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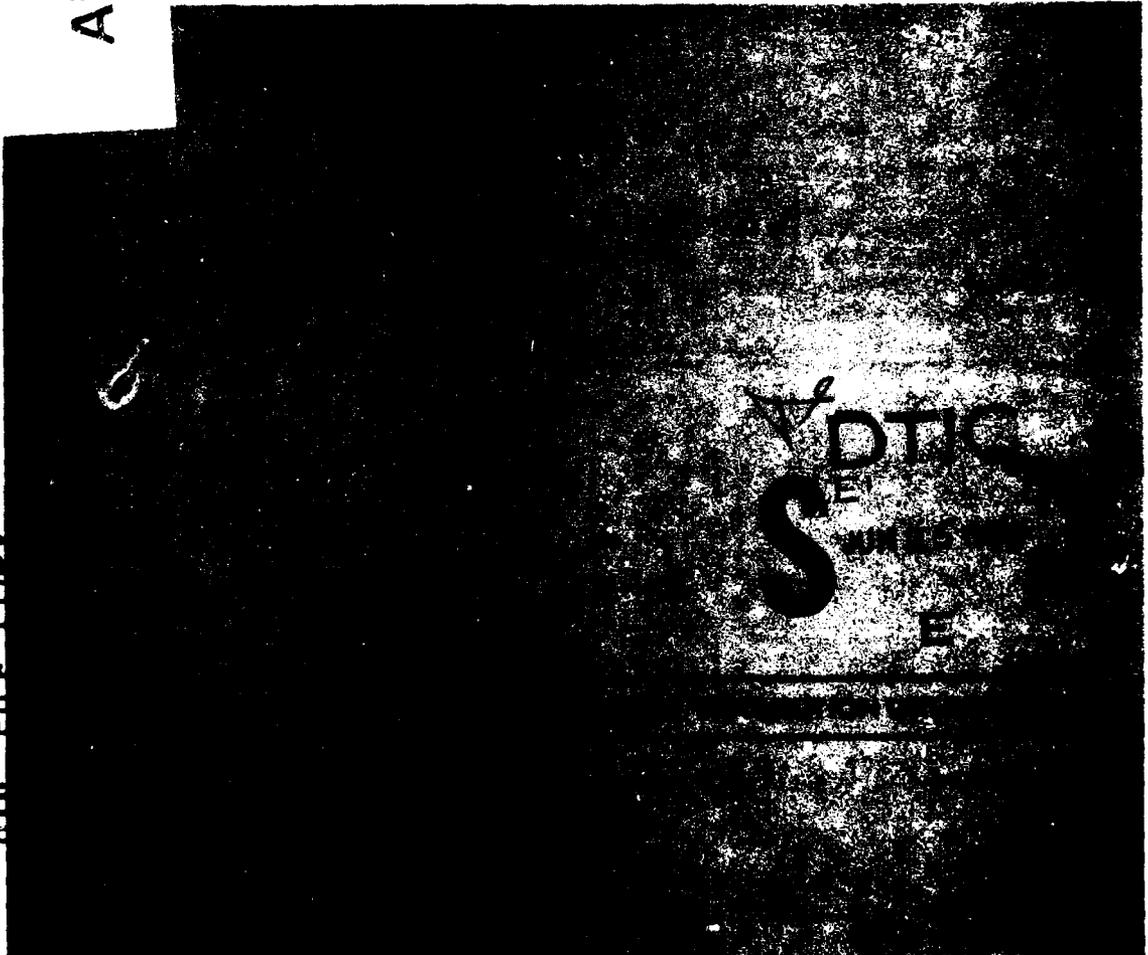
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**A NUMERICAL ALGORITHM FOR  
CHAINED AGGREGATION AND  
MODIFIED CHAINED AGGREGATION**

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<p>A computer implementation of chained aggregation and modified chained aggregation using orthogonal transformations is presented. The numerical advantages associated with orthogonal matrices are highlighted. The developed algorithm is then employed to identify a reduced-order model of a large space structure. With the reduced-order model, an output feedback design is carried out. The design is shown to produce an acceptable result on the full order model.</p>												

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A NUMERICAL ALGORITHM FOR CHAINED AGGREGATION  
AND MODIFIED CHAINED AGGREGATION

BY

HAL STANLEY THARP

B.S., University of Missouri-Rolla, 1981

THESIS

Submitted in partial fulfillment of the requirements  
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## CHAPTER 1

## INTRODUCTION

The chained aggregation procedure was first introduced in [1] in the context of reduced-order modelling of large-scale systems. The chained aggregation procedure transforms the original system into the Generalized Hessenberg Representation (GHR). Once placed in the GHR, the reduced-order modelling analysis is carried out.

Since the introduction of the chained aggregation procedure, much more research has been done [2,3,4,5]. The work that has followed has not been constrained to the reduced-order modelling problem. But, it has expanded the possible applications of the chained aggregation procedure to include many control system problems. For a thorough discussion of chained aggregation and the GHR for control system design, the author recommends consulting [6], where this issue has been specifically addressed in a geometric setting.

The algorithm developed in this thesis uses the numerical advantages associated with orthogonal matrices to implement the basic chained aggregation procedure. Included in the algorithm is an enhanced procedure, called modified chained aggregation (MCA), which has been introduced in earlier literature [2,6,7]. Several numerical advantages of orthogonal matrices are included herein; more discussion may be found in [8,9,10,11,12].

The orthogonal matrices are obtained during the algorithm by using the singular value decomposition (SVD) of particular matrices. Briefly, the SVD is used to identify the linearly independent and linearly dependent rows and columns of the particular matrix. With the identification, the decomposition generates orthonormal vectors spanning the subspaces associated with the above sets of rows and columns. These orthonormal vectors may then be judiciously grouped to form orthogonal matrices to be used within the algorithm.

The organization of this thesis is as follows. Chapter 2 presents the SVD and steps through the chained aggregation algorithm showing how SVD has been incorporated. The development of the modified chained aggregation algorithm is contained in Chapter 3. The chained aggregation algorithm is used in Chapter 4 to help in the design of an output feedback controller for a particular large flexible space structure. Chapter 5 presents the conclusion.

A summary of definitions and the notation used throughout this thesis follow. Given a subspace  $S$ , denoted by bold, capital roman letters, its orthogonal complement will be represented by  $S^\perp$ . The range space and the null space of a matrix will be denoted by  $R[\cdot]$  and  $N[\cdot]$ , respectively.  $A^\dagger$  is used to represent the pseudo-inverse of the matrix  $A$ . The transpose of a matrix  $A$  will be denoted by  $A^T$ . The set of all  $m \times n$  matrices of rank  $r$  with coefficients in the real number field,  $R$ , will be denoted by  $R_r^{m \times n}$ . The working precision of the computer will be represented by  $\epsilon$ . On a given computer, the value of  $\epsilon$  equals the smallest number which when added to one equals one. The singular values of a matrix will be denoted by  $\sigma_i$ . The matrix norms  $\|\cdot\|_2$  and  $\|\cdot\|_F$  correspond to the matrix 2-norm and the

matrix Frobenius norm, respectively. If  $A \in R^{m \times n}$ , then

$$\|A\|_2 = \max_{\|x\|_2 = \|y\|_2 = 1} |y^T A x| ,$$

where

$$\|x\|_2 = \left( \sum_{i=1}^n \xi_i^2 \right)^{1/2} = (x^T x)^{1/2}$$

$$x = (\xi_1, \xi_2, \dots, \xi_n)^T .$$

$$\|A\|_F = \left( \sum_{i=1}^m \sum_{j=1}^n a_{ij}^2 \right)^{1/2} .$$

The dimension of a vector space will be denoted by  $d(\cdot)$ . The notation

$$\text{sp} \begin{bmatrix} 0 \\ X \end{bmatrix}$$

represents the vector space spanned by the non-zero elements of the columns of  $X$  as they vary over the real numbers. The rank of a matrix will be denoted by  $\rho[\cdot]$ .

## CHAPTER 2

## SINGULAR VALUE DECOMPOSITION AND THE CHAINED AGGREGATION ALGORITHM

2.1. Introduction

Chained aggregation as introduced in [1] identifies the information structure of the system by aggregating the system with respect to the output. Once aggregated, the system exhibits the Generalized Hessenberg Representation (GHR) structure which has been shown to stimulate many possible design procedures [1,2,3,4,5,6].

A design procedure used in this thesis is model reduction. Model reduction arises out of the simple interconnecting structure displayed in the GHR and by identifying the feedback coupling between subsystems which is weak or nonexistent. The resulting model retains the strongly observable modes from the outputs rather than retaining the dominant system modes as in modal reduction. Throughout the following discussion the subsystem composed of the strongly observable modes will be referred to as the aggregate subsystem, while the residual subsystem will refer to the remaining subsystem.

Associated with the chained aggregation procedure are many state space transformations. It is shown below these transformations can be performed using orthogonal matrices which are numerically robust, in contrast to the nonorthogonal transformations described in most of the previous literature [1,2,3,4,7].

The following section reviews the singular value decomposition (SVD) along with some of its properties. The SVD is then incorporated into the steps of the chained aggregation algorithm as shown in Section 3. Section 4 highlights a consequence of the chained aggregation algorithm, its ability to check the observability and controllability of a system.

## 2.2. Singular Value Decomposition and Its Properties

The SVD will be introduced by the following theorem.

Theorem 2.2.1[8]: Let  $A \in R_r^{m \times n}$ . Then there exist orthogonal matrices  $U \in R^{m \times m}$  and  $V \in R^{n \times n}$  such that

$$A = U \Sigma V^T \quad , \quad (2.2.1)$$

where

$$\Sigma = \begin{bmatrix} S & 0 \\ 0 & 0 \end{bmatrix}$$

and  $S = \text{diag}(\sigma_1, \sigma_2, \dots, \sigma_r)$  with  $\sigma_1 \geq \dots \geq \sigma_r > 0$ .

Proof: See [8].

The product  $U \Sigma V^T$  is the singular value decomposition of the A matrix. The numbers  $\sigma_1, \sigma_2, \dots, \sigma_r$  together with  $\sigma_{r+1} = \dots = \sigma_n = 0$  are called the singular values of A and are the positive square roots of the eigenvalues of  $A^T A$ .

The following well-known properties of SVD make it useful in the chained aggregation algorithm.

Two different matrix norms associated with  $\sigma_1, \dots, \sigma_n$  can easily be defined:

$$\|A\|_2 = \sigma_1$$

$$\|A\|_F = (\sigma_1^2 + \dots + \sigma_n^2)^{1/2} .$$

Our main interest in singular values will be for rank determination. Thus, knowing that the singular values are not very sensitive to perturbations in the matrix insures a good rank determination. The change in the singular values are known to be bounded by the magnitude of the matrix perturbation.

Theorem 2.2.2[11]: Let  $A, B \in R^{m \times n}$  have singular values  $\sigma_1 \geq \dots \geq \sigma_n$  and  $\tau_1 \geq \dots \geq \tau_n$ , respectively. Then

$$|\sigma_i - \tau_i| \leq \|A - B\|_2 \quad (i = 1, 2, \dots, n).$$

Proof: See [11].

The concern over matrix perturbations is related to the fact that infinite precision arithmetic cannot be performed on a computer. For this reason, when the singular values of a matrix  $A$  are desired, the computed singular values are actually the exact singular values of a matrix slightly perturbed from  $A$ , say  $A + E$ . A more extensive discussion can be found in [8,10].

To determine the rank of a matrix, all of its singular values are compared with  $\gamma = \epsilon \cdot \|A\|$ , where the particular norm used can be selected by

the user; the number of  $\sigma_i$ 's greater than  $\gamma$  determines the rank [10]. Looked at in this way, the smallest singular value,  $\sigma_r$ , greater than  $\gamma$  gives a measure as to how far away the A matrix is from another matrix of smaller rank.

Another important outcome of SVD is the identification of the four fundamental subspaces [9] of a matrix. Suppose  $F \in R_r^{m \times n}$  has an SVD given by

$$F = U \Sigma V^T = \begin{bmatrix} U_1 & U_2 \end{bmatrix} \begin{bmatrix} S & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} V_1^T \\ V_2^T \end{bmatrix}, \quad (2.2.2)$$

where  $S = \text{diag}(\sigma_1, \dots, \sigma_r)$  with  $\sigma_1 \geq \dots \geq \sigma_r > 0$  and  $U$  and  $V$  are partitioned compatibly, i.e.,  $U_1 \in R^{m \times r}$ ,  $V_1 \in R^{n \times r}$ , etc. With this notation  $U_1$ ,  $U_2$  and  $V_1$ ,  $V_2$  produce orthonormal bases for the four fundamental subspaces,  $R[F]$ ,  $R^\perp[F]$ ,  $N^\perp[F]$ ,  $N[F]$  [8]. Figure 2.1 redrawn from [8] relates these subspaces.

Associated with the matrix  $F \in R_r^{m \times n}$  are two different vector spaces,  $R^m$  and  $R^n$ . Figure 2.1 illustrates how the  $F$  matrix can induce direct sum decompositions of these two vector spaces. In  $R^n$  the columns of  $V_2$  form an orthogonal basis for the  $N[F]$  while the columns of  $V_1$  span the remainder of  $R^n$  with an orthogonal basis. Similarly, the columns of  $U_1$  form an orthogonal basis for the  $R[F]$  in  $R^m$  while the columns of  $U_2$  span the remainder of  $R^m$  with an orthogonal basis. The mappings between these subspaces is also indicated. The  $F$  matrix maps the space spanned by  $V_1$  into the  $R[F]$ , i.e., the space spanned by  $U_1$ . The pseudo-inverse of  $F$  performs a map in the opposite direction. The space spanned by the columns of  $V_2$  is mapped into the origin in  $R^m$  by the  $F$  matrix. The space spanned by the

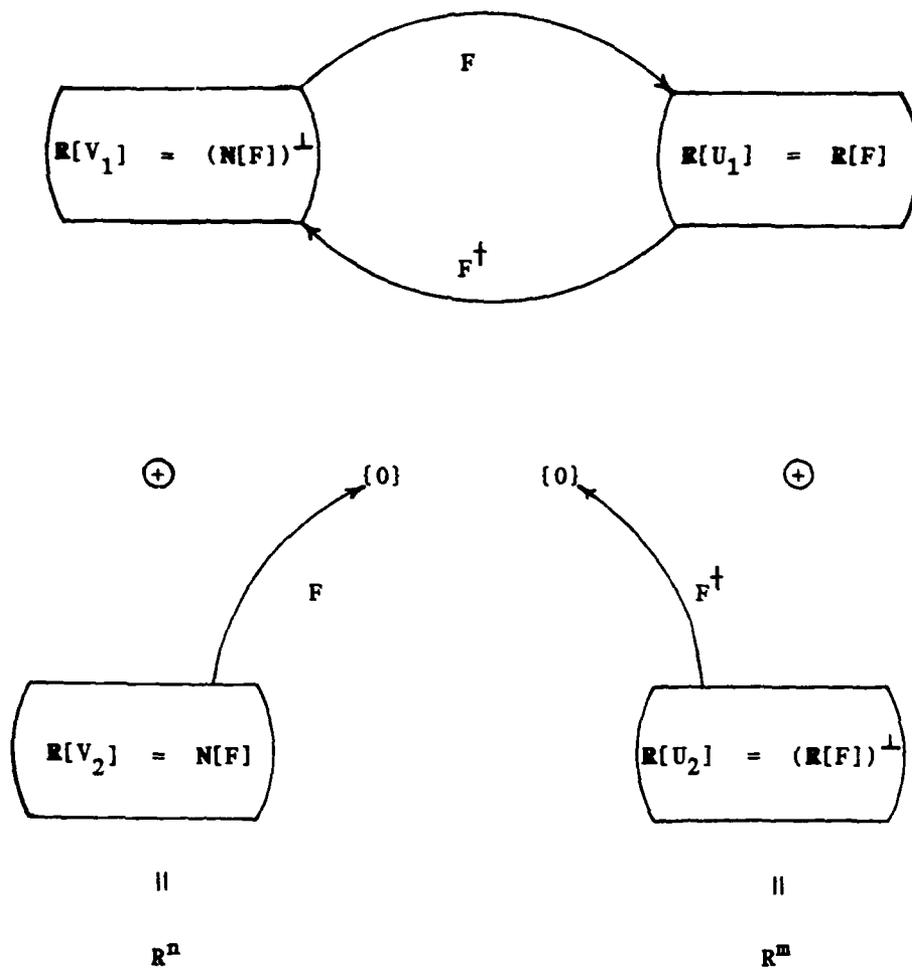


Figure 2.1: The Four Fundamental Subspaces

columns of  $U_2$  is mapped into the origin in  $R^n$  by  $F^\dagger$ .

The pseudo-inverse of  $F$  can be obtained from the SVD of  $F$

$$F^\dagger = V \Sigma^\dagger U^T = \begin{bmatrix} V_1 & V_2 \end{bmatrix} \begin{bmatrix} S^{-1} & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} U_1^T \\ U_2^T \end{bmatrix}, \quad (2.2.3)$$

where  $S^{-1} = \text{diag}(\frac{1}{\sigma_1}, \dots, \frac{1}{\sigma_r})$ ,  $\sigma_1 \geq \dots \geq \sigma_r > 0$ , and  $U$  and  $V$  are obtained from (2.2.2).

In general, SVD is the only numerically reliable method of generating basis for these subspaces, since  $U$  and  $V$  are partitioned into  $[U_1, U_2]$  and  $[V_1, V_2]$ , according to the smallest singular value [8].

Further discussion of Figure 2.1 will be postponed until after the chained aggregation algorithm has been presented.

The advantage of using SVD within the chained aggregation algorithm lies in the fact that the bases vectors generated by SVD are orthonormal. Thus, constructing transformation matrices from these orthonormal vectors results in orthogonal transformations. Several well-known numerical advantages associated with orthogonal matrices useful in the chained aggregation algorithm are:

- (1) Orthogonal matrices are easy to invert,  $U^{-1} = U^T$ .
- (2) Orthogonal matrices are perfectly conditioned with respect to the 2-norm,  $\|AU\|_2 = \|A\|_2$ .
- (3) Orthogonal matrices lend themselves to backward error analyses [11]. For example, suppose an error  $F$  is introduced into the result of an

orthogonal transformation. Let  $E = UFU^T$ . From the second characteristic above

$$\|E\|_2 = \|UFU^T\|_2 = \|FU^T\|_2 = \|F\|_2$$

and

$$U^T(A + E)U = U^TAU + U^TEU = U^TAU + F.$$

In other words, a perturbation in the result can be accounted for by a perturbation of the same magnitude in the original problem. This guarantees that if there exists an uncertainty in the original  $A$  matrix of magnitude  $\delta$ , then the resulting transformed system will have an uncertainty of the same  $\delta$  magnitude.

(4) Orthogonal transformations only rotate the axes, each axis maintaining its exact relation to the others throughout [12]. It should be mentioned that not all orthogonal matrices represent pure rotations as can be seen from a simple example. Consider the orthogonal matrix

$$P = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}.$$

This matrix reflects every point  $(x,y)$  into its mirror image  $(y,x)$  across the  $45^\circ$  line  $y = x$ , which is not a true rotation.

In [1] orthogonal matrices have not been used for the transformation matrices and consequently the matrices used can be very ill conditioned and result in a numerically unstable algorithm.

### 2.3. The Chained Aggregation Algorithm

The chained aggregation algorithm transforms any given system of the form

$$\dot{x} = Ax + Bu \quad (2.3.1a)$$

$$y = Cx, \quad (2.3.1b)$$

where  $A \in R^{n \times n}$ ,  $B \in R^{n \times m}$ , and  $C \in R^{1 \times n}$  into the GHR using only the information structure of the system. The GHR is given by

$$\dot{z} = Fz + Gu \quad (2.3.2a)$$

$$y = Dz, \quad (2.3.2b)$$

where

$$F = \begin{bmatrix} F_{11} & F_{12} & 0 & \dots & 0 & 0 \\ F_{21} & F_{22} & F_{23} & 0 & \dots & 0 & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ F_{j1} & F_{j2} & \dots & F_{jj} & F_{j,j+1} & 0 & \dots & 0 \\ \vdots & \vdots \\ F_{k-2,1} & F_{k-2,2} & \dots & \dots & \dots & \dots & F_{k-2,k-1} & 0 \\ F_{k-1,1} & F_{k-1,2} & \dots & \dots & \dots & \dots & F_{k-1,k-1} & F_{k-1,k} \\ F_{k,1} & F_{k,2} & \dots & \dots & \dots & \dots & F_{k,k-1} & F_{k,k} \end{bmatrix}$$

$$G = \begin{bmatrix} G_1 \\ G_2 \\ \vdots \\ G_k \end{bmatrix}, \quad D = \begin{bmatrix} D_1 & 0 & \dots & 0 \end{bmatrix}$$

with  $F_{i,i} \in R^{r_i \times r_i}$ ,  $r_i \geq r_{i+1}$ ,  $\sum_{i=1}^k r_i = n$ , and  $D_1 \in R^{r_1 \times r_1}$ . The following steps comprise the chained aggregation algorithm.

**2.3.1. Algorithm**

Let  $A \in R^{n \times n}$ ,  $B \in R^{n \times m}$ , and  $C \in R^{r_1 \times n}$  with  $C$  having full row rank.

Initialization:  $A^1 = A$ ,  $C = C$ ,  $\tau = 0$ ,  $p = n$ ,  $\gamma = s \parallel A_{11}$ , and  $i = 1$ .

Step 1: Perform a column compression [10] on the C matrix by using SVD. The linearly independent columns of C will be compressed to the left by post multiplying C by the V matrix resulting from SVD. If  $V^i = [V_1^i, V_2^i]$  with  $V_1^i \in R^{n \times r_1}$  and  $V_2^i \in R^{n \times (n-r_1)}$ , then

$$C = U^i \Sigma^i V^{iT}$$

results in

$$CV^i = C[V_1^i, V_2^i] = [D_1 \quad 0] .$$

Step 2: Initialize the transformation matrix

$$T^i = V^{iT} .$$

Step 3: Perform a state space transformation on the  $A^i$  matrix. This transformation can be broken down into four smaller and separate transformations. Since at most only two of the four smaller transformations are needed, this allows for fewer calculations during the execution of the algorithm.

$$V^{iT} A^i V^i = \begin{bmatrix} V_1^{iT} A^i V_1^i & V_1^{iT} A^i V_2^i \\ V_2^{iT} A^i V_1^i & V_2^{iT} A^i V_2^i \end{bmatrix}$$

$$= \begin{bmatrix} A_{11}^i & A_{12}^i \\ A_{21}^i & A_{22}^i \end{bmatrix} .$$

Let  $\rho = \rho - r_i$ .

Compute only  $A_{12}^i = V_1^{iT} A^i V_2^i \in R^{r_i \times \rho}$  at this step.

Step 4: Compress the columns of  $A_{12}^i$  using SVD.

$$A_{12}^i = U^{i+1} \Sigma^{i+1} V^{(i+1)T}$$

$$A_{12}^i [V_1^{i+1}, V_2^{i+1}] = [F_{i,i+1}, 0] .$$

where  $F_{i,i+1} \in R^{r_i \times r_{i+1}}$  and  $V^{i+1} \in R^{\rho \times \rho}$ .

Step 5: Check the singular values of  $A_{12}^i$ .

If all  $\sigma_j$ 's  $< \gamma$  ( $j = 1, 2, \dots, r_i$ ), then exit 1.

If all  $\sigma_j$ 's  $\geq \gamma$  ( $j = 1, 2, \dots, r_{i+1} \leq r_i$ ), then exit 2.

Otherwise, continue with  $\tau = \tau + (\text{number of } \sigma_j \text{'s } \geq \gamma)$ .

Step 6: Update the transformation matrix.

$$T^{i+1} = \begin{bmatrix} I_\tau & 0 \\ 0 & V^{(i+1)T} \end{bmatrix} T^i ,$$

where  $I_\tau$  implies  $I \in R^{\tau \times \tau}$ .

Step 7: Calculate the  $A_{22}^i$  submatrix.

$$A_{22}^i = V_2^{iT} A^i V_2^i \in R^{\rho \times \rho} .$$

Step 8: Let  $A^{i+1} = A_{22}^i$ ,  $i = i + 1$ . Go to Step 3.

Exit 1: The system aggregates.  $F = TAT^T$ ,  $G = TB$ ,  $D = CT^T$ , where  $F_{i,i+1} = 0$ .

Exit 2: The system does not aggregate.  $F = TAT^T$ ,  $G = TB$ ,  $D = CT^T$ , where

$F_{i,i+1}$  has full column rank.

Upon exit from this algorithm the original system has been transformed into the GHR using orthogonal matrices, a numerically stable transformation process.

The chained aggregation algorithm identifies the supremal A-invariant subspace in the  $N[C]$  [13]. This can be understood by referring to Eq. (2.3.2). In the new bases the supremal A-invariant subspace in the  $N[C]$  is immediately seen to be

$$\text{sp} \begin{bmatrix} 0 \\ X \end{bmatrix},$$

where  $X \in R^{s \times 1}$ , and  $s = d(F_{k,k})$ .

Any vector lying in this space is obviously A-invariant, i.e.,

$$F \begin{bmatrix} 0 \\ X \end{bmatrix} \subset \begin{bmatrix} 0 \\ X \end{bmatrix}$$

and lies in the  $N[C]$ ,

$$[D_1 \ 0 \ 0] \begin{bmatrix} 0 \\ 0 \\ X \end{bmatrix} = [0].$$

To better understand Figure 2.1, consider the system at step 3 on the first pass through the algorithm. Aggregation will occur at this stage if and only if the  $N[C]$  is A-invariant, i.e.,  $AN[C] \subset N[C]$ . If the F matrix in Figure 2.1 is replaced by the C matrix of the system, the columns of  $V_2$  are seen to span the  $N[C]$  and therefore  $AV_2 \subset V_2$ . This immediately forces the  $A_{12}$  submatrix to be zero

$$A_{12} = V_1^T A V_2 C V_1^T V_2 = 0 .$$

Thus, by using Figure 2.1 and noting what causes aggregation, an understanding of why the  $A_{12}$  submatrix must be zero can be obtained.

#### 2.4. Observability and Controllability Tests

An immediate consequence of the algorithm is its ability to test the observability of a system in a numerically stable manner. By considering the dual problem  $(A^T, B^T)$ , the controllability of a system can also be checked. Algorithms similar to the chained aggregation algorithm dealing specifically with the controllability problem have been given in [10,12,14].

The following definition is needed.

Definition 2.4.1: The pair  $(A,C)$  is said to aggregate, if when represented in the GHR the  $F_{k-1,k}$  submatrix equals zero.

The tests using the chained aggregation algorithm may now be given.

Theorem 2.4.2: The following statements are equivalent:

1. The pair  $(A,C)$  is unobservable.
2. The system  $(A,C)$  will aggregate.

Proof: ( 1 implies 2 ).

If the pair  $(A,C)$  is unobservable, then the Hautus test will result in a matrix of rank less than  $n$ . Since observability is invariant to a state

space transformation, the Hautus test may be applied to the GHR induced by the pair (A,C)

$$\begin{bmatrix} F_{11}^{-\lambda I} & F_{12} & 0 & \dots & 0 \\ F_{21} & F_{22}^{-\lambda I} & F_{23} & 0 & \dots & 0 \\ \vdots & & & & & \vdots \\ \vdots & & & & & \vdots \\ \vdots & & & & & 0 \\ F_{k-1,1} & F_{k-1,2} & \dots & F_{k-1,k-1}^{-\lambda I} & F_{k-1,k} \\ F_{k,1} & F_{k,2} & \dots & F_{k,k-1} & F_{k,k}^{-\lambda I} \\ D_1 & 0 & \dots & & 0 \end{bmatrix} .$$

Because of the GHR construction, the only manner in which the above matrix can have rank less than  $n$  for any  $\lambda$  is for the  $F_{k-1,k}$  submatrix to be zero. This is exactly the condition for aggregation.

( 2 implies 1 ) is now clear. If the system aggregates, then  $F_{k-1,k} = 0$  and the pair (A,C) is unobservable, since the rank of the above matrix is less than  $n$  for any eigenvalue of the system.  $\square$

The dual result follows immediately.

Theorem 2.4.3: The following statements are equivalent:

1. The pair  $(A,B)$  is uncontrollable.
2. The system  $(A^T, B^T)$  will aggregate.

Proof: Similar to the above proof.

## CHAPTER 3

## MODIFIED CHAINED AGGREGATION

3.1. Introduction

In the basic chained aggregation algorithm, only the output information structure of the system is used. By incorporating the input structure, the system can be forced to aggregate, using state feedback, when the  $\mathbf{R}[B_1]$  contains the  $\mathbf{R}[A_{12}]$ , where  $A_{12}$  and  $B_1$  are the submatrices generated during one of the steps in the algorithm. The ability of the input to satisfy the above condition is determined using the singular value decomposition (SVD) to identify the rows of  $B_1$  which are linearly independent. By the proper choice of input,  $u$ , these linearly independent rows can then be used to annihilate the largest possible subblock of the  $A_{12}$  submatrix. Further explanation is given below.

This process, called modified chained aggregation (MCA), has been developed in [2] for use in Three-Control-Component-Design (TCCD). The concept of TCCD [2,6,7] arises in the Generalized Hessenberg Representation (GHR) structure. Briefly, this hierarchical design procedure uses the input in three specific ways. First, the input is used to force aggregation. Second, the aggregate dynamics are adjusted to the specifications of the designer. Third, if enough input structure exists the residual dynamics can be adjusted.

The application of the above concepts has been carried over into controller design for a special class of nonlinear systems [5], thus

broadening the scope of problems capable of solution using the developed algorithms.

An algorithm [10] similar to MCA appearing at approximately the same time, although the implementation had not been completed, was motivated by determination of the supremal  $(A,B)$ -invariant subspace in the  $N[C]$  [13].

Section 2 demonstrates how the input structure is identified and used to enhance the chained aggregation algorithm. The steps of an implemented algorithm which accomplishes the goals of both procedures above [2,10] are contained in Section 3.

### 3.2. Identifying The Input Structure

To motivate the use of the input structure within the chained aggregation algorithm, consider the following example.

Suppose the system after one stage of chained aggregation has the following form:

$$\begin{bmatrix} \dot{z}_1 \\ \dot{z}_2 \end{bmatrix} = \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} + \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} u \quad (3.2.1a)$$

$$y = \begin{bmatrix} D_1 & 0 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} . \quad (3.2.1b)$$

Aggregation occurs when  $A_{12} = 0$ . If  $A_{12} \neq 0$ , but  $R[A_{12}] \subset R[B_1]$ , then by selecting the input  $u = -B_1^\dagger A_{12} z_2$ , the system can be forced to aggregate. This assumes the states  $z_2$  are available for feedback. If these states are

not explicitly available, then some type of dynamic feedback must be introduced to reconstruct them. If  $\mathcal{R}[A_{12}] \not\subseteq \mathcal{R}[B_1]$ , then the MCA algorithm identifies the largest subspace of  $A_{12}$  contained in the  $\mathcal{R}[B_1]$  and performs another step of chained aggregation using the subspace of  $A_{12}$  not contained in the  $\mathcal{R}[B_1]$  as the aggregating matrix.

SVD is used to calculate the  $\mathcal{R}[B_1]$ , thus a numerically stable computation is obtained. To identify the  $\mathcal{R}[B_1]$  a row compression is performed within the MCA algorithm. The orthogonal transformation which achieves this row compression is then treated as a state space transformation which is used to transform the system matrix. After transforming the system matrix, the  $A_{12}$  submatrix is divided into two submatrices; one submatrix  $\widetilde{A}_{12}$  is not in the  $\mathcal{R}[B_1]$ , and the other submatrix  $\bar{A}_{12}$  is. If  $\bar{B}_1$  represents the compressed rows of  $B_1$ , then by using the feedback  $u = -\bar{B}_1^\dagger \bar{A}_{12} \bar{z}_2$ , the  $\bar{A}_{12}$  submatrix can be annihilated in the system matrix. Again, the states  $\bar{z}_2$  have been assumed to be available.

Consider the SVD of the  $B_1$  submatrix

$$B_1 = U \Sigma V^T = \begin{bmatrix} U_1 & U_2 \end{bmatrix} \begin{bmatrix} S & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} V_1^T \\ V_2^T \end{bmatrix}, \quad (3.2.2)$$

where  $U_1 \in \mathbb{R}^{n_1 \times r}$ ,  $U_2 \in \mathbb{R}^{n_1 \times (n_1-r)}$ ,  $S = \text{diag}(\sigma_1, \sigma_2, \dots, \sigma_r)$ , and the  $\sigma_j$ 's are the singular values of  $B_1$ . For ease in implementing the algorithm the rows of the  $B_1$  submatrix are compressed down. To achieve this result,  $B_1$  must be premultiplied by  $[U_2, U_1]^T$ .

$$\begin{aligned}
\begin{bmatrix} U_2^T \\ U_1^T \end{bmatrix} B_1 &= \begin{bmatrix} U_2^T B_1 \\ U_1^T B_1 \end{bmatrix} = \begin{bmatrix} U_2^T \\ U_1^T \end{bmatrix} [U_1 \quad U_2] \begin{bmatrix} S & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} V_1^T \\ V_2^T \end{bmatrix} \\
&= \begin{bmatrix} U_2^T U_1 & U_2^T U_2 \\ U_1^T U_1 & U_1^T U_2 \end{bmatrix} \begin{bmatrix} S V_1^T \\ 0 \end{bmatrix} = \begin{bmatrix} 0 & I_{n_1-r} \\ I_r & 0 \end{bmatrix} \begin{bmatrix} S V_1^T \\ 0 \end{bmatrix} \\
&= \begin{bmatrix} 0 \\ S V_1^T \end{bmatrix} = \begin{bmatrix} 0 \\ \bar{B}_1 \end{bmatrix} . \tag{3.2.3}
\end{aligned}$$

The resulting  $\bar{B}_1$  submatrix has full row rank. If the original B matrix had the form  $B = [B_1^T, B_2^T]^T$ , then the desired row compression in the  $B_1$  submatrix can be carried out by performing a state space transformation with the following matrix.

$$T = \begin{bmatrix} U_2^T & 0 \\ U_1^T & 0 \\ 0 & I_{n-n_1} \end{bmatrix} . \tag{3.2.4}$$

Performing a state space transformation with this matrix results in the following structure:

$$T A T^T = \begin{bmatrix} U_2^T & 0 \\ U_1^T & 0 \\ 0 & I \end{bmatrix} \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} \begin{bmatrix} U_2 & U_1 & 0 \\ 0 & 0 & I \end{bmatrix}$$

$$= \begin{bmatrix} U_2^T A_{11} U_2 & U_2^T A_{11} U_1 & U_2^T A_{12} \\ U_1^T A_{11} U_2 & U_1^T A_{11} U_1 & U_1^T A_{12} \\ A_{12} U_2 & A_{21} U_1 & A_{22} \end{bmatrix} = \begin{bmatrix} A'_{11} & \tilde{A}_{12} \\ A'_{21} & A_{22} \end{bmatrix} . \quad (3.2.5)$$

If  $\tilde{A}_{12} \neq 0$ , then it is used as the aggregating matrix in the next step of chained aggregation.

The above technique is used throughout the MCA algorithm.

### 3.3. The Modified Chained Aggregation Algorithm

Initialization:  $A^1 = A \in R^{n \times n}$ ,  $B^1 = B \in R^{n \times m}$ ,  $C \in R^{r_1 \times n}$ ,  $\beta = 0$ ,  $\eta = 0$ ,  
 $\rho = n$ ,  $\tau = 0$ ,  $\alpha = 0$ ,  $i = 1$ .

Step 1: Compress the columns of C using SVD

$$C = U^i \Sigma^i V^{iT} .$$

This implies

$$C \begin{bmatrix} V_1^i & V_2^i \end{bmatrix} = \begin{bmatrix} U_1^i & U_2^i \end{bmatrix} \begin{bmatrix} S^i & 0 \\ 0 & 0 \end{bmatrix} = \begin{bmatrix} U_1^i S^i & 0 \end{bmatrix} ,$$

where  $V_1^i \in R^{n \times r_1}$  and  $V_2^i \in R^{n \times (n-r_1)}$ . Let  $\alpha = r_1$ .

Step 2: Initialize the transformation matrix

$$T^i = V^{iT} .$$

Step 3: Calculate the  $A_{12}^i$  submatrix

$$A_{12}^i = V_1^{iT} A^i V_2^i , \quad A_{12}^i \in R^{\alpha \times (\rho - \alpha)} .$$

If  $A_{12}^i = 0$ , then exit 1.

Step 4: Calculate  $\hat{B}^i$

$$\hat{B}^i = \begin{bmatrix} I_r & 0 \\ 0 & v^i T \end{bmatrix} B^i, \quad \hat{B}^i = \begin{bmatrix} 0 \\ \hat{B}_1^i \\ \hat{B}_2^i \end{bmatrix},$$

where  $0 \in R^{\eta \times m}$ ,  $\hat{B}_1^i \in R^{\hat{\beta}_1 \times m}$ , and  $\hat{B}_2^i \in R^{(n-\hat{\beta}_1-\eta) \times m}$  with  $\hat{\beta}_1 = \alpha + \beta$ .

Step 5: Compress the rows of  $\hat{B}_1^i$  down using SVD

$$\hat{B}_1^i = \hat{U}^i \hat{\Sigma}^i \hat{V}^i T,$$

$$\begin{bmatrix} \hat{U}_2^i T \\ \hat{U}_1^i T \end{bmatrix} \hat{B}_1^i = \begin{bmatrix} 0 \\ \hat{U}_1^i T \hat{B}_1^i \end{bmatrix} = \begin{bmatrix} 0 \\ \bar{B}_1^i \end{bmatrix},$$

where  $\bar{B}_1^i \in R^{\beta \times m}$ .

Note: The value for  $\beta$  has changed between steps 4 and 5. It now equals the number of linearly independent rows in the  $\hat{B}_1^i$  submatrix.

Step 6: Update the B matrix

$$B^{i+1} = \begin{bmatrix} 0 & (\eta x m) \\ 0 & ((\hat{\beta}_1 - \beta) x m) \\ \bar{B}_1^{-i} & (\beta x m) \\ \hat{B}_2^i & ((n - \hat{\beta}_1 - \eta) x m) \end{bmatrix}$$

Step 7: Update the transformation matrix

$$T^i = \begin{bmatrix} I_\eta & 0 & 0 \\ 0 & \hat{U}_2^{iT} & 0 \\ 0 & \hat{U}_1^{iT} & 0 \\ 0 & 0 & I_{\rho-a} \end{bmatrix} T^i$$

Step 8: Update the  $A_{12}^i$  submatrix

$$\tilde{A}_{12}^i = U_2^{iT} A_{12}^i, \text{ where } \tilde{A}_{12}^i \in R^{(\hat{\beta}_1 - \beta) x (\rho - a)}$$

$$\bar{A}_{12}^i = U_1^{iT} A_{12}^i, \text{ where } \bar{A}_{12}^i \in R^{\beta x (\rho - a)}$$

If  $\tilde{A}_{12}^i = 0$ , then exit 1.

Step 9: Calculate the  $A_{22}^i$  submatrix

$$A_{22}^i = V_2^{iT} A_{22}^i, \text{ where } A_{22}^i \in R^{(\rho - a) x (\rho - a)}$$

$$\rho = \rho - a$$

$$\tau = \tau + a$$

$$i = i + 1$$

Step 10: Compress the columns of  $\tilde{A}_{12}^{i-1}$

$$\widetilde{A}_{12}^{i-1} = U^i \Sigma^i V_1^i T^i,$$

$$\widetilde{A}_{12}^{i-1} \begin{bmatrix} V_1^i \\ V_2^i \end{bmatrix} = \begin{bmatrix} U_1^i S^i \\ 0 \end{bmatrix},$$

where  $V_1^i \in R^{\rho \times \alpha}$  and  $V_2^i \in R^{\rho \times (\rho - \alpha)}$ .

If  $\alpha = \rho$ , then exit 2.

Step 11: Update the transformation matrix

$$T^i = \begin{bmatrix} I_\tau & 0 \\ 0 & V_1^i T^i \\ 0 & V_2^i T^i \end{bmatrix} T^{i-1}.$$

Step 12: Compute the new  $A_{12}^i$  submatrix

$$A_{12}^i = \begin{bmatrix} -(i-1) V_2^i \\ A_{12}^{i-1} V_2^i \\ V_1^i T^i A_{22}^{i-1} V_2^i \end{bmatrix},$$

where  $A_{12}^i \in R^{(\alpha + \beta) \times (\rho - \alpha)}$ .

If  $A_{12}^i = 0$ , then exit 1.

Step 13:  $\eta = \tau - \alpha$ . Go to Step 4.

Exit 1: The system will aggregate.  $F = T A T^T$ ,  $G = T B$ , and  $D = C T^T$ , where  $T = T^i$ .

Exit 2: The system will not aggregate.  $F = T A T^T$ ,  $G = T B$ , and  $D = C T^T$ , where  $T = T^i$ .

## CHAPTER 4

## OUTPUT FEEDBACK DESIGN USING THE CHAINED AGGREGATION ALGORITHM

4.1. Introduction

Because of the computational and numerical difficulties associated with large scale systems, a reduced-order model of the system is advantageous during the design process. As stated in Chapter 2, the Generalized Hessenberg Representation (GHR) of a system lends itself nicely to the possibility of identifying a suitable reduced-order model. By comparing the sizes of the submatrices using an appropriately selected norm generated during each stage of chained aggregation, a trade-off between reduced-order model dimension and subsystem coupling can be made to obtain the desired reduced-order model. The resulting reduced-order model contains the strongly observable modes, by construction, which may or may not be the dominant system modes.

This technique of generating a reduced-order model has been conducted on a particular large space structure. The general space structure problem is introduced in Section 2. Section 3 contains the description of the particular structure which was studied. The design procedure which was carried out is detailed in the final section.

4.2. Introduction of the General Large Space Structure Problem

Large Space Structure (LSS) problems have received a great deal of attention. The LSS themselves are usually quite flexible because of weight

restrictions imposed during their transport or deployment in space. The problems are further complicated due to the zero damping environment of space and the light natural damping of the structure itself. A recent review of the literature on LSS Control can be found in [15] with more information available in [16-23].

Initially these systems are often modelled by partial differential equations. For a practical solution, one must reduce the infinite dimensional problem down to one of finite dimension. The most popular method of reducing the infinite dimensional problem has been the finite element method [15], a structural analysis technique. The differential equations resulting from the finite element method are

$$M\ddot{q} + Kq = B_F u \quad (4.2.1a)$$

$$y = C_V \dot{q} \quad , \quad (4.2.1b)$$

where  $q \in R^n$ ,  $u \in R^m$ ,  $y \in R^r$ , and the constant matrices  $M$ ,  $K$ ,  $B_F$ , and  $C_V$  are of compatible dimensions.  $M$  is the mass matrix, which in general is positive semidefinite, and  $K$  is the stiffness matrix, which is positive definite. The physical nature of most LSS problems allows the damping to be neglected in the modelling, i.e., there are no terms involving  $\dot{q}$  in Eq. (4.2.1a).

To perform chained aggregation on the system it must be represented in state space form. A common method to obtain this representation has been to simultaneously diagonalize  $M$  and  $K$  with a unitary matrix  $\bar{M}$  [17,18] such that

$$\mathbf{a}^T \mathbf{M} \mathbf{a} = \mathbf{I} \quad \text{and} \quad \mathbf{a}^T \mathbf{K} \mathbf{a} = \Omega^2.$$

By introducing the transformation  $q = \mathbf{a} \eta$  Eq. (4.2.1) becomes

$$\ddot{\eta} + \Omega^2 \eta = \mathbf{a}^T \mathbf{B}_F \mathbf{u} \quad (4.2.2a)$$

$$y = \mathbf{C}_V \mathbf{a} \dot{\eta} \quad (4.2.2b)$$

A state space model of the system in Eq. (4.2.2) can now be constructed. Let

$$\mathbf{x} = \begin{bmatrix} \eta \\ \dot{\eta} \end{bmatrix}.$$

Then Eq. (4.2.2) can be written in state space form.

$$\begin{bmatrix} \dot{\eta} \\ \ddot{\eta} \end{bmatrix} = \begin{bmatrix} 0 & \mathbf{I} \\ -\Omega^2 & 0 \end{bmatrix} \begin{bmatrix} \eta \\ \dot{\eta} \end{bmatrix} + \begin{bmatrix} 0 \\ \mathbf{a}^T \mathbf{B}_F \end{bmatrix} \mathbf{u}, \quad (4.2.3a)$$

$$y = [0 \quad \mathbf{C}_V \mathbf{a}] \begin{bmatrix} \eta \\ \dot{\eta} \end{bmatrix}. \quad (4.2.3b)$$

If  $M$  is positive definite then another state space description can be obtained by multiplying through in Eq. (4.2.1) by  $M^{-1}$ . Letting

$$\mathbf{x} = \begin{bmatrix} q \\ \dot{q} \end{bmatrix}$$

yields

$$\begin{bmatrix} \ddot{q} \\ \dot{q} \\ q \end{bmatrix} = \begin{bmatrix} 0 & I \\ -M^{-1}K & 0 \end{bmatrix} \begin{bmatrix} q \\ \dot{q} \\ q \end{bmatrix} + \begin{bmatrix} 0 \\ M^{-1}B_F \end{bmatrix} u \quad (4.2.4a)$$

$$y = [0 \ C_v] \begin{bmatrix} q \\ \dot{q} \\ q \end{bmatrix} . \quad (4.2.4b)$$

The latter state space description was used in the design process because the original coordinates  $(q^T, \dot{q}^T)^T$  are retained in the state space description.

For ease in discussion, the following equations are introduced, with the obvious equivalence with Eq. (4.2.4)

$$\dot{x} = Ax + Bu \quad (4.2.5a)$$

$$y = Cx . \quad (4.2.5b)$$

#### 4.3. A Physical Problem Description

The structure analyzed herein has been proposed by Charles Stark Draper Labs and can be seen in Figure 4.1. All of the numerical values are summarized in Appendix B. This same structure has been analyzed in [19] using positivity concepts.

The tetrahedral apex represents the antennae feed, with members 1-6 forming the support structure and bi-peds 7-8, 9-10, and 11-12 being supports/controls which are fixed to an inertially stabilized (assumed) antenna dish. The physical nature of the problem allows sensors to be placed only on the bi-peds; no sensors can be placed on the feed itself.

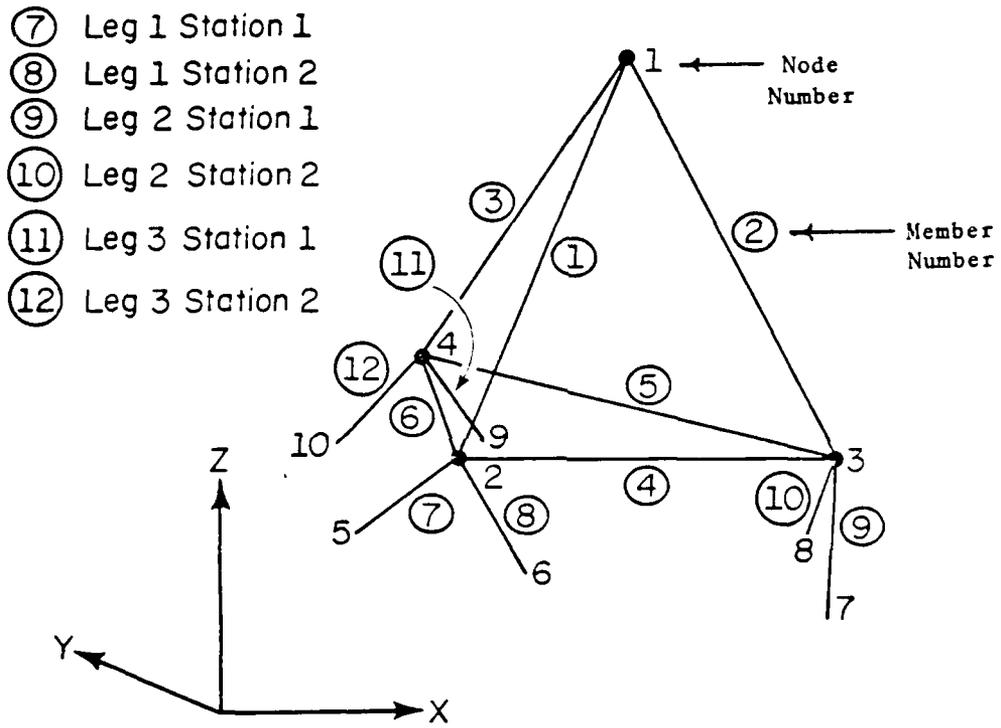


Figure 4.1: Draper Tetrahedral Truss

The actuators control the elongation and contraction of the bi-peds. Only velocity information has been used in the system model; displacement of the bi-peds is not sensed or controlled.

Because uncertainty in the model parameters exists, a perturbed system must be studied. A perturbed system is simply different M and K matrices. For the design to be acceptable, the objective must be satisfied for both the nominal and perturbed systems.

The objective is to damp the x and y deflection of the feed, node 1, to less than .0004 and .00025 units, respectively, in 20 seconds. Thus, the problem is to control the apex in the presence of modelling uncertainty and without directly controlling or measuring its motion or position.

#### 4.4. The Design Procedure

The design process began by verifying the observability and controllability of both the nominal and perturbed systems using the chained aggregation algorithm. The eigenvalues of the two systems were also computed and can be found in Table 4.1.

The next step was to obtain a reduced order model which accurately represented the overall system in general and included the desired x and y deflection modes of node 1 in particular.

The original output structure, the C matrix, of the system contained only velocity measurements of the three bi-peds and by aggregating the system with respect to this information, the x and y deflections of node 1 would be forced into the residual subsystem, an undesirable result. To circumvent this problem a C matrix containing both the controlled outputs,

Table 4.1: Nominal and Perturbed System Eigenvalues

SYSTEM EIGENVALUES				
NOMINAL	$0 \pm j12.92$	$0 \pm j10.28$	$0 \pm j9.25$	$0 \pm j8.54$
	$0 \pm j4.76$	$0 \pm j4.66$	$0 \pm j4.20$	$0 \pm j3.40$
	$0 \pm j2.96$	$0 \pm j2.89$	$0 \pm j1.66$	$0 \pm j1.34$
PERTURBED	$0 \pm j13.97$	$0 \pm j10.92$	$0 \pm j10.30$	$0 \pm j8.94$
	$0 \pm j5.71$	$0 \pm j5.68$	$0 \pm j5.15$	$0 \pm j3.85$
	$0 \pm j3.56$	$0 \pm j2.96$	$0 \pm j1.47$	$0 \pm j1.17$

the  $x$  and  $y$  displacement of node 1, and the measured outputs, the original, nominal  $C$  matrix, was constructed.

Using this  $C$  matrix together with the nominal system matrix  $A$ , four steps of the chained aggregation algorithm were implemented with the system not aggregating. The transformation matrix resulting from this aggregation process was then used to transform the nominal system,  $(A,B,C)$ , and the perturbed system,  $(A^P,B^P,C^P)$ . The following structure for both systems was identified

$$\begin{bmatrix} \dot{z}_a \\ z_a \\ \dot{z}_r \\ z_r \end{bmatrix} = \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} \begin{bmatrix} z_a \\ z_r \end{bmatrix} + \begin{bmatrix} B_1 \\ 0 \end{bmatrix} u \quad (4.4.1a)$$

$$y = [C_1 \ 0] \begin{bmatrix} z_a \\ z_r \end{bmatrix}, \quad (4.4.1b)$$

where  $z_a \in R^{16}$ ,  $z_r \in R^8$ ,  $u \in R^6$ ,  $y \in R^6$ , and the matrices are partitioned accordingly.

The eigenvalues of the  $A_{11}$  and  $A_{22}$  submatrices, subsequently referred to as the aggregate and residual subsystems, respectively, were computed and are in Table 4.2. Two immediate conclusions are obtained by comparing the eigenvalues in Table 4.1 with those in Table 4.2. First, the two sets of eigenvalues are both purely imaginary and nearly equal. Second, the lower frequencies were not necessarily placed in the aggregate subsystem, but

Table 4.2: Nominal and Perturbed Subsystem Eigenvalues

SUBSYSTEM EIGENVALUES				
NOMINAL				
AGGREGATE	$0 \pm j8.04$	$0 \pm j7.43$	$0 \pm j7.43$	$0 \pm j4.63$
	$0 \pm j4.59$	$0 \pm j4.20$	$0 \pm j1.94$	$0 \pm j1.43$
RESIDUAL	$0 \pm j12.00$	$0 \pm j3.52$	$0 \pm j3.02$	$0 \pm j2.96$
PERTURBED				
AGGREGATE	$0 \pm j8.49$	$0 \pm j8.36$	$0 \pm j8.36$	$0 \pm j5.64$
	$0 \pm j5.62$	$0 \pm j5.15$	$0 \pm j1.75$	$0 \pm j1.24$
RESIDUAL	$0 \pm j13.16$	$0 \pm j3.50$	$0 \pm j3.35$	$0 \pm j2.66$

instead the strongly observable modes have been forced into the aggregate.

This differs from a modal decomposition of the system where the lower frequency modes are retained to form a reduced order model and the remaining modes are discarded [24]. With the chained aggregation procedure the important modes are those modes which influence the observable modes of the system the most. It is not necessarily concerned with the relative frequencies of the modes.

The effect of the neglected modes, both residual and infinite dimensional, on the reduced order model has been referred to in the literature as controller and observer spillover [17,18]. This refers to how the unmodelled modes are affected by the input and how they affect the output, respectively.

An initial check to see how much coupling existed from the residual subsystem into the aggregate subsystem was performed by comparing the sizes of the submatrices involved. The size used for each submatrix was the matrix 2-norm, i.e., the largest singular value. The norms computed were

$$\|A_{11}\|_2 = 81.92 \quad , \quad \|A_{12}\|_2 = 6.32$$

$$\|A_{21}\|_2 = 94.40 \quad , \quad \|A_{22}\|_2 = 148.37 \quad ,$$

and

$$\|A_{11}^P\|_2 = 94.13 \quad , \quad \|A_{12}^P\|_2 = 5.07$$

$$\|A_{21}^p\|_2 = 97.88 \quad , \quad \|A_{22}^p\|_2 = 178.18 \quad .$$

The differences in magnitude suggested the coupling was weak and could be neglected [25].

Further analysis supporting this claim was obtained from a geometric setting, following the work in [6] on near unobservability. Intuitively, if the residual subsystem was nearly unobservable in the aggregate subsystem, then the coupling of the residual into the aggregate would be considered weak, i.e., the  $A_{12}$  submatrix would have little influence on the aggregate states. As shown later this was made more rigorous by showing that the subspace

$$U = \mathbf{R} \begin{bmatrix} A_{12} \\ A_{22} \end{bmatrix}$$

was near the subspace

$$V = \mathbf{R} \begin{bmatrix} 0 \\ A_{22} \end{bmatrix} .$$

This suggested that the residual was nearly unobservable by the aggregate, so the  $A_{12}$  submatrix was neglected in the analysis.

To strengthen the concept of one subspace being near another, canonical angles are defined.

Definition 4.4.1 [6,26]: Let  $U$  and  $V$  be subspaces of  $\mathbf{R}^n$  with orthonormal bases  $U$  and  $V$ , respectively. Let  $\sigma_i$  be the singular values of  $U^T V$ . Then the canonical angles between  $U$  and  $V$  are the numbers

$$\theta_i = \text{Cos}^{-1} \sigma_i \quad \square$$

Referring to Figure 2.1 a basis for  $U$  and a basis for  $V$  was obtained by performing singular value decomposition on both matrices  $[A_{12}^T, A_{22}^T]^T$  and  $[0, A_{22}^T]^T$ , separately, and using the generated  $U_1$  submatrix for each basis. The canonical angles between subspaces  $U$  and  $V$  were then obtained using Definition (4.4.1) and can be found in Table 4.3 for both the nominal and perturbed systems. In general, the canonical angles were small and the two subspaces were considered near each other.

Another motivation for neglecting the coupling due to the  $A_{12}$  submatrix is because of the structure of the transformed  $C$  matrix and the fact that output feedback is being used, i.e., the  $A_{12}$  submatrix will not be affected by the feedback.

Table 4.3: Canonical Angles Between  $U$  and  $V$  For The Nominal and Perturbed Systems

CANONICAL ANGLES				
NOMINAL	0.0 °	0.0 °	0.0 °	7.3 °
	20.5 °	29.9 °	34.6 °	42.4 °
PERTURBED	0.0 °	0.0 °	12.6 °	13.0 °
	21.5 °	29.9 °	34.6 °	42.4 °

By neglecting the coupling and noting that the residual subsystem was stable, the aggregate subsystem yielded the following reduced order model which was used in the design process.

$$\dot{z}_a = A_{11}z_a + B_1u \quad (4.4.2a)$$

$$y = C_1z_a \quad (4.4.2b)$$

This model as well as the reduced order perturbed model were verified to be controllable and observable by using the chained aggregation algorithm.

Because all of the eigenvalues in the aggregate were imaginary, some type of damping had to be introduced. The structure of the transformed nominal input and nominal output matrices suggested that output feedback,  $u = -Ky$ , be used to introduce the desired damping. The gain matrix,  $K$ , was obtained using the procedure outlined in [27,28]; more background material is given in [29,30]. This design approach begins by solving a reference optimal state-feedback linear quadratic regulator problem. The eigenvectors associated with the closed-loop system matrix are then determined. If there are  $r$  system outputs, then  $r$  of these eigenvectors are retained in the reduced-order output feedback problem, i.e., an  $r$ -dimensional eigenspace of the reference problem is retained.

To achieve the desired objective for the  $x$  and  $y$  deflections of node one, the appropriate  $Q$  and  $R$  matrices had to be selected. The following analysis led to the desired weighting matrices. The input weightings were selected to be equal and large so that the input energy would not be excessive. The weighting on the states was not as straightforward. After

the necessary transformations were carried out to place the system in the correct structure, the x and y deflections were composed largely of states 15 and 16 with states 13 and 14 corresponding to their respective velocities. Because the x and y deflections as well as their velocities were nearly uncontrollable in the reduced-order model, less weighting than might be expected on these states had to be used. Looking at the feedback structure, states 1-6 were weighted very heavily and states 7-11 were hardly weighted, by comparison. State 12 did require more damping, so it was weighted appropriately. These conclusions were drawn after preliminary trials and observing how the various states related to one another and how their magnitudes compared with the other states. The resulting x and y deflections for both reduced order models can be seen in Figures 4.2 and 4.3.

To verify that the above gain matrix, K, resulted in a desirable design for the full order systems, it was applied to both the nominal and perturbed full order models. The resulting x and y deflections can be seen in Figures 4.4 and 4.5.

By examining the trajectories of the full order systems one can see the slight error introduced by using the reduced-order model during the design procedure. The x deflections are seen to meet the required objective, but the y deflections require 28 and 34 seconds to meet the stricter objective in the nominal and perturbed systems, respectively.

The use of suboptimal dynamic output feedback [27,28,29] could possibly increase the flexibility and robustness of the solution and should be investigated in future work.

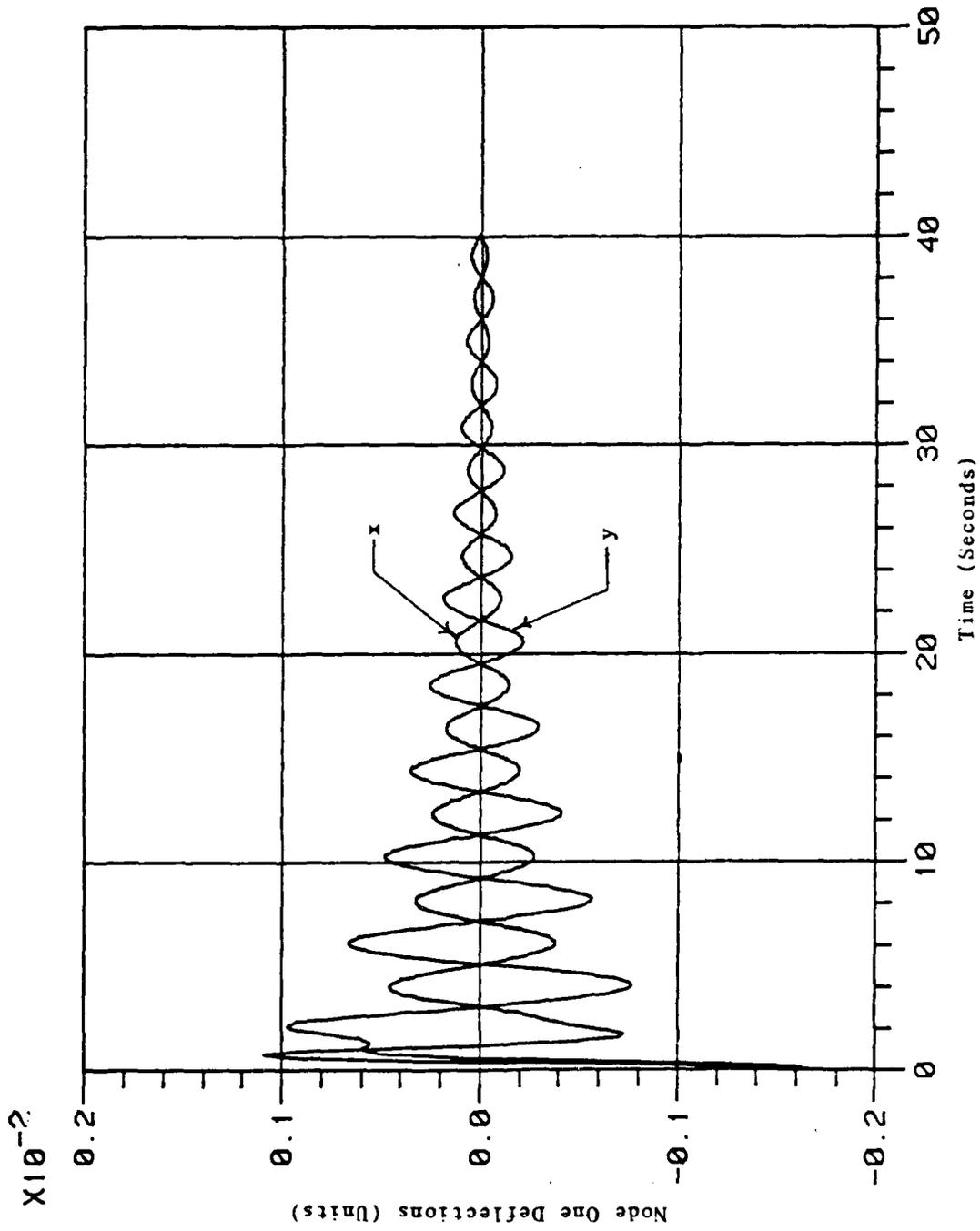


Figure 4.2 Trajectories for the nominal reduced-order model



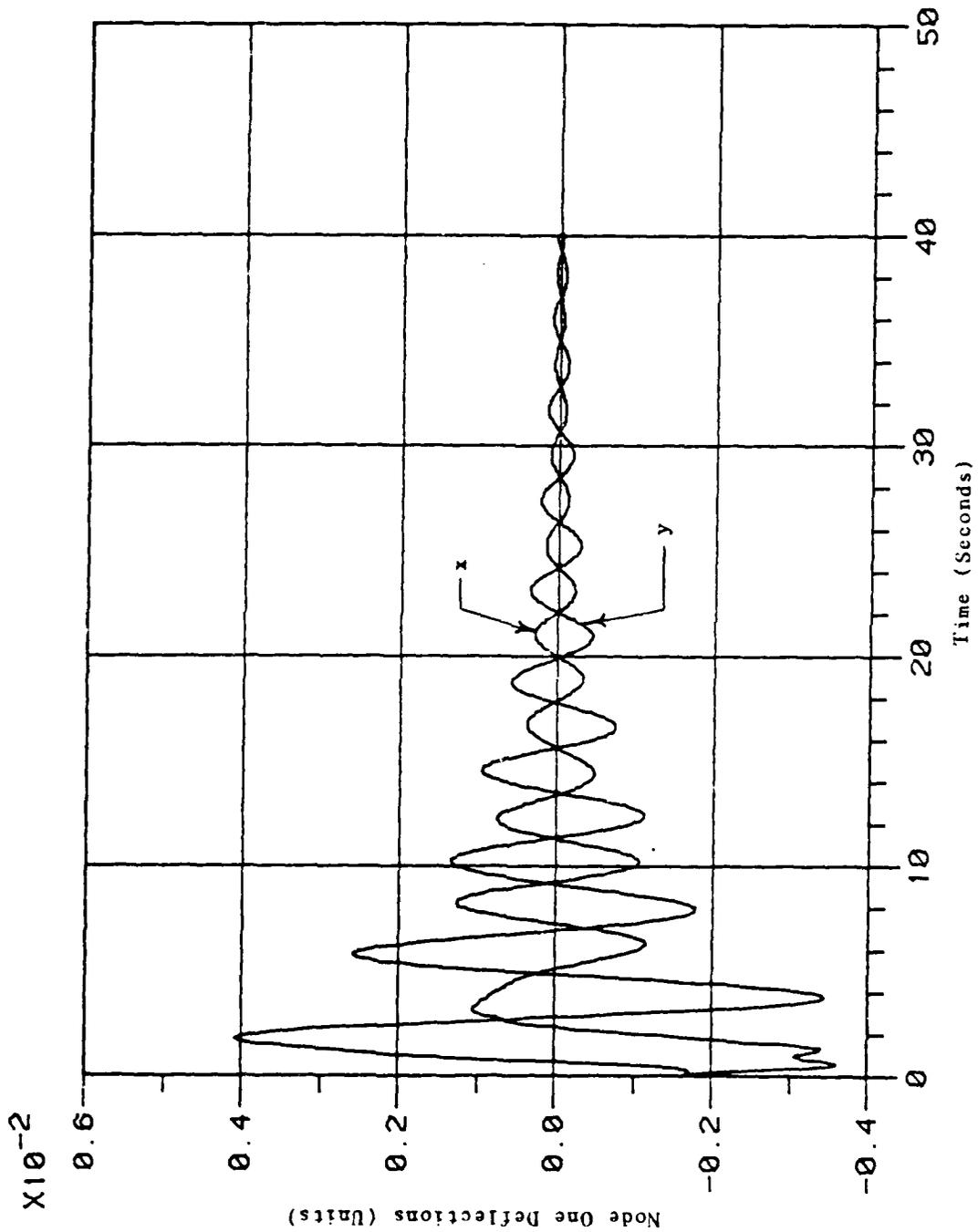


Figure 4.4 Trajectories for the nominal full-order model

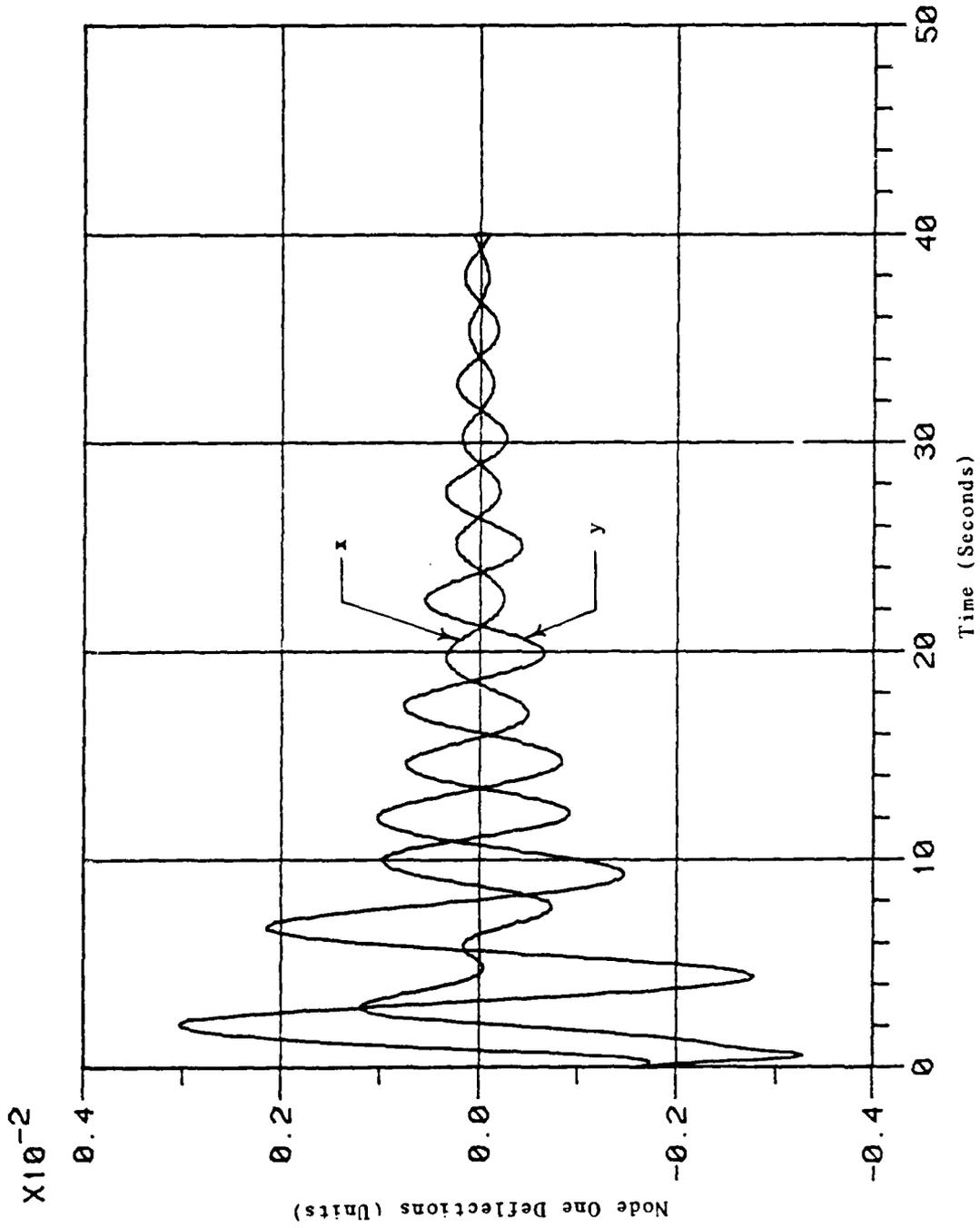


Figure 4.5 Trajectories for the perturbed full-order model

## CHAPTER 5

## CONCLUSION

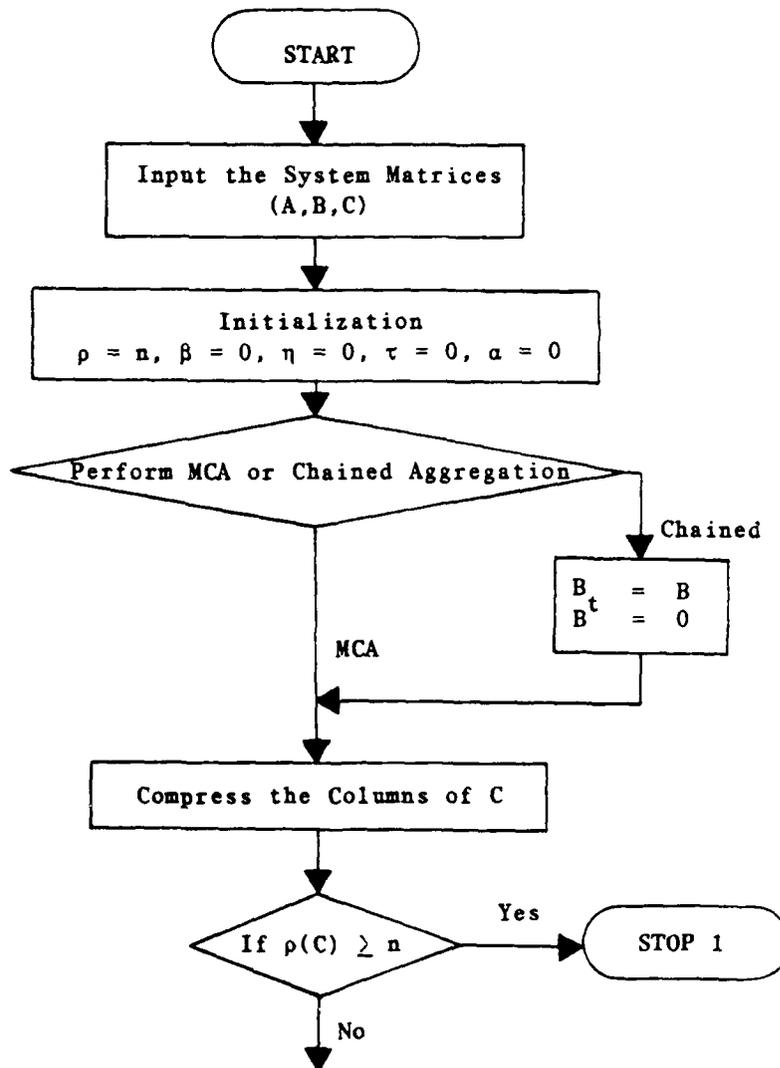
A computer implementation of chained aggregation and modified chained aggregation using orthogonal transformation matrices has been presented. To obtain the orthogonal matrices the singular value decomposition has been incorporated into the algorithm whenever a state space transformation must be performed. Because orthogonal matrices have been used, the problem sensitivity will usually not be altered.

In Chapter 4 the algorithm has been used in the design of a control for a particular large space structure prototype. The reduced-order model suggested by using the chained aggregation algorithm contains the desired information structure, the  $x$  and  $y$  deflections of node one, and can be used during the design process and, or in the physical implementation of the control, if a dynamical feedback is to be used.

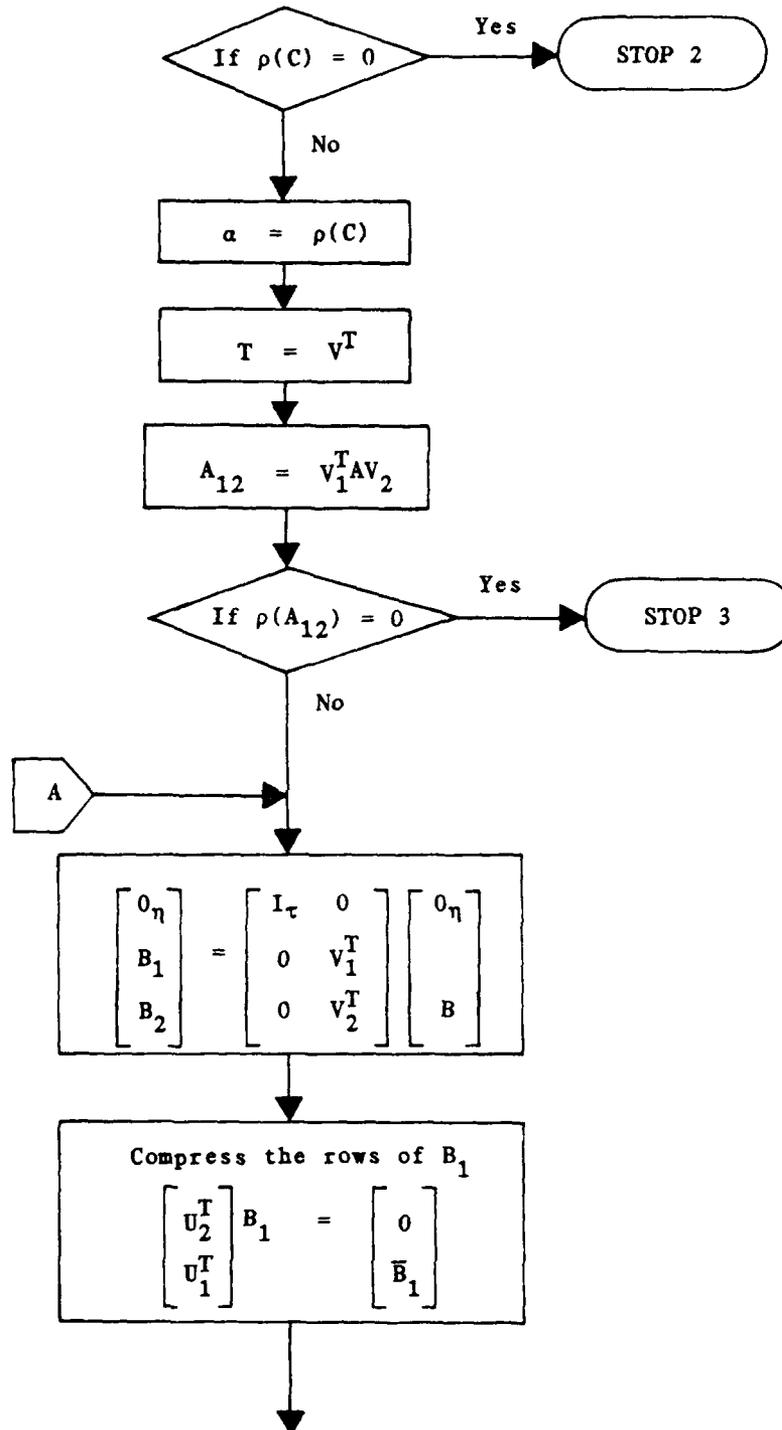
Future research may now focus on the numerical solution of practical problems using the design schemes presented in past Generalized Hessenberg Representation articles.

APPENDIX A  
SUPPORTING SOFTWARE

The two algorithms developed in Chapters 2 and 3 have been incorporated into a single computer program. The program has been written in FORTRAN with the singular value decomposition subroutine taken from LINPACK [31]. A flowchart of the software follows.



Flowchart continued on next page.



Flowchart continued on next page.

$$\begin{bmatrix} 0 \\ 0 \\ \bar{B}_1 \\ B_2 \end{bmatrix} = \begin{bmatrix} I_\eta & 0 & 0 \\ 0 & U_2^T & 0 \\ 0 & U_1^T & 0 \\ 0 & 0 & I \end{bmatrix} \begin{bmatrix} 0 \\ B_1 \\ B_2 \end{bmatrix}$$

$$T = \begin{bmatrix} I_\eta & 0 & 0 \\ 0 & U_2^T & 0 \\ 0 & U_1^T & 0 \\ 0 & 0 & I \end{bmatrix} T$$

$$\bar{A}_{12} = U_1^T A_{12}$$

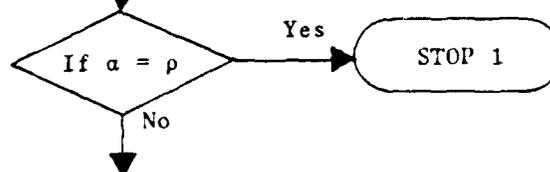
$$\tilde{A}_{12} = U_2^T A_{12}$$

$$A_{22} = V_2^T A V_2$$

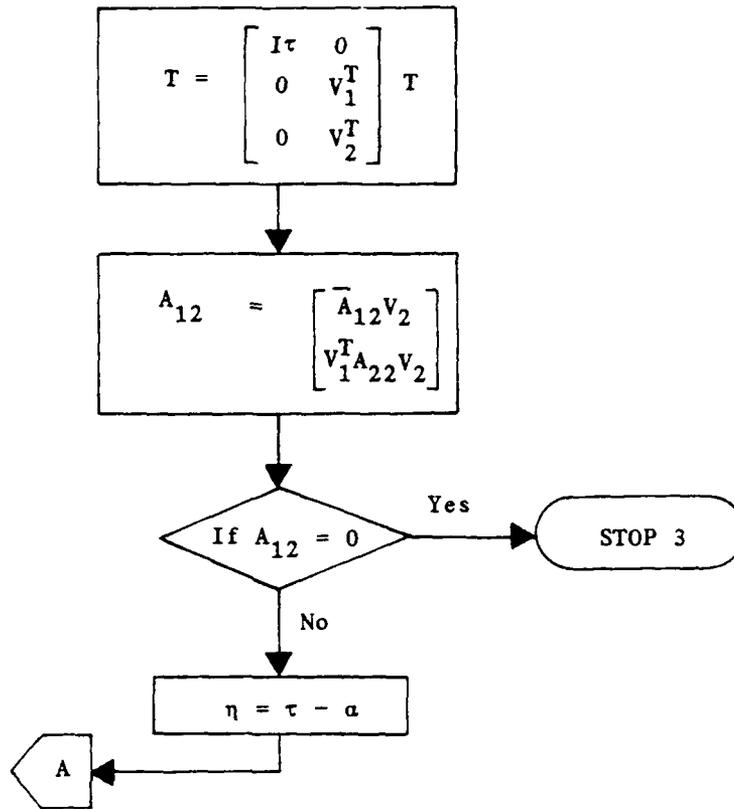
$$\rho = \rho - \alpha$$

$$\tau = \tau + \alpha$$

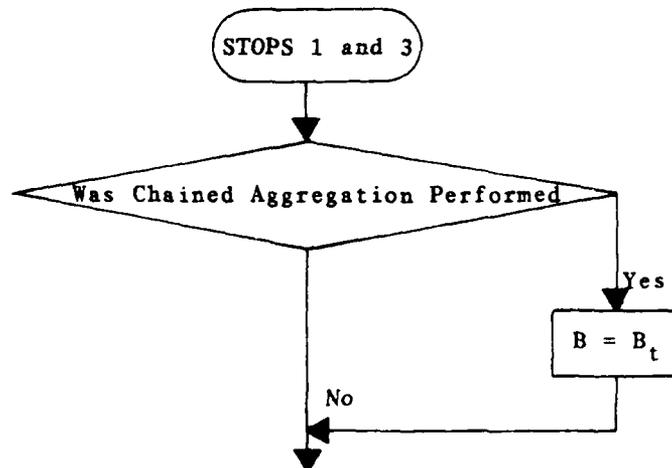
Compress the columns of  $\tilde{A}_{12}$



Flowchart continued on next page.



- STOP:
1. System will not aggregate.
  2. No C matrix.
  3. System will aggregate.



Flowchart continued on next page.

$$F = TAT^T, G = TB, D = CT^T$$

An explanation of the variable names follows:

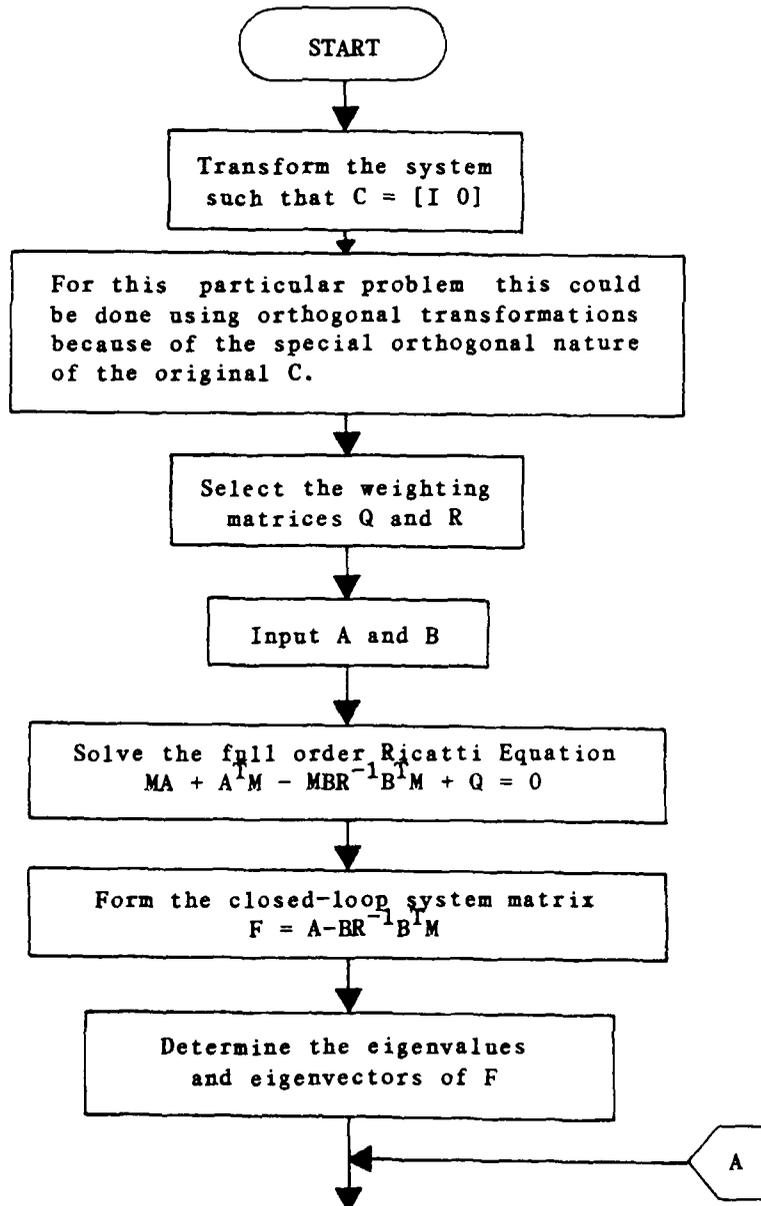
- $\alpha$  = The number of linearly independent columns in the C and  $A_{12}$  submatrices. It is redefined after every column compression which is performed on these submatrices.
- $\beta$  = The number of linearly independent rows in the  $B_1$  submatrix. It is redefined after every compression of the rows of  $B_1$ .
- $\tau$  = The sum of the  $\alpha$ 's as they are generated.
- $\rho$  = The size of the current residual subsystem.
- $\eta$  = The number of zero rows identified in the top of the B matrix.

The equivalence between the greek symbols used herein and the variable names used in the actual computer program are as follows.

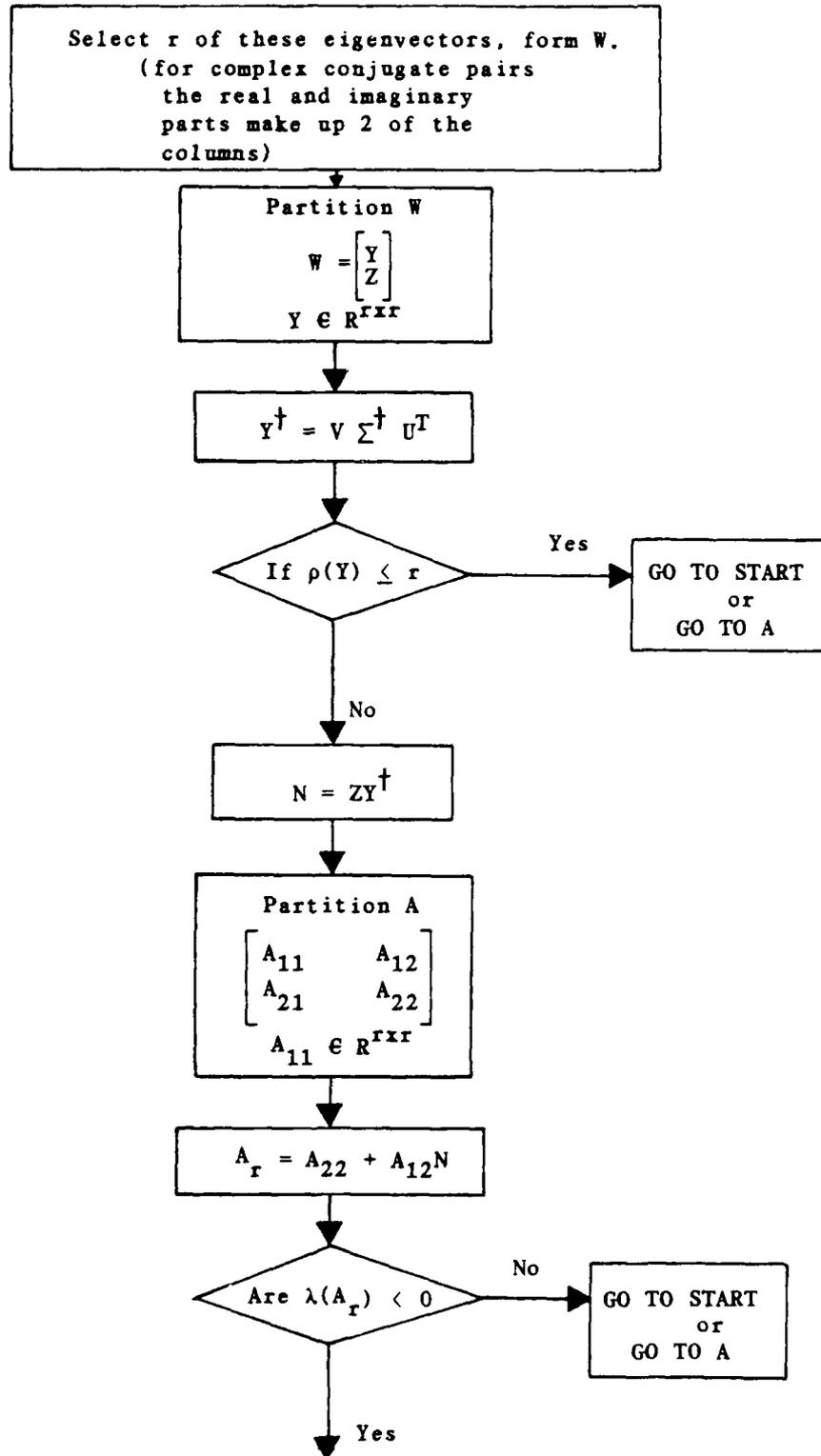
- $\tau$  = NIDE  
 $\eta$  = NOZERO  
 $\alpha$  = NZ  
 $\beta$  = NZB  
 $\rho$  = SIZA

During the design process in Chapter 4 additional software was developed. Many of the routine linear matrix manipulations were performed using LAS [32]. The software required to compute the gain matrix, K, was a

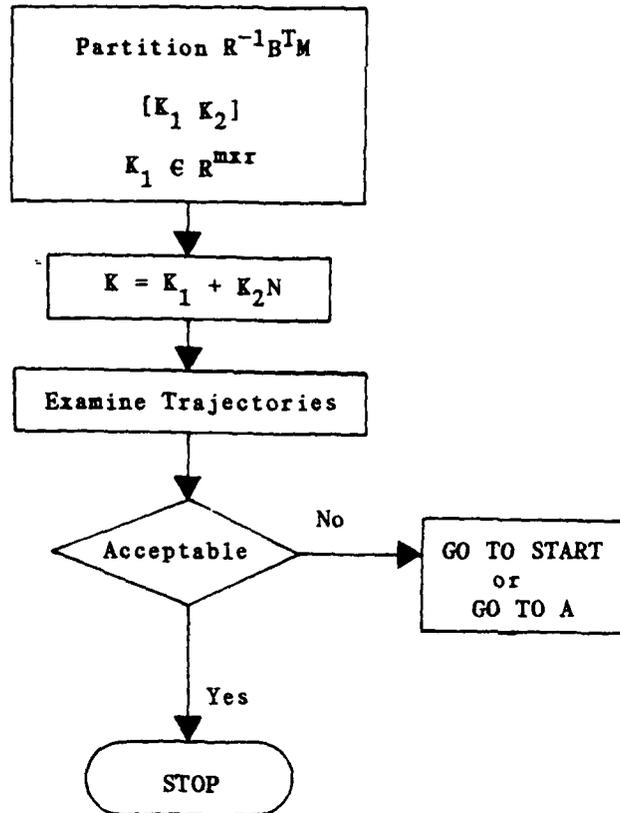
mixture of LAS code and FORTRAN software. The IMSL subroutine EIGRF was used to obtain the eigenvalues and eigenvectors of the closed-loop matrix. A flowchart description of the steps involved follows:



Flowchart continued on next page.



Flowchart continued on next page.



Software independent of LAS was written to generate the system trajectories using the initial condition, the state transition matrix, the total time, and the step size. The state transition matrix was obtained using the  $e^{At}$  operator in LAS. A graphing routine which allows the plotting of any of the resulting system trajectories, as well as the  $x$  and  $y$  deflections of node one was also developed.

## APPENDIX B

## NUMERICAL VALUES ASSOCIATED WITH THE LARGE SPACE STRUCTURE

The numerical values associated with Eq. (4.2.1) for both the nominal and perturbed systems are given in Tables B.1,B.2,B.3,B.4 and Tables B.5,B.6, respectively. Note that matrices  $B_F$  and  $C_v$  are identical for both systems. If the state space representation in Eq. (4.2.3) is desired, the required  $\bar{a}$  matrices are given in Tables B.7 and B.8. The relationship between the coordinates  $(q^T, \dot{q}^T)^T$  and the nodes of Figure 4.1 can be found in Table B.9. The transformation matrix used to generate Eq. (4.4.1) for both the nominal and perturbed systems is given in Table B.10. All of the reduced-order system matrices  $(A_{11}, B_1, C_1)$  and  $(A_{11}^P, B_1^P, C_1^P)$  are contained in Tables B.11,B.12,B.13 and Tables B.14,B.15, and B.16, respectively. To obtain the system used during the design of the K feedback matrix, the transformation matrix in Table B.17 was used. Tables B.18 and B.19 contain the final Q and R matrices used to generate the K feedback matrix which is given in Table B.20.





Table B.3: The  $B_F$  Matrix
$$B_F = \begin{bmatrix} .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ -.3535 & .3536 & .0000 & .0000 & .0000 & .0000 \\ .6124 & -.6123 & .0000 & .0000 & .0000 & .0000 \\ -.7071 & -.7071 & .0000 & .0000 & .0000 & .0000 \\ .0000 & .0000 & -.3536 & .3535 & .0000 & .0000 \\ .0000 & .0000 & -.6123 & .6124 & .0000 & .0000 \\ .0000 & .0000 & -.7071 & -.7071 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & .7071 & -.7071 \\ .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & -.7071 & -.7071 \end{bmatrix}$$

Table B.4: The  $C_y$  Matrix
$$C_y = \begin{bmatrix} .0000 & .0000 & .0000 & -.3535 & .6124 & -.7071 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .3536 & -.6123 & -.7071 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & -.3536 & -.6123 & -.7071 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .3535 & .6124 & -.7071 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .7071 & .0000 & -.7071 \\ .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & -.7071 & .0000 & -.7071 \end{bmatrix}$$



Table B.6: Stiffness Matrix for the Perturbed System

33.75	15.16	42.87	-30.00	-17.32	-48.99	-3.75	2.17	6.12	.00	.00	.00
15.16	16.25	24.75	-17.32	-10.00	-28.29	2.17	-1.25	-3.54	.00	-5.00	7.07
42.87	24.75	100.00	-48.99	-28.29	-80.00	6.12	-3.54	-10.00	.00	7.07	-10.00
-30.00	-17.32	-48.99	193.26	46.32	48.98	-120.00	.00	.00	-30.00	-51.96	.00
-17.32	-10.00	-28.29	46.32	139.78	28.29	.00	.00	.00	-51.96	-90.00	.00
-48.99	-28.29	-80.00	48.98	28.29	133.03	.00	.00	.00	.00	.00	.00
-3.75	2.17	6.12	-120.00	.00	.00	167.01	-31.16	-6.12	-30.00	51.96	.00
2.17	-1.25	-3.54	.00	.00	.00	-31.16	131.02	3.54	51.96	-90.00	.00
6.12	-3.54	-10.00	.00	.00	.00	-6.12	3.54	63.03	.00	.00	.00
.00	.00	.00	-30.00	-51.96	.00	-30.00	51.96	.00	113.03	.00	.00
.00	-5.00	7.07	-51.96	-90.00	.00	51.96	-90.00	.00	.00	185.00	-7.07
.00	7.07	-10.00	.00	.00	.00	.00	.00	.00	.00	-7.07	63.03

K =

Table B.7:  $\delta$  Matrix for the Nominal System

-.3444	.5429	-.0492	.0573	-.1369	.0000	.0557	-.0758	.1445	-.0058	.1594	.0837
.5964	.3135	-.0284	-.0992	-.0791	.0000	-.0965	-.0438	.0835	.0100	.0921	.0483
.0000	-.1990	.3788	-.0001	-.3441	.0000	.0000	.1837	.2702	.0000	.2580	.1587
-.0311	.1263	.3125	-.1760	.1621	-.2041	-.0344	.0470	.2125	-.2242	-.1517	-.4059
.0538	.0729	.1805	.3046	.0936	.3535	.0596	.0272	.1228	.3883	-.0876	-.2343
.0000	.0976	.0652	.0000	-.4969	.0000	.0000	.0978	-.3266	.0000	-.3117	-.1611
-.0508	.1098	.2727	-.2388	.1620	-.2041	-.0288	.0368	-.1414	.3846	-.1619	.2996
.0652	.0416	.1274	.3409	.0731	-.3535	.0564	.0325	-.3096	.0368	.3311	-.1449
.0638	-.0673	.1371	-.0916	-.0757	.0001	.4873	-.4696	-.0150	-.0118	.0009	-.0082
-.0311	.0909	.2466	-.1759	.1444	.4082	-.0345	.0466	-.3389	-.2241	.2058	.0269
.0756	.0742	.1726	.3771	.1037	.0000	.0532	.0157	.0323	-.3147	-.3058	.3304
-.0638	-.0673	.1372	.0915	-.0757	.0000	-.4872	-.4698	-.0150	.0119	.0009	-.0082

4 =

Table B.8:  $\mathbf{A}$  Matrix for the Perturbed System

-.2471	.3999	.0637	.0275	-.0878	.0000	-.0266	-.0299	.0991	-.0034	.0637	.0321
.4279	.2309	.0368	-.0476	-.0507	.0000	.0461	-.0173	.0572	.0058	.0368	.0185
.0000	-.1489	.4000	.0000	-.1299	.0000	.0000	.0878	.1729	.0000	.0959	.0644
-.0196	.0833	.1984	-.1718	.3095	-.2041	.0337	.0407	.1076	-.2286	-.2401	-.4026
.0398	.0481	.1145	.2977	.1786	.3535	-.0584	.0236	.0621	.3960	-.1386	-.2324
.0000	.0681	.2010	.0000	-.3514	.0000	.0000	.0355	-.4953	.0000	-.2605	-.1305
-.0361	.0700	.1548	-.2512	.2866	-.2041	.0273	.0274	-.1679	.3783	-.0863	.3204
.0435	.0225	.0680	.3436	.1224	-.3535	-.0548	.0280	-.2198	.0455	.3944	-.1587
.0440	-.0472	.0978	-.0819	.0114	.0001	-.4913	-.4875	-.0111	-.0147	.0070	-.0090
-.0196	.0545	.1363	-.1718	.2494	.4082	.0338	.0380	-.2743	-.2286	.2984	.0227
.0530	.0494	.1000	.3894	.1868	.0000	-.0511	.0098	-.0355	-.3049	-.2719	.3568
-.0440	-.0472	.0978	.0819	.0114	.0000	.4909	-.4879	-.0111	.0147	.0070	-.0090

Table B.9: Relationship Between the Coordinates and the Nodes

- $q_1 (\dot{q}_1) \equiv$  Displacement (Velocity) of node 1 in the negative x direction.  
 $q_2 (\dot{q}_2) \equiv$  Displacement (Velocity) of node 1 in the negative y direction.  
 $q_3 (\dot{q}_3) \equiv$  Displacement (Velocity) of node 1 in the negative z direction.  
 $q_4 (\dot{q}_4) \equiv$  Displacement (Velocity) of node 2 in the negative x direction.  
 $q_5 (\dot{q}_5) \equiv$  Displacement (Velocity) of node 2 in the negative y direction.  
 $q_6 (\dot{q}_6) \equiv$  Displacement (Velocity) of node 2 in the negative z direction.  
 $q_7 (\dot{q}_7) \equiv$  Displacement (Velocity) of node 3 in the negative x direction.  
 $q_8 (\dot{q}_8) \equiv$  Displacement (Velocity) of node 3 in the negative y direction.  
 $q_9 (\dot{q}_9) \equiv$  Displacement (Velocity) of node 3 in the negative z direction.  
 $q_{10} (\dot{q}_{10}) \equiv$  Displacement (Velocity) of node 4 in the negative x direction.  
 $q_{11} (\dot{q}_{11}) \equiv$  Displacement (Velocity) of node 4 in the negative y direction.  
 $q_{12} (\dot{q}_{12}) \equiv$  Displacement (Velocity) of node 4 in the negative z direction.

Table B.10: Transformation matrix which generates Eq. (4.4.1)  
 $T = [ T_1, T_2, T_3 ]$

1.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	1.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.3104	-.4680	-.2701	-.4736	.0660	.4352
.0000	.0000	-.0002	-.3374	.5846	.0003	.5133	.0934
.0000	.0000	.4170	.0379	.0222	-.6324	-.0673	-.4554
.0000	.0000	.1492	.0171	.0101	.1074	.0730	.0017
.0000	.0000	-.0001	-.0236	.0406	.0000	-.0325	.0460
.0000	.0000	.0000	-.2887	.5000	.0000	-.2887	-.5000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.5646	-.4162	-.2401	.5909	-.1369	-.1567
.0000	.0000	-.0003	-.2285	.3958	.0002	-.3900	.4890
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	-.0044	-.0058	-.0034	.0002	.0076	-.0036
.0000	.0000	-.2904	-.3933	-.2272	.0200	.5403	-.2494
.0000	.0000	-.5517	-.4487	-.2591	-.1211	-.4185	-.1283

Table B.10: (Continued)

.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	-.2192
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	-.4494
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
-.0030	.4097	-.1606	-.0030	.0000	.0000	.0000	.0000
-.0049	-.3374	-.3979	.0049	.0000	.0000	.0000	.0000
-.0118	-.4283	.1691	-.0118	.0000	.0000	.0000	.0000
-.6905	.0381	.0624	-.6916	.0000	.0000	.0000	.0000
.7046	-.0237	.0513	-.7036	.0000	.0000	.0000	.0000
.0003	.5773	-.0001	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	-.9996	-.0288	.0000	.0000
.0000	.0000	.0000	.0000	.0288	-.9996	.0000	.0000
.0851	-.2043	-.0398	.0852	.0000	.0000	.0000	.0000
-.0653	-.2285	.5824	.0652	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	-.6203	.6515
.0000	.0000	.0000	.0000	.0000	.0000	.0002	.0001
.0000	.0000	.0000	.0000	.0000	.0000	-.6875	-.3336
.0002	.0007	.0084	.0002	.0000	.0000	.3776	.4628
.0200	.0543	.5924	.0203	.0000	.0000	-.0055	-.0067
-.1210	-.3203	-.2984	-.1210	.0000	.0000	-.0001	-.0002



Table B.11: Nominal reduced-order system matrix  
 $A = [ A_1, A_2 ]$

	.00	.00	.00	.00	.00	.00	.00	.00
	.00	.00	.00	.00	.00	.00	.00	.00
	-1.83	1.06	.00	.00	.00	.00	.00	.00
	-18.34	-10.59	.00	.00	.00	.00	.00	.00
	.00	1.67	.00	.00	.00	.00	.00	.00
	.00	1.67	.00	.00	.00	.00	.00	.00
	8.95	5.17	.00	.00	.00	.00	.00	.00
	.89	-.52	.00	.00	.00	.00	.00	.00
$A_1 =$	.00	.00	-.18	.43	.29	-.29	-.21	-.37
	.00	.00	-.15	.30	-.24	.24	.61	-.30
	.00	.00	.18	.57	-.29	.31	-.28	.39
	.00	.00	-.64	-.10	.52	.46	.05	.27
	.00	.00	.62	.02	.48	.51	.04	-.33
	.00	.00	.25	.25	.41	-.41	.52	.52
	13.93	6.67	.00	.00	.00	.00	.00	.00
	6.10	6.06	.00	.00	.00	.00	.00	.00

Table B.11: (Continued)

	.00	.00	.00	.00	.00	.00	-1.00	.03
	.00	.00	.00	.00	.00	.00	-.03	-1.00
	17.19	12.86	-10.53	13.76	-13.33	-4.47	.00	.00
	-42.45	-23.86	-40.56	.87	-.17	-4.48	.00	.00
	-27.22	19.99	18.54	-10.96	-10.40	-7.22	.00	.00
	26.20	-18.52	-21.41	-10.50	-10.67	7.22	.00	.00
	20.70	-48.97	19.77	-.43	-.34	-9.17	.00	.00
	33.66	24.04	-26.28	-6.35	6.71	-9.17	.00	.00
$A_2 =$	.00	.00	.00	.00	.00	.00	.00	.00
	.00	.00	.00	.00	.00	.00	.00	.00
	.00	.00	.00	.00	.00	.00	.00	.00
	.00	.00	.00	.00	.00	.00	.00	.00
	.00	.00	.00	.00	.00	.00	.00	.00
	.00	.00	.00	.00	.00	.00	.00	.00
	23.77	-.57	19.98	-1.26	1.44	.00	.00	.00
	12.83	1.02	10.78	-.68	-2.66	.00	.00	.00





Table B.14: Perturbed reduced-order system matrix  
 $A^P = [ A_1, A_2 ]$

$$A_1 = \begin{bmatrix} .00 & .00 & .00 & .00 & .00 & .00 & .00 & .00 \\ .00 & .00 & .00 & .00 & .00 & .00 & .00 & .00 \\ -2.75 & 1.59 & .00 & .00 & .00 & .00 & .00 & .00 \\ -22.01 & -12.71 & .00 & .00 & .00 & .00 & .00 & .00 \\ .00 & 2.50 & .00 & .00 & .00 & .00 & .00 & .00 \\ .00 & 2.50 & .00 & .00 & .00 & .00 & .00 & .00 \\ 10.74 & 6.20 & .00 & .00 & .00 & .00 & .00 & .00 \\ 1.34 & -.77 & .00 & .00 & .00 & .00 & .00 & .00 \\ .00 & .00 & -.18 & .43 & .29 & -.29 & -.21 & -.37 \\ .00 & .00 & -.15 & .30 & -.24 & .24 & .61 & -.30 \\ .00 & .00 & .18 & .57 & -.29 & .31 & -.28 & .39 \\ .00 & .00 & -.64 & -.10 & .52 & .46 & .05 & .27 \\ .00 & .00 & .62 & .02 & .48 & .51 & .04 & -.33 \\ .00 & .00 & .25 & .25 & .41 & -.41 & .52 & .52 \\ 8.54 & 3.91 & .00 & .00 & .00 & .00 & .00 & .00 \\ 3.55 & 3.95 & .00 & .00 & .00 & .00 & .00 & .00 \end{bmatrix}$$

Table B.14: (Continued)

$$A_2 = \begin{bmatrix} .00 & .00 & .00 & .00 & .00 & .00 & -1.00 & .03 \\ .00 & .00 & .00 & .00 & .00 & .00 & -.03 & -1.00 \\ 21.77 & 16.49 & -13.08 & 20.69 & -19.97 & -6.71 & .00 & .00 \\ -53.20 & -30.20 & -51.69 & 1.56 & -.31 & -6.71 & .00 & .00 \\ -34.35 & 25.48 & 23.42 & -16.51 & -15.55 & -10.83 & .00 & .00 \\ 32.83 & -23.27 & -27.74 & -15.68 & -16.06 & 10.83 & .00 & .00 \\ 25.94 & -61.98 & 25.19 & -.76 & -.63 & -13.76 & .00 & .00 \\ 42.25 & 30.32 & -33.84 & -9.43 & 10.12 & -13.76 & .00 & .00 \\ .00 & .00 & .00 & .00 & .00 & .00 & .00 & .00 \\ .00 & .00 & .00 & .00 & .00 & .00 & .00 & .00 \\ .00 & .00 & .00 & .00 & .00 & .00 & .00 & .00 \\ .00 & .00 & .00 & .00 & .00 & .00 & .00 & .00 \\ .00 & .00 & .00 & .00 & .00 & .00 & .00 & .00 \\ .00 & .00 & .00 & .00 & .00 & .00 & .00 & .00 \\ 14.20 & -.42 & 11.82 & -1.03 & 1.08 & .00 & .00 & .00 \\ 7.66 & .77 & 6.38 & -.56 & -2.00 & .00 & .00 & .00 \end{bmatrix}$$





Table B.17: Transformation used during the design of the feedback matrix  $K$   
 $T = [ T_1, T_2 ]$

$$T_1 = \begin{bmatrix} .0000 & .0000 & .0000 & .9455 & .0000 & .0000 & .3255 & .0000 \\ .0000 & .0000 & .0000 & .3255 & .0000 & .0000 & -.9455 & .0000 \\ .0000 & .0000 & -.3262 & .0000 & .0000 & .0000 & .0000 & .9453 \\ .0000 & .0000 & -.9453 & .0000 & .0000 & .0000 & .0000 & -.3262 \\ .0000 & .0000 & .0000 & .0000 & 1.0000 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & .0000 & 1.0000 & .0000 & .0000 \\ .2198 & .1269 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ -.0006 & .0008 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ -.1990 & -.1149 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ .0950 & .0549 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ -.0678 & .1173 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ -.0001 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ -.9082 & -.2308 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \\ -.2715 & .9490 & .0000 & .0000 & .0000 & .0000 & .0000 & .0000 \end{bmatrix}$$

Table B.17: (Continued)

.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000
.9549	-.0001	.1541	-.0030	.0000	.0000	.0000	.0000
.0002	1.0000	-.0001	.0000	.0000	.0000	.0000	.0000
.2143	-.0002	-.9493	.0039	.0000	.0000	.0000	.0000
-.0264	.0000	-.0366	-.9929	.0001	.0000	.0000	.0000
.0000	-.0001	.0000	-.0001	-.9908	.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	-1.0000	.0000	.0000
.0000	.0000	.0000	.0000	.0000	.0000	-.8801	-.4748
.0000	.0000	.0000	.0000	.0000	.0000	-.4748	.8801
.1970	-.0003	.2623	-.1146	.0348	.0001	.0000	.0000
-.0523	-.0009	-.0696	.0304	.1310	.0001	.0000	.0000



Table B.19: Input weighting matrix R

$$R = \begin{bmatrix} 10^3 & 0 & 0 & 0 & 0 & 0 \\ 0 & 10^3 & 0 & 0 & 0 & 0 \\ 0 & 0 & 10^3 & 0 & 0 & 0 \\ 0 & 0 & 0 & 10^3 & 0 & 0 \\ 0 & 0 & 0 & 0 & 10^3 & 0 \\ 0 & 0 & 0 & 0 & 0 & 10^3 \end{bmatrix}$$

Table B.20: Output feedback gain matrix K

$$K = \begin{bmatrix} 31.6249 & .0024 & .0087 & -.0134 & -.0140 & .0086 \\ .0024 & 31.6249 & .0086 & -.0140 & -.0134 & .0087 \\ -.0039 & -.0025 & 31.6224 & .0006 & .0011 & -.0005 \\ .0125 & .0134 & -.0002 & 31.6228 & .0006 & -.0013 \\ .0134 & .0125 & -.0013 & .0006 & 31.6228 & -.0002 \\ -.0025 & -.0039 & -.0005 & .0011 & .0006 & 31.6224 \end{bmatrix}$$

## APPENDIX C

## PROGRAM LISTING

```

CHARACTER*1      ANS      , CFRMT  , AFRMT  , BFRMT
CHARACTER*20     FANAME   , FCNAME  , FBNAME  , NAME
CHARACTER*20     INAME
INTEGER          I        , J        , NCC     , NRC
INTEGER          NM       , NMIN     , IERR    , NOZERO
INTEGER          FA12    , NIDE     , NZ      , SOS
INTEGER          NRB     , NCB     , SIZA   , NZB
INTEGER          K       , ID      , JD     , NRGDMB
INTEGER          NMINB   , FA12S   , NRA12S , STEP
INTEGER          FCHND   , NCBTMP

REAL             WORK(100)
REAL             A(100,100) , B(100,100) , G(100,100)
REAL             C(100,100) , A12(100,100) , TA12(100,100)
REAL             U(100,100) , V(100,100) , T(100,100)
REAL             E(100)    , GDMB(100,100) , TDMB(100,100)
REAL             A12B(100,100) , A12S(100,100) , DMB(100,100)
REAL             NORM     , SIZCHK
REAL             SIGMA(100)

LOGICAL          INFO

```

```

*
*****
*   VERSION aggregate.f CREATED DECEMBER 22,1982 BY: HAL THARP   *
*****
*
*   TO COMPILE THIS PROGRAM:
*   f77 -u -o agg aggregate.f
*
*****
*   VARIABLE TABLE:  MAIN PROGRAM  *
*****
*
*   A       :   CONTAINS THE A MATRIX IN THE STATE SPACE DESCRIPTION.
*
*   ANS     :   A CHARACTER VARIABLE WHICH IS USED TO CONTAIN THE
*               RESPONSE OF THE USER TO A QUESTION.
*
*   A12     :   CONTAINS THE CURRENT A12 SUBMATRIX.
*
*   A12B    :   CONTAINS THE SUBMATRIX RESULTING FROM TRANSFORMING
*               A12 WITH PART OF THE U MATRIX GENERATED DURING THE
*               ROW COMPRESSION OF A B SUBMATRIX. THIS MATRIX IS
*               CONTAINED IN THE RANGE OF THE INPUT.
*
*   A12S    :   CONTAINS THE SUBMATRIX RESULTING FROM TRANSFORMING
*               A12 WITH PART OF THE U MATRIX GENERATED DURING THE

```

\*                   ROW COMPRESSION OF A B SUBMATRIX. THIS MATRIX IS  
 \*                   NOT CONTAINED IN THE RANGE OF THE INPUT.  
 \*  
 \* B               : CONTAINS THE B MATRIX IN THE STATE SPACE DESCRIPTION.  
 \*  
 \* C               : CONTAINS THE C MATRIX IN THE STATE SPACE DESCRIPTION.  
 \*  
 \* DMB            : A DUPLICATE OF GDMB WHICH IS PASSED TO THE SSVDC  
 \*                   SUBROUTINE. THIS MUST BE DONE BECAUSE THE MATRIX  
 \*                   RETURNED FROM SSVDC IS ALTERED FROM THE ORIGINAL  
 \*                   MATRIX PASSED.  
 \*  
 \* E               : VECTOR THAT ORDINARILY CONTAINS ZEROES. IT IS USED  
 \*                   IN THE SSVDC ROUTINE. FOR MORE INFORMATION CONSULT  
 \*                   LINPACK USERS' GUIDE, DONGARRA, et.al. CHPT 11.  
 \*  
 \* FA12           : A FLAG WHICH IS ZERO IF THE A12 SUBMATRIX IS ZERO  
 \*                   AND ONE OTHERWISE.  
 \*  
 \* FA12S          : A FLAG WHICH IS ZERO IF THE A12S SUBMATRIX IS ZERO  
 \*                   AND ONE OTHERWISE.  
 \*  
 \* FCHND          : A FLAG WHICH IS SET TO 1 WHEN CHAINED AGGREGATION IS  
 \*                   PERFORMED AND 0 WHEN MODIFIED CHAINED AGGREGATION IS  
 \*                   PERFORMED.  
 \*  
 \* F\_NAME         : CONTAINS THE NAME OF THE FILE WHERE THE (A,B,C) MATRICES  
 \*                   ARE STORED.  
 \*  
 \* \_FRMT          : CONTAINS THE FORMAT METHOD USED IN THE STORAGE OF THE  
 \*                   PARTICULAR (A,B,C) MATRIX. a,A = SPARSE OR b,B =  
 \*                   NORMAL.  
 \*  
 \* G               : THE ARRAY USED TO STORE THE SUBMATRIX GENERATED DURING  
 \*                   THE TRANSFORMATION OF THE B MATRIX. THIS SUBMATRIX IS  
 \*                   THEN PLACED IN THE CORRECT LOCATION WITHIN B.  
 \*  
 \* GDMB           : A TEMPORARY ARRAY WHICH CONTAINS THE SUBMATRIX OF THE  
 \*                   B MATRIX WHOSE ROWS ARE TO BE COMPRESSED.  
 \*  
 \* IERR           : VARIABLE CONTAINING ZERO WHEN THE SINGULAR VALUES HAVE  
 \*                   BEEN COMPUTED CORRECTLY. SEE LINPACK USERS' GUIDE,  
 \*                   CHPT. 11 WHEN IERR IS NOT EQUAL TO ZERO.  
 \*  
 \* INAME          : CHARACTER VARIABLE WHICH IS THE NAME OF THE FILE  
 \*                   CONTAINING THE STAGE INFORMATION. IT IS NOT USED IF  
 \*                   INFO IS FALSE.  
 \*  
 \* INFO           : A LOGICAL VARIABLE WHICH IS TRUE WHEN THE USER REQUESTS  
 \*                   THE STAGE INFORMATION TO BE OUTPUT INTO A FILE.  
 \*  
 \* I,J,K          : INTEGER VARIABLES USED WITHIN DO LOOPS AS THE COUNTERS.  
 \* ID,JD

\*  
\* NAME : A CHARACTER VARIABLE USED TO IDENTIFY THE PARTICULAR  
\* MATRIX BEING INPUT INTO THE PROGRAM.  
\*  
\* NCBTMP : AN INTEGER VARIABLE USED TO STORE THE NUMBER OF  
\* COLUMNS IN THE ORIGINAL B MATRIX WHEN CHAINED AGGREGATION  
\* IS PERFORMED.  
\*  
\* NC\_ : CONSTANT CONTAINING THE COLUMN DIMENSION OF THE PARTICULAR  
\* MATRIX (B,C,ETC.).  
\*  
\* NIDE : KEEPS TRACK OF THE NUMBER OF NON-ZERO SINGULAR VALUES  
\* GENERATED BY COMPRESSING THE C MATRIX AND THE A12S  
\* SUBMATRICES. THIS IS THE NUMBER OF IDENTITY ELEMENTS  
\* NEEDED IN THE UPPER LEFT HAND CORNER WHEN UPDATING THE  
\* TRANSFORMATION MATRIX.  
\*  
\* NM : CONSTANT CONTAINING THE MAXIMUM POSSIBLE DIMENSION OF THE  
\* MATRICES PASSED TO THE SINGULAR VALUE DECOMPOSITION  
\* ROUTINE (SSVDC). CURRENTLY SET EQUAL TO 100.  
\*  
\* NMIN : AN INTEGER VARIABLE CONTAINING THE MINIMUM OF THE NUMBER  
\* OF COLUMNS OR THE NUMBER OF ROWS IN THE C MATRIX OR AN  
\* A12S SUBMATRIX.  
\*  
\* NMINB : AN INTEGER VARIABLE CONTAINING THE MINIMUM OF THE NUMBER  
\* OF COLUMNS OR THE NUMBER OF ROWS OF THE B SUBMATRIX WHICH  
\* IS PASSED TO SSVDC. THIS IS THE MAXIMUM NUMBER OF NON-  
\* ZERO SINGULAR VALUES POSSIBLE FOR THE PARTICULAR SUBMATRIX  
\*  
\* NORM : CONSTANT CONTAINING THE NORM OF THE ORIGINAL A MATRIX.  
\*  
\* NOZERO : KEEPS TRACK OF THE NUMBER OF ZERO ROWS IN THE INPUT  
\* MATRIX.  
\*  
\* NR\_ : CONSTANT CONTAINING THE ROW DIMENSION OF THE PARTICULAR  
\* MATRIX (B,C,ETC.).  
\*  
\* NZ : AN INTEGER CONTAINING THE NUMBER OF NON-ZERO SINGULAR  
\* VALUES RESULTING FROM A DECOMPOSITION OF THE C MATRIX  
\* OR AN A12 SUBMATRIX.  
\*  
\* NZB : NUMBER OF NON-ZERO SINGULAR VALUES OBTAINED AFTER PASSING  
\* PORTIONS OF THE B MATRIX TO THE SSVDC ROUTINE.  
\*  
\* SIGMA : VECTOR CONTAINING THE SINGULAR VALUES RESULTING FROM THE  
\* SSVDC ROUTINE.  
\*  
\* SIZA : CONTAINS THE DIMENSION OF THE A MATRIX. INITIALLY IT IS  
\* SET EQUAL TO SOS, BUT THEN IS UPDATED TO KEEP TRACK OF THE  
\* DIMENSION OF THE A22 SUBMATRIX.  
\*  
\* SIZCHK : CONSTANT CONTAINING THE PRODUCT OF NORM AND THE MACHINE

```

*           EPSILON.  ELEMENTS SMALLER THAN THIS IN THE SSVDC ROUTINE
*           ARE TREATED AS BEING ZERO.
*
*   SOS      :   CONSTANT CONTAINING THE DIMENSION OF THE STATE (SIZE OF
*               STATE).
*
*   STEP     :   KEEPS TRACK OF THE NUMBER OF MODIFIED OR CHAINED STEPS
*               PERFORMED.
*
*   T        :   ARRAY CONTAINING THE TRANSFORMATION MATRIX WHICH IS
*               CONTINUALLY UPDATED DURING THE ALGORITHM.
*
*   TA12     :   TEMPORARY STORAGE ARRAY WHICH IS USED DURING THE
*               COMPUTATION OF A12, SINCE A12 IS COMPUTED IN TWO STAGES.
*
*   TDMB     :   TEMPORARY STORAGE ARRAY WHICH IS USED DURING THE UPDATING
*               OF THE TRANSFORMATION MATRIX, BECAUSE THE UPDATE MUST BE
*               DONE IN TWO STAGES.
*
*   U        :   ORTHOGONAL MATRIX WHOSE COLUMNS CONTAIN THE LEFT SINGULAR
*               VECTORS OF THE MATRIX PASSED TO THE SSVDC ROUTINE.
*
*   V        :   ORTHOGONAL MATRIX WHOSE COLUMNS ARE THE RIGHT SINGULAR
*               VECTORS OF THE MATRIX PASSED TO THE SSVDC ROUTINE.
*
*   WORK     :   VECTOR USED IN THE SSVDC ROUTINE.

```

```

*****

```

```

*   INITIALIZE THE COUNTING VARIABLES
*   NOZERO = 0
*   NIDE   = 0
*   NM     = 100
*   NZB    = 0
*   STEP   = 1
*
*   FREQUENTLY USED FORMAT STATEMENTS
10  FORMAT (A)
50  FORMAT (100(F12.5))
*
*   WRITE (6,100)
100 FORMAT ('*****
           /*** MODIFIED OR CHAINED AGGREGATION **'
           /'*****')

```

```

*****
*   INPUT THE SYSTEM MATRICES *
*****
*
*   NAME = 'C' MATRIX.'
*   CALL INPUT(C,NRC,NCC,NAME,CFRMT,FCNAME)
*
*   DETERMINE THE SMALLEST OF THE TWO DIMENSIONS

```

```

      NMIN = MIN(NRC,NCC)
*
*   INITIALIZE THE SIZE OF THE SYSTEM AND THE SIZE OF A
      SOS = NCC
      SIZA = SOS
*
      NAME = '"A" MATRIX.'
      CALL INPUT(A,SOS,SOS,NAME,AFRMT,FANAME)
*
*   SELECT THE NORM TO BE USED FOR THE A MATRIX.
625  WRITE (6,650)
650  FORMAT ('ENTER THE NORM OF THE SYSTEM MATRIX, A. '
           /' 1. LARGEST ELEMENT OF A '
           /' 2. TWO-NORM (LARGEST SINGULAR VALUE)'
           /' 3. FROBENIUS NORM'
           /' ENTER 1, 2, OR 3 >', $)
*
      READ (5,*) I
      IF (I .EQ. 3) GO TO 800
      IF (I .EQ. 2) GO TO 750
      IF (I .NE. 1) GO TO 625
*
*   FIND THE LARGEST ELEMENT OF A AND USE THIS AS THE NORM.
*
      NORM = 0.0
      DO 700 J=1, SOS
        DO 700 I=1, SOS
          IF (ABS(A(I,J)) .GE. NORM) NORM = ABS(A(I,J))
700  CONTINUE
      GO TO 850
*
*   COMPUTE THE TWO NORM
*
      CALL DUP(A,DMB,SOS,SOS)
750  CALL SSVDC(DMB,NM,SOS,SOS,SIGMA,E,U,NM,V,NM,WORK,00,IERR)
      IF (IERR .EQ. 0) GO TO 760
      WRITE (6,755)
755  FORMAT ('SINGULAR VALUES OF A NOT COMPUTED CORRECTLY'
           /'SEE LINPACK MANUAL FOR CASE WHEN (IERR .NE. 0)')
      STOP
*
760  NORM = SIGMA(1)
      GO TO 850
*
*   COMPUTE THE FROBENIUS NORM
*
800  NORM = 0
      DO 825 I=1, SOS
        DO 825 J=1, SOS
          NORM = NORM + A(I,J)*A(I,J)
825  CONTINUE
      NORM = SQRT(NORM)
*

```

```

850  WRITE (6,860)  NORM
860  FORMAT ('THE NORM OF A EQUALS: ',F12.3)
*
*   CALCULATE SIZCHK: ELEMENTS SMALLER THAN SIZCHK
*   ARE TREATED AS ZEROES.  (MACHINE EPSILON = 2.0**(-24))
*
      SIZCHK = ABS(NORM*((2.0)**(-24)))
      NAME = "'B" MATRIX.'
      CALL  INPUT(B,NRB,NCB,NAME,BFRMT,FBNAME)
*
900  CONTINUE
*****
*   CHOOSE BETWEEN PERFORMING MODIFIED OR CHAINED  *
*****
*
      FCHND = 0
950  WRITE (6,1000)
1000 FORMAT ('DO YOU WANT TO PERFORM MODIFIED'
            /'OR CHAINED AGGREGATION?'
            /'      1) MODIFIED'
            /'      2) CHAINED'
            /'ENTER 1 OR 2 >',$)
*
      READ (5,10) ANS
      IF (ANS .EQ. '1') GO TO 2200
      IF (ANS .EQ. '2') GO TO 2000
*
      WRITE (6,1100)
1100 FORMAT ('INCORRECT ENTRY.',//)
      GO TO 950
*
2000 CONTINUE
*   SET THE CHAINED FLAG
      FCHND = 1
*
*   STORE THE NUMBER OF COLUMNS IN THE ORIGINAL B
*   IN A TEMPORARY NAME
      NCBTMP = NCB
      NCB = 1
*
*   CREATE THE NEEDED NULL B MATRIX FOR CHAINED
      DO 2100 I=1,NRB
         B(I,1) = 0.0
2100 CONTINUE
2200 CONTINUE
*****
*   COMPRESS THE COLUMNS OF THE C MATRIX  *
*****
*
*   EVENTUALLY WE WILL ONLY NEED TO HAVE THE V MATRIX RETURNED.
*   FOR NOW WE WANT TO HAVE U AND V AVAILABLE FOR CHECKING PURPOSES.
*
      CALL  SSVDC(C,NM,NRC,NCC,SIGMA,E,U,NM,V,NM,WORK,11,IERR)

```

```

*
* COMPUTE THE NUMBER OF NON-ZERO SINGULAR VALUES.
* DISPLAY THE U AND V MATRIX IF YOU WISH.
*
  NAME = 'THE C MATRIX'
*
  CALL USV(U, SIGMA, V, SIZCHK, NMIN, NZ, NRC, NCC, NAME)
*
* CHECK THE SIZE OF NZ FOR THE TRIVIAL CASE.
  IF (NZ .EQ. 0) GO TO 60600
*
*****
* INITIALIZE THE TRANSFORMATION MATRIX *
*****
  DO 4000 I=1, SOS
    DO 4000 J=1, SOS
      T(I,J)=V(J,I)
4000 CONTINUE
  WRITE (6,4200)
4200 FORMAT ('WOULD YOU LIKE TO SEE THE T MATRIX?', $)
  READ (5,10) ANS
  IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 4500
  CALL OUTPUT(T, SOS, SOS, SIZCHK)
4500 CONTINUE
*
* CHECK IF THE "C" MATRIX HAS RANK EQUAL TO THE ORDER OF THE SYSTEM.
*
  IF (NZ .EQ. SOS) GO TO 60700
*
*****
* CALCULATE THE A12 SUBMATRIX *
*****
*
* SET THE A12 FLAG EQUAL TO ZERO
  FA12 = 0
  DO 5000 I=1, NZ
    DO 5000 J=1, SIZA
      TA12(I,J) = 0.0
    DO 5000 K=1, SIZA
      TA12(I,J) = TA12(I,J) + V(K,I) * A(K,J)
5000 CONTINUE
  DO 5500 I=1, NZ
    DO 5500 J=1, SIZA - NZ
      A12(I,J) = 0.0
      JD = NZ + J
      DO 5500 K=1, SIZA
        A12(I,J) = A12(I,J) + TA12(I,K) * V(K,JD)
      IF (ABS(A12(I,J)) .GE. SIZCHE) FA12 = 1
5500 CONTINUE
*
  WRITE (6,5600)
5600 FORMAT ('WOULD YOU LIKE TO SEE THE A12 SUBMATRIX? >', $)
  READ (5,10) ANS

```

```

      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 5850
      CALL OUTPUT(A12,NZ,SIZA-NZ,SIZCHK)
*
5850 CONTINUE
* WAS A12 = 0 (FA12 = 0)
      IF (FA12 .EQ. 0) GO TO 50000
*
5900 CONTINUE
*
*****
* COMPUTE THE NEW B MATRIX *
*****
*
      DO 6000 I=1,SIZA
        DO 6000 J=1,NCB
          G(I,J) = 0.0
          DO 6000 K=1,SIZA
            G(I,J) = G(I,J) + V(K,I) * B(NIDE+K,J)
6000 CONTINUE
*
      IF (FCHND .EQ. 1) GO TO 6450
*
      WRITE (6,6050)
6050 FORMAT ('WOULD YOU LIKE TO SEE THE NEW PORTION OF B? >', '$)
      READ (5,10) ANS
      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 6150
      CALL OUTPUT(G,SIZA,NCB,SIZCHK)
*
6150 CONTINUE
* STORE THIS UPDATED SECTION OF THE B MATRIX
* IN THE APPROPRIATE LOCATION OF THE ENTIRE B MATRIX.
*
      DO 6200 I=1,SIZA
        ID = NIDE + I
        DO 6200 J=1,NCB
          B(ID,J) = G(I,J)
6200 CONTINUE
*
      WRITE (6,6300)
6300 FORMAT ('WOULD YOU LIKE TO SEE THE ENTIRE B MATRIX? >', '$)
      READ (5,10) ANS
      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 6450
      CALL OUTPUT(B,SOS,NCB,SIZCHK)
*
6450 CONTINUE
* CREATE A DUMMY MATRIX COMPOSED OF
* THE FIRST NZB+NZ ROWS OF B, STARTING
* WITH THE FIRST NON-ZERO ROW (NOZERO+1).
*
      DO 6500 I=1,NZB+NZ
        ID = NOZERO + I
        DO 6500 J=1,NCB
          GDMB(I,J) = B(ID,J)

```

```

6500 CONTINUE
*
IF      (FCHND .EQ. 1) GO TO 6750
*
WRITE   (6,6600)
6600 FORMAT ('WOULD YOU LIKE TO SEE THE SUBMATRIX'
            /'OF B WHICH IS TO BE DECOMPOSED? >', $)
READ    (5,10) ANS
IF      ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 6750
CALL    OUTPUT(GDMB,NZB+NZ,NCB,SIZCHK)
*
6750 CONTINUE
NRGDMB = NZB + NZ
NMINB  = MIN(NRGDMB,NCB)
*
CALL    DUP(GDMB,DMB,NRGDMB,NCB)
*
* PASS THE DMB TO SSVDC TO COMPRESS ITS ROWS.
* ONLY RETURN THE U MATRIX. WE DO NOT WANT TO OVER-
* WRITE THE CURRENT V MATRIX.
*
CALL    SSVDC(DMB,NM,NRGDMB,NCB,SIGMA,E,U,NM,V,NM,WORK,10,IERR)
*
IF      (FCHND .EQ. 0) GO TO 6800
NZB    = 0
* SKIP B AND T UPDATE
GO TO 10465
*
6800 CONTINUE
* COMPUTE THE NUMBER OF NON-ZERO SINGULAR VALUES.
* DISPLAY THE U MATRIX IF DESIRED.
*
NAME   = 'A B SUBMATRIX.'
*
CALL    USV(U,SIGMA,V,SIZCHK,NMINB,NZB,NRGDMB,NCB,NAME)
*
* CHECK TO SEE IF GDMB WAS EQUAL TO ZERO.
* IF SO, THEN SKIP THE B AND T UPDATE.
*
IF      (NZB .EQ. 0) GO TO 10465
*
*****
* UPDATE THE B MATRIX *
*****
*
* ZERO OUT THE APPROPRIATE ELEMENTS IN THE B MATRIX.
* THIS SUBMATRIX IS THE SIZE OF GDMB.
*
DO 10000 I=1,NRGDMB
  ID = NOZERO + I
  DO 10000 J=1,NCB
    B(ID,J) = 0.0
10000 CONTINUE

```

```

*
*   PERFORM THE TRANSFORMATION ON THE B MATRIX
*   WITH THE U MATRIX, COMPRESSING THE ROWS OF
*   THE NEW B DOWN.
*
      DO 10100  I=1,NZB
          ID = NOZERO + NRGDMB - NZB + I
          DO 10100  J=1,NCB
              DO 10100  K=1,NRGDMB
                  B(ID,J) = B(ID,J) + U(K,I) * GDMB(K,J)
10100 CONTINUE
*
      WRITE (6,10150)
10150 FORMAT ('WOULD YOU LIKE TO SEE THE TRANSFORMED B MATRIX'
             /'AFTER THE APPROPRIATE ROWS HAVE BEEN COMPRESSED? >', '$)
      READ (5,10) ANS
      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 10165
      CALL OUTPUT(B,SOS,NCB,SIZCHK)
*
10165 CONTINUE
*****
*   UPDATE THE TRANSFORMATION MATRIX *
*****
*
*   THIS MUST BE DONE IN TWO STAGES, BECAUSE WE
*   COMPRESS THE ROWS DOWN IN THE B SUBMATRIX.
*
*   CALCULATE THE UPPER PART OF THE NEW T MATRIX.
*
      DO 10210  I=1,NRGDMB-NZB
          ID = NZB + I
          DO 10210  J=1,SOS
              TDMB(I,J) = 0.0
              DO 10210  K=1,NRGDMB
                  TDMB(I,J) = TDMB(I,J) + U(K,ID) * T(NOZERO+K,J)
10210 CONTINUE
*
*   CALCULATE THE LOWER PART OF THE NEW T MATRIX.
*
      DO 10220  I=1,NZB
          ID = NRGDMB - NZB + I
          DO 10220  J=1,SOS
              TDMB(ID,J) = 0.0
              DO 10220  K=1,NRGDMB
                  TDMB(ID,J) = TDMB(ID,J) + U(K,I) * T(K+NOZERO,J)
10220 CONTINUE
*
      WRITE (6,10250)
10250 FORMAT ('WOULD YOU LIKE TO SEE THE UPDATED ROWS IN T'
             /'DUE TO THE U GENERATED WHILE COMPRESSING THE'
             /'ROWS OF B? >', '$)
      READ (5,10) ANS
      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 10265

```

```

      CALL OUTPUT(TDMB, NRGDMB, SOS, SIZCHK)
*
10265 CONTINUE
*
* STORE TDMB IN THE APPROPRIATE LOCATION WITHIN T
*
      DO 10300 I=1, NRGDMB
        ID = NOZERO + I
        DO 10300 J=1, SOS
          T(ID, J) = TDMB(I, J)
10300 CONTINUE
*
      WRITE (6, 10350)
10350 FORMAT ('WOULD YOU LIKE TO SEE THE NEW T? >', $)
      READ (5, 10) ANS
      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 10365
      CALL OUTPUT(T, SOS, SOS, SIZCHK)
*
10365 CONTINUE
*
*****
* UPDATE THE A12 SUBMATRIX WITH THIS U *
* STATE SPACE TRANSFORMATION. *
*****
*
* A12 WILL BE DIVIDED INTO TWO PARTS, A12B AND A12S.
* CALCULATE A12B.
      DO 10400 I=1, NZB
        DO 10400 J=1, SIZA-NZ
          A12B(I, J) = 0.0
          DO 10400 K=1, NRGDMB
            A12B(I, J) = A12B(I, J) + U(K, I) * A12(K, J)
10400 CONTINUE
*
      WRITE (6, 10450)
10450 FORMAT ('WOULD YOU LIKE TO SEE THE A12B SUBMATRIX? >', $)
      READ (5, 10) ANS
      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 10465
      CALL OUTPUT(A12B, NZB, SIZA-NZ, SIZCHK)
*
10465 CONTINUE
*
* CALCULATE A12S.
* SET THE A12S=0 FLAG EQUAL TO ZERO.
      FA12S = 0
      DO 10500 I=1, NRGDMB - NZB
        ID = NZB + I
        DO 10500 J=1, SIZA-NZ
          A12S(I, J) = 0.0
          DO 10500 K=1, NRGDMB
            A12S(I, J) = A12S(I, J) + U(K, ID) * A12(K, J)
            IF (ABS(A12S(I, J)) .GT. SIZCHK) FA12S = 1
10500 CONTINUE

```

```

*
  WRITE (6,10550)
10550 FORMAT ('WOULD YOU LIKE TO SEE THE A12S SUBMATRIX? >'.,$)
  READ (5,10) ANS
  IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 10565
  CALL OUTPUT(A12S,NRGDMB-NZB,SIZA-NZ,SIZCHK)
*
10565 CONTINUE
*
  IF (FA12S .EQ. 0) GO TO 50200
*
*****
* CALCULATE THE A22 SUBMATRIX. *
*****
*
* TA12 IS USED AS THE INTERMEDIATE STORAGE LOCATION.
*
  DO 10600 I=1,SIZA-NZ
    ID = NZ + I
    DO 10600 J=1,SIZA
      TA12(I,J) = 0.0
      DO 10600 K=1,SIZA
        TA12(I,J) = TA12(I,J) + V(K,ID) * A(K,J)
10600 CONTINUE
*
* STORE THE A22 SUBMATRIX IN THE UPPER LEFT HAND
* CORNER OF THE A MATRIX.
*
  DO 10700 I=1,SIZA-NZ
    DO 10700 J=1,SIZA-NZ
      JD = NZ + J
      A(I,J) = 0.0
      DO 10700 K=1,SIZA
        A(I,J) = A(I,J) + TA12(I,K) * V(K,JD)
10700 CONTINUE
*
  WRITE (6,10750)
10750 FORMAT ('WOULD YOU LIKE TO SEE THE A22 SUBMATRIX? >'.,$)
  READ (5,10) ANS
  IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 10760
  CALL OUTPUT(A,SIZA-NZ,SIZA-NZ,SIZCHK)
10760 CONTINUE
*
* UPDATE THE SIZA VARIABLE TO BE THE SIZE OF THE
* NEW A22 SUBMATRIX.
*
  SIZA = SIZA - NZ
*
* UPDATE THE VARIABLE REPRESENTING THE NUMBER OF
* IDENTITY ELEMENTS. (THIS VARIABLE IS USED DURING
* THE T UPDATE WITH V.)
*
  NIDE = NIDE + NZ

```

AD-A142 394

A NUMERICAL ALGORITHM FOR CHAINED AGGREGATION AND  
MODIFIED CHAINED AGGREGATION(U) ILLINOIS UNIV AT URBANA  
DECISION AND CONTROL LAB H S THARP SEP 83 DC-62

3/2

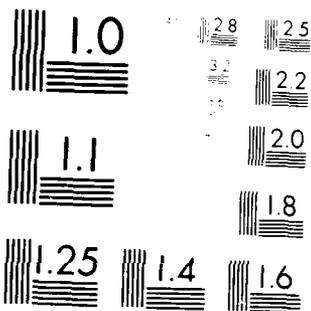
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MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

```

*
*****
* IDENTIFICATION OF STEP TO USER *
*****
*
* INDICATE TO USER WHAT STEP IN THE DECOMPOSITION
* HE IS IN.
*
      NAME = ' '
      IF (FCHND .EQ. 0) NAME = 'MODIFIED'
      WRITE (6,10770) STEP , NAME
10770 FORMAT (/ '*****'
              / 'THIS COMPLETES ',I3,' STAGE(S) OF ',A8,
              / 'CHAINED AGGREGATION. ')
      WRITE (6,10772) NIDE , NIDE
10772 FORMAT (/ 'THE AGGREGATE SYSTEM IS NOW ',I3,' x ',I3,
              / '*****')
      IF (STEP .NE. 1) GO TO 10780
      WRITE (6,10774)
10774 FORMAT (/ 'WOULD YOU LIKE THIS INFORMATION TO BE'
              / 'WRITTEN OUT TO A FILE? >', $)
      READ (5,10) ANS
      IF ((ANS .EQ. 'Y').OR.(ANS .EQ. 'y')) GO TO 10775
      INFO = .FALSE.
      GO TO 10780
10775 INFO = .TRUE.
      WRITE (6,10776)
10776 FORMAT (/ 'ENTER THE FILE NAME >', $)
      READ (5,10) INAME
      OPEN (UNIT=3,FILE=INAME)
      REWIND 3
      WRITE (3,10778)
10778 FORMAT (/ 'THIS FILE CONTAINS THE INFORMATION ON'
              / 'HOW THE AGGREGATE SYSTEM GROWS WITH'
              / 'EACH STEP OF MODIFIED CHAINED AGGREGATION.',/)
      CLOSE (UNIT=3)
*
10780 IF (.NOT. INFO) GO TO 10790
      OPEN (UNIT=3,FILE=INAME)
      WRITE (3,10785) STEP , NIDE , NIDE
10785 FORMAT (/ 'AFTER ',I3,' STAGE(S) OF MODIFIED CHAINED'
              / 'AGGREGATION, THE AGGREGATE SYSTEM IS'
              / ',I3,' x ',I3)
*
10790 CONTINUE
      STEP = STEP + 1
*
*****
* COMPRESS THE COLUMNS OF A12S *
*****
*
* WILL RETURN BOTH U AND V MATRICES FOR NOW.

```

```

*
  NRA12S = NRGDMB - NZB
* RECALL NCA12S = SIZA.
*
  CALL SSVDC(A12S,NM,NRA12S,SIZA,SIGMA,E,U,NM,V,NM,WORK,11,IERR)
*
  NAME = 'THE A12S SUBMATRIX.'
  NMIN = MIN(NRA12S,SIZA)
*
  CALL USV(U,SIGMA,V,SIZCHK,NMIN,NZ,NRA12S,SIZA,NAME)
*
* IF NZ EQUALS SIZA THEN THE SYSTEM WILL NOT AGGREGATE.
* THIS IS BECAUSE A12S HAS FULL COLUMN RANK.
*
  IF (NZ .EQ. SIZA) GO TO 60800
*
*****
* UPDATE T *
*****
*
* DO THE UPDATE IN TWO STEPS.
* COMPUTE AFFECTED ROWS OF T.
*
  DO 10800 I=1,SIZA
    DO 10800 J=1,SOS
      TDMB(I,J) = 0.0
    DO 10800 K=1,SIZA
      TDMB(I,J) = TDMB(I,J) + V(K,I) * T(NIDE+K,J)
10800 CONTINUE
*
* STORE THESE AFFECTED ROWS IN THE APPROPRIATE LOCATION
* WITHIN T.
*
  DO 10900 I=1,SIZA
    ID = NIDE + I
    DO 10900 J=1,SOS
      T(ID,J) = TDMB(I,J)
10900 CONTINUE
*
  WRITE (6,10950)
10950 FORMAT ('WOULD YOU LIKE TO SEE THIS NEW T'
             /'AFTER BEING UPDATED WITH V? >','$)
  READ (5,10) ANS
  IF ((ANS .NE. 'V').AND.(ANS .NE. 'y')) GO TO 10970
  CALL OUTPUT(T,SOS,SOS,SIZCHK)
10970 CONTINUE
*
*****
* COMPUTE THE NEW A12 SUBMATRIX *
*****
*
* SET THE A12=0 FLAG TO ZERO.
  FA12 = 0

```

```

*
* CALCULATE THE UPPER HALF OF THE A12 SUBMATRIX.
*
DO 11000 I=1,NZB
DO 11000 J=1,SIZA-NZ
JD = NZ + J
A12(I,J) = 0.0
DO 11000 K=1,SIZA
A12(I,J) = A12(I,J) + A12B(I,K) * V(K,JD)
IF (ABS(A12(I,J)) .GT. SIZCHK) FA12 = 1
11000 CONTINUE
*
* CALCULATE THE LOWER HALF OF THE A12 SUBMATRIX IN
* TWO SECTIONS.
*
DO 11100 I=1,NZ
DO 11100 J=1,SIZA
TA12(I,J) = 0.0
DO 11100 K=1,SIZA
TA12(I,J) = TA12(I,J) + V(K,I) * A(K,J)
11100 CONTINUE
*
DO 11200 I=1,NZ
ID = NZB + I
DO 11200 J=1,SIZA - NZ
JD = NZ + J
A12(ID,J) = 0.0
DO 11200 K=1,SIZA
A12(ID,J) = A12(ID,J) + TA12(I,K) * V(K,JD)
IF (ABS(A12(ID,J)) .GT. SIZCHK) FA12 = 1
11200 CONTINUE
*
WRITE (6,11250)
11250 FORMAT ('WOULD YOU LIKE TO SEE THE NEW A12 SUBMATRIX? >',$)
READ (5,10) ANS
IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 11270
CALL OUTPUT(A12,NZB+NZ,SIZA-NZ,SIZCHK)
11270 CONTINUE
*
* CHECK TO SEE IF A12=0. IF SO, SYSTEM AGGREGATES.
IF (FA12 .EQ. 0) GO TO 50000
*
*
* UPDATE THE VARIABLE REPRESENTING THE NUMBER OF ZERO
* ROWS IN THE B MATRIX.
*
NOZERO = NIDE - NZB
*
*****
* CONTINUE THE PROCESS OF MODIFIED CHAINED AGGREGATION. *
*****
*
40900 GO TO 5900

```

```

*
*****
* PROGRAM EXITS *
*****
*
50000 WRITE (6,50100)
50100 FORMAT ('PROGRAM EXIT. SYSTEM AGGREGATES.'
             /'THE A12 SUBMATRIX = 0.')
```

GO TO 70000

```

*
50200 WRITE (6,50250)
50250 FORMAT ('PROGRAM EXIT. SYSTEM WILL AGGREGATE.'
             /'THE MATRIX A12S = 0.')
```

GO TO 70000

```

*
*****
* PROGRAM EXITS ASSOCIATED WITH NO AGGREGATION. *
*****
*
60600 WRITE (6,60650)
60650 FORMAT ('PROGRAM EXIT. TRIVIAL CASE'
             /'THE C MATRIX IS ZERO.')
```

GO TO 80000

```

*
60700 WRITE (6,60750)
60750 FORMAT ('PROGRAM EXIT. SYSTEM WILL NOT AGGREGATE.'
             /'THE C MATRIX HAS A RANK EQUAL TO THE'
             /'DIMENSION OF THE SYSTEM.')
```

GO TO 70000

```

*
60800 WRITE (6,60850)
60850 FORMAT ('PROGRAM EXIT. SYSTEM WILL NOT AGGREGATE.'
             /'THE A12S SUBMATRIX HAS FULL COLUMN RANK.')
```

GO TO 70000

```

*
70000 CONTINUE
      WRITE (6,70100)
70100 FORMAT ('WOULD YOU LIKE TO SEE THE TRANSFORMED'
             /'SYSTEM MATRICES? >',*)
      READ (5,10) ANS
      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 80000
*
* COMPUTE THE TRANSFORMED A MATRIX.
*
      CALL MULT(T,0,AFRMT,FANAME,SOS,SOS,A,1,AFRMT,FANAME,SOS,SOS,TDMB)
      DO 70200 I=1,SOS
        DO 70200 J=1,SOS
          DMB(I,J) = T(J,I)
70200 CONTINUE
*
      CALL MULT(TDMB,0,AFRMT,FANAME,SOS,SOS,DMB,0,AFRMT,FANAME,SOS,
              SOS,A)
```

```

*
  WRITE (6,70300)
70300 FORMAT ('THIS IS THE TRANSFORMED "A" MATRIX:')
      CALL OUTPUT(A,SOS,SOS,SIZCHK)
*
* COMPUTE THE TRANSFORMED "B" MATRIX.
*
  IF (FCHND .EQ. 1) NCB = NCBTMP
*
  CALL MULT(T,0,BFRMT,FBNAME,SOS,SOS,B,1,BFRMT,FBNAME,SOS,NCB,G)
*
  WRITE (6,70400)
70400 FORMAT ('THIS IS THE TRANSFORMED "B" MATRIX.')
      CALL OUTPUT(G,SOS,NCB,SIZCHK)
*
* COMPUTE THE TRANSFORMED "C" MATRIX.
* (RECALL DMB IS THE TRANSPOSE OF THE "T" MATRIX.)
*
  CALL MULT(C,1,CFRMT,FCNAME,NRC,NCC,DMB,0,CFRMT,FCNAME,
           SOS,SOS,TDMB)
*
  WRITE (6,70500)
70500 FORMAT ('THIS IS THE TRANSFORMED "C" MATRIX.')
      CALL OUTPUT(TDMB,NRC,NCC,SIZCHK)
*
  WRITE (6,70600)
70600 FORMAT ('WOULD YOU LIKE TO SEE THE FINAL "T" MATRIX? >'.,$)
      READ (5,10) ANS
      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 70800
*
  CALL OUTPUT(T,SOS,SOS,SIZCHK)
*
70800 WRITE (6,70900)
70900 FORMAT ('WOULD YOU LIKE TO SEE THE FINAL "T" TRANSPOSE'
           /'MATRIX? >'.,$)
      READ (5,10) ANS
      IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 80000
*
  CALL OUTPUT(DMB,SOS,SOS,SIZCHK)
*
80000 CONTINUE
      STOP
      END

```

```

*****
* SUBROUTINES USED IN PROGRAM ABOVE *
*****

```

```

*****
* SUBROUTINE USV *
*****

```

```

* THIS SUBROUTINE COMPUTES THE NUMBER OF NON-ZERO

```

- \* SINGULAR VALUES ASSOCIATED WITH A DECOMPOSED
- \* MATRIX. IT ALSO ASKS IF YOU WOULD LIKE TO SEE
- \* THE U AND/OR V MATRIX CREATED DURING THE DECOMPOSITION.
- \* DEPENDING ON WHERE IN THE PROGRAM USV IS CALLED.

```

SUBROUTINE USV(U, SIGMA, V, SIZCHK, MIN, N, NR, NC, TYPE)
CHARACTER*1      ANS
CHARACTER*20     TYPE
REAL             U(100,100) , V(100,100) , SIGMA(100)
REAL             SIZCHK
INTEGER          MIN      , N      , NR      , NC
INTEGER          I       , IERR

```

- \* FORMAT STATEMENTS USED

```

910  FORMAT (A)
950  FORMAT (100(F12.5))

```

```

WRITE (6,990) TYPE
990  FORMAT ('THIS DECOMPOSITION IS OF ',A)

```

```

WRITE (6,1000)
1000 FORMAT ('WOULD YOU LIKE TO SEE THE U MATRIX? >'. $)
READ (5,910) ANS
IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 2050

```

```

WRITE (6,1500)
1500 FORMAT ('THE CORRESPONDING U MATRIX IS:')
CALL DSPLAY(U, NR, NR)

```

```

2050 CONTINUE

```

```

WRITE (6,2100)
2100 FORMAT ('THE SINGULAR VALUES ARE:')
WRITE (6,950) (SIGMA(I), I=1, MIN)

```

```

CHECK THE MAGNITUDE OF THE SINGULAR VALUES
N=0
DO 2200 I=1, MIN
IF (SIGMA(I).LT.SIZCHK) GO TO 2300
N=N+1
2200 CONTINUE

```

```

2300 WRITE (6,2350) N
2350 FORMAT ('THE NUMBER OF INDEPENDENT COLUMNS IN'
/'THE DECOMPOSED MATRIX IS: ', I5)

```

```

IF (TYPE .EQ. 'A B SUBMATRIX.') GO TO 3050
WRITE (6,2400)
2400 FORMAT ('WOULD YOU LIKE TO SEE THE V MATRIX? >'. $)
READ (5,910) ANS
IF ((ANS .NE. 'Y').AND.(ANS .NE. 'y')) GO TO 3050

```

```

WRITE (6,2500)

```

```

2500 FORMAT ('THE CORRESPONDING V MATRIX IS:')
      CALL  DSPLAY(V,NC,NC)
*
3050 CONTINUE
*
      WRITE (6,3500) IERR
3500 FORMAT ('IERR EQUALS ',I4)
      RETURN
      END
*
*****
* SUBROUTINE DUP *
*****
*
* THIS SUBROUTINE DUPLICATES A MATRIX. THIS IS NEEDED
* SINCE WHEN A MATRIX IS PASSED TO SSVDC IT RETURNS IN
* AN ALTERED FORM.
*
      SUBROUTINE DUP(SOURCE,DUMMY,NROW,NCOL)
*
      REAL      SOURCE(100,100)      , DUMMY(100,100)
      INTEGER   NROW                  , NCOL
      INTEGER   I                      , J
*
      DO 1000 I=1,NROW
        DO 1000 J=1,NCOL
          DUMMY(I,J) = SOURCE(I,J)
1000 CONTINUE
      RETURN
      END
*
*****
* SUBROUTINE OUTPUT *
*****
*
* THIS SUBROUTINE ALLOWS THE USER TO SEE THE
* PARTICULAR MATRIX ON THE SCREEN IN EITHER F6.3
* FORMAT OR SIMPLY AS X'S AND O'S (IF THE STRUCTURE
* IS ALL THAT IS DESIRED). THE USER MAY ALSO OUTPUT
* THE MATRIX TO A FILE IN EITHER OF THESE FORMATS.
* THE USER MUST SUPPLY THE FILENAME TO BE USED.
*
      SUBROUTINE OUTPUT(X,NROW,NCOL,SIZCHK)
      CHARACTER*1      ANS
      CHARACTER*1      XC(100,100)
      CHARACTER*20     FNAME
      REAL              X(100,100)      , SIZCHK
      INTEGER           I                  , J
      INTEGER           NROW              , NCOL
      INTEGER           FORM
      LOGICAL           FOUT
*
* FREQUENTLY USED FORMAT STATEMENTS.

```

```

*
10  FORMAT (8(F9.3,1X))
15  FORMAT (7(E15.7,1X))
20  FORMAT (A)
30  FORMAT (40(A,2X))
*
50  WRITE (6,100)
100 FORMAT ('WHAT FORMAT DO YOU WISH TO SEE'
           /'THIS MATRIX IN?'
           /'      1) NUMERICAL VALUES'
           /'      2) STRUCTURE ONLY (X AND O)'
           /'ENTER 1 OR 2 >', $)
*
      READ (5,150) FORM
150  FORMAT (I1)
*
      WRITE (6,200)
200  FORMAT ('WOULD YOU LIKE THIS MATRIX STORED'
           /'IN A FILE? >', $)
*
      READ (5,20) ANS
      IF ((ANS .EQ. 'Y').OR.(ANS .EQ. 'y')) GO TO 275
      FOUT = .FALSE.
      GO TO 400
*
275  WRITE (6,300)
300  FORMAT ('ENTER THE FILENAME FOR THIS MATRIX >', $)
      READ (5,20) FNAME
      FOUT = .TRUE.
*
400  IF (FORM .EQ. 1) GO TO 500
      IF (FORM .EQ. 2) GO TO 1000
      WRITE (6,450)
450  FORMAT ('INCORRECT ENTRY(S).', //)
      GO TO 50
*
500  CALL DSPLAY(X, NROW, NCOL)
      IF (.NOT. FOUT) RETURN
*
600  OPEN (UNIT=1, FILE=FNAME)
      REWIND 1
      WRITE (1,*) NROW , NCOL
      DO 650 I=1, NROW
          WRITE (1,15) (X(I,J), J=1, NCOL)
650  CONTINUE
      CLOSE (UNIT=1)
      RETURN
*
*
1000 DO 1050 I=1, NROW
      DO 1050 J=1, NCOL
          XC(I,J) = 'O'
          IF (ABS(X(I,J)) .GT. SIZCHK) XC(I,J) = 'X'

```

1050 CONTINUE

```

*
  IF      (FOUT) GO TO 1300
  DO 1100 I=1,NROW
    WRITE (6,30) (XC(I,J),J=1,NCOL)
1100 CONTINUE
  RETURN

```

```

*
1300 OPEN  (UNIT=1,FILE=FNAME)
  REWIND 1
  DO 1400 I=1,NROW
    WRITE (6,30) (XC(I,J),J=1,NCOL)
    WRITE (1,30) (XC(I,J),J=1,NCOL)
1400 CONTINUE
  CLOSE (UNIT=1)
  RETURN
  END

```

```

*****
* SUBROUTINE INPUT *
*****

```

```

* THIS SUBROUTINE READS IN THE APPROPRIATE MATRIX FROM
* A DATA FILE. THE MATRIX MAY BE STORED IN NORMAL FORM
* OR AS A SPARSE MATRIX. YOU ARE ALSO ALLOWED THE ABILITY
* TO VERIFY THE MATRIX READ IN.

```

```

SUBROUTINE INPUT(X,NROW,NCOL,TYPE,FRMT,FNAME)
CHARACTER*1   ANS      , FRMT
CHARACTER*20  FNAME    , TYPE
REAL          X(100,100)
INTEGER       I        , J
INTEGER       NROW     , NCOL
INTEGER       NR       , NC

  WRITE (6,200) TYPE
200  FORMAT ('ENTER THE NAME OF THE DATA FILE FOR THE ',A11,' >',$,)
  READ  (5,300) FNAME
300  FORMAT (A)
  IF    (TYPE .EQ. '"A" MATRIX.') GO TO 252
  WRITE (6,250) TYPE
250  FORMAT ('ENTER THE DIMENSIONS OF THE ',A10,' (ROWS x COLS). >',$,)
  READ  (5,*) NROW,NCOL

  WRITE (6,255)
255  FORMAT ('WHAT FORMAT IS THIS MATRIX IN?'
    /'   A) SPARSE'
    /'   B) NORMAL'
    /'   ENTER A OR B >',$,)
  READ  (5,300) FRMT
  IF    ((FRMT .EQ. 'A').OR.(FRMT .EQ. 'a')) GO TO 310
  IF    ((FRMT .EQ. 'B').OR.(FRMT .EQ. 'b')) GO TO 305
  GO TO 252

```

```

*
305 OPEN (UNIT=1,FILE=FNAME)
    REWIND 1
    READ (1,*) NR , NC
    IF ((NR .EQ. NROW).AND.(NC .EQ. NCOL)) GO TO 307
    WRITE (6,306)
306 FORMAT ('PROGRAM EXIT! MATRIX DIMENSIONS WHICH WERE'
           /'INPUT AND THOSE IN THE DATAFILE DO NOT AGREE.')
```

STOP

```

307 READ (1,*) ((X(I,J),J=1,NCOL),I=1,NROW)
    CLOSE (UNIT=1)
    GO TO 350
*
*
310 DO 308 I=1,NROW
      DO 308 J=1,NCOL
        X(I,J)=0.0
308 CONTINUE
*
OPEN (UNIT=1,FILE=FNAME)
REWIND 1
312 READ (1,*,END=350) I , J , X(I,J)
    GO TO 312
*
350 WRITE (6,360) TYPE
360 FORMAT ('DO YOU WANT TO VERIFY THE ',A10,'? >',$)
    READ (5,300) ANS
    IF ((ANS.NE.'Y').AND.(ANS.NE.'y')) RETURN
    WRITE (6,400) TYPE
400 FORMAT ('THE FOLLOWING ',A10,' WAS READ IN:')
    CALL DSPLAY(X,NROW,NCOL)
1000 CONTINUE
*
RETURN
END
*
*****
* SUBROUTINE MULT *
*****
*
* THIS SUBROUTINE MULTIPLIES TWO MATRICES TOGETHER AND
* RETURNS THE RESULT IN P. ONE OR BOTH OF THE FILES MAY
* HAVE TO BE READ IN FROM DATAFILES, THIS OPTION IS CON-
* TROLLED BY A FLAG FOR EACH MATRIX.
* 1 MEANS READ THE FILE IN FROM A DATAFILE.
* 0 MEANS THE MATRIX WAS PASSED IN THE CALL.
* *FRMT INDICATES THE FORMAT THE PARTICULAR
* MATRIX IS STORED IN.
*
SUBROUTINE MULT(X,XF,XFRMT,XNAME,NRX,NCX,Y,YF,YFRMT,YNAME,NRY,
               NCF,P)
CHARACTER*1 XFRMT , YFRMT
CHARACTER*20 XNAME , YNAME
```

```

LOGICAL      XF      , YF
INTEGER      I      , J      , K
INTEGER      NRX     , NRY     , NCX     , NCY
INTEGER      RD      , CD
REAL         X(100,100), Y(100,100), P(100,100)
*
IF      (NCX .EQ. NRY) GO TO 50
WRITE  (6,30)
30    FORMAT ('THE MATRICES ARE NOT COMPATABLE!')
      STOP
*
* DOES THE MATRIX NEED TO BE READ IN FROM A DATA FILE?
*
50    IF      (.NOT.XF) GO TO 500
*
* WHAT FORMAT IS THE MATRIX IN? (A=SPARSE,B=NORMAL)
*
IF      ((XFRMT .EQ. 'A').OR.(XFRMT .EQ. 'a')) GO TO 300
IF      ((XFRMT .EQ. 'B').OR.(XFRMT .EQ. 'b')) GO TO 200
WRITE  (6,100)
100   FORMAT ('THE X MATRIX IN THE MULT SUBROUTINE'
             /'WAS NOT ASSIGNED A FORMAT TYPE')
      STOP
*
200   OPEN  (UNIT=1,FILE=XNAME)
      REWIND 1
      READ  (1,*) RD , CD
      READ  (1,*) ((X(I,J),J=1,NCX),I=1,NRX)
      CLOSE (UNIT=1)
      GO TO 500
*
300   DO 350 I=1,NRX
        DO 350 J=1,NCX
          X(I,J) = 0.0
350   CONTINUE
*
      OPEN  (UNIT=1,FILE=XNAME)
      REWIND 1
360   READ  (1,*,END=500) I , J , X(I,J)
      GO TO 360
*
* DOES THE Y MATRIX NEED TO BE READ IN FROM A DATAFILE?
*
500   IF      (.NOT.YF) GO TO 1000
*
* WHAT FORMAT IS THE "Y" MATRIX IN? (A=SPARSE,B=NORMAL)
*
IF      ((YFRMT .EQ. 'A').OR.(YFRMT .EQ. 'a')) GO TO 800
IF      ((YFRMT .EQ. 'B').OR.(YFRMT .EQ. 'b')) GO TO 600
WRITE  (6,550)
550   FORMAT ('THE "Y" MATRIX IN THE MULT SUBROUTINE'
             /'WAS NOT ASSIGNED A FORMAT TYPE')
      STOP

```

```

*
600 OPEN (UNIT=1,FILE=YNAME)
    REWIND 1
    READ (1,*) RD , CD
    READ (1,*) ((Y(I,J),J=1,NCY),I=1,NRY)
    CLOSE (UNIT=1)
    GO TO 1000
*
800 DO 850 I=1,NRY
    DO 850 J=1,NCY
        Y(I,J) = 0.0
850 CONTINUE
*
    OPEN (UNIT=1,FILE=YNAME)
    REWIND 1
860 READ (1,*,END=1000) I , J , Y(I,J)
    GO TO 860
*
1000 DO 1200 I=1,NRY
    DO 1200 J=1,NCY
        P(I,J) = 0.0
        DO 1200 K=1,NCX
            P(I,J) = P(I,J) + X(I,K)*Y(K,J)
1200 CONTINUE
    RETURN
    END
*
*****
* SUBROUTINE DSPLAY *
*****
*
* THIS SUBROUTINE ALLOWS A MATRIX TO BE
* DISPLAYED ON THE TERMINAL SCREEN IN
* GROUPS OF 8 COLUMNS.
*
    SUBROUTINE DSPLAY(X,NROW,NCOL)
    INTEGER I , J , START
    INTEGER NROW , NCOL , FINISH
    REAL X(100,100)
*
    START = 1
    FINISH = 8
100 IF (FINISH .GE. NCOL) FINISH = NCOL
    WRITE (6,150) START , FINISH
150 FORMAT (/ ' COLS. ',I3,' TO ',I3)
    DO 200 I=1, NROW
        WRITE (6,175) (X(I,J),J=START,FINISH)
175 FORMAT (8(F9.3,1X))
200 CONTINUE
    IF (FINISH .GE. NCOL) GO TO 300
    START = START + 8
    FINISH = FINISH + 8
    GO TO 100

```





```

C   FORTRAN ABS, AMAX1, MAX0, MIN0, MOD, SQRT
C
C   INTERNAL VARIABLES
C
C   INTEGER I, ITER, J, JOBU, K, KASE, KK, L, LL, LLS, LM1, LP1, LS, LU, M, MAXIT,
*   MM, MM1, MP1, NCT, NCTP1, NCU, NRT, NRTP1
C   REAL SDOT, T, R
C   REAL B, C, CS, EL, EMM1, F, G, SNRM2, SCALE, SHIFT, SL, SM, SN, SMM1, T1, TEST,
*   ZTEST
C   LOGICAL WANTU, WANTV
C
C
C   SET THE MAXIMUM NUMBER OF ITERATIONS.
C
C   MAXIT = 30
C
C   DETERMINE WHAT IS TO BE COMPUTED.
C
C   WANTU = .FALSE.
C   WANTV = .FALSE.
C   JOBU = MOD(JOB,100)/10
C   NCU = N
C   IF (JOBU .GT. 1) NCU = MIN0(N,P)
C   IF (JOBU .NE. 0) WANTU = .TRUE.
C   IF (MOD(JOB,10) .NE. 0) WANTV = .TRUE.
C
C   REDUCE X TO BIDIAGONAL FORM, STORING THE DIAGONAL ELEMENTS
C   IN S AND THE SUPER-DIAGONAL ELEMENTS IN E.
C
C   INFO = 0
C   NCT = MIN0(N-1,P)
C   NRT = MAX0(0,MIN0(P-2,N))
C   LU = MAX0(NCT,NRT)
C   IF (LU .LT. 1) GO TO 170
C   DO 160 L = 1, LU
C     LP1 = L + 1
C     IF (L .GT. NCT) GO TO 20
C
C     COMPUTE THE TRANSFORMATION FOR THE L-TH COLUMN AND
C     PLACE THE L-TH DIAGONAL IN S(L).
C
C     S(L) = SNRM2(N-L+1,X(L,L),1)
C     IF (S(L) .EQ. 0.0E0) GO TO 10
C     IF (X(L,L) .NE. 0.0E0) S(L) = SIGN(S(L),X(L,L))
C     CALL SSCAL(N-L+1,1.0E0/S(L),X(L,L),1)
C     X(L,L) = 1.0E0 + X(L,L)
10    CONTINUE
C     S(L) = -S(L)
20    CONTINUE
C     IF (P .LT. LP1) GO TO 50
C     DO 40 J = LP1, P
C       IF (L .GT. NCT) GO TO 30
C       IF (S(L) .EQ. 0.0E0) GO TO 30

```

```

C
C      APPLY THE TRANSFORMATION.
C
      T = -SDOT(N-L+1,X(L,L),1,X(L,J),1)/X(L,L)
      CALL SAXPY(N-L+1,T,X(L,L),1,X(L,J),1)
30    CONTINUE
C
C      PLACE THE L-TH ROW OF X INTO E FOR THE
C      SUBSEQUENT CALCULATION OF THE ROW TRANSFORMATION.
C
      E(J) = X(L,J)
40    CONTINUE
50    CONTINUE
      IF (.NOT.WANTU .OR. L .GT. NCT) GO TO 70
C
C      PLACE THE TRANSFORMATION IN U FOR SUBSEQUENT BACK
C      MULTIPLICATION.
C
      DO 60 I = L, N
          U(I,L) = X(I,L)
60    CONTINUE
70    CONTINUE
      IF (L .GT. NCT) GO TO 150
C
C      COMPUTE THE L-TH ROW TRANSFORMATION AND PLACE THE
C      L-TH SUPER-DIAGONAL IN E(L).
C
      E(L) = SNRM2(P-L,E(LP1),1)
      IF (E(L) .EQ. 0.0E0) GO TO 80
      IF (E(LP1) .NE. 0.0E0) E(L) = SIGN(E(L),E(LP1))
      CALL SSCAL(P-L,1.0E0/E(L),E(LP1),1)
      E(LP1) = 1.0E0 + E(LP1)
80    CONTINUE
      E(L) = -E(L)
      IF (LP1 .GT. N .OR. E(L) .EQ. 0.0E0) GO TO 120
C
C      APPLY THE TRANSFORMATION.
C
      DO 90 I = LP1, N
          WORK(I) = 0.0E0
90    CONTINUE
      DO 100 J = LP1, P
          CALL SAXPY(N-L,E(J),X(LP1,J),1,WORK(LP1),1)
100   CONTINUE
      DO 110 J = LP1, P
          CALL SAXPY(N-L,-E(J)/E(LP1),WORK(LP1),1,X(LP1,J),1)
110   CONTINUE
120  CONTINUE
      IF (.NOT.WANTV) GO TO 140
C
C      PLACE THE TRANSFORMATION IN V FOR SUBSEQUENT
C      BACK MULTIPLICATION.
C

```

```

                DO 130 I = LP1, P
                  V(I,L) = E(I)
130             CONTINUE
140             CONTINUE
150             CONTINUE
160 CONTINUE
170 CONTINUE
C
C   SET UP THE FINAL BIDIAGONAL MATRIX OR ORDER M.
C
      M = MINO(P,N+1)
      NCTP1 = NCT + 1
      NRTP1 = NRT + 1
      IF (NCT .LT. P) S(NCTP1) = X(NCTP1,NCTP1)
      IF (N .LT. M) S(M) = 0.0E0
      IF (NRTP1 .LT. M) E(NRTP1) = X(NRTP1,M)
      E(M) = 0.0E0
C
C   IF REQUIRED, GENERATE U.
C
      IF (.NOT.WANTU) GO TO 300
      IF (NCU .LT. NCTP1) GO TO 200
      DO 190 J = NCTP1, NCU
        DO 180 I = 1, N
          U(I,J) = 0.0E0
180       CONTINUE
          U(J,J) = 1.0E0
190       CONTINUE
200       CONTINUE
      IF (NCT .LT. 1) GO TO 290
      DO 280 LL = 1, NCT
        L = NCT - LL + 1
        IF (S(L) .EQ. 0.0E0) GO TO 250
        LP1 = L + 1
        IF (NCU .LT. LP1) GO TO 220
        DO 210 J = LP1, NCU
          T = -SDOT(N-L+1,U(L,L),1,U(L,J),1)/U(L,L)
          CALL SAXPY(N-L+1,T,U(L,L),1,U(L,J),1)
210       CONTINUE
220       CONTINUE
          CALL SSCAL(N-L+1,-1.0E0,U(L,L),1)
          U(L,L) = 1.0E0 + U(L,L)
          LM1 = L - 1
          IF (LM1 .LT. 1) GO TO 240
          DO 230 I = 1, LM1
            U(I,L) = 0.0E0
230         CONTINUE
240         CONTINUE
          GO TO 270
250       CONTINUE
          DO 260 I = 1, N
            U(I,L) = 0.0E0
260         CONTINUE

```

```

          U(L,L) = 1.0E0
270      CONTINUE
280      CONTINUE
290      CONTINUE
300      CONTINUE
C
C      IF IT IS REQUIRED, GENERATE V.
C
      IF (.NOT.WANTV) GO TO 350
      DO 340 LL = 1, P
        L = P - LL + 1
        LP1 = L + 1
        IF (L .GT. NRT) GO TO 320
        IF (E(L) .EQ. 0.0E0) GO TO 320
        DO 310 J = LP1, P
          T = -SDOT(P-L,V(LP1,L),1,V(LP1,J),1)/V(LP1,L)
          CALL SAXPY(P-L,T,V(LP1,L),1,V(LP1,J),1)
310      CONTINUE
320      CONTINUE
        DO 330 I = 1, P
          V(I,L) = 0.0E0
330      CONTINUE
          V(L,L) = 1.0E0
340      CONTINUE
350      CONTINUE
C
C      MAIN ITERATION LOOP FOR THE SINGULAR VALUES.
C
      MM = M
      ITER = 0
360      CONTINUE
C
C      QUIT IF ALL THE SINGULAR VALUES HAVE BEEN FOUND.
C
      ...EXIT
      IF (M .EQ. 0) GO TO 620
C
C      IF TOO MANY ITERATIONS HAVE BEEN PERFORMED, SET
C      FLAG AND RETURN.
C
      IF (ITER .LT. MAXIT) GO TO 370
      INFO = M
C
      .....EXIT
      GO TO 620
370      CONTINUE
C
C      THIS SECTION OF THE PROGRAM INSPECTS FOR
C      NEGLIGIBLE ELEMENTS IN THE S AND E ARRAYS. ON
C      COMPLETION THE VARIABLES KASE AND L ARE SET AS FOLLOWS.
C
      KASE = 1      IF S(M) AND E(L-1) ARE NEGLIGIBLE AND L.LT.M
      KASE = 2      IF S(L) IS NEGLIGIBLE AND L.LT.M
      KASE = 3      IF E(L-1) IS NEGLIGIBLE, L.LT.M, AND

```

```

C           S(L), ..., S(M) ARE NOT NEGLIGIBLE (QR STEP).
C           KASE = 4     IF E(M-1) IS NEGLIGIBLE (CONVERGENCE).
C
DO 390 LL = 1, M
  L = M - LL
C  ...EXIT
  IF (L .EQ. 0) GO TO 400
  TEST = ABS(S(L)) + ABS(S(L+1))
  ZTEST = TEST + ABS(E(L))
  IF (ZTEST .NE. TEST) GO TO 380
  E(L) = 0.0E0
C  .....EXIT
  GO TO 400
380  CONTINUE
390  CONTINUE
400  CONTINUE
  IF (L .NE. M - 1) GO TO 410
  KASE = 4
  GO TO 480
410  CONTINUE
  LP1 = L + 1
  MP1 = M + 1
  DO 430 LLS = LP1, MP1
    LS = M - LLS + LP1
C  ...EXIT
  IF (LS .EQ. L) GO TO 440
  TEST = 0.0E0
  IF (LS .NE. M) TEST = TEST + ABS(E(LS))
  IF (LS .NE. L + 1) TEST = TEST + ABS(E(LS-1))
  ZTEST = TEST + ABS(S(LS))
  IF (ZTEST .NE. TEST) GO TO 420
  S(LS) = 0.0E0
C  .....EXIT
  GO TO 440
420  CONTINUE
430  CONTINUE
440  CONTINUE
  IF (LS .NE. L) GO TO 450
  KASE = 3
  GO TO 470
450  CONTINUE
  IF (LS .NE. M) GO TO 460
  KASE = 1
  GO TO 470
460  CONTINUE
  KASE = 2
  L = LS
470  CONTINUE
480  CONTINUE
  L = L + 1
C
C  PERFORM THE TASK INDICATED BY KASE.
C

```

```

GO TO (490,520,540,570), KASE
C
C
C
490 CONTINUE
MM1 = M - 1
F = E(M-1)
E(M-1) = 0.0E0
DO 510 KK = L, MM1
K = MM1 - KK + L
T1 = S(K)
CALL SROTG(T1,F,CS,SN)
S(K) = T1
IF (K .EQ. L) GO TO 500
F = -SN*E(K-1)
E(K-1) = CS*E(K-1)
500 CONTINUE
IF (WANTV) CALL SROT(P,V(1,K),1,V(1,M),1,CS,SN)
510 CONTINUE
GO TO 610
C
C
C
520 CONTINUE
F = E(L-1)
E(L-1) = 0.0E0
DO 530 K = L, M
T1 = S(K)
CALL SROTG(T1,F,CS,SN)
S(K) = T1
F = -SN*E(K)
E(K) = CS*E(K)
IF (WANTU) CALL SROT(N,U(1,K),1,U(1,L-1),1,CS,SN)
530 CONTINUE
GO TO 610
C
C
C
PERFORM ONE OR STEP.
C
C
540 CONTINUE
CALCULATE THE SHIFT.
SCALE = AMAX1(ABS(S(M)),ABS(S(M-1)),ABS(E(M-1)),ABS(S(L)),
ABS(E(L)))
SM = S(M)/SCALE
SMM1 = S(M-1)/SCALE
EMM1 = E(M-1)/SCALE
SL = S(L)/SCALE
EL = E(L)/SCALE
B = ((SMM1 + SM)*(SMM1 - SM) + EMM1**2)/2.0E0
C = (SM*EMM1)**2
SHIFT = 0.0E0
IF (B .EQ. 0.0E0 .AND. C .EQ. 0.0E0) GO TO 550

```

```

      SHIFT = SQRT(B**2+C)
      IF (B .LT. 0.0E0) SHIFT = -SHIFT
      SHIFT = C/(B + SHIFT)
550  CONTINUE
      F = (SL + SM)*(SL - SM) - SHIFT
      G = SL*EL
C
C      CHASE ZEROS.
C
      MM1 = M - 1
      DO 560 K = L, MM1
        CALL SROTG(F,G,CS,SN)
        IF (K .NE. L) E(K-1) = F
        F = CS*S(K) + SN*E(K)
        E(K) = CS*E(K) - SN*S(K)
        G = SN*S(K+1)
        S(K+1) = CS*S(K+1)
        IF (WANTV) CALL SROT(P,V(1,K),1,V(1,K+1),1,CS,SN)
        CALL SROTG(F,G,CS,SN)
        S(K) = F
        F = CS*E(K) + SN*S(K+1)
        S(K+1) = -SN*E(K) + CS*S(K+1)
        G = SN*E(K+1)
        E(K+1) = CS*E(K+1)
        IF (WANTU .AND. K .LT. N)
          * CALL SROT(N,U(1,K),1,U(1,K+1),1,CS,SN)
560  CONTINUE
      E(M-1) = F
      ITER = ITER + 1
      GO TO 610
C
C      CONVERGENCE.
C
570  CONTINUE
C
C      MAKE THE SINGULAR VALUE POSITIVE.
C
      IF (S(L) .GE. 0.0E0) GO TO 580
      S(L) = -S(L)
      IF (WANTV) CALL SSCAL(P,-1.0E0,V(1,L),1)
580  CONTINUE
C
C      ORDER THE SINGULAR VALUE.
C
590  IF (L .EQ. MM) GO TO 600
      ...EXIT
      IF (S(L) .GE. S(L+1)) GO TO 600
      T = S(L)
      S(L) = S(L+1)
      S(L+1) = T
      IF (WANTV .AND. L .LT. P)
        * CALL SSWAP(P,V(1,L),1,V(1,L+1),1)
      IF (WANTU .AND. L .LT. N)

```

```

      *          CALL SSWAP(N,U(1,L),1,U(1,L+1),1)
          L = L + 1
          GO TO 590
600      CONTINUE
          ITER = 0
          M = M - 1
610      CONTINUE
          GO TO 360
620      CONTINUE
          RETURN
          END
          REAL FUNCTION SNRM2 ( N, SX, INCX)
          INTEGER          NEXT,      N ,      INCX
          INTEGER          MN ,      I ,      J
          REAL  SX(1),  CUTLO, CUTHI, HITEST, SUM, XMAX, ZERO, ONE
          DATA  ZERO, ONE /0.0E0, 1.0E0/

C
C      EUCLIDEAN NORM OF THE N-VECTOR STORED IN SX() WITH STORAGE
C      INCREMENT INCX .
C      IF N .LE. 0 RETURN WITH RESULT = 0.
C      IF N .GE. 1 THEN INCX MUST BE .GE. 1
C
C          C.L.LAWSON, 1978 JAN 08
C
C      FOUR PHASE METHOD      USING TWO BUILT-IN CONSTANTS THAT ARE
C      HOPEFULLY APPLICABLE TO ALL MACHINES.
C          CUTLO = MAXIMUM OF SQRT(U/EPS)  OVER ALL KNOWN MACHINES.
C          CUTHI = MINIMUM OF SQRT(V)      OVER ALL KNOWN MACHINES.
C      WHERE
C          EPS = SMALLEST NO. SUCH THAT EPS + 1. .GT. 1.
C          U   = SMALLEST POSITIVE NO.  (UNDERFLOW LIMIT)
C          V   = LARGEST NO.             (OVERFLOW LIMIT)
C
C      BRIEF OUTLINE OF ALGORITHM..
C
C      PHASE 1      SCANS ZERO COMPONENTS.
C      MOVE TO PHASE 2 WHEN A COMPONENT IS NONZERO AND .LE. CUTLO
C      MOVE TO PHASE 3 WHEN A COMPONENT IS .GT. CUTLO
C      MOVE TO PHASE 4 WHEN A COMPONENT IS .GE. CUTHI/M
C      WHERE M = N FOR I() REAL AND M = 2*N FOR COMPLEX.
C
C      VALUES FOR CUTLO AND CUTHI..
C      FROM THE ENVIRONMENTAL PARAMETERS LISTED IN THE IMSL CONVERTER
C      DOCUMENT THE LIMITING VALUES ARE AS FOLLOWS..
C      CUTLO, S.P.  U/EPS = 2**(-102) FOR HONEYWELL.  CLOSE SECONDS ARE
C                  UNIVAC AND DEC AT 2**(-103)
C                  THUS CUTLO = 2**(-51) = 4.44089E-16
C      CUTHI, S.P.  V = 2**127 FOR UNIVAC, HONEYWELL, AND DEC.
C                  THUS CUTHI = 2**(63.5) = 1.30438E19
C      CUTLO, D.P.  U/EPS = 2**(-67) FOR HONEYWELL AND DEC.
C                  THUS CUTLO = 2**(-33.5) = 8.23181D-11
C      CUTHI, D.P.  SAME AS S.P.  CUTHI = 1.30438D19
C      DATA CUTLO, CUTHI / 8.232D-11, 1.304D19 /

```

```

C   DATA CUTLO, CUTHI / 4.441E-16, 1.304E19 /
C   DATA CUTLO, CUTHI / 4.441E-16, 1.304E19 /
C
C   IF(N .GT. 0) GO TO 10
C       SNRM2 = ZERO
C       GO TO 300
C
C   10 ASSIGN 30 TO NEXT
C       SUM = ZERO
C       NN = N * INCX
C
C                                           BEGIN MAIN LOOP
C
C   I = 1
C   20 GO TO NEXT,(30, 50, 70, 110)
C   30 IF( ABS(SX(I)) .GT. CUTLO) GO TO 85
C       ASSIGN 50 TO NEXT
C       XMAX = ZERO
C
C
C           PHASE 1. SUM IS ZERO
C
C   50 IF( SX(I) .EQ. ZERO) GO TO 200
C       IF( ABS(SX(I)) .GT. CUTLO) GO TO 85
C
C
C           PREPARE FOR PHASE 2.
C
C   ASSIGN 70 TO NEXT
C   GO TO 105
C
C
C           PREPARE FOR PHASE 4.
C
C   100 I = J
C       ASSIGN 110 TO NEXT
C       SUM = (SUM / SX(I)) / SX(I)
C   105 XMAX = ABS(SX(I))
C       GO TO 115
C
C
C           PHASE 2. SUM IS SMALL.
C           SCALE TO AVOID DESTRUCTIVE UNDERFLOW.
C
C   70 IF( ABS(SX(I)) .GT. CUTLO ) GO TO 75
C
C
C           COMMON CODE FOR PHASES 2 AND 4.
C           IN PHASE 4 SUM IS LARGE. SCALE TO AVOID OVERFLOW.
C
C   110 IF( ABS(SX(I)) .LE. XMAX ) GO TO 115
C       SUM = ONE + SUM * (XMAX / SX(I))**2
C       XMAX = ABS(SX(I))
C       GO TO 200
C
C   115 SUM = SUM + (SX(I)/XMAX)**2
C       GO TO 200
C
C
C           PREPARE FOR PHASE 3.
C

```

```

75 SUM = (SUM * XMAX) * XMAX
C
C
C   FOR REAL OR D.P. SET HITEST = CUTHI/N
C   FOR COMPLEX      SET HITEST = CUTHI/(2*N)
C
85 HITEST = CUTHI/FLOAT( N )
C
C           PHASE 3.  SUM IS MID-RANGE.  NO SCALING.
C
DO 95 J =I,NN,INCX
IF(ABS(SX(J)) .GE. HITEST) GO TO 100
95  SUM = SUM + SX(J)**2
   SNRM2 = SQRT( SUM )
   GO TO 300
C
200 CONTINUE
   I = I + INCX
   IF ( I .LE. NN ) GO TO 20
C
C           END OF MAIN LOOP.
C
C           COMPUTE SQUARE ROOT AND ADJUST FOR SCALING.
C
   SNRM2 = XMAX * SQRT(SUM)
300 CONTINUE
   RETURN
   END
   SUBROUTINE  SSCAL(N,SA,SX,INCX)
C
C   SCALES A VECTOR BY A CONSTANT.
C   USES UNROLLED LOOPS FOR INCREMENT EQUAL TO 1.
C   JACK DONGARRA, LINPACK, 3/11/78.
C
   REAL SA,SX(1)
   INTEGER I,INCX,M,MPI,N,NINCX
C
   IF(N.LE.0)RETURN
   IF(INCX.EQ.1)GO TO 20
C
C           CODE FOR INCREMENT NOT EQUAL TO 1
C
   NINCX = N*INCX
   DO 10 I = 1,NINCX,INCX
     SX(I) = SA*SX(I)
10 CONTINUE
   RETURN
C
C           CODE FOR INCREMENT EQUAL TO 1
C
C           CLEAN-UP LOOP

```

```

20 M = MOD(N,5)
   IF( M .EQ. 0 ) GO TO 40
   DO 30 I = 1,M
     SX(I) = SA*SX(I)
30 CONTINUE
   IF( N .LT. 5 ) RETURN
40 MP1 = M + 1
   DO 50 I = MP1,N,5
     SX(I) = SA*SX(I)
     SX(I + 1) = SA*SX(I + 1)
     SX(I + 2) = SA*SX(I + 2)
     SX(I + 3) = SA*SX(I + 3)
     SX(I + 4) = SA*SX(I + 4)
50 CONTINUE
   RETURN
   END
   REAL FUNCTION SDOT(N, SX, INCX, SY, INCY)

C
C   FORMS THE DOT PRODUCT OF TWO VECTORS.
C   USES UNROLLED LOOPS FOR INCREMENTS EQUAL TO ONE.
C   JACK DONGARRA, LINPACK, 3/11/78.
C
   REAL SX(1), SY(1), STEMP
   INTEGER I, INCX, INCY, IX, IY, M, MP1, N

C
   STEMP = 0.0E0
   SDOT = 0.0E0
   IF(N.LE.0)RETURN
   IF(INCX.EQ.1.AND.INCY.EQ.1)GO TO 20

C
C   CODE FOR UNEQUAL INCREMENTS OR EQUAL INCREMENTS
C   NOT EQUAL TO 1
C
   IX = 1
   IY = 1
   IF(INCX.LT.0)IX = (-N+1)*INCX + 1
   IF(INCY.LT.0)IY = (-N+1)*INCY + 1
   DO 10 I = 1,N
     STEMP = STEMP + SX(IX)*SY(IY)
     IX = IX + INCX
     IY = IY + INCY
10 CONTINUE
   SDOT = STEMP
   RETURN

C
C   CODE FOR BOTH INCREMENTS EQUAL TO 1
C
C   CLEAN-UP LOOP
C
20 M = MOD(N,5)
   IF( M .EQ. 0 ) GO TO 40
   DO 30 I = 1,M

```

```

      STEMP = STEMP + SX(I)*SY(I)
30  CONTINUE
      IF( N .LT. 5 ) GO TO 60
40  MP1 = M + 1
      DO 50 I = MP1,N,5
          STEMP = STEMP + SX(I)*SY(I) + SX(I + 1)*SY(I + 1) +
          * SX(I + 2)*SY(I + 2) + SX(I + 3)*SY(I + 3) + SX(I + 4)*SY(I + 4)
50  CONTINUE
60  SDOT = STEMP
      RETURN
      END
      SUBROUTINE SAXPY(N, SA, SX, INCX, SY, INCY)
C
C      CONSTANT TIMES A VECTOR PLUS A VECTOR.
C      USES UNROLLED LOOP FOR INCREMENTS EQUAL TO ONE.
C      JACK DONGARRA, LINPACK, 3/11/78.
C
      REAL SX(1),SY(1),SA
      INTEGER I, INCX, INCY, IX, IY, M, MP1, N
C
      IF(N.LE.0)RETURN
      IF (SA .EQ. 0.0) RETURN
      IF(INCX.EQ.1.AND.INCY.EQ.1)GO TO 20
C
C      CODE FOR UNEQUAL INCREMENTS OR EQUAL INCREMENTS
C      NOT EQUAL TO 1
C
      IX = 1
      IY = 1
      IF(INCX.LT.0)IX = (-N+1)*INCX + 1
      IF(INCY.LT.0)IY = (-N+1)*INCY + 1
      DO 10 I = 1,N
          SY(IY) = SY(IY) + SA*SX(IX)
          IX = IX + INCX
          IY = IY + INCY
10  CONTINUE
      RETURN
C
C      CODE FOR BOTH INCREMENTS EQUAL TO 1
C
C      CLEAN-UP LOOP
C
20  M = MOD(N,4)
      IF( M .EQ. 0 ) GO TO 40
      DO 30 I = 1,M
          SY(I) = SY(I) + SA*SX(I)
30  CONTINUE
      IF( N .LT. 4 ) RETURN
40  MP1 = M + 1
      DO 50 I = MP1,N,4
          SY(I) = SY(I) + SA*SX(I)
          SY(I + 1) = SY(I + 1) + SA*SX(I + 1)

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      SY(I + 2) = SY(I + 2) + SA*SX(I + 2)
      SY(I + 3) = SY(I + 3) + SA*SX(I + 3)
50  CONTINUE
      RETURN
      END
      SUBROUTINE SROTG(SA, SB, C, S)
C
C   CONSTRUCT GIVENS PLANE ROTATION.
C   JACK DONGARRA, LINPACK, 3/11/78.
C
      REAL SA, SB, C, S, ROE, SCALE, R, Z
C
      ROE = SB
      IF( ABS(SA) .GT. ABS(SB) ) ROE = SA
      SCALE = ABS(SA) + ABS(SB)
      IF( SCALE .NE. 0.0 ) GO TO 10
         C = 1.0
         S = 0.0
         R = 0.0
         GO TO 20
10  R = SCALE*SQRT((SA/SCALE)**2 + (SB/SCALE)**2)
      R = SIGN(1.0, ROE)*R
      C = SA/R
      S = SB/R
20  Z = 1.0
      IF( ABS(SA) .GT. ABS(SB) ) Z = S
      IF( ABS(SB) .GE. ABS(SA) .AND. C .NE. 0.0 ) Z = 1.0/C
      SA = R
      SB = Z
      RETURN
      END
      SUBROUTINE SROT (N, SX, INCX, SY, INCY, C, S)
C
C   APPLIES A PLANE ROTATION.
C   JACK DONGARRA, LINPACK, 3/11/78.
C
      REAL SX(1), SY(1), STEMP, C, S
      INTEGER I, INCX, INCY, IX, IY, N
C
      IF(N.LE.0)RETURN
      IF(INCX.EQ.1.AND.INCY.EQ.1)GO TO 20
C
C   CODE FOR UNEQUAL INCREMENTS OR EQUAL INCREMENTS NOT EQUAL
C   TO 1
C
      IX = 1
      IY = 1
      IF(INCX.LT.0)IX = (-N+1)*INCX + 1
      IF(INCY.LT.0)IY = (-N+1)*INCY + 1
      DO 10 I = 1, N
         STEMP = C*SX(IX) + S*SY(IY)
         SY(IY) = C*SY(IY) - S*SX(IX)
         SX(IX) = STEMP

```

```

      IX = IX + INCX
      IY = IY + INCY
10  CONTINUE
      RETURN

C
C      CODE FOR BOTH INCREMENTS EQUAL TO 1
C
20  DO 30 I = 1,N
      STEMP = C*SX(I) + S*SY(I)
      SY(I) = C*SY(I) - S*SX(I)
      SX(I) = STEMP
30  CONTINUE
      RETURN
      END
      SUBROUTINE SSWAP (N,SX,INCX,SY,INCY)

C
C      INTERCHANGES TWO VECTORS.
C      USES UNROLLED LOOPS FOR INCREMENTS EQUAL TO 1.
C      JACK DONGARRA, LINPACK, 3/11/78.
C
      REAL SX(1),SY(1),STEMP
      INTEGER I,INCX,INCY,IX,IY,M,MP1,N

C
      IF(N.LE.0)RETURN
      IF(INCX.EQ.1.AND.INCY.EQ.1)GO TO 20

C
C      CODE FOR UNEQUAL INCREMENTS OR EQUAL INCREMENTS NOT EQUAL
C      TO 1
C
      IX = 1
      IY = 1
      IF(INCX.LT.0)IX = (-N+1)*INCX + 1
      IF(INCY.LT.0)IY = (-N+1)*INCY + 1
      DO 10 I = 1,N
          STEMP = SX(IX)
          SX(IX) = SY(IY)
          SY(IY) = STEMP
          IX = IX + INCX
          IY = IY + INCY
10  CONTINUE
      RETURN

C
C      CODE FOR BOTH INCREMENTS EQUAL TO 1
C
C
C      CLEAN-UP LOOP
C
20  M = MOD(N,3)
      IF( M .EQ. 0 ) GO TO 40
      DO 30 I = 1,M
          STEMP = SX(I)
          SX(I) = SY(I)
          SY(I) = STEMP

```

```
30 CONTINUE
  IF( N .LT. 3 ) RETURN
40 MP1 = M + 1
  DO 50 I = MP1,N,3
    STEMP = SX(I)
    SX(I) = SY(I)
    SY(I) = STEMP
    STEMP = SX(I + 1)
    SX(I + 1) = SY(I + 1)
    SY(I + 1) = STEMP
    STEMP = SX(I + 2)
    SX(I + 2) = SY(I + 2)
    SY(I + 2) = STEMP
50 CONTINUE
  RETURN
  END
```

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