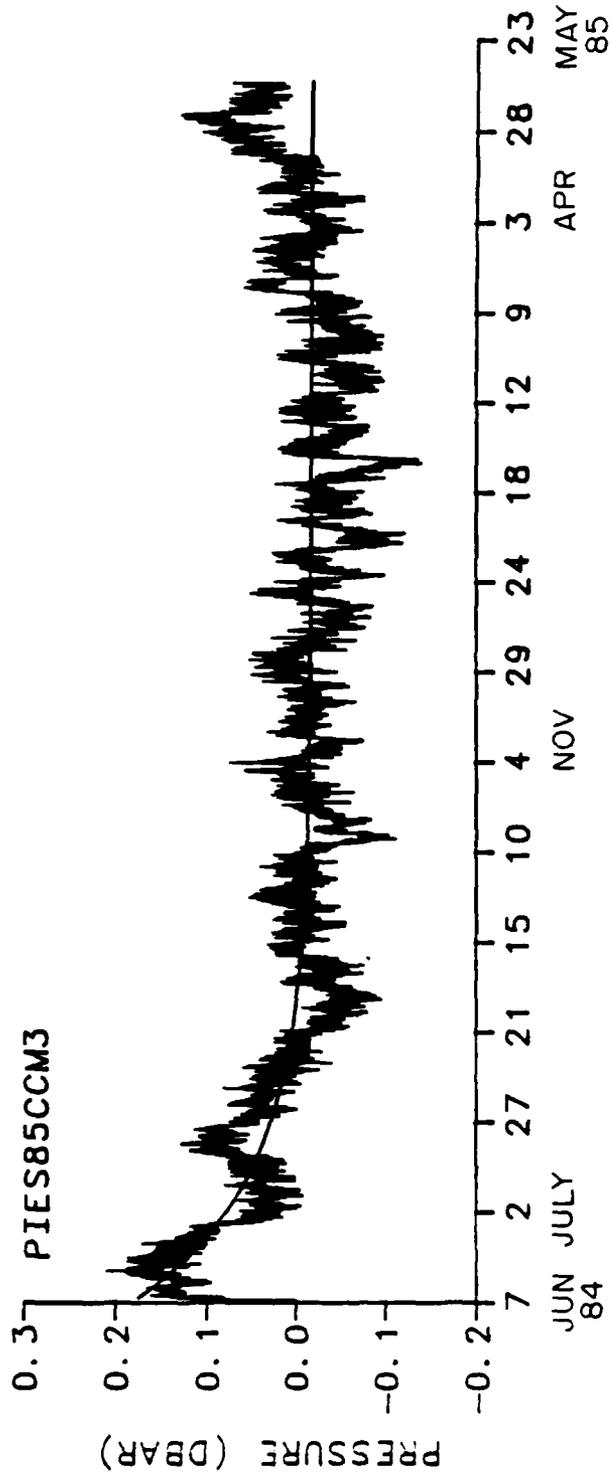


Figure 11.10 Dedided pressure record of PIES85CCM3

12. FULLY PROCESSED RECORDS

The low-pass filtered temperature and bottom pressure records are presented for each instrument. The 40HRLP temperature records are shown first. These are followed by the 40HRLP, detided, dedrifted pressure records.

The time scale is the same for all plots, with each increment corresponding to 10 days. The axis begins on 0000 GMT of the first date labelled. Since the measurements at several of the sites were obtained by two or more instruments, the data for January to May 1984 is repeated in the figures to show coinciding measurements. Each record is labelled with the instrument names above the appropriate portions.

The vertical scale for each variable is consistent between instruments. Each increment corresponds to 0.05 dbar for the bottom pressure measurements and 0.04°C for the temperatures.

The sampling interval is 6 hours for all the records. The length and start and end times of the data records are tabulated in Section 9.

12.1 Temperature: 40HRLP data

The 40HRLP temperature records are shown in Figures 12.1 to 12.3. The square-pulse nature of the temperature records has been rounded somewhat by the low-pass filtering. Visually, the temperature records from different sites have overall only a small amount of coherence; many pulses are quite different from one site to another.

12.2 Pressure: detided, dedrifted, 40HRLP data

The 40HRLP bottom pressure records are shown in Figures 12.4 to 12.6. Visually, the coherence between pressure records at neighboring sites is quite high. We have identified some of the major pressure events with the passage of Gulf Stream rings offshore and their

coalescence into the Gulf Stream (Bane and Watts, 1985). Pressure and temperature records at the same site do not appear to be very coherent, although some events occur simultaneously in both.

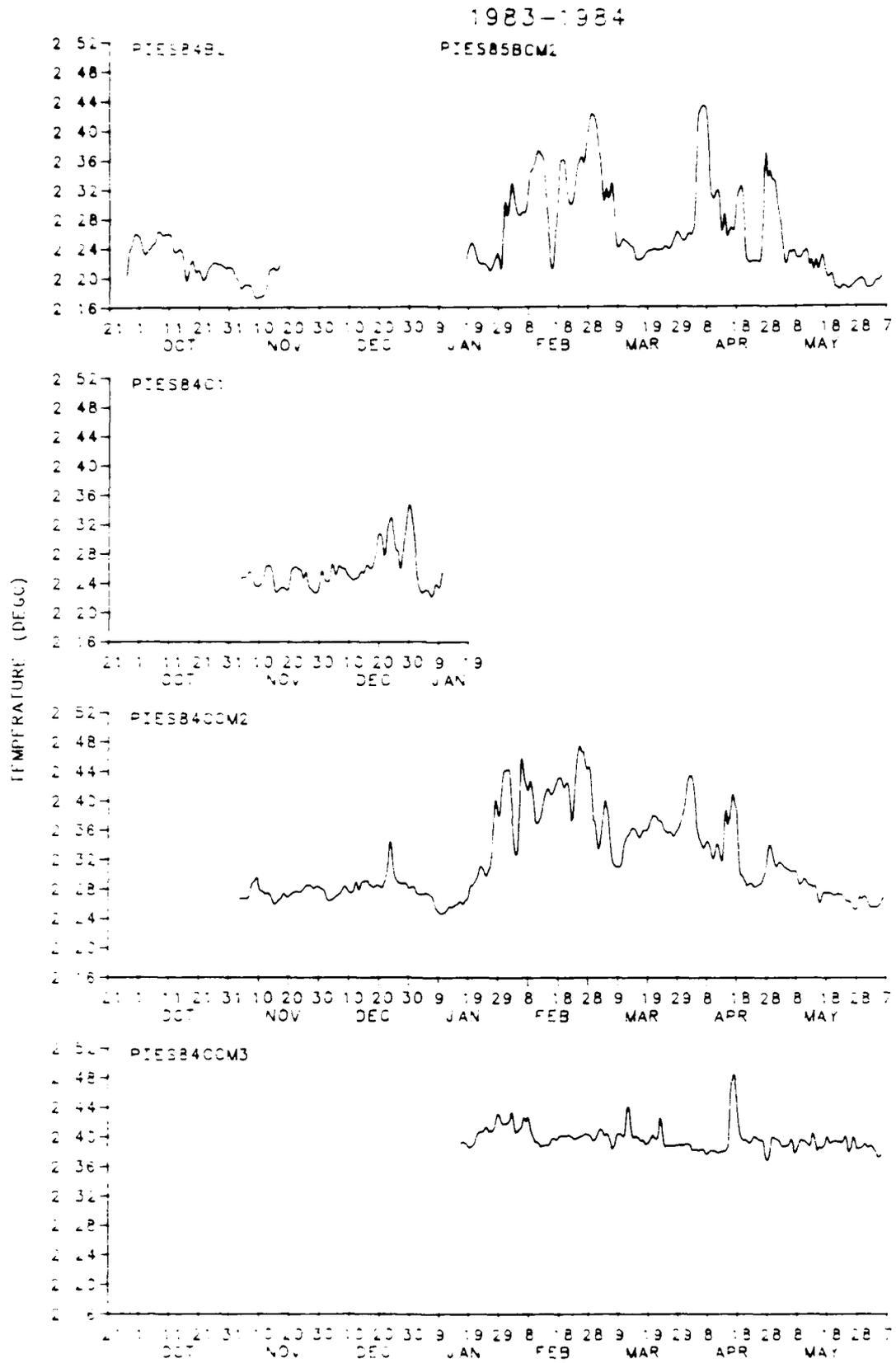


Figure 12.1 40HRLP temperature records for 1983-1984

1984-1985

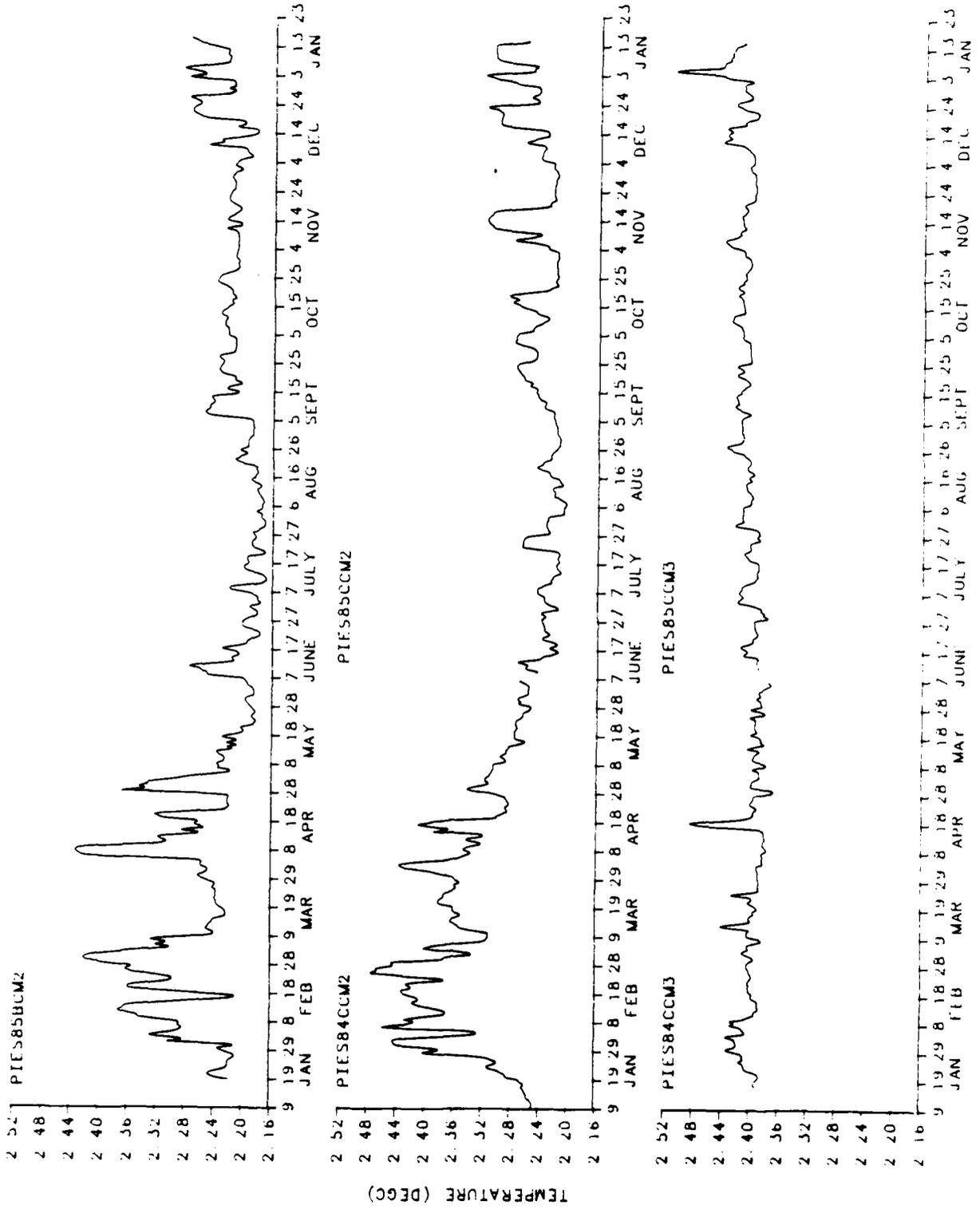


Figure 12.2 40HRLP temperature records for 1984-1985

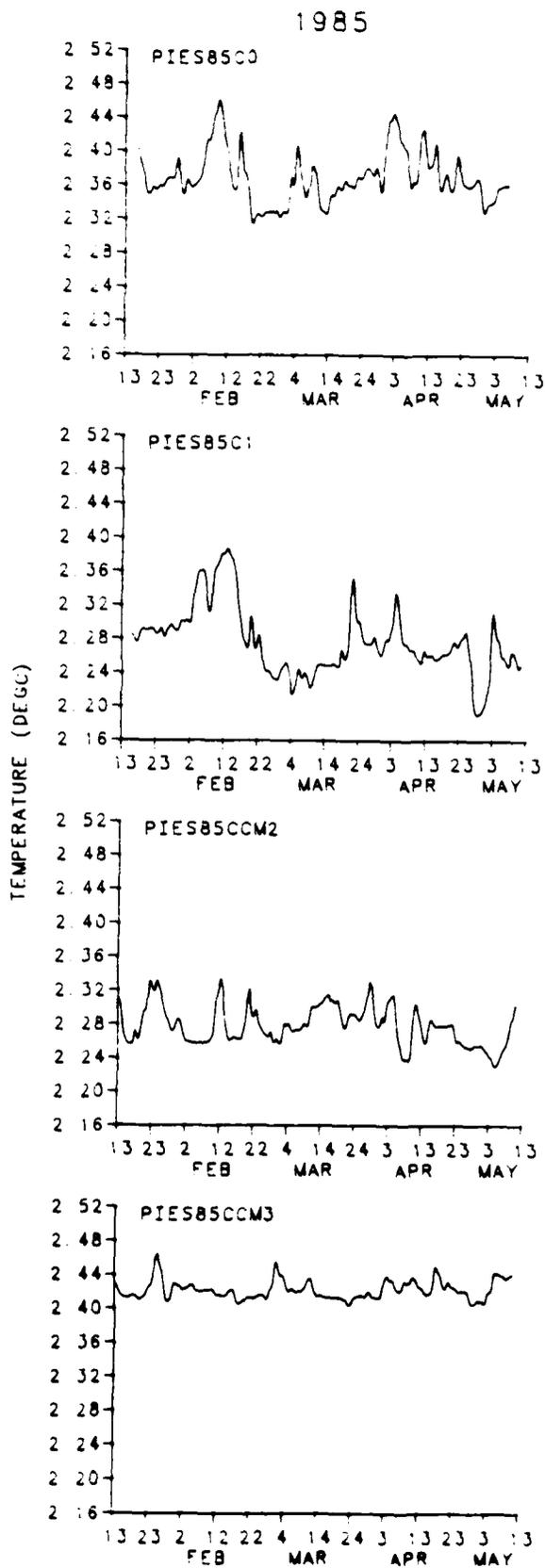


Figure 12.3 40HRLP temperature records for 1985

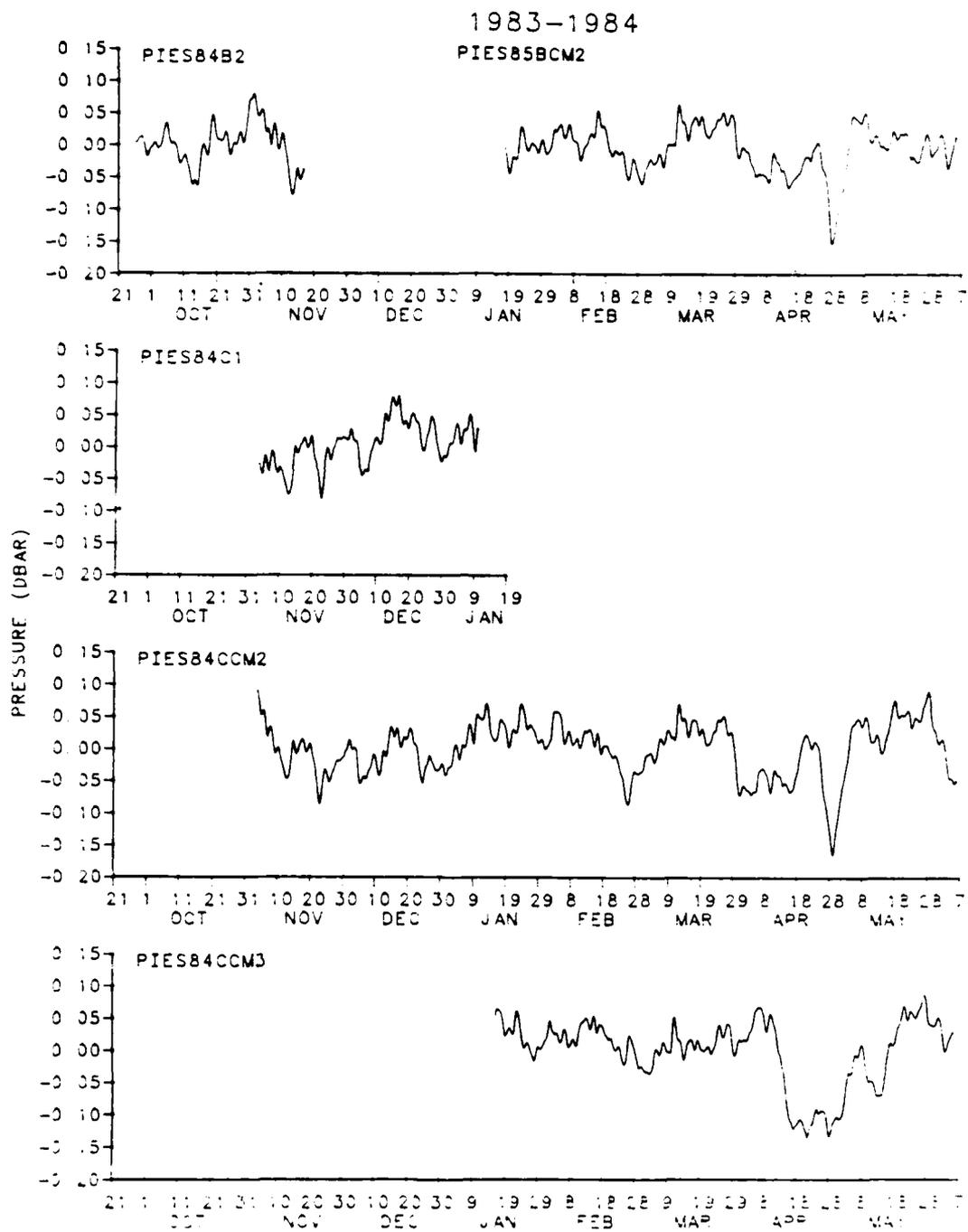


Figure 12.4 40HRLP bottom pressure records for 1983-1984

1984-1985

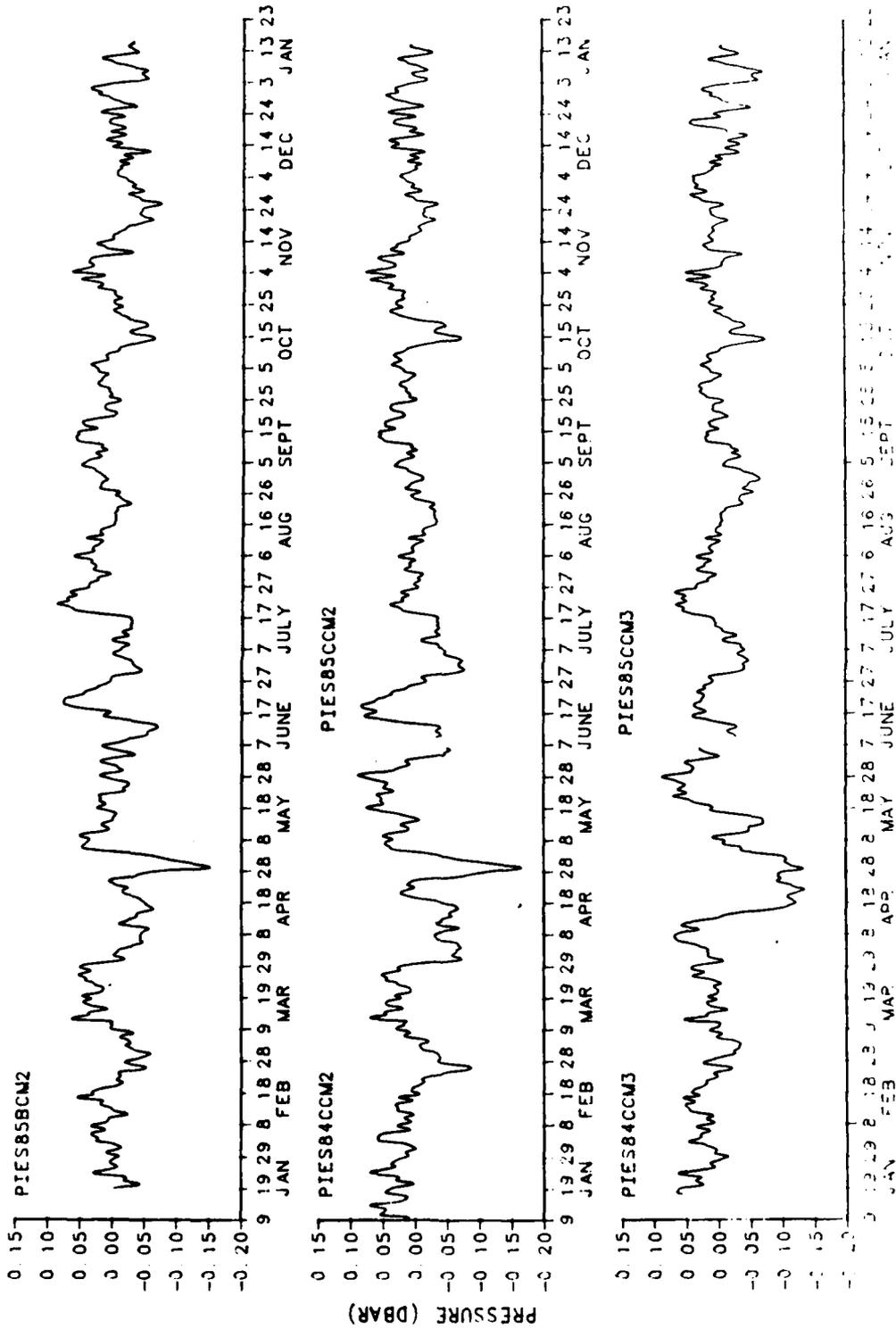


Figure 12.5 40HRLP bottom pressure records for 1984-1985

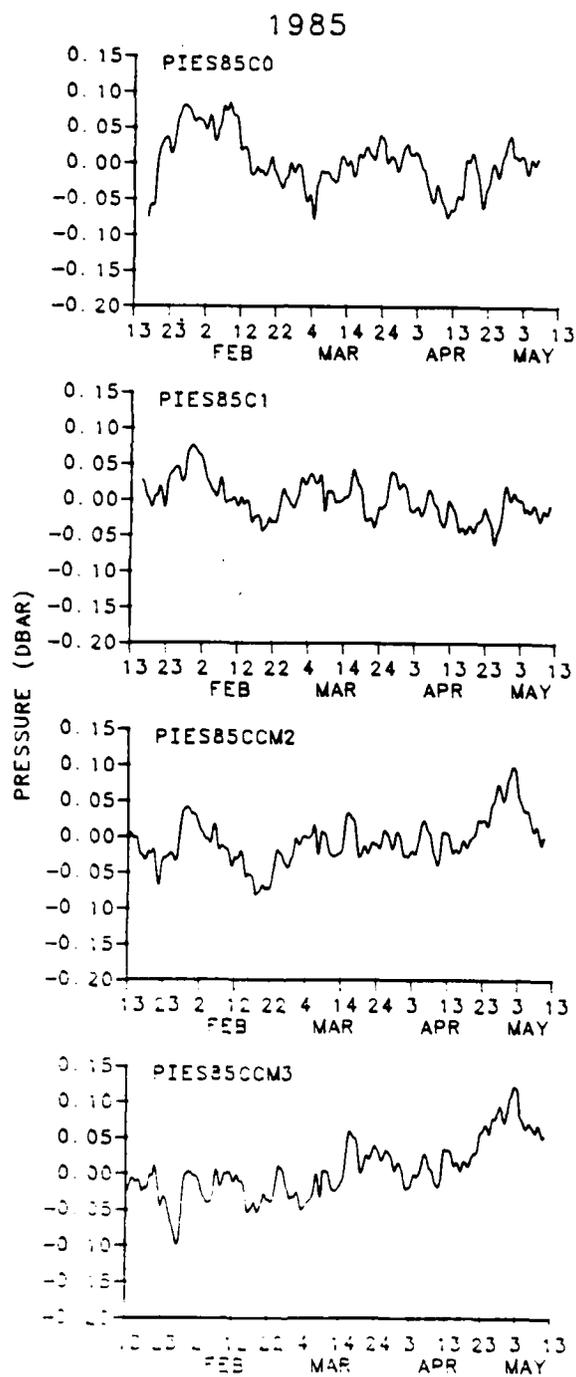


Figure 12.6 40HRLP bottom pressure records for 1985

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the first six days of deployment.

We estimate the residual error in the final pressure records, after the "dedrifting" calculations, to be typically 0.02 dbar r.m.s. (or 0.06 dbar r.m.s.) if the first 6 days of the record are excluded (or included, respectively). This low drift-error opens many possibilities for studies that require knowledge of the low-frequency dynamic pressure signal in the deep ocean. ←

Part I on Methods contains a short review of bottom pressure measurement in the deep ocean, a description of the sensors that we used, a discussion of their performance and drift relative to type of construction and prior pressurization history ("preconditioning"), and estimates of the accuracy of the dedrifted pressure records.

In Part II of this report, the full data processing is described, including calibration parameters, corrections for the influence of temperature variations on the pressure sensor, and parameterization to remove sensor drift errors by least-squares regression onto an exponentially decaying time-dependence. Time series are plotted which illustrate several steps in the processing: the edited half-hourly pressure records, the dedrifted pressures with drift-model curves superimposed, and the low-pass filtered, "dedrifted" pressure records (i.e., after subtracting the estimated drift curve).

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