### Studies of Coercive Force of Permanent Magnet Materials

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Post Office Box 7711
Research Triangle Park, NC 27709

**Report Date:**
31 January, 1984

**Number of Pages:**
12

**Type of Report & Period Covered:**
Final Report
1/1/83 - 31/12/83

**Contract or Grant Number(s):**
DAAG29-83-K-0024

**Distribution Statement:**
Approved for public release: distribution unlimited.

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**Abstract:**
Permanent magnets were prepared by sintering on-stoichiometry Sm$_{2}$Co$_{17}$ and Sm$_{2}$Co$_{17}$ doped with Fe, Mn, Zr, and Hf. Coercive forces ($H_C$) were low, < 1 kOe. Although doping increases anisotropy field, it does not enhance $H_C$ except for Mn as dopant. In this case, doping increases $H_C$ about two-fold. In these systems $H_C$ seems to be nucleation-controlled. It is postulated that nucleation occurs at the oxidized surface where anisotropy is weak or negative. Surfaces were investigated by Auger spectroscopy with results consistent with the postulated mechanism. To test for effects of surface roughness, powders were washed with acid. No increase.

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**Key Words:**
Subscript H, Subscript C, Thickness.
In $\mu_{\text{r}}$ was observed. Samples ground under pentane and liquid nitrogen showed no significant difference in $\mu_{\text{r}}$. Oxygen content was about 3000 ppm by weight in the finished magnets. Results suggest that coercive force of the so-called 2-17 (which are actually 2-phase mixtures of components with 1:5 and 2:17 stoichiometry) originates with the component having 1:5 stoichiometry.
Studies of Coercive Force of Rare Earth Permanent Magnet Materials

by

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FINAL REPORT
January 31, 1984
to
U.S. Army Research Office

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I. Introduction

The so-called 2:17 rare earth-cobalt magnets are actually polycomponent, polyphase systems. Typically these are represented by the formula \( \text{Sm(Co,Fe,Mn,Cu,Zr)}_z \) with \( z \) equalling approximately 7.2. The material consists primarily (if not exclusively) of a 1:5 phase and a 2:17 phase. The composition of the phases and the roles of the various components is currently a topic of active inquiry. The origin of the large coercive force of these materials, which gives rise to their high energy product (> 30 MGOe) is unclear. It is evident that elucidating the mechanism governing coercive force is virtually impossible in such a complex system.

In the present program, on-stoichiometry \( \text{Sm}_2\text{Co}_{17} \) together with \( \text{Sm}_2(\text{Co}_{1-x}M_x)_{17} \) ternary alloys have been studied to obtain information in regard to the coercive force of (1) single phase 2:17 stoichiometry materials and (2) the effect of dopants \( M \) where \( M = \text{Mn,Fe,Zr and Hf} \). In addition, the effect of acid washes of ball-milled powder and grinding under liquid nitrogen were investigated, the former to remove sharp points and the latter to suppress oxidation. The existence of surface disturbances - sharp points (roughness) - or oxidation facilitates nucleation of inverse domains and hence degrades coercive force.

II. Experimental Results

A. Properties of Pure \( \text{Sm}_2\text{Co}_{17} \)

This is easily prepared by melting pure Sm and Co together in the proper proportions. High purity Sm obtained from the Ames laboratory was used. The structure of the \( \text{Sm}_2\text{Co}_{17} \) was rhombohedral with lattice constants as follows:

<table>
<thead>
<tr>
<th></th>
<th>This work</th>
<th>Literature (average)</th>
</tr>
</thead>
<tbody>
<tr>
<td>( a_0(\text{Å}) )</td>
<td>8.402 ± 0.005</td>
<td>8.408 ± 0.03</td>
</tr>
<tr>
<td>( c_0(\text{Å}) )</td>
<td>12.216 ± 0.008</td>
<td>12.212 ± 0.024</td>
</tr>
</tbody>
</table>
The room temperature magnetic properties determined were as follows:

<table>
<thead>
<tr>
<th>Property</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Saturation magnetization</td>
<td>$113.5 \pm 1.5$ emu/g, $26.5 \pm 0.3$ $\mu_B$ /f.u.</td>
</tr>
<tr>
<td>Anisotropy field</td>
<td>$60.0 \pm 1.6$ kOe</td>
</tr>
<tr>
<td>Curie temperature</td>
<td>$920 \pm 2.5$°C</td>
</tr>
<tr>
<td>$4\pi M_0$</td>
<td>$12.4$ kG</td>
</tr>
<tr>
<td>$(BH)_{max}$</td>
<td>$38.4$ MGoe</td>
</tr>
</tbody>
</table>

The intrinsic coercive force ($H_C$) of Sm$_2$Co$_{17}$ is shown in Figs. 1 and 2. It is dependent upon the time of ball milling and the sintering temperature employed to make the sintered compacts. Ball milling was done under a saturated hydrocarbon. $H_C$ values are seen to be quite small, ranging from $< 100$ Oe to $\sim 650$ Oe. These values were not increased by ball-milling under liquid nitrogen or by the acid washes. As indicated in the Introduction, liquid nitrogen ball milling was employed in an attempt to reduce oxidation of the material during ball-milling. It is felt that oxidation is deleterious to $H_C$ for reasons set forth below in Section III.

The beneficial effects of increased ball-milling time is ascribed to a better particle size achieved using longer milling times. In samples milled for only 5 hours there were many particles exceeding 10 μm in size. These large particles were fewer in number in samples milled for 19 hours. However, in both cases oxidation was extensive. The finished sintermagnets contained $\sim 3500$ ppm oxygen, about 200-fold greater than in the starting materials.

B. Properties of Doped Sm$_2$Co$_{17}$

In numerous studies from this laboratory, R$_2$Co$_{17}$ systems have been doped with Cr, Mn, Fe, Ni, Cu, Ti, Zr, Hf and V and studied magnetically. Curie temperatures, saturation magnetization and anisotropy fields have been determined as a function of the amount of dopant, i.e., the amount of transition element from the above group which has been substituted for cobalt. It has been found that most of the dopants increase $H_A$, the anisotropy field. Zr was found to be
One of the features needed in a high energy magnet is a large coercive force. This may or may not develop out of a large $H_A$. In the present study the effect of dopants Mn, Fe, Zr and Hf on $H_C$ was examined. Results are shown in Figs. 3-5. The data show that Fe, Zr or Hf as substituents have little effect on coercive force, but replacement of Co by Mn (see Fig. 4) sharply enhances coercive force. Thus the special effect of Zr in augmenting $H_A$ does not carry over into an enhanced $H_C$.

III. Surface Features and Coercive Force

If the Stoner-Wohlfarth coherent rotation model were valid, intrinsic coercive force would be identical with the anisotropy field, $H_A$. Since $H_A$ is $\sim 60$ kOe for Sm$_2$Co$_{17}$, $H_C$ via this model would be $\sim 60$ kOe. Instead (see Figs. 1 and 2), it is 0.1 to 0.3 kOe, smaller by a factor $\geq 200$. Obviously, magnetization reversal takes place more readily than expected by the Stoner-Wohlfarth model. It seems to occur via a nucleation and growth model. Thus, $H_C$ may be controlled either by nucleation or by pinning of domain walls. If nucleation occurs easily, wall pinning will control $H_C$. It appears that nucleation is very easy for Sm$_2$Co$_{17}$ (and also wall pinning is weak).

The author holds the view that nucleation occurs at or near the surface of Sm$_2$Co$_{17}$. Auger spectroscopy measurements show for this material that the top 30 Å (≈ 10 atom layers) is heavily oxidized. This region, characterized as Sm$_x$Co$_y$O$_z$, bears only slight structural resemblance to the limiting cases Sm$_2$Co$_{17}$ (i.e., $x = 2$, $y = 17$, $z = 0$) and Sm$_2$O$_3$ (i.e., $x = 2$, $y = 0$, $z = 3$). Sm and Co in these cases will not exhibit their normal single-ion anisotropy characteristics, i.e., strongly uniaxial. Instead, as shown by Jin, Sm may exhibit weak uniaxial anisotropy or even planar anisotropy. At these points, nuclei of inverse domains could easily form and then sweep through the sample, giving rise to the low observed coercive force.
Studies on LaCo₅ and PrCo₅ support the ideas advanced in the preceding paragraph. LaCo₅ magnets exhibit $H_c$ of about 9 kOe, whereas PrCo₅ can seldom be formed with $H_c$ greater than 4 kOe. Auger spectroscopy shows that PrCo₅ is more heavily oxidized at the surface than LaCo₅.

Since oxidation produces the regions where nucleation occurs, it follows that oxidation is deleterious for $H_c$.

IV. The Coercive Force Mechanism

Ideas expressed in the preceding section, while seeming reasonable, are speculative. In the continuation work supported by the ARO at Carnegie-Mellon University it is hoped to subject these ideas to experimental test. The mechanism governing coercive force of rare earth-cobalt permanent magnet materials is a matter of acute controversy, and the mechanism proposed by the author is just one of the mechanisms proposed.

Some support for the author's ideas is provided by the results obtained for Sm₂Co₁₆.₅Mn₅. This is the only ternary for which $H_c$ substantially exceeded that of Sm₂Co₁₇. Doping with Fe, Hf or Zr left $H_c$ unmodified. In extensive studies of polycomponent systems containing Mn, it is found that Mn segregates to the surface. If the surface is important for determining $H_c$, it is to be expected that Mn doping will be effective in modifying $H_c$.

If coercive force can be understood and controlled, it will be an advance of the first rank in regard to rare earth-cobalt permanent magnet materials. Many materials are known with energy products ≥ 50 MGOe. These energy products could be realized experimentally if $H_c > 13$ kOe could be achieved.
V. Personnel Involved

W. E. Wallace, Principal Investigator
E. Schwab, Research Associate
F. Pourarian, Research Assistant Professor
K. Smith, Research Associate
L. Linck, Secretary
E. Boltich, Graduate Student

VI. Degrees Earned

E. Boltich, Ph.D. degree

VII. References


14. K. Inomata, "Individual Co Site Contributions to the Magnetic Anisotropy and NMR Investigation of Y$_2$(Co$_{1-x}$M$_x$)$_{17}$ (M = Cu,Al)," ibid., B23, 2076 (1981).

15. H. M. Jin et al., "Magnetic Anisotropy of Sm$^{3+}$ Near Point Defects in SmCo$_5$ and Sm$_3$Co$_{17}$," Proc. of the 6th International Workshop on Rare Earth-Cobalt Permanent Magnets and Their Applications, held in Baden, Austria, August 31 -September 2, 1982, J. Fidler, Editor, p. 549.

Fig. 1 Influence of time of ball milling on $H_c^1$ for finished magnet.
( ) gives the density in g/ml.

19 hrs. ball milling

5 hrs. ball milling

Sintering Temp. (°C)
Fig. 2 Intrinsic coercive force vs. sintering temperature for Sm$_2$Co$_{17}$ magnets. All alloys ball milled under toluene for 4-5 hrs. at 300°K, unless stated otherwise.

- Sm$_{2.08}$Co$_{17}$, annealed 1 h at 1200°C
- Sm$_{2.09}$Co$_{17}$, annealed 1 h at 1200°C
  no liquid during milling
- Sm$_{2.24}$Co$_{17}$, annealed 1 wk at 1130°C
- Sm$_{2.25}$Co$_{17}$, used as cast
- Sm$_{2.03}$Co$_{17}$, annealed 1 h at 1200°C
- Sm$_{2.02}$Co$_{17}$, annealed 1 h at 1200°C
  ball milled without liquid at 77°K
Fig. 3  Intrinsic coercive force of Sm$_2$Co$_{17}$ and Sm$_2$Co$_{16}$Fe magnets vs. sintering temperature.
Fig. 4  Intrinsic coercive force of $\text{Sm}_2\text{Co}_{17}$ and $\text{Sm}_2\text{Co}_{16.5}\text{Mn}_{0.5}$ vs. sintering temperature.

$\text{Sm}_{2.15}\text{Co}_{16.5}\text{Mn}_{0.5}$ ball milled 22 hrs. under pentane.

$\text{Sm}_{2.25}\text{Co}_{17}$ ball milled 19 hrs. under pentane
Fig. 5 Intrinsic coercive force of Sm$_2$Co$_{17-x}$Zr$_x$(Hf)$_x$ magnets versus sintering temperature. Sm$_2$Co$_{16.5}$Zr$_{0.5}$ (o); Sm$_2$Co$_{16.8}$Zr$_{0.2}$ (o); Sm$_2$Co$_{16.7}$Hf$_{0.3}$ (x).

Initial alloy contained Sm excess for oxidation compensation.

No excess Sm in initial alloy.

<table>
<thead>
<tr>
<th>Sm$<em>2$Co$</em>{16.5}$Zr$_{0.5}$</th>
<th>892</th>
</tr>
</thead>
<tbody>
<tr>
<td>Sm$<em>2$Co$</em>{16.8}$Zr$_{0.2}$</td>
<td>885 ($H_A = 78.6$ kOe)</td>
</tr>
<tr>
<td>Sm$<em>2$Co$</em>{16.7}$Hf$_{0.3}$</td>
<td>885 ($H_A = 66.6$ kOe)</td>
</tr>
</tbody>
</table>

(All values determined on sintered magnets.)