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MODELS OF WEATHER ENVIRONMENTS ADVERSE TO ELECTRO-OPTICAL SYSTEMS--ETC(U)

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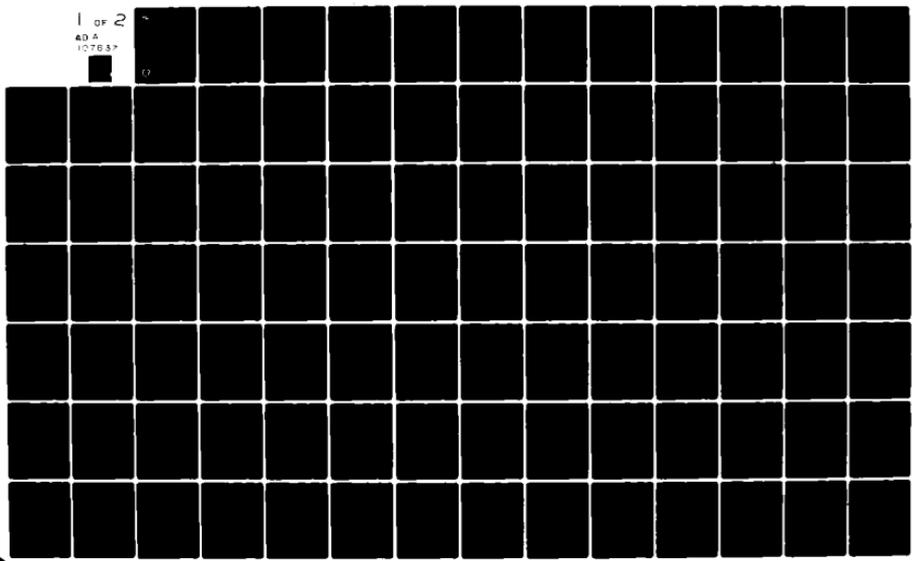
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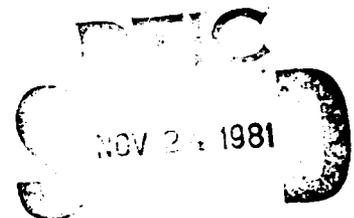
**MODELS OF WEATHER ENVIRONMENTS ADVERSE  
TO ELECTRO-OPTICAL SYSTEMS**

SEPTEMBER 1981

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Contract Monitor: Ronald M. Cionco

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US Army Electronics Research and Development Command

**Atmospheric Sciences Laboratory**

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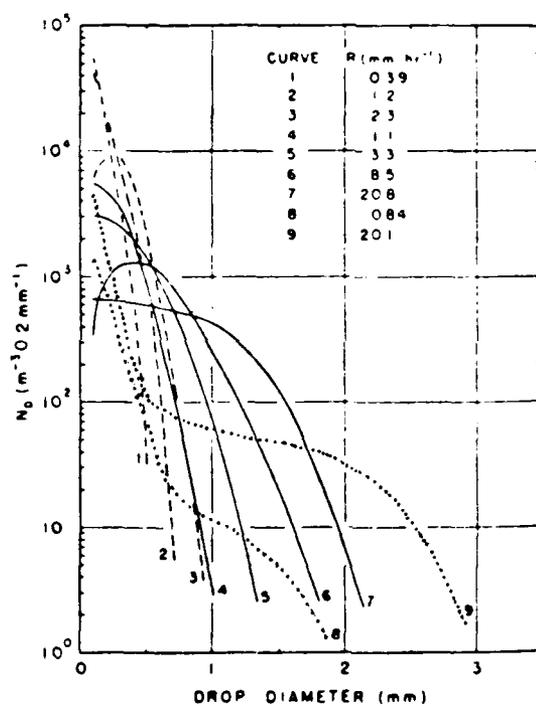


Fig. 20 Variety of Raindrop Size Distributions

TABLE 7. MODERATE RAIN (6 MM/HR) FOR SUMMER MID-LATITUDES

RAIN MODEL	ATMOSPHERE	MODERATE RAIN - 6 MM/HR		45 N MODEL - MID-LATITUDE	
HEIGHT (KM)	PRESSURE (MB)	TEMPERATURE (DEG K)	RELATIVE HUMIDITY	CLOUD CONTENT (GM/CM <sup>3</sup> )	RAIN RATE (MM/HR)
0.000	1013.00	287.20	1.000	0.0000	6.000
.250	983.00	286.20	1.000	.2000	5.500
.500	954.00	285.10	1.000	.2800	4.400
.750	925.00	284.00	1.000	.3200	3.500
1.000	899.00	282.70	1.000	.3300	3.000
1.250	872.00	281.20	1.000	.3400	2.400
1.500	846.00	280.00	1.000	.3500	1.900
1.750	820.00	278.50	1.000	.3500	1.500
2.000	795.00	277.30	1.000	.3500	1.100
2.500	747.00	274.40	1.000	.3500	.600
3.000	701.00	271.20	1.000	.3500	.200
3.500	658.00	268.50	1.000	.3100	-0.000
4.000	616.00	265.00	1.000	.2500	-0.000
4.500	577.00	261.00	1.000	.1800	-0.000
5.000	540.00	258.00	1.000	.1300	-0.000
5.500	505.00	254.50	1.000	.0900	-0.000
6.000	472.00	251.50	1.000	.0500	-0.000
6.500	440.00	248.20	1.000	.0300	-0.000
7.000	410.00	242.20	1.000	.0100	-0.000
7.500	382.00	238.00	1.000	-0.0000	-0.000
8.000	356.00	234.50	1.000	-0.0000	-0.000
8.500	330.00	229.00	1.000	-0.0000	-0.000
9.000	307.00	225.00	.980	-0.0000	-0.000
9.500	285.00	220.00	.950	-0.0000	-0.000
10.000	264.00	223.20	.850	-0.0000	-0.000
11.000	226.00	216.70	.400	-0.0000	-0.000
12.000	193.00	216.70	.160	-0.0000	-0.000
13.000	165.00	216.70	.060	-0.0000	-0.000
14.000	141.00	216.70	.041	-0.0000	-0.000
15.000	120.00	216.70	.031	-0.0000	-0.000
16.000	103.00	216.70	.023	-0.0000	-0.000
17.000	87.98	216.70	.019	-0.0000	-0.000
18.000	75.00	216.70	.016	-0.0000	-0.000
19.000	64.10	216.70	.014	-0.0000	-0.000
20.000	54.70	216.70	.012	-0.0000	-0.000
22.000	40.00	218.70	.007	-0.0000	-0.000
24.000	29.30	220.70	.004	-0.0000	-0.000
26.000	21.50	222.70	.002	-0.0000	-0.000
28.000	15.70	224.70	.001	-0.0000	-0.000
30.000	1.70	226.70	-0.000	-0.0000	-0.000
35.000	5.60	237.00	-0.000	-0.0000	-0.000
40.000	2.80	251.00	-0.000	-0.0000	-0.000
45.000	.40	265.00	-0.000	-0.0000	-0.000
50.000	.80	270.70	-0.000	-0.0000	-0.000

TABLE 8. HEAVY RAIN (15 MM/HR) FOR MID-LATITUDES

RAIN MODEL	ATMOSPHERE	HEAVY RAIN - 15 MM/HR		45 N MODEL - MID-LATITUDE	
HEIGHT (KM)	PRESSURE (MB)	TEMPERATURE (DEG K)	RELATIVE HUMIDITY	CLOUD CONTENT (GM/CM <sup>3</sup> )	RAIN RATE (MM/HR)
0.000	1013.00	287.20	1.000	0.0000	15.000
.250	983.00	286.20	1.000	.3000	14.600
.500	954.00	285.10	1.000	.4300	14.300
.750	925.00	284.00	1.000	.4300	13.900
1.000	899.00	282.70	1.000	.4500	13.500
1.250	872.00	281.20	1.000	.4500	13.200
1.500	846.00	280.00	1.000	.4500	12.900
1.750	820.00	278.50	1.000	.4500	12.600
2.000	795.00	277.30	1.000	.4500	12.300
2.500	747.00	274.40	1.000	.4500	11.600
3.000	701.00	271.20	1.000	.4500	11.100
3.500	658.00	268.50	1.000	.4500	10.700
4.000	616.00	265.00	1.000	.4500	10.300
4.500	577.00	261.00	1.000	.4500	10.000
5.000	540.00	258.00	1.000	.4500	9.700
5.500	505.00	254.50	1.000	.4500	9.500
6.000	472.00	251.50	1.000	.4500	9.300
6.500	440.00	248.20	1.000	.4500	9.100
7.000	410.00	242.20	1.000	.4500	8.900
7.500	382.00	238.00	1.000	.4500	8.700
8.000	356.00	234.50	1.000	.4500	8.500
8.500	330.00	229.00	1.000	.4500	8.300
9.000	307.00	225.00	.980	.4500	8.100
9.500	285.00	220.00	.950	.4500	7.900
10.000	264.00	223.20	.850	.4500	7.700
11.000	226.00	216.70	.400	.4500	7.500
12.000	193.00	216.70	.160	.4500	7.300
13.000	165.00	216.70	.060	.4500	7.100
14.000	141.00	216.70	.041	.4500	6.900
15.000	120.00	216.70	.031	.4500	6.700
16.000	103.00	216.70	.023	.4500	6.500
17.000	87.98	216.70	.019	.4500	6.300
18.000	75.00	216.70	.016	.4500	6.100
19.000	64.10	216.70	.014	.4500	5.900
20.000	54.70	216.70	.012	.4500	5.700
22.000	40.00	218.70	.007	.4500	5.500
24.000	29.30	220.70	.004	.4500	5.300
26.000	21.50	222.70	.002	.4500	5.100
28.000	15.70	224.70	.001	.4500	4.900
30.000	1.70	226.70	-0.000	.4500	4.700
35.000	5.60	237.00	-0.000	.4500	4.500
40.000	2.80	251.00	-0.000	.4500	4.300
45.000	.40	265.00	-0.000	.4500	4.100
50.000	.80	270.70	-0.000	.4500	3.900

TABLE 9. HEAVY RAIN (15 MM/HR) FOR TROPICAL LATITUDES

TROPICAL - 15 N HEAVY RAIN OF 15 MM/HR					
HEIGHT (KM)	PRESSURE (MB)	TEMPERATURE (DEG K)	RELATIVE HUMIDITY	CLOUD CONTENT (GM/CM <sup>3</sup> )	RAIN RATE (MM/HR)
0.000	1013.00	298.00	.900	-0.0000	15.000
.250	985.00	297.20	1.000	.2000	14.500
.500	957.00	296.00	1.000	.3500	14.000
.750	930.00	295.00	1.000	.4000	13.500
1.000	904.00	293.00	1.000	.4500	13.000
1.250	878.00	291.10	1.000	.4500	12.600
1.500	853.00	292.60	1.000	.4500	12.200
1.750	828.00	291.40	1.000	.4500	11.900
2.000	804.00	269.50	1.000	.4500	11.600
2.500	758.00	287.10	1.000	.4500	11.000
3.000	714.00	285.10	1.000	.4500	10.500
3.500	672.00	282.00	1.000	.4500	10.200
4.000	632.00	280.60	1.000	.4500	9.900
4.500	594.00	278.00	1.000	.4500	9.700
5.000	558.00	275.40	1.000	.4500	9.500
5.500	524.00	273.00	1.000	.4500	9.300
6.000	491.00	270.20	1.000	.4500	9.100
6.500	460.00	267.20	1.000	.4400	8.900
7.000	431.00	264.30	1.000	.3600	8.700
7.500	403.00	261.20	1.000	.3000	8.500
8.000	376.00	257.80	1.000	.2500	8.300
8.500	351.00	254.40	1.000	.1900	8.100
9.000	328.00	251.00	1.000	.1400	7.900
9.500	305.00	248.00	1.000	.0800	7.700
10.000	284.00	242.90	1.000	.0300	7.500
11.000	247.00	234.80	1.000	.0200	7.300
12.000	211.00	235.60	1.000	.0100	7.100
13.000	181.00	216.20	1.000	-0.0000	6.900
14.000	154.00	206.30	1.000	-0.0000	6.700
15.000	131.00	196.50	1.000	-0.0000	6.500
16.000	110.00	192.60	.600	-0.0000	6.300
17.000	92.30	194.80	.350	-0.0000	6.100
18.000	77.60	198.80	.120	-0.0000	5.900
19.000	65.50	202.90	.055	-0.0000	5.700
20.000	55.50	206.70	.025	-0.0000	5.500
22.000	40.10	214.80	.008	-0.0000	5.300
24.000	29.30	219.20	.002	-0.0000	5.100
26.000	21.50	223.60	.001	-0.0000	4.900
28.000	16.90	227.70	-0.000	-0.0000	4.700
30.000	11.80	232.40	-0.000	-0.0000	4.500
35.000	5.84	245.00	-0.000	-0.0000	4.300
40.000	2.79	258.50	-0.000	-0.0000	4.100
45.000	1.58	269.00	-0.000	-0.0000	3.900
50.000	.86	273.00	-0.000	-0.0000	3.700

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number)  Weather models are developed to depict hour by hour variations of scattering media--the atmosphere--important to Army electro-optical system performance. Dynamic models are presented for specifying particle size distributions in horizontal and vertical directions for haze, fog, cloud, and rain conditions given only routinely available meteorological data. Case studies show that these models perform well individually and when used together. This effort should be viewed as the first step in developing dynamic models that are		



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## I INTRODUCTION

### 1.1 GENERAL

#### 1.1.1 Contract/Scope

This work was accomplished under Contract Number DAAD07-80-C-1147 with the U.S. Army White Sands Missile Range. The contract became effective on 7 February 1980 and constituted less than one half man year of technical effort. The Contracting Officer's Technical Representative is:

Mr. Ronald Cionco  
Atmospheric Sciences Laboratory  
Attn: DELAS-BE-C  
White Sands Missile Range, NM 88002

### 1.1.2 Overview

Environmental conditions often dictate effectiveness of Army offensive and defensive weapon systems. Such things as terrain, vegetation, and weather determine in what direction, how far, and what degree of clarity a target can be acquired, isolated, and distinguished from its surroundings. For a particular season and theater of operation, weather offers the greatest day to day change that influences weapon system performance. Studies are being conducted to develop techniques to determine "seeability" or obscuration from natural as well as battlefield induced contaminants. Considerable attention is being directed towards electro-optical (EO) energy absorption due to gaseous molecules, scattering due to haze, smoke, fog, cloud, rain, snow or hail, and beam wandering due to small scale turbulence and temperature fluctuations. Obscuration due to scattering, however, depends greatly upon the energy wavelength of the viewing sensor relative to type, number and size distribution of atmospheric litho- and hydrometeors.

The scattering process itself behaves nonlinearly and, by necessity, obscuration models must consider such meteorological microphysical features as number concentration and size distribution of particles. It is unreasonable to expect observations of these microphysical features within a battlefield environment. Thus it becomes necessary to work within the scope of routinely available weather information to infer the microfea-

tures and to define the actual scattering medium. Geo-Atmospherics Corporation has developed weather models to depict hour by hour variations of scattering media important to Army weapon system performance.

Better instruments and experimental data gathering programs are necessary to establish reliable data bases of atmospheric microphysical features of liquid and solid particles associated with the wide range of possible global weather. These data must have the accuracy demanded for basic studies on their impact on design and operation of EO systems. To date, a number of static models have been developed to represent atmospheric particles for a particular type of environment. For example, aerosol models have been generated to represent "typical" conditions expected to be found in Continental or maritime regions or at different levels in the atmosphere. Some of these models are:

- A. Rural Model - which is to represent the natural midlatitude environment found in the country or in clean air urban regions found after a cold front passage.
- B. Urban Model - which is to represent the industrial aerosols found in cities and in rural regions experiencing air stagnation and subsequent air pollution build-up.
- C. Maritime Model - which is to represent the open ocean regions at least 300 km offshore with a moderate surface air wind speed.

- D. Tropospheric Model - which is to normally represent the turbulent layer of the atmosphere between the top of the boundary layer (about 2 km) and the tropopause (2 to 18 km, depending upon season and, to a greater extent, latitude) as well as those special boundary layer cases when the surface air layer over land is calm and clean (meteorological range greater than 40 km).
- E. High Level Models - which is to represent aerosol distributions within the stable stratosphere (from the tropopause to about 20 km) and the mesosphere (from the top of the stratosphere to about 80 km).

Similar types of static models have been developed for fog, cloud, and rain conditions. The atmosphere is, however, a fluid in motion that produces continuous rather than discrete spectrums.

What we have done here is to take the first step in developing dynamic models that relate particle type, concentration, size distribution, and their vertical variation to observed dynamics and thermodynamics of the atmosphere that exist at any instant in time. A ground rule established was that only routinely available standard surface and upper air observations and/or forecasts would be available for use in a real-world battlefield environment. As such, a number of simplifying assumptions had to be made, to use meso and synoptic scale data to depict microscale features. Not all gaps were closed and much remains to be done but significant advances

were made in dynamically modeling litho- and hydro-meters important to operational performance of Electro - Optical Systems.

## 1.2 MODELING EQUATIONS

### 1.2.1 General

There is no question that adverse weather is detrimental to electromagnetic energy propagation. Theoretical and application techniques have been developed to simulate atmospheric radiative transfer effects to derive obscuration expected for any sensor. What is required is a quantitative description of the scattering medium that is needed in order to be able to derive obscuration. The problem is how to map three dimensional distributions of microphysical scattering media given only routinely available surface and upper air meteorological information.

Before discussing the techniques used to develop the dynamical models for fog, cloud, and rain conditions, it is worthwhile to consider the different characteristics associated with the two most popular analytical methods used to depict particle size distributions, namely the power law and the exponential (modified gamma) equations. The equations will be presented and discussed to show shapes and characteristics responsive to the wide variety of atmospheric particles. For the purposes of this study the particle sizes vary by six orders of magnitude. Each type of particle has a typical mode radius and range of values, as shown in Table I. Although size distributions vary within each category which must be considered, it is equally important to develop modeling schemes that account for the extreme variations among different meteorological events.

TABLE 1 Typical Atmospheric Particle Sizes

Particle Type	Mode Radius micrometers	Radius Range micrometers
Continental Aerosols	0.02	.002 - 20
Maritime Aerosols	0.2	.02 - 20
New Fog ( 1 hr )	4	1 - 40
Old (Evolved) Fog ( 2 hr )	10	1 - 80
Fair Weather Cumulus	3.5	1 - 10
Stratus/Stratocumulus	4	1 - 15
Altostratus	5	1 - 18
Nimbostratus	5	1 - 40
Cumulonimbus	6	1 - 100
Mist (0.05 mm/hr)	75	6 - 550
Drizzle (0.25 mm/hr)	150	6 - 750
Light Rain (1 mm/hr)	175	6 - 1250
Moderate Rain (4 mm/hr)	200	6 - 1750
Heavy Rain (16 mm/hr)	225	6 - 2250

### 1.2.2 Power Law Size Distribution

One of the most popular methods in use today to represent solid aerosols in the atmosphere was developed by Junge in 1958. From many of his aerosol measurement studies he found the concentration peaked at a radius of about  $0.02 \mu\text{m}$  but remained linearly distributed between about  $0.1$  to  $10 \mu\text{m}$ , when plotted on a log log scale. This linear range covers the most optically interesting phenomena in a hazy atmosphere. The smaller aerosols in this range provide a bluish tinge to thin haze, those around  $0.3 \mu\text{m}$  are most important in determining what we call visibility in haze, and the larger aerosols, which are fewer in number, can provide beautiful red sunsets. Therefore, Junge's power law representation of aerosol size distribution and concentration is very appropriate in defining  $E_0$  responses to haze and it is simple to derive from measured data and simple to use.

Junge's power - law size distribution function is:

$$n(r) = \frac{dN}{d \log r} = C r^{-v} \quad (1)$$

where  $n(r)$  is the number of particles per unit interval of radius and per unit volume,  $C$  is the surface air particle concentration factor,  $r$  is the aerosol radius in  $\mu\text{m}$ , and the exponent  $v$  defines the slope of the distribution curve.

Often the nonlogarithmic form of equation (1) is desired. Since

$$d \log r = 0.434 d \ln r \text{ and } d \ln r = \frac{dr}{r}$$

then equation (1) can be rewritten as:

$$n(r) = -\frac{dN}{dr} = 0.434 C r^{-(v+1)} \quad (2)$$

We will use this form of the power - law equation. Therefore the particle concentration (N) say for all particles equal to or greater than radius r, becomes the integral of equation (2) as

$$N = 0.434 C \int_{r_1}^{\infty} r^{-(v+1)} dr \quad (3)$$

The units for droplet or aerosol concentrations,  $n(r)$ , are  $\text{cm}^{-3} \mu\text{m}^{-1}$ .

Therefore the units for total particle concentrations above a given radius are  $\text{cm}^{-3}$ .

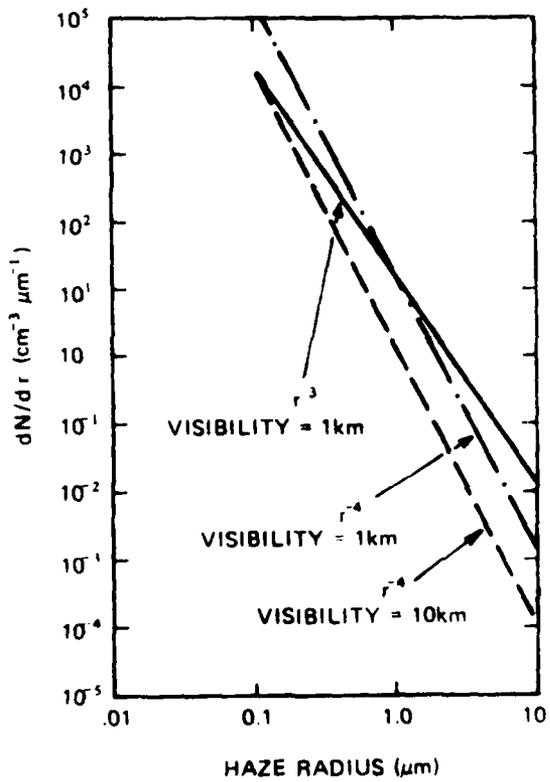


Fig. 1. Power Law Size Distributions.

Figure 1 shows how the power law size distribution given in Eq. (2) varies as a function of the exponent  $v$  and the factor  $C$ . Plotted in Fig. 1 is the aerosol concentration as a function of haze particle size radius. These plots are made for continental air near the earth's surface assuming two different slope factors  $v$  and two visibilities, which effect the concentration factor  $C$ . Later we will describe the rational and equations we developed to specify  $C$  and  $v$  according to changing meteorological features. For now, we want to demonstrate how the power law distribution changes with a fixed  $C$  and variable  $v$  and for a fixed  $v$  with variable  $C$ . Fig. 1 shows two visibilities, 1 and 10 km, which translates to concentration factors  $C$  of 30 and 3, respectively. The exponents shown correspond to  $v$  values of 3 and 2.

Notice in Fig. 1 for a constant concentration factor, visibility 1 km, as the exponent slope factor  $v$  decreases in value the aerosol size distribution curve becomes more shallow resulting in fewer numbers of smaller particles and larger concentrations of larger size particles. Typical values of  $v$  are 2 and 3 for fog and haze particles, respectively, and are shown plotted in Fig. 1 for 1 km visibility conditions. It is not unusual to have both haze and fog present during 1 km visibility conditions. Fig. 1 also shows that curves for a fixed value of  $v$  are parallel but displaced vertically according to the value of the concentration factor  $C$  which

represents the number of particles restricting the visibility. Thus by relating the value of  $v$  and  $C$  to meteorological events it is possible to derive corresponding particle size distributions.

### 1.2.3 Exponential or Gamma Distribution

One disadvantage of the above described power law distribution function is that the curve is linear on a log log plot. This means that if a preferred concentration of particle sizes occurs then a peak would exist in the distribution and may not be well represented by the power law approach. Haze, fog, cloud, and rain particles often have a Pearson type III or log-normal distribution where the number of particles increases rapidly as particle radius increases and reaches a peak value after which there is a slower decay or trailing off of particles at increasingly larger sizes. The exponential or gamma distribution can handle these types of distributions but at the expense of greater complexity than the power law distribution.

A popular form of the exponential function is given by Deirmendjian as

$$n(r) = dN / dr = A r^{\alpha} \exp(-Br^{\gamma}) \quad (4)$$

where  $n(r)$  units are  $\text{cm}^{-3} \mu\text{m}^{-1}$ , with particle radius  $r$  in micrometers, and  $A$ ,  $B$ ,  $\alpha$ , and  $\gamma$  being positive constants. Taking the derivative of Eq. (4) and setting it equal to zero gives the mode radius,  $r_c$ , that represents the radius of maximum concentration occurring at the peak of the size distribution curve and is expressed analytically as

$$r_C^\gamma = \alpha / B \gamma \quad (5)$$

The concentration,  $N$ , or total number of particles per unit volume can be derived by taking the integral of Eq. (4) between the limits of zero and infinity to obtain

$$N = A \gamma^{-1} B^{-(\alpha+1)/\gamma} \Gamma\left(\frac{\alpha+1}{\gamma}\right) \quad (6)$$

where  $\Gamma$  represents the gamma function. From this we can see that the coefficient  $A$  is proportional to the visibility or number concentration of atmospheric particles and is given by

$$A = N \gamma B^{(\alpha+1/\gamma)} / \Gamma(\alpha+1/\gamma) \quad (7)$$

Most often  $\gamma$  is set equal to 1 for computation simplicity and to reduce Eq. (6) so that the gamma function is finite if  $\alpha+1 > 0$  and if  $\alpha+1$  is an integer then

$$\Gamma(\alpha+1) = \alpha! \quad (8)$$

Thus with the above simplifications of  $\gamma = 1$  and  $\alpha+1$  an integer, Equations (4), (5), (6), and (7) can be rewritten

$$n(r) = dN/dr = A r^\alpha \exp(-Br) \quad (9)$$

$$r_C = \alpha / B \quad (10)$$

$$N = A \alpha! B^{-(\alpha+1)} \quad (11)$$

and

$$A = (N / \alpha!) B (\alpha + 1) \quad (12)$$

Normally what is done is to select constant values for  $A$ ,  $B$ ,  $\alpha$ ,  $N$ , and  $r_c$  to represent static conditions for a given fog, cloud, or rain type in order to specify particular models to represent "average" particle size conditions. We are interested here in developing dynamical models of particle size distribution by turning the above so called "constants" into variables that are related to the type and changes of actual weather observations. Therefore let us now attempt to translate these "constants" in terms of meteorological variables.

The linear mean radius,  $r_m$ , is the sum of all the droplet radii divided by the total number of droplets so

$$r_m = \frac{1}{N} \int_0^{\infty} r n(r) dr \quad (13)$$

$$= \frac{1}{N} \frac{A (\alpha + 1)!}{B (\alpha + 1)} \quad (14)$$

so

$$r_m = (\alpha + 1) / B \quad (15)$$

therefore

$$r_m = (\alpha + 1) r_c / \alpha \quad (16)$$

By definition the fog or cloud liquid water content,  $W_L$ , gives the total mass concentration of liquid water by

$$W_L \text{ (g m}^{-3}\text{)} = 10^{-6} (4\pi/3) \rho_w \int_0^{\infty} r^3 n(r) dr \quad (17)$$

where  $\rho_w$  is the density of water in  $\text{g cm}^{-3}$  and  $r$  is in micrometers.

Expanding Eq. (17) gives

$$W_L = 10^{-6} (4\pi/3) \rho_w A (\alpha + 3)! / B^{(\alpha + 4)} \quad (18)$$

Meteorologically speaking the density of water is essentially one  $\text{g cm}^{-3}$ , the liquid water content can be inferred from visibility observations in fog, the particle displacement along a moist adiabat in clouds, and the intensity for rainfall, and the coefficient  $B$  is defined by the mode radius as shown in Eq. (10). Thus we can solve for the coefficient  $A$  in Eq. (18) and obtain

$$A = 10^{+6} (4\pi/3)^{-1} (\alpha/r_c)^{(\alpha + 4)} W_L / (\alpha + 3)! \quad (19)$$

Cloud and fog droplet observations show that the mode radius  $r_c$  varies with such things as cloud or fog type, age, and height above cloud or fog base. Assuming we can reasonably approximate the mode radius and liquid water content then we are left with only the shape factor  $\alpha$  as a variable needed before we can specify particle size distributions given by Eq. (9).

We have made a number of calculations to show how the particle size distribution changes according to individual changes in liquid water content, mode radius, and curve shape factor. First, Fig. 2 shows two different ways used to plot particle size distributions. The top log-log plot is a computer output solution of the above gamma equation for five

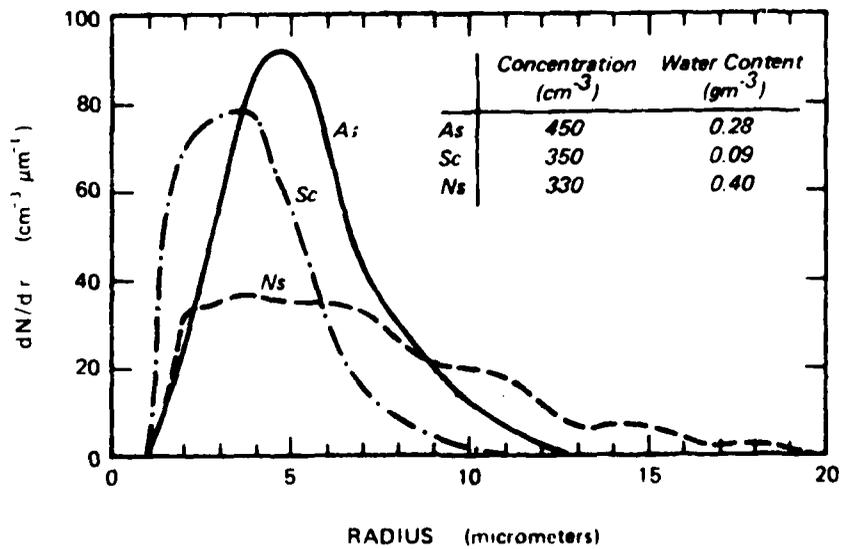
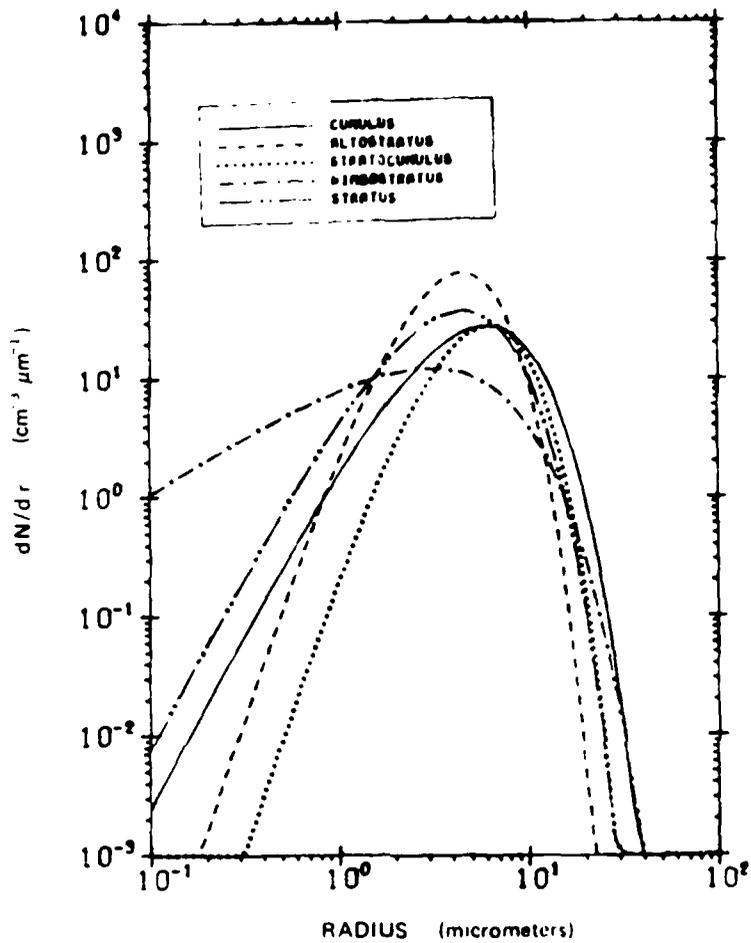


Fig. 2. Two Ways to Plot Cloud Particle Size Distributions.

different cloud types. The bottom linear plot of observed particles for altostratus (As), stratocumulus (Sc), and nimbostratus (Ns) clouds shows the familiar Pearson type III distribution. There is no preferred way to present such data. We will use mostly the log-log method because smaller concentrations of particles can be plotted with greater ease.

Figures 3, 4, and 5 show how the particle size distribution given by the exponential function varies when only one variable is allowed to change. Plots in Fig. 3 depict two orders of magnitude change in liquid water content while the mode radius,  $r_c = 4 \mu\text{m}$ , and shape factor,  $\alpha = 4$ , remain constant. What is most striking in Fig. 3 is that the maximum density  $dN/dr$  varies from about 4.5 to 450 droplets per unit volume and radius interval ( $\text{cm}^{-3}, \mu\text{m}^{-1}$ ) which represents significant differences in density of or visibility in clouds or fogs. Thus if we can infer the mode radius and shape factor for a specific type of fog or cloud then we can infer the number density of the droplets by obtaining a measure of the liquid water content.

We made calculations to show how variations in the shape factor coefficient  $\alpha$  could be used to represent narrow or broad distributions in particle sizes. Fig. 4 shows, for a fixed liquid water content and mode radius, that as one selects higher and higher values for  $\alpha$  one obtains sharper and sharper curves that represent a more narrow distribution of particle sizes. Also note that as the drop size distributions become broader, the number density decreases for the most frequently occurring particles while increasing for the small and large particles. Therefore, by knowing something about the variance or distribution of particle sizes associated with particular fogs or clouds it should be possible to select an appropriate shape factor.

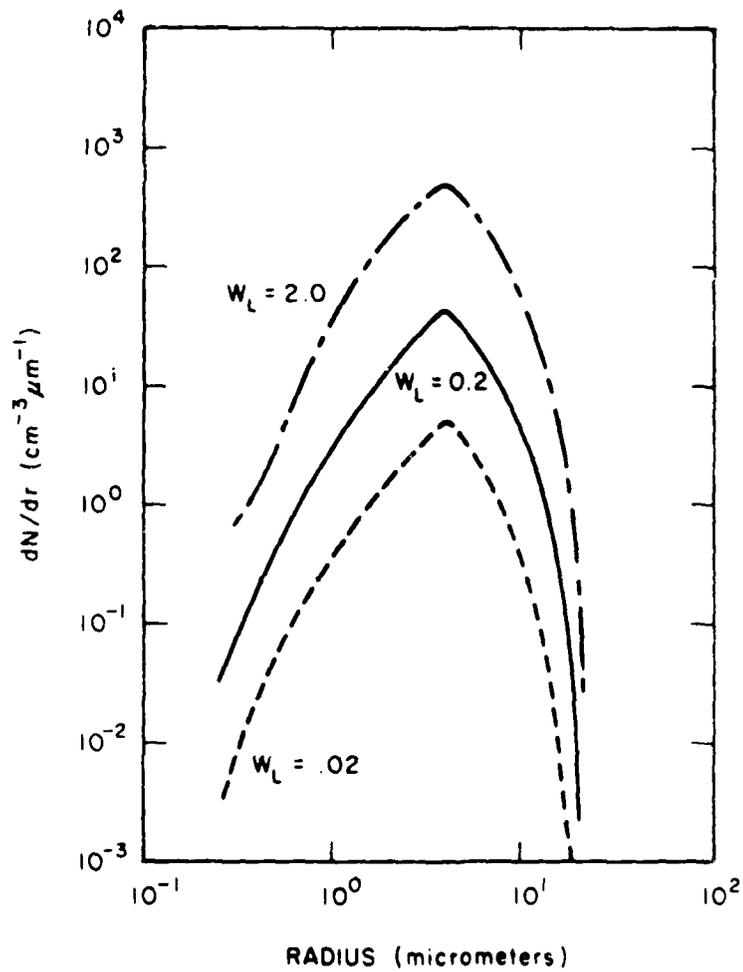


Fig. 3. Exponential Function Size Distributions For Three Liquid Water Contents,  $W_L = 0.02, 0.2,$  and  $2.0 \text{ g m}^{-3}$ , With Constant Mode Radius,  $r_C = 4$  micrometers, and Shape Factor,  $\alpha = 4$ .

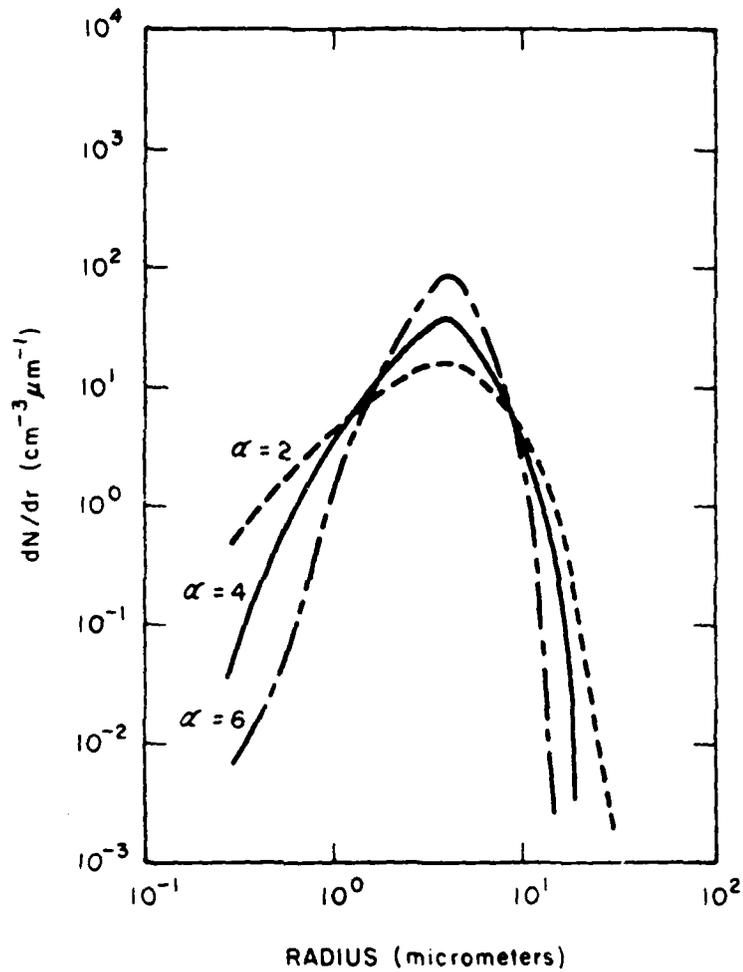


Fig. 4. Exponential function, Size Distributions For Three Shape Factors,  $\alpha = 2, 4,$  and  $6,$  With Constant Liquid Water Content,  $W_L = 0.2 \text{ gm}^{-3},$  and Mode Radius,  $r_c = 4$  micrometers.

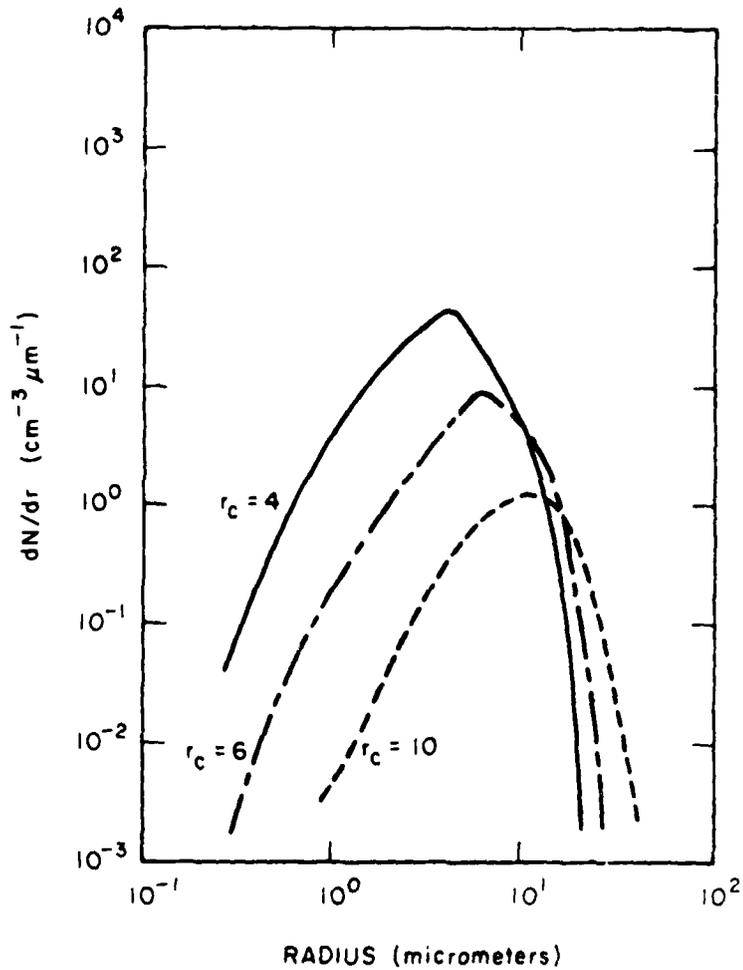


Fig. 5.

Exponential Function Size Distributions For Three Mode Radii,  $r_c = 4, 6,$  and  $10$  micrometers, With Constant Liquid Water Content,  $W_l = 0.2 \text{ gm}^{-3}$ , and Shape Factor,  $\alpha = 4$ .

Lastly, we calculated droplet density for three environments where the most frequently occurring particle size was 4, 6, and 10 micrometers. During these computations, the liquid water content and shape factor were held constant. The results, Fig. 5, show the peak curve displacement corresponds with the selected mode radii and the peak number density of particles decreases as mode radius increases. Often a particular mode radius is representative of a particular type of fog or cloud. Thus by having information or observations on the liquid water content, the radius of the most frequently found droplet, and the variance or breath of particle sizes, we can select variables in the exponential or gamma function equation to depict a wide range of unimodal particle size distributions.

In the following report we will be using both the power law and exponential size distribution concepts described above to develop litho- and hydro-meteor models that can be specified given only routinely available weather observations.

## 2 DYNAMIC MODELS OF PARTICLE SIZES

### 2.1 LITHOMETEORS

#### 2.1.1 Continental

##### 2.1.1.1 Ground Level Variations

The underlying surface (land, ocean, vegetative, barren), soil type (humus, clay, rocky), soil condition (wet, dry, compacted, loose), atmospheric stability (convective, stable), and wind speed (soil erosion, vertical and horizontal advection) are important in determining type, concentration, and size distribution of lithometer particles as a function of space, time, and height in the atmosphere. To further complicate matters some dust grains are nonhygroscopic while others, especially salt containing particles, are highly hygroscopic. These hygroscopic particles include many well known things as salt from the sea, tars and resins from organic plants, smoke from industrial and battlefield fires, and the usual sulfate and nitrate chemicals from organic, combustion, and photochemical processes. The thing is, hygroscopic particles are not only important as light scatterers but also provide particle size changes as the ambient relative humidity approaches saturation and also provide the most active condensation nuclei needed in the cloud physics process of cloud/fog droplet and precipitation formation. In fact studies have been conducted to show light attenuation or visual range restriction as relative humidity increases, Fig. 6. The

important fact to us is that visual range or visibility is nearly linearly related to variations in relative humidity greater than about seventy per cent. That is to say that we

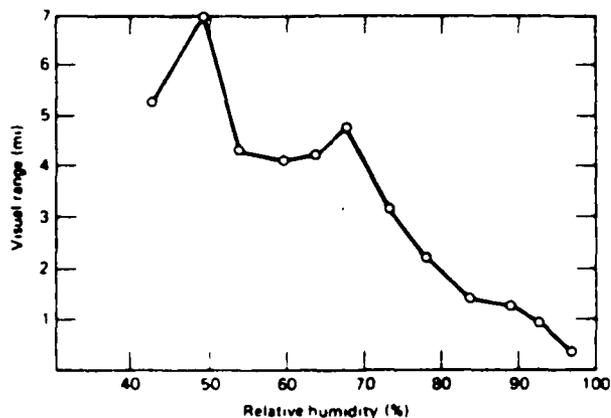


Fig. 6. Variation In Visual Range With Relative Humidity.

will consider variations in the particle size as a function of relative humidity to be incorporated in meteorological observations of visual range or visibility.

Dust particles, lithometeors, or haze are usually contained within the radius size range of 0.01 to 10 micrometers with a peak or most frequent particle radius of about 0.02 micrometers. There are two points of most interest to this study. First, most Army electro-optical systems are degraded or adversely effected by particle sizes equal to or greater than 0.1 micrometer in radius. Second, particle size observations at the earth's surface, at different geographical locations (Baltimore, Minneapolis, and Seattle) representing east - west coast and mid-sections of U.S.A., and day and night aerosol observations (Los Angeles) all show distributions

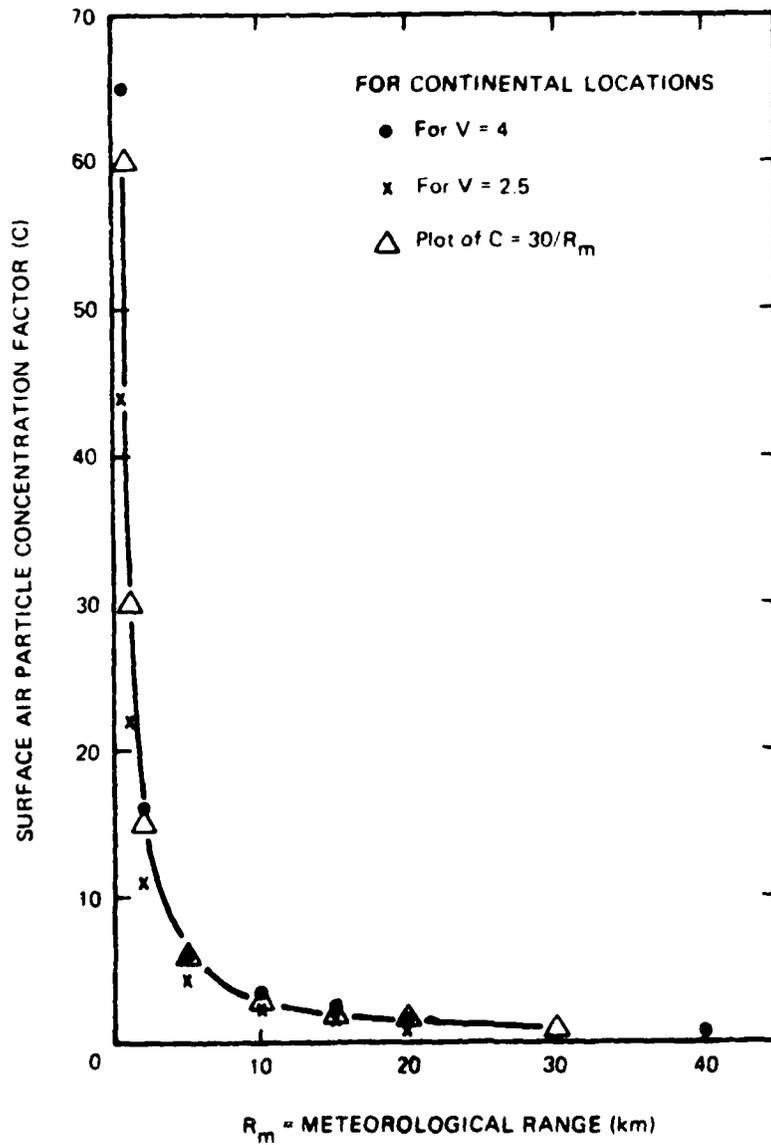


Fig. 7. Surface Air Haze Particle Concentration Factor Versus Meteorological Range.

having a  $r^{-4}$  dependence as given in Eq. (2). That is to say, the continental aerosol size distribution at the earth's surface follows a power law curve whose exponent is -4. The exponent in Eq. (2) is  $-(v + 1)$ , therefore, a value of  $v = 3$  is typical of ground level haze aerosols. The number density or vertical displacement of this curve, however, can vary considerably depending upon the number of particles suspended in the air at a given instant in time, which in turn is related to meteorological visibility.

Before Eq. (2) can be solved to derive the number density of haze aerosols it is necessary to obtain a measure of the particle concentration factor  $C$ . McCartney has shown that this concentration factor is directly proportional to the backscatter coefficient which in turn is proportional to the meteorological range,  $R_m$ , at optical wavelengths. We have plotted his values of the surface air particle concentration factor ( $C$ ) as a function of meteorological range ( $R_m$ ) in kilometers, see Fig. 7. McCartney presented data points for  $v$  in Eq. (2) equal to 2.5 and 4. From Fig. 7 it can be seen that our derived equation

$$C = 30 / R_m \quad (20)$$

represents a reasonable fit to these data. More importantly, Eq. (20) allows us to use visibility observations reported over standard meteorological networks to infer variations in the number density of haze particles as weather conditions vary.

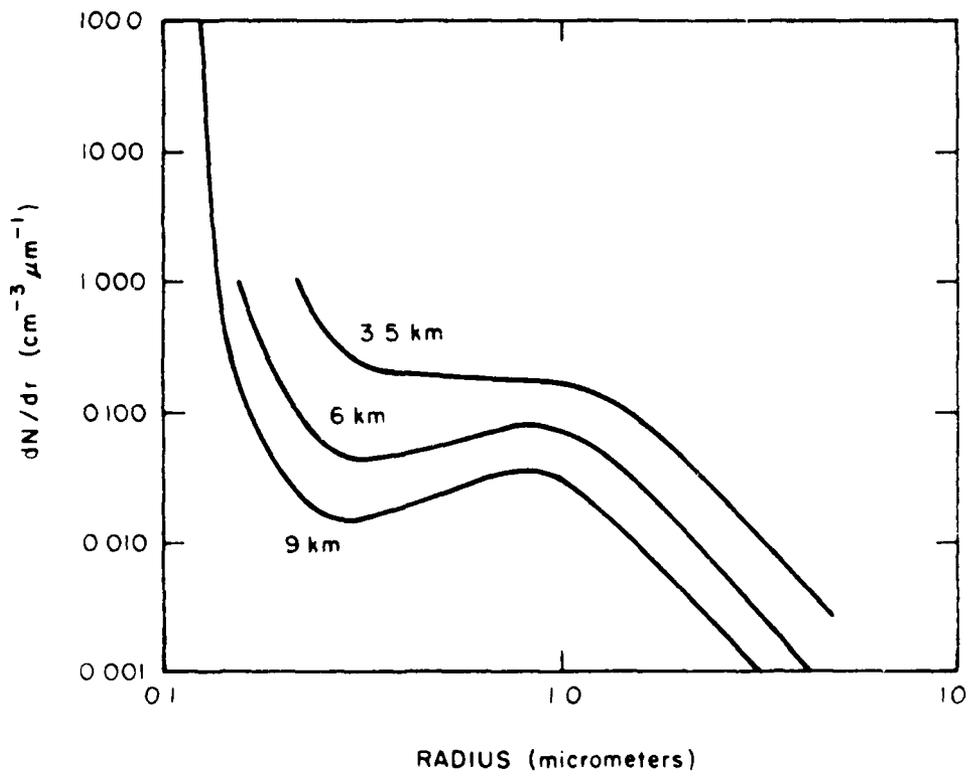


Fig. 8. Observations Over Death Valley.

#### 2.1.1.2 Upper Level Variations

Aerosol variations with respect to geographical location and meteorological conditions decrease with height and often are considered to be non-existent near the troposphere, about 10 km. A bimodal distribution of aerosols is sometimes observed to increase with height above the earth's surface. In a static time dependent atmosphere it is not unusual for small particles to coagulate and form an ever-increasing size of lower concentration particles. There are, however, atmospheric regions where other forces retard this action and the maintenance or production of small particles remains high. Such appears to be the case in or around the tropopause height. This effect is shown in part by observations taken by Blifford (1970) over Death Valley, as shown in Fig. 8, for three different heights, namely 3.5, 6, and 9km. This figure also shows the gravitational settling effect on large particles so that a fewer number of larger particles exist at higher altitudes.

A great deal of dispersion exists among investigators in terms of what the vertical distribution is for atmospheric aerosol particle concentrations. This is clearly illustrated by Fig. 9. For example, the spread at 12km shows a dispersion of more than an order of magnitude. A typical "clear" atmospheric profile of aerosol concentration as a function of height is presented in Fig. 9 as plotted values of "C", which correspond to a clear atmosphere having a 23km range of visibility. Superimposed upon

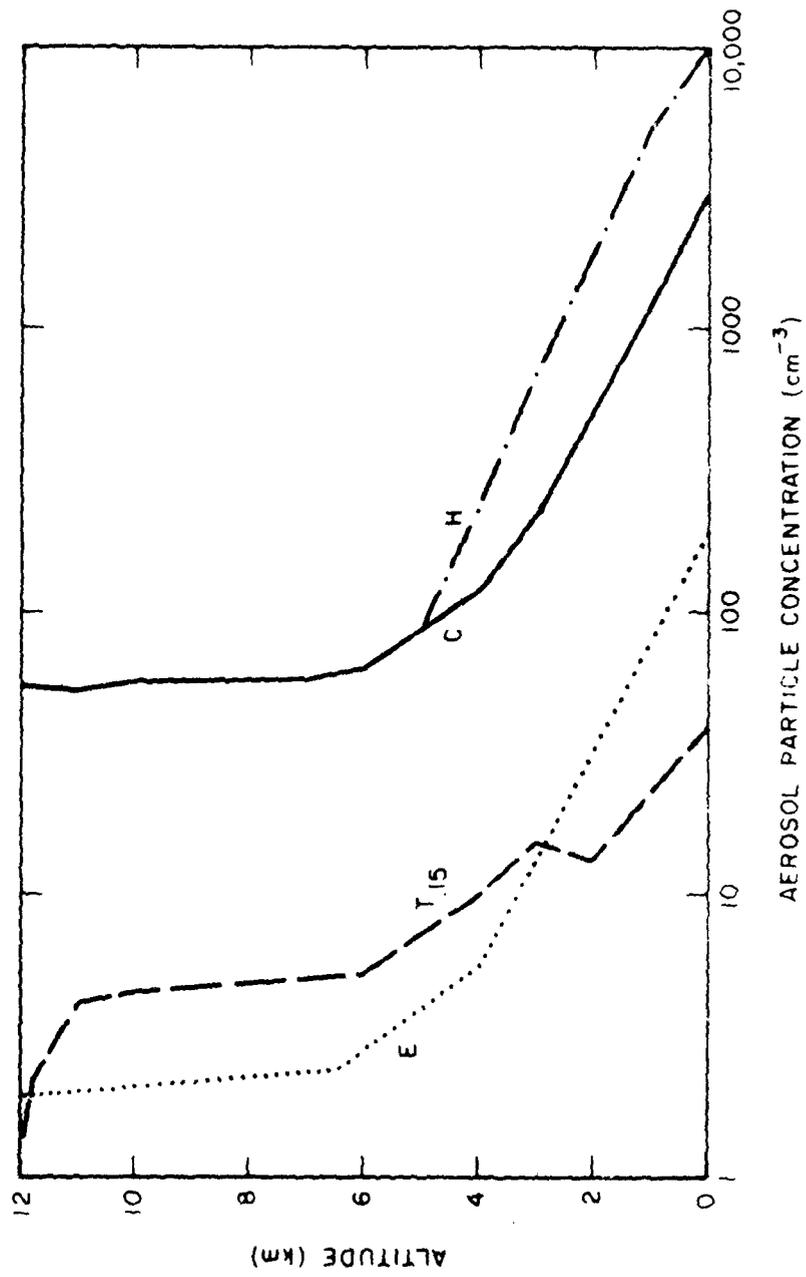


Fig. 9. Comparison of Vertical Variation of Aerosol Models.

this "clear" plot are a series of "H" values representing a hazy atmosphere whose influence extends from the ground surface to 5 km, above which the "hazy" and clear atmosphere have the same aerosol number concentrations. For this case, the hazy atmosphere corresponds with a ground level horizontal visibility of 5km. Also plotted for comparison is Toon's and Pollock's data ( $T_{.15}$ ) for aerosol number concentrations for particles equal to or greater than 0.15 micrometers in radius that are found between the surface and 12km. Elterman's early data in 1964 resulted in a straight line in Fig. 9 extending from the surface to 10km, but more recent data in 1968 with better instrumentation displayed a break at 4 km with a small change or nearly constant value of particle concentration with height, see Fig. 9. As shown in Fig. 9, the hazy and clear models as well as the Elterman and Toon's data plots include those particle sizes that are most important in either remotely probing the atmosphere or studying optical or infrared radiational characteristics of the atmosphere. What is not shown, however, is how these particle size distributions change with height and changing weather environments.

We were looking for a measure of the change in particle size distribution as altitude increases above ground level. Blifford's balloon borne observations over Death Valley, Fig. 8, showed that the particle density not only decreased with height but so did the slope of the particle dis-

tribution curve. More recent aircraft data were collected over Western Europe by Cress, see Fig. 10, which showed similar results. In general the observed distributions near the surface had a  $r^{-4}$  while those at about 5km had a  $r^{-2}$  slope. Cress plotted the exponent of  $r$  as the Junge Slope as a function of height and for spring, summer, and fall. We obtained a linear fit to the fall data, Fig. 11, and derived

$$v = 3 - Z / 2 \quad (21)$$

where the Junge Slope =  $-(v + 1)$  as given in the power-law Eq. (2), and  $Z$  is the height about ground surface in km. The airborne equipment sampled aerosol sizes from 0.2 to 6 micrometers. Observations were taken under a wide range of meteorological conditions, including clear and overcast skies and visibilities varying from excellent down to 5km. A scatter of data points exists at all heights and should be expected due to physical variations previously discussed, e.g. underlying surface, atmospheric stability, wind, etc. Cress summer Junge Slope observations have about the same slope found in the fall data but the surface value for the Junge Slope is -5. This implies that the warmer and dryer underlying surface and more unstable boundary layer during summertime generates a larger number of smaller aerosols. The spring observations, Fig. 12, had a curvilinear distribution of Junge Slope with height and no one linear

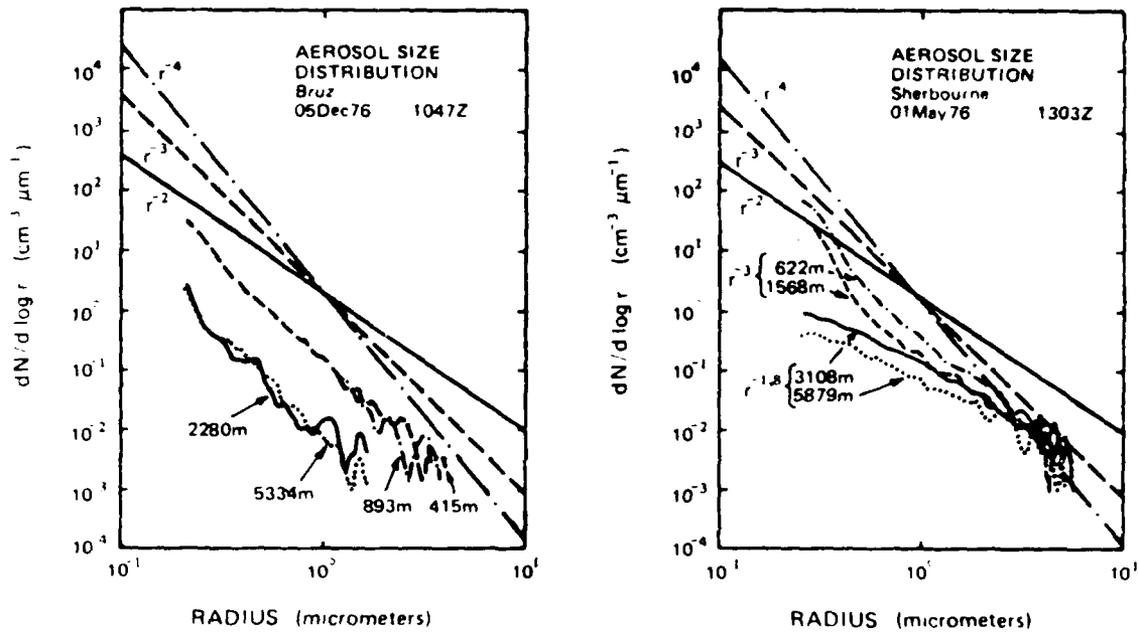
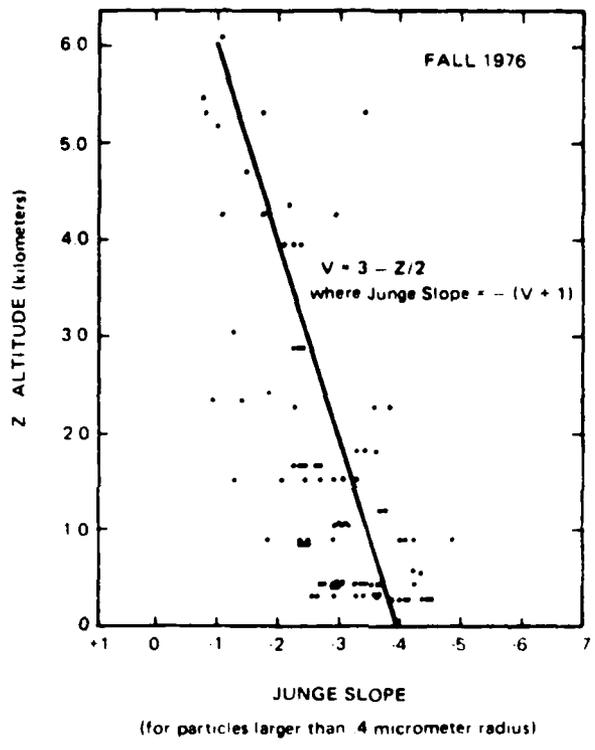


Fig.10. Aircraft Aerosol Observations at Different Heights.



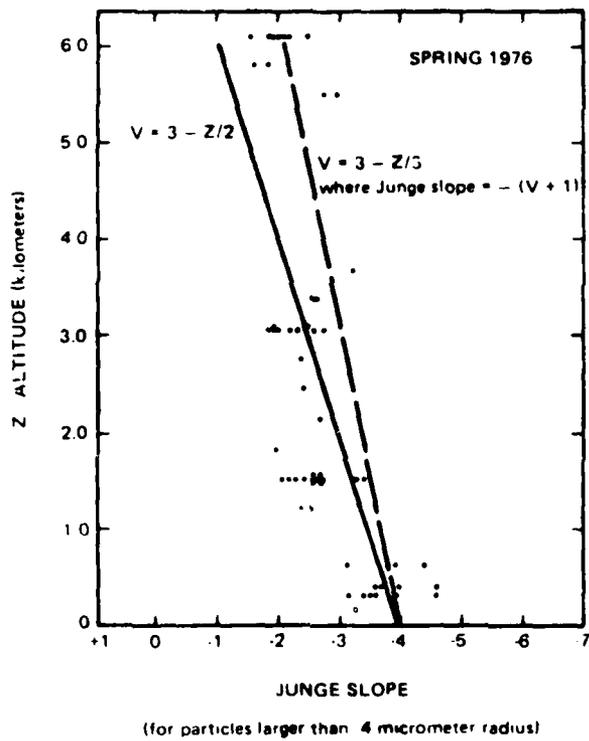


Fig.12. Spring Variation of Junge Slope With Height.

curve covers the entire range of data. For the fall and spring data a linear relation can be obtained between the surface and 4 km by using Eq. (21) and holding the Junge Slope constant at -2 for heights above 4 km. The same can be applied to the summer data so that the summer equation becomes

$$v = 4 - Z / 2 \quad (22)$$

where again the Junge Slope =  $-(v + 1)$  as given in the power - law Eq. (2), and  $Z$  is the height above ground in km and can not exceed a value of 4km. At heights above 4km in summer  $v$ , equals a constant value of 2 so the Junge Slope remains constant at -3.

We now want to obtain an equation to describe the decrease in the total aerosol concentration with height. Fig. 9 shows two models and two data sets and, although they vary widely in the value for particle concentration at a specified level, they all show an exponential decrease with height from the surface to about 5km. Above that height, total particle concentration remains essentially constant up to the tropopause. In 1954 Penndorf derived

$$N_z = N_0 \exp (- Z / H) \quad (23)$$

to give the total number concentration of aerosols at a given height,  $N_z$ , as a function of the total concentration at ground level,  $N_0$ , the height in

the atmosphere in km,  $Z$ , and a term called the scale height in km,  $H$ . Penndorf's data suggested variations in  $H$  from 1.2 to 1.4 km. More recently in 1970, Elterman made simultaneous observations of meteorological range ( $R_m$ ), optical attenuation coefficients, and aerosol scale height. In Fig. 13, we have plotted his data points and derived

$$H = 0.8 + R_m / 30 \quad (24)$$

where  $H$  and  $R_m$  are in km. This Eq. (24) applies for visibilities ranging from 0 to 18 km. The scale height remains constant at 1.4 km for visibilities greater than 18 km. By using Equations (23) and (24) it can be seen that as surface visibility increases the aerosol concentration with height decreases.

Thus it is possible to use the relations developed in this section to specify number density, concentration, and vertical distribution of aerosols as a function of routinely available weather data.

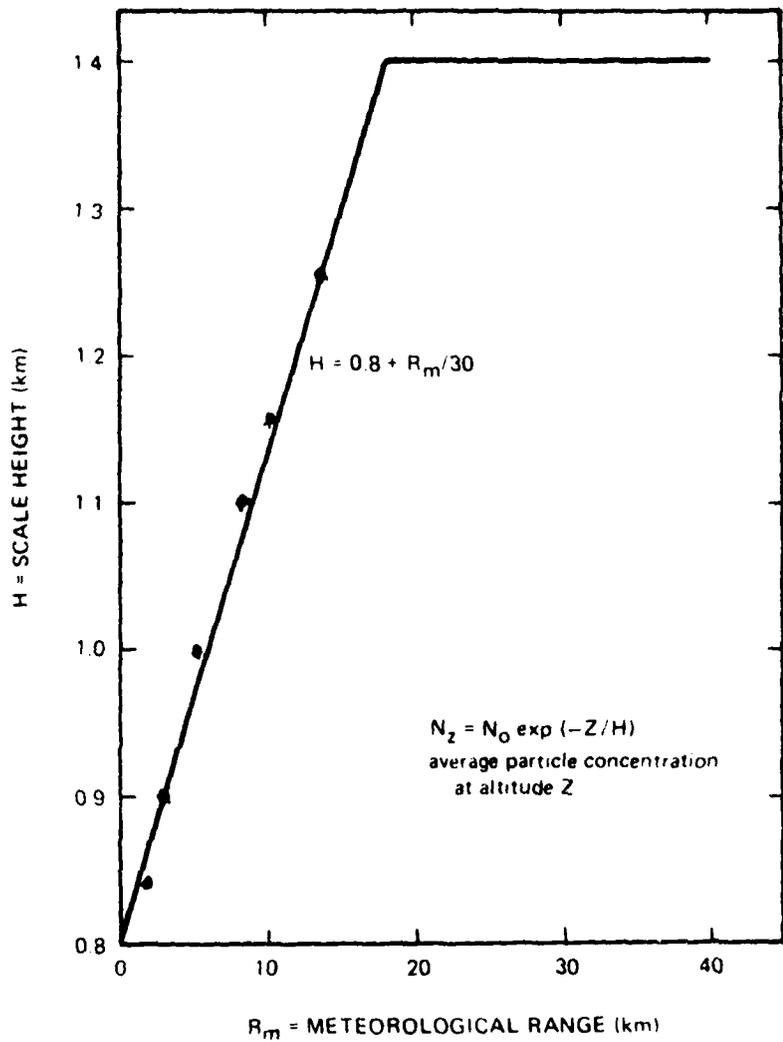


Fig. 13. Aerosol Scale Height Versus Meteorological Range.

### 2.1.1.3 Dynamic Procedure

Now we will present our sequence of steps taken to use standard meteorological observations to infer continental haze particle size distributions having radii equal to or greater than 0.1 micrometer. These steps are:

1. Determine surface air particle concentration factor  $C$  from the observed meteorological range ( $R_m$ ) in kilometers where  $C = 30 / R_m$ .
2. Derive the surface air particle size distribution using  $n(Z,r) = \frac{dN}{dr} = 0.434Cr^{-(v+1)}$  where  $n(Z,r)$  is in units of  $\text{cm}^{-3} \mu\text{m}^{-1}$  and  $v$  is an exponential factor related to the type of aerosol and the altitude above the earth's surface. We found the haze exponential factor as a function of altitude  $Z$  in kilometers to be  $v = 3 - Z/2$  for times other than summer months, which is valid from the surface to 4 km where  $v$  remains constant at one for higher altitudes. During summer months  $v = 4 - Z/2$  from the surface to 4 km above which  $v$  remains constant at 2.
3. Determine the average particle concentration  $N(o,r)$  at the earth's surface by using the equations for  $C$  and  $n(Z,r)$  above and integrating the latter for spring and fall

conditions from  $r$  to infinity. Thus

$$N(o,r) = 0.434 C (1/3)r^{-3}$$

For summer conditions

$$N(o,r) = 0.434 C (1/4)r^{-4}$$

4. Compute the decrease in average particle concentration  $N(Z,r)$  as altitude (in kilometers) increases above the ground using our empirical equation

$$N(Z,r) = N(o,r) \exp(-Z/H)$$

where  $H$  is the atmospheric scale height in km that varies with meteorological range as follows

$$H = 0.8 + R_m/30$$

where  $H$  reaches a constant value of 1.4 for very high visibilities (i.e.  $R_m \geq 18$  km).

5. After deriving the average particle concentration at a particular height  $N(Z,r)$ , the size distribution value  $n(Z,r)$  is

$$n(z,r) = v r^{-1} N(Z,r)$$

or

$$n(Z,r) = (3 - Z/2) r^{-1} N(Z,r) \text{ for spring and fall}$$

and

$$n(Z,r) = (4 - Z/2) r^{-1} N(Z,r) \text{ for summer}$$

where  $Z$  in the right hand side of the equations can never exceed 4 km.

Following the above steps, we made computations for aerosol size

distributions at 1.8 and 6.1 km to correspond with Cress's aircraft observations in western Europe, Fig. 14 and 15. Cress particle size measuring equipment was restricted to detections over the radius range from 0.2 to 6  $\mu\text{m}$ . Considerable scatter exists in his observations which were taken over a wide variety of weather conditions ranging from clear to overcast skies and from excellent visibility down to a minimum of 5 km.

Now assuming the surface visibility is 20 km ( the same as used in the AFGL Rural Model ), the surface air particle concentration factor C equals 1.5 and the scale height equals 1.4. So the average particle concentration  $N(0,r)$  at the earth's surface is for spring and fall

$$N(0,r) = 0.434 (1.5) \left(\frac{1}{r}\right) r^{-3}$$

$$N(0,0.1) = 217 \text{ cm}^{-3} \text{ for particles } \geq 0.1 \mu\text{m}$$

$$N(0,0.2) = 27.12 \text{ cm}^{-3} \text{ for 20 km visibility and particles } \geq 0.2 \mu\text{m}$$

$$N(0,0.4) = 3.4 \text{ cm}^{-3} \text{ for particles } \geq 0.4 \mu\text{m}$$

and

$$N(0,1.0) = 0.22 \text{ cm}^{-3} \text{ for 20 km visibility and particles } \geq 1.0 \mu\text{m}$$

At an altitude of 1.8 km then

$$N(1.8,r) = N(0,r) e^{-\left(\frac{1.8}{1.4}\right)}$$

$$N(1.8,0.1) = 60.0 \text{ cm}^{-3} \text{ for particles } \geq 0.1 \mu\text{m}$$

$$N(1.8,0.2) = 7.50 \text{ cm}^{-3} \text{ for particles } \geq 0.2 \mu\text{m}$$

$$N(1.8,0.4) = 0.94 \text{ cm}^{-3} \text{ for particles } \geq 0.4 \mu\text{m}$$

$$N(1.8,1.0) = 0.06 \text{ cm}^{-3} \text{ for particles } \geq 1.0 \mu\text{m}$$

then

$$n(1.8, r) = \left(3 - \frac{Z}{2}\right) r^{-1} N(1.8, r)$$

$$n(1.8, 0.2) = 78.8 \text{ cm}^{-3} \mu\text{m}^{-1} \text{ for } r = 0.2 \mu\text{m}$$

$$n(1.8, 1.0) = 0.13 \text{ cm}^{-3} \mu\text{m}^{-1} \text{ for } r = 1.0 \mu\text{m}$$

At an altitude of 6.1 km, where Cress aircraft observations were taken over western Europe, and assuming a 20 km surface visibility then

$$N(6.1, 0.2) = 0.35 \text{ cm}^{-3} \text{ for particles } \geq 0.2 \mu\text{m}$$

$$N(6.1, 1.0) = 0.003 \text{ cm}^{-3} \text{ for particles } \geq 1.0 \mu\text{m}$$

and

$$n(6.1, 0.2) = 1.75 \text{ cm}^{-3} \mu\text{m}^{-1} \text{ for } r = 0.2 \mu\text{m}$$

$$n(6.1, 1.0) = 0.003 \text{ cm}^{-3} \mu\text{m}^{-1} \text{ for } r = 1.0 \mu\text{m}$$

Since from Eqs. (1) and (2)  $dN/d \log r = (r/0.434) n(Z, r)$  then at 1.8 km

$$dN/d \log r = 36.3 \text{ cm}^{-3} \mu\text{m}^{-1} \text{ for } r = 0.2 \mu\text{m}$$

$$dN/d \log r = 0.3 \text{ cm}^{-3} \mu\text{m}^{-1} \text{ for } r = 1.0 \mu\text{m}$$

then at 6.1 km

$$dN/d \log r = 0.81 \text{ cm}^{-3} \mu\text{m}^{-1} \text{ for } r = 0.2 \mu\text{m}$$

$$dN/d \log r = 0.007 \text{ cm}^{-3} \mu\text{m}^{-1} \text{ for } r = 1.0 \mu\text{m}$$

In order to provide a means for comparison with our GAC Model, plots are shown in Figs. 14 and 15 for Cress's aircraft data, Blifford's impactor data, and two models of the Air Force Geophysics Laboratory (AFGL) i.e., AFGL tropospheric Model and the AFGL Rural Model for a 20 km visibility. It can be seen that the GAC Model provides the best fit.

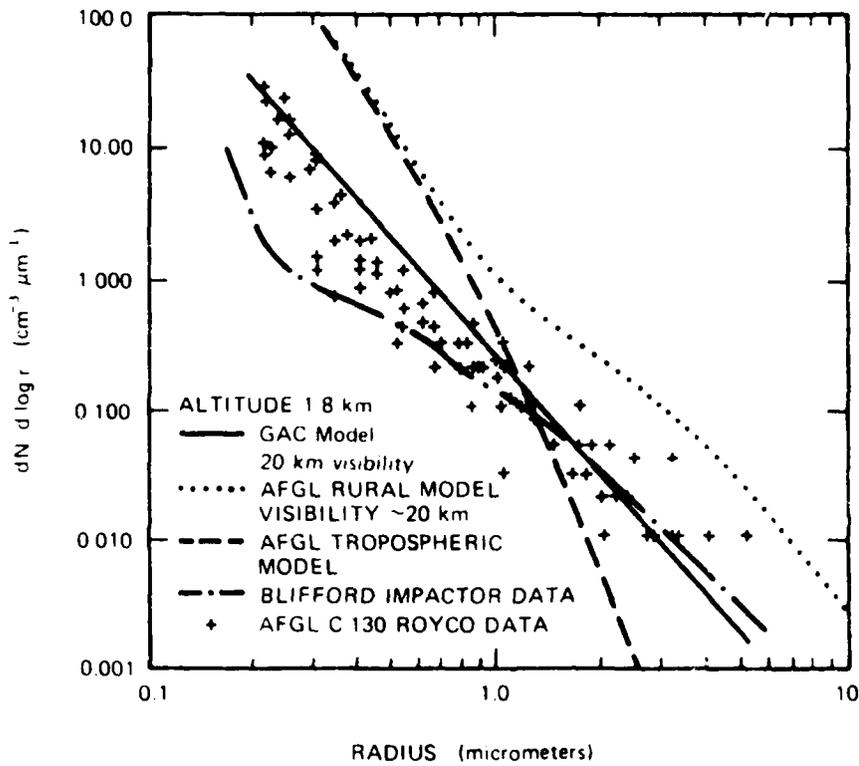


Fig. 14. Comparison of Aerosol Models at 1.8 km.

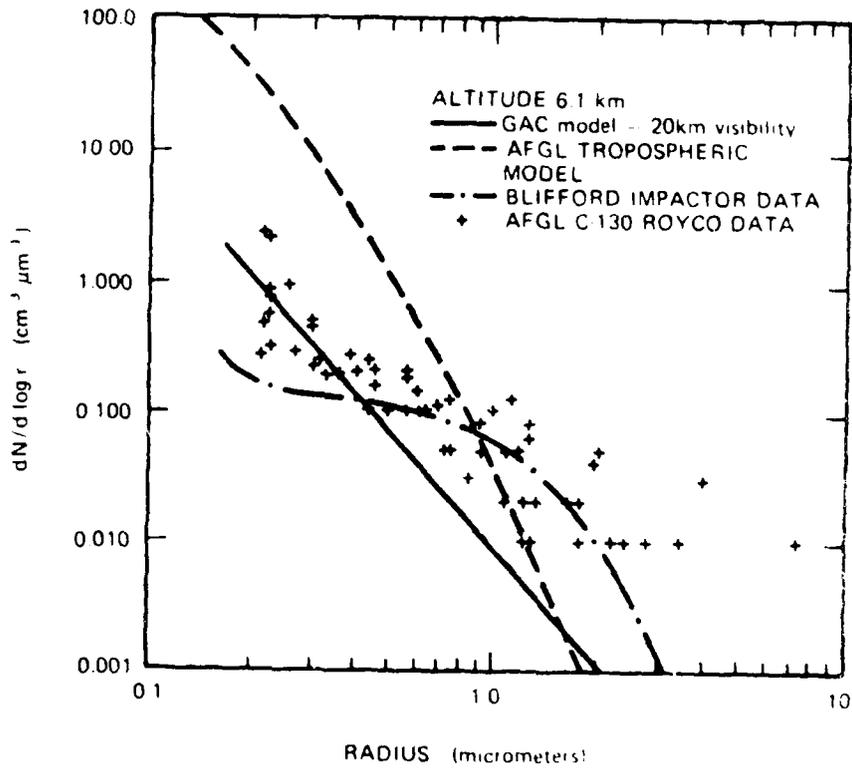


Fig. 15. Comparison of Aerosol Models at 6.1 km.

## 2.2 HYDROMETEORS

### 2.2.1 Fog

#### 2.2.1.1 Ground and Upper Level Variations

This section on hydrometeors will cover fog, cloud, and rain drop size distributions. An overview of these features can be obtained from Fig. 16 where it shows about a 12 order of magnitude change in number density and about half that change for representing the possible range in droplet radii. Often in the real world there is a number of possible combinations of hydro - and litho- meteors occurring simultaneously. High pressure regions with clear skies and stable boundary layers are conducive to good radiational cooling and fog formation. Also it is not unreasonable to expect trapping of haze particles in the stable surface air layer and to have a mixture of both haze and fog particles. Other event combinations occur, such as drizzle and fog, yet we tend to focus our modelling efforts on a simple event representation. That is also done here, however, provisions are made and results shown to combine outputs from multi models to better simulate all reported weather.

Many types of fog exist to produce large spatial and temporal variations in "seeability." Recent improvements and technology advances in both particle sampling and sizing instruments and observational platforms needs to be exploited in carefully conceived and implemented field ex-

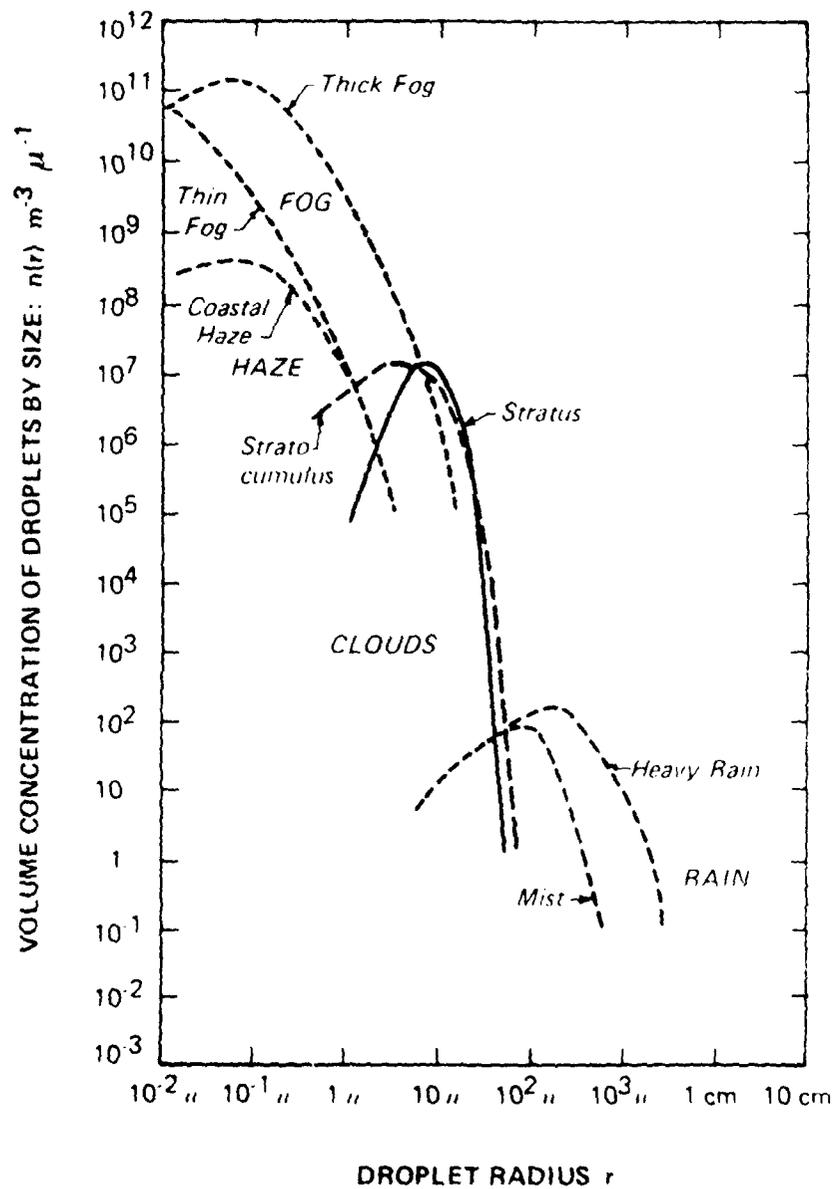


Fig. 16. Volume Concentration of Water Droplets by Size (Counted in  $1\text{-}\mu\text{m}$  Intervals of Droplet Radius)

perimental and data analysis programs. Such data are basic to defining microphysical structure as well as to generating synoptic and mesoscale models as done here.

Fog conditions often go through three distinct stages, i.e. initial oscillatory, steady dense, and break up stage. Particle sizes during the initial oscillatory stage usually have a narrow range of values, the most frequently occurring radius is small, the liquid water content is less, and haze and fog particles combine to weight the size distribution to smaller sizes. Dense persistent fogs are older in character, having higher liquid water content, broader range of particle sizes, larger mode radius, and greater EO attenuation. The break up stage depends greatly upon the fog type, formation, density, thickness, and physical processes producing the break up. The particle size distribution of breaking-up fog reverts back more to a haze like character with an ever decreasing residual peak in the concentration of the larger mode radius. Typical fog parameters are shown in the following Table 2.

Table 2. Typical Fog Parameters

<u>Parameter</u>	<u>Fog type</u>			
	<u>Radiation (new)</u>	<u>Radiation (old)</u>	<u>Valley</u>	<u>Advection</u>
mode radius ( $\mu\text{m}$ )	4	10	8	10
breath of size distribution	narrowest	broad	broad	broadest
vertical depth (m)	variable	200	150	400

The time period that usually separates new from old fogs is on the order of 2 hours after formation. Several other names have been used to describe these fog types. For example newly formed fogs are sometimes called "selective fog." Older or dissipating fogs may be called "stable fog" or "evolving fog." Likewise advection fog near the sea shore is called "coastal fog." Often "low mountain fog" is called valley fog and stratus clouds intersecting a mountain are called "high mountain fog." We know the preferred mode radius of fog has seasonal, geographical, and meteorological variations that need better definition. Until these refined data become available, for our purpose, the above listed mode radius will be used.

Liquid water content of a fog must be specified in order to define the fog density or concentration of droplets. Sensors do exist for directly measuring liquid water content and these are the most accurate and reliable but are not too feasible within a battlefield environment. Horizontal visibility observations are available from routine and nonstandard observational sources and may be used to infer liquid water content of fog. A number of experimental studies have been made of liquid water content and atmospheric visibility. We have averaged some of these results and plotted three curves in Fig. 17 to depict liquid water content versus visibility for coastal fog and two inland fog types (new and old). The equations used in this study

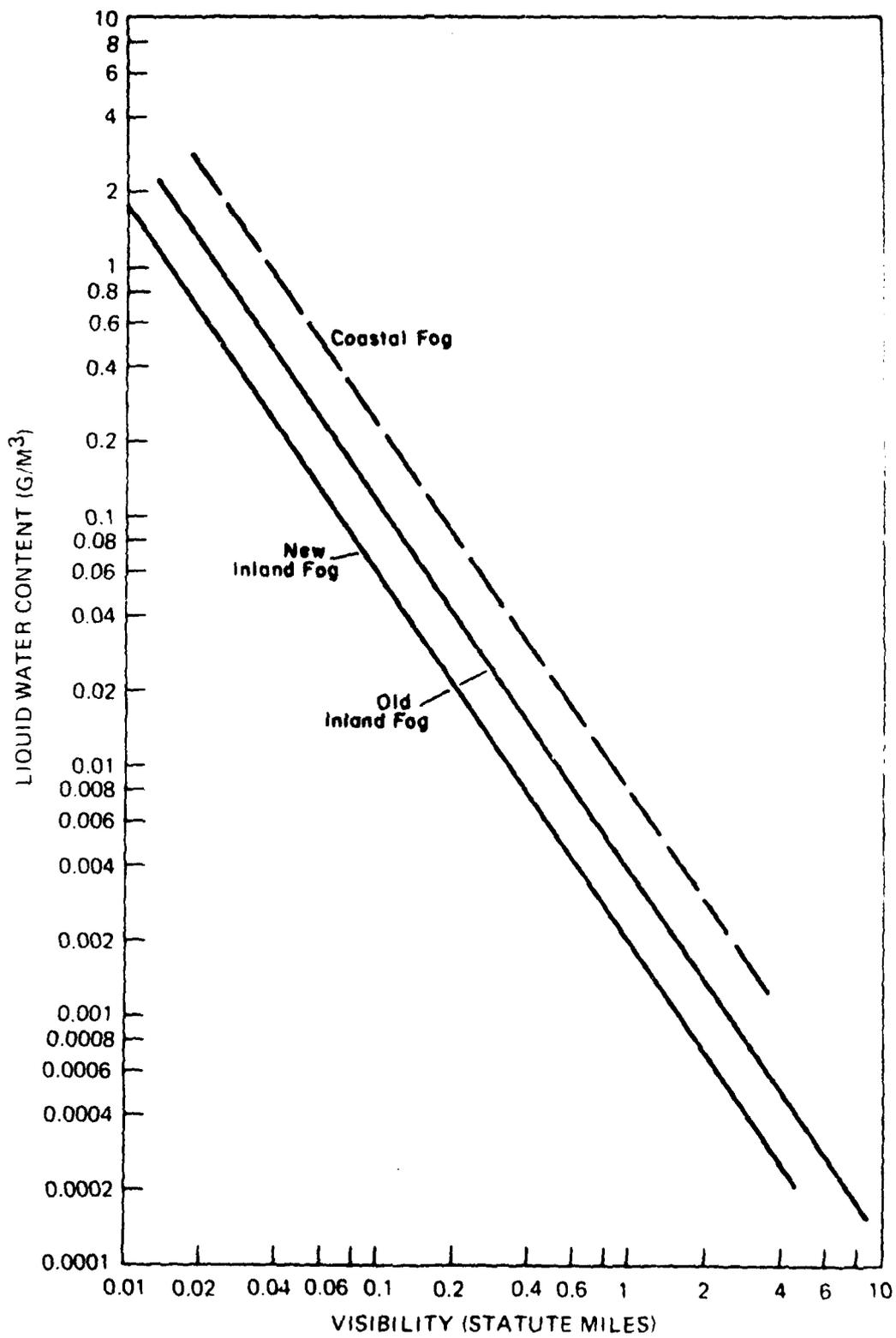


Fig. 17. Relationship between Visibility and Liquid Water Content in Fog

to derive fog liquid water content,  $W_L$  in  $g\ m^{-3}$  as a function of meteorological visual range,  $R_m$  in miles, are

$$\text{Coastal Fog} \quad W_L = (27.15 R_m)^{-1.43} \quad (25)$$

$$\text{Inland Fog} \quad W_L = (41.7 R_m)^{-1.54} \quad (26)$$

Old

$$\text{New} \quad W_L = (58.8 R_m)^{-1.54} \quad (27)$$

By comparing information from Table 2 and Fig. 17 it can be seen that the narrowness or breath of drop size distributions is dependent on fog type which in turn is related to liquid water content. That is to say that for a fixed visibility, liquid water content is higher and the drop size distribution broader for coastal than for either inland fog types. In order for modelling techniques to be representative the exponential function shape factor  $\alpha$  must vary as fog density varies to produce a size distribution which is very narrow ( where  $\alpha$  is large ) when the liquid water content is low and very broad ( where  $\alpha$  is small ) when liquid water content is high. We analyzed a wide variety of droplet size distributions to obtain the following shape factor relationship

$$\alpha = 1 - 1.4 \ln W_L \quad (28)$$

where  $W_L$  is the fog liquid water content in  $g\ m^{-3}$ . For computational

simplicity and so that our equations in section 1 of this report would not have to increase in complexity, we placed two restrictions on the value of  $\alpha$ , first it can never be less than one, and second it must be rounded off if necessary to be a whole integer.

The composition of inland fog normally varies with height above ground level. The number of fog droplets per unit volume usually increases from the ground to the top of the fog. Larger droplets and higher liquid water content are usually found at the base of inland fogs whereas coastal fogs are more homogeneous in the vertical. For older and more stable inland fogs the drop size distributions become more narrow and unimodal and the mean radius decreases with increasing altitude above the surface. For a composite of old inland radiational and valley fogs we found average vertical variations for mode radius  $r_c$  and liquid water content  $W_L$  to be

$$d r_c / d Z = - 1 \mu m / 100 \text{ feet} \quad (29)$$

and 
$$d W_L / d Z = - 0.4 \text{ g m}^{-3} / 100 \text{ feet} \quad (30)$$

with a minimum value of  $4 \mu m$  applicable to  $r_c$ . Observations of coastal, advection, or marine fogs often show nearly constant or increasing liquid water content with increasing height in the fog. For this paper we will assume constant conditions prevail from the surface to the top of coastal fogs.

#### 2.2.1.2 Dynamic Procedure

1. Use the output of analyses of meteorological surface and upper air observations, such as our CFAS (Cloud Fog Analysis System) or our CIVAS (Cloud/Icing/Visibility Analysis System), to identify the type, age, and thickness of fog, other restrictions to visibility such as haze, mist, etc., and the visibility.
2. Select the applicable mode radii  $r_c$  from Table 2.
3. Derive the ground level liquid water content from either Eqs. (25), (26), or (27).
4. Compute the shape factor from Eq. (28).
5. Obtain the coefficient A from Eq. (19).
6. Derive the B coefficient from Eq. (10).
7. Determine the particle size distribution  $n(r)$  from Eq. (9).
8. Derive the total number concentration of droplets for all radii using Eq. (11).
9. Plot the output of steps 7 and 8 to depict surface level fog droplet conditions.
10. Determine if other constituents are also restricting the visibility and solve for and incorporate their contributions to the overall particle size distribution.
11. Derive the vertical variation of  $r_c$  and  $W_L$  from Eqs. (29) and (30) and incorporate and repeat step 4 through 10 to obtain particle

size distribution at any desired level within the fog layer.

Using the above steps we computed particle size distribution for observations (Justo 1979) of haze and radiation fog. Meyer's (1980) data showed that a good linear relation exists between visual ranges equal to or greater than 5 km and the cumulative number concentration of haze particles. The number concentration almost remains constant for haze/fog conditions with visual ranges from 1 to 5 km. For visual ranges less than about 1 km a linear relation exists between the number concentration and visual range in dense fog. Therefore, for fog and haze conditions, the haze component of particle size distribution was computed for a visual range of 5 km and was held constant and added to the fog contribution which varied with visual range. Our results are shown in Fig. 18 for two reported visibilities, 2.1 and 0.39 km. For comparison, observed size distributions are shown for three observation times 0725, 0730 and 0800 and visibilities 2.1, 1.4, and 0.39 km, respectively. It is striking, however, how good the major features and time trends are represented by our haze/fog model.

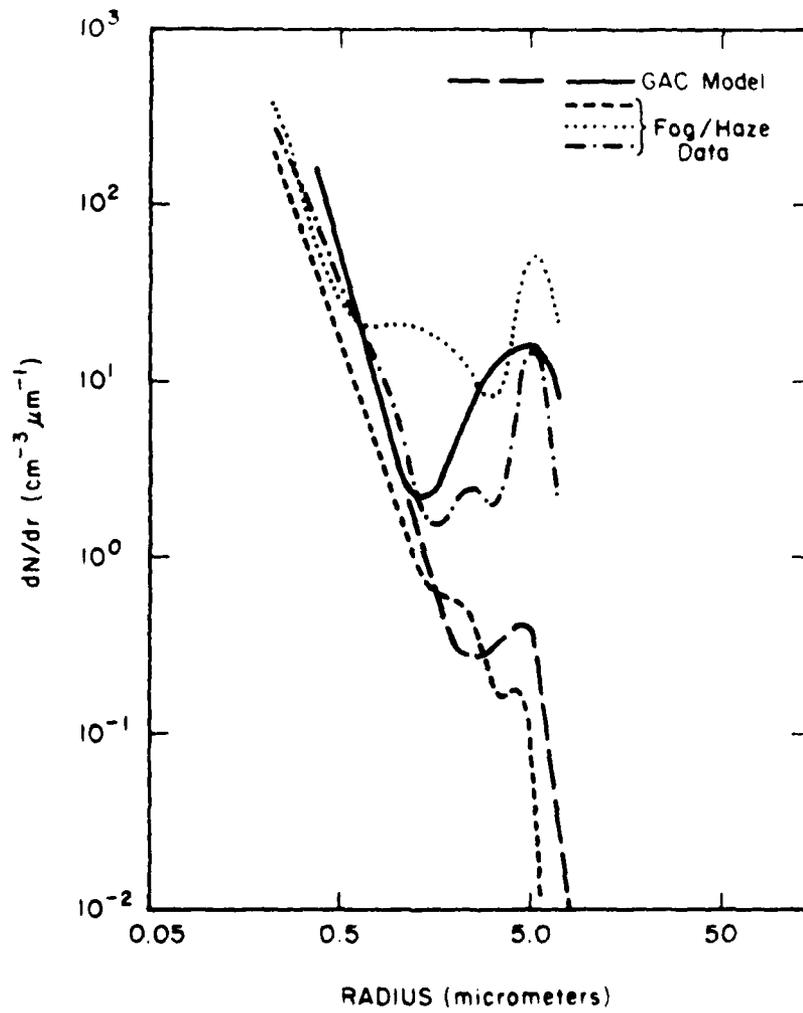


Fig. 18. GAC Haze-Fog Model Compared With Observed Data

## 2.2.2 Cloud

### 2.2.2.1 Cloud Base and In Cloud Variations

We have had a great deal of difficulty looking for common denominators that are applicable to the many cloud physics studies. This is due in part to the fact that most investigators direct their attention to one particular cloud type and then do not measure all variables important to a more generalized study. For example, Table 1 shows that for a particular cloud type there is a most frequent particle radius that occurs on the average for all seasons and types of conditions. Yet it is not unreasonable to expect that cloud particles and their distribution are dependent upon the environment in which they are formed. We have tried to take these features into account from a meso- and synoptic-scale point of view, knowing full well that certain micro-scale features must either be neglected, averaged, or inferred from current observations.

Our desire is to be able to derive cloud characteristics at the cloud base and heights within the cloud, given only standard meteorological observations.

We have found that clouds formed primarily by convection (cumulus and cumulonimbus), turbulence (Stratus, stratocumulus, and altocumulus) and horizontal convergence (altostratus, as well as altocumulus) exhibit distinctive features but, most often when looked at in detail, their microphysics is dictated by the temperature, pressure, dew point, and vertical motion that exists

at the cloud base and levels within the cloud. That is to say, originally it was thought that each cloud type would have to be treated separately. Now, however, we found that cloud base characteristics and their vertical variation within a cloud could be formulated using the most recent surface and upper air observation.

Lewis (1951) compiled tables displaying cloud droplet and liquid water content for a large number of aircraft observations segmented into three broad cloud type categories, i.e. stratus and stratocumulus, alto-stratus and alto-cumulus, and cumulus or cumulonimbus. Separating these categories geographically between the Pacific Coast and other regions of the United States showed that in general cloud drops for corresponding west coast cloud types are about 2 micrometers larger in radius. Although cloud base temperature and to a lesser extent the cloud base pressure height contribute to changes in the mean particle size we were unsure whether sufficient differences existed between clouds on the Pacific Coast versus those in Eastern U.S.A. We used data prepared by the Naval Weather Service in 1976 on "Climatic Study of the Near Coastal Zone" from two publications, "East Coast of the United States" and "West Coast of the United States." On the average the surface air temperature is 10°F warmer in the winter at San Francisco than at Philadelphia and the reverse in summer, so the yearly surface air temperatures are about the same value. More important, however, is that the west coast

clouds occur significantly more frequently at lower heights with warmer cloud base temperatures. This is especially noticeable during the winter when most of the clouds exist and when more than 50 per cent of the west coast clouds have a ceiling height of less than 1000 feet whereas only 15 per cent are found at the same low levels on the east coast. We also analyzed Selby's drop size measurements in low level stratus in another country, England, (Blifford 1970). This was interesting since most of the individual cases gave a mode radius of 2 micrometers for cloud droplets within the lower 30 to 60 meters of their stratus clouds. Such small droplets near the cloud base are reported more frequently in the later literature as instrument measuring technology improved. The main point is that major features of these liquid clouds from wide geographical locations were found to be represented by our following procedures. Spatial distribution of the microstructure of cloud liquid water content varies considerably in both horizontal and vertical directions. This is especially true for convective type storms where vertical cloud development is more pronounced, vertical motions are higher, the total cloud cellular structure is often composed of a combination of individual sub cells, and the turbulent motions produce more entrainment of drier ambient air which reduces the available liquid water and causes gradients in the actual liquid water content. A possibility does exist to use remote probing techniques to better define the actual cloud microstructure. However, since this study is

restricted to using standard surface and upper air observations, we have developed techniques to depict major features associated with these meso-scale phenomena. Using information contained in our CIVAS (cloud/icing visibility analysis system) we can specify the cloud base height and temperature, cloud type, and vertical and horizontal extent. From this we can compute the available liquid water content produced by cloud air rising along its moist adiabatic lapse rate. This approach produces the amount of liquid water that can be expected at each level in the cloud. As discussed above some of this water has to go to injecting moisture into the dry entrained air to bring it to saturation and thus the actual liquid water contained at any cloud level is less than that expected from purely adiabatic processes. Furthermore this effect and moisture reduction increases with altitude in the cloud. A number of cloud physics studies have been made showing the changes of the ratio of actual cloud liquid water to that expected adiabatically as a function of height above the cloud base, Pruppacher (1980). In general the actual liquid water is a high percentage of that available near the cloud base and decreases to nearly a quarter of that available by one kilometer above the cloud base and remains essentially constant at higher cloud levels. We have fitted these data with a linear curve covering the first kilometer of the cloud and a constant value of 0.2 for the liquid water content ratio at higher levels in the cloud. The equations are

and 
$$W_L / W_{AL} = 1 - 0.8 Z_{ACB} \text{ for } Z_{ACB} = 0 \text{ to } 1 \text{ km} \quad (31)$$

$$W_L / W_{AL} = 0.2 \quad \text{for } Z_{ACB} > 1 \text{ km} \quad (32)$$

where  $Z$  is the height in km above the cloud base and the ratio is the cloud liquid water content ( $W_L$ ) relative to the cloud liquid water content available ( $W_{AL}$ ) through moist adiabatic processes. This information will be combined with other cloud characteristics to obtain a measure of size distribution and number concentration of cloud droplets at different heights in the cloud.

Complicated equations are necessary to precisely derive the complicated pseudoadiabatic lapse rate as a function of temperature and pressure at the cloud condensation level, including both the liquid or ice stage of the cloud. Another set of equations is necessary to derive the saturation mixing ratio over water and over ice as a function of air temperature and pressure within the clouds. By incrementally solving these equations it is possible to derive the available liquid water at each level in a cloud. This precision is unwarranted at this time. Considering the uncertainties in other approximations to depicting cloud microphysical features, we have derived the following simplified equations to derive the available liquid water concentration,  $W_{AL}$ , produced by moist adiabatically lifted air

for the first kilometer in the cloud

$$W_{AL} = (1.42 + 0.05 T_{CB}) Z_{ACB} \quad (33)$$

and for heights greater than one kilometer above cloud base

$$W_{AL} = 1.42 + 0.05 T_{CB} + (0.84 + 0.035 T_{CB}) (Z_{ACB} - 1) \quad (34)$$

where  $W_{AL}$  is in  $g\ m^{-3}$ ,  $T_{CB}$  is the cloud base temperature in  $^{\circ}C$  and  $Z_{ACB}$  is the height above cloud base in km.

Next we wanted to obtain a quantitative method to derive the mode radius  $r_c$  since this is a necessary variable in utilizing the previously described exponential distribution. The peak radius of a size distribution curve was found to be directly proportional to the amount of liquid water and the cloud base temperature. We empirically derived

$$r_c = \left( \frac{3.17 \times 10^4 W_L}{340 - 8 T_{CB}} \right)^{1/3} \quad (35)$$

where  $r_c$  is the mode radius in micrometers,  $W_L$  is the cloud liquid water content in  $g\ m^{-3}$ , and  $T_{CB}$  is the cloud base temperature in  $^{\circ}C$ . This equation was derived assuming a shape factor  $\alpha = 2$  and using continental cumulus cloud data to derive  $N = 340 - 8 T_{CB}$  in order to relate the average total cloud base droplet concentration to cloud base temperature. Because of the limited time available for this study, this equation was then used for all cloud types. In order to derive the mode radius at the cloud

base, we assumed no entrainment within the first tenth of a kilometer of the cloud to derive  $W_L$ , which is then dependent only upon the cloud base temperature. Therefore, the mode radius  $r_c$  at any cloud base is given only by the cloud base temperature, producing mode radii equal to 2.8, 3.5, and 4.5 micrometers for cloud base temperatures of 10, 20 and 30°C respectively.

We then explored two methods to depict vertical changes of the mode radius within a cloud. We used aircraft observations, Blifford 1970, of summer cumulus and obtained the following best fit equation

$$r_{c,Z} = r_{c,Z_{CB}} + 2.3 Z_{ACB} \quad (36)$$

where  $r_{c,Z}$  and  $r_{c,Z_{CB}}$  is the mode radius at any height  $Z$  within the cloud and at the height  $Z_{CB}$  of the cloud base, respectively, and  $Z_{ACB}$  is the height in kilometers above cloud base. The other method was to use the above equations to derive liquid content and mode radius at any given height within a cloud of known base temperature. Also used was Eq. (28) to derive the shape factor  $\alpha$ , Eqs. (10) and (12) to derive the B and A coefficients, and Eq. (11) to derive the total droplet concentration  $N$  per cubic centimeter volume. Before looking at detailed comparisons of computed versus observed droplet characteristics as a function of height within a cloud, we will look at comparisons with more grossly averaged cloud characteristics.

Observations from 5 different investigators (aufm Kampe & Weickman 1957) were combined to produce a frequency distribution of mean linear droplet radius and water content for layer (stratus) clouds, fair weather cumulus, and cumulus congestus or cumulonimbus. We assumed an average cloud base temperature of 15°C and used the observed liquid water content to compute the expected mode radius. The results are:

<u>Cloud Type</u>	<u>Observed</u>		<u>mode radius</u>	<u>Computed</u>	<u>difference</u>
	<u>liquid water</u>	<u>mean radius</u>		<u>mode radius</u>	
stratus	0.15	5.5	3.7	2.8	0.9
fair weather cumulus	0.6	5.5	3.7	4.4	0.7
cumulonimbus	2.4	12.5	8.3	6.9	1.4

The internal microphysical structure of layer clouds (aufm Kampe & Weickman 1957) was subjected to the same analysis and assumptions as above to obtain averaged conditions for the base, middle, and top of these clouds. The results are:

<u>Cloud Type</u>	<u>Location</u>	<u>Observed</u>		<u>mode radius</u>	<u>Computed</u>	<u>difference</u>
		<u>liquid water</u>	<u>mean radius</u>		<u>mode radius</u>	
stratus	base	0.03	5.5	3.7	1.6	2.1
nimbostratus	middle	0.15	5.5	3.7	2.8	0.9
	top	0.3	8.4	5.5	3.5	2.0
stratocumulus	base	0.15	5.5	3.7	2.8	0.9

<u>Cloud Type (cont.)</u>	<u>Location</u>	liquid <u>water</u>	<u>Observed</u>		<u>Computed</u>		<u>difference</u>
			<u>mean radius</u>	<u>mode radius</u>	<u>mode radius</u>	<u>mode radius</u>	
altocumulus	middle	0.30	5.5	3.7	3.5	0.2	
(altostratus)	top	0.15	5.5	3.7	2.8	0.9	

It is interesting that the differences between computed and observed mode radius are about one micrometer for almost all cloud types, except stratus where computed values are about two micrometers too small.

We looked at greater vertical detail of cumulus cloud observations (aufm Kampe & Weickman 1957) and used both methods described above to compute expected conditions. In this case the average cloud base temperature was 25°C and we obtained the following comparisons for cumulus clouds:

<u>Height Within Cloud</u>	<u>Observed</u>			<u>Computed "A"</u>			<u>Computed "B"</u>		
	<u>r<sub>c</sub></u>	<u>W<sub>L</sub></u>	<u>N</u>	<u>r<sub>c</sub></u>	<u>W<sub>L</sub></u>	<u>N</u>	<u>r<sub>c</sub></u>	<u>W<sub>L</sub></u>	<u>N</u>
base	2.0	0.15	330	3.8	0.25	246	3.8	0.25	246
1 km	9.2	1.0	150	4.8	0.53	153	6.1	0.53	74
3 km	9.9	2.8	60	6.4	1.22	50	10.7	1.22	10
5 km	7.9	2.0	50	7.4	1.91	52	15.3	1.01	13

where computed "B" uses empirical Eq. (36) relating mode radius as a function of only initial conditions at cloud base and height above it where as computed "A" uses the computed vertical distribution of liquid water and

the corresponding shape factor and mode radius for a given cloud base temperature. In all cases, total particle number content is best obtained at all levels within a cumulus cloud by using method "A", whereas in most cases method "B" provides the best representation of the mode radius. The liquid water content is computed the same for both methods and is always somewhat smaller than observed. This implies our entrainment equation is exerting slightly greater influence than required for this case. Actually, with a higher liquid water content computed, a larger mode radius would be computed and method "A" would be most applicable overall.

#### 2.2.2.2 Dynamic Procedure

1. Using objective surface and upper air analysis techniques, such as CIVAS, obtain cloud type, cloud base temperature, cloud height above ground level, and horizontal and vertical extent.
2. Compute the liquid water content applicable at or near the cloud base using Eq. (33) with  $Z_{ACB} = 0.1$  km.
3. Combine the cloud base temperature and liquid water content in Eq. (35) to derive expected cloud base droplet mode radius.
4. Derive the cloud liquid water content as a function height in the cloud by applying either Eqs. (33) or (34) and applying the entrainment factor Equations (31) or (32), depending upon height above cloud base.
5. Determine the exponential shape factor using Eq. (28) at each desired height in the cloud where liquid water content was computed.
6. Use Eqs. (9), (10), (11), and (12) to derive the details of the number concentration and drop size distribution as a function of horizontal and vertical distance within the cloud.

### 2.2.3 Rain

#### 2.2.3.1 Ground and Upper Level Variations

Wartime radar research provided special urgency in measuring raindrop size distribution. In 1943 Laws and Parsons began a new approach to the problem by collecting raindrop size data and relating them to the intensity of precipitation. They found as rain intensity increased so did the average raindrop size. Also they could use climatological rain rate data to infer drop sizes and effects on radar for different geographical locations and seasons of the year. Today our communications and weather reporting network is such that daily and hourly routine meteorological observations are available on a global basis. After World War II the Stormy Weather Research Group at McGill University studied weather radar responses to rainfall. Marshall and Palmer (1948) then found that the raindrop size distribution relative to rain rate could be fitted by

$$N(D) = N_0 \exp(-bD) \quad (37)$$

where  $N(D)$  is the number raindrop per unit volume ( $m^3$ ) and per unit drop diameter  $D$  (mm),  $N_0$  is the limiting value of  $N(D)$  for  $D = 0$  and is often taken as  $N_0 = 8000 m^{-3} mm^{-1}$  and the coefficient  $b$  in units  $mm^{-1}$  is related to the rainfall rate ( $R$ ) in  $mm hr^{-1}$  by

$$b = 4.1 R^{-0.21} mm^{-1} \quad (38)$$

Fig. 19 shows the raindrop size distribution as a function of rainfall rate, Laws and Parson data (broken line), and observations at Ottawa (dotted lines). It can be seen that good correspondence exists for all raindrop sizes and rainfall rates except for the smaller drops where the Marshall-Palmer method overpredicts the number of small raindrops. There is also an upper raindrop size limit because large drops (5 or 6 mm) become unstable and break up. Cole et al (1969) suggests limiting the Marshall-Palmer method to raindrop diameters between 0.75 and 2.25 mm for rain rates around  $1 \text{ mm hr}^{-1}$ , between 1.25 and 3 mm for rain rates near  $5 \text{ mm hr}^{-1}$ , and between 1.5 and 4.5 mm for rain rates greater than  $25 \text{ mm hr}^{-1}$ . In general, however, the Marshall-Palmer method performs reasonably well to provide an average drop size spectrum for a given rainrate. In Switzerland, Joss found the Marshall-Palmer model performed well for the same type of continuous precipitation in which it was developed but for drizzle and thunderstorm precipitation the coefficient  $N_0$  had to be increased and decreased by a factor of 4 and 1/8th, respectively.

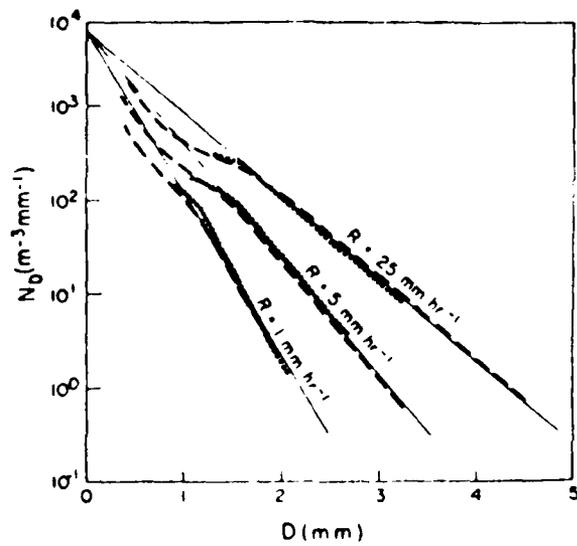


Fig. 19 Raindrop Size Distribution Vs. Rainfall Intensity

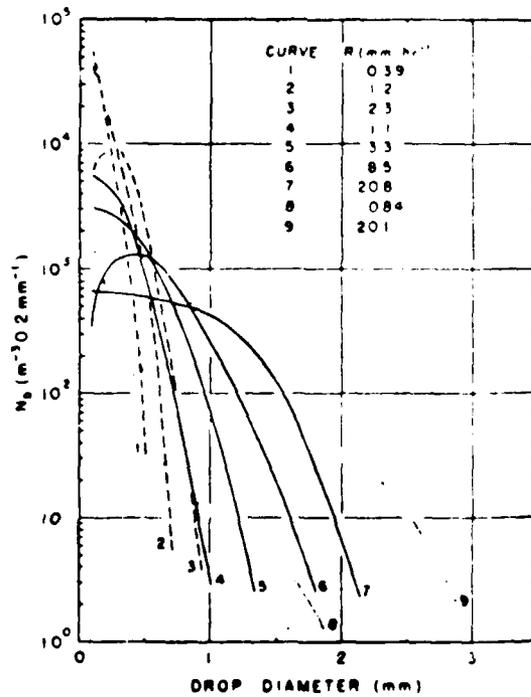


Fig. 20 Variety of Raindrop Size Distributions

Fig. 20 shows the large variety of raindrop size distributions that exist for different geographical locations, type of rain, and rainfall intensity. Blanchard's curves 1 - 3 are for Hawaiian in-cloud measurements made at or near the dissipating edge of non-freezing orographic clouds, while curves 4 - 7 represent data taken at the cloud base. Curves 8 - 9 are for non-orographic rain distributions. Curves 1 - 3 are typical of what is expected in a combined light rain, drizzle, and cloud environment, that is the particle size distribution is narrow and the peak frequency occurs at very small drop sizes. From the cloud base to the earth's surface it can be seen that the peak frequency or mode drop diameter increases and the distribution broadens as rainfall intensity increases. This is also observed in our particle size and number concentration distribution for mist, drizzle, light rain, moderate rain, and heavy rain in Tables 3, 4, 5, and 6, respectively.

TABLE 3 Mist and Drizzle Particles

PARTICLE SIZE AND NUMBER CONCENTRATION DISTRIBUTION

WEATHER TYPE	PARTICLE NUMBER DENSITY ( $\text{Km}^{-3}$ )	PARTICLE RADIUS (Km)
--------------	--	----------------------

MIST

(0.05 mm/hr)	$6 \times 10^9$	$6.5 \times 10^{-9}$
	$13 \times 10^9$	$15 \times 10^{-9}$
	$51 \times 10^9$	$35 \times 10^{-9}$
	$69 \times 10^9$	$75 \times 10^{-9}$
	$51 \times 10^9$	$150 \times 10^{-9}$
	$10 \times 10^9$	$250 \times 10^{-9}$
	$2 \times 10^9$	$350 \times 10^{-9}$
	$.5 \times 10^9$	$450 \times 10^{-9}$
	$.1 \times 10^9$	$550 \times 10^{-9}$

DRIZZLE

(.25 mm/hr)	$6 \times 10^9$	$6.5 \times 10^{-9}$
	$13 \times 10^9$	$15 \times 10^{-9}$
	$51 \times 10^9$	$35 \times 10^{-9}$
	$80 \times 10^9$	$75 \times 10^{-9}$
	$85 \times 10^9$	$150 \times 10^{-9}$
	$26 \times 10^9$	$250 \times 10^{-9}$
	$9 \times 10^9$	$350 \times 10^{-9}$
	$3 \times 10^9$	$450 \times 10^{-9}$
	$1 \times 10^9$	$550 \times 10^{-9}$
	$.3 \times 10^9$	$650 \times 10^{-9}$
$.1 \times 10^9$	$750 \times 10^{-9}$	

TABLE 4 Light Rain Particles

PARTICLE SIZE AND NUMBER CONCENTRATION DISTRIBUTION

WEATHER TYPE	PARTICLE NUMBER DENSITY ( $Km^{-3}$ )	PARTICLE RADIUS ( $Km$ )
<u>LIGHT RAIN</u>		
(1 mm/hr)	$6 \times 10^9$	$6.5 \times 10^{-9}$
	$13 \times 10^9$	$15 \times 10^{-9}$
	$51 \times 10^9$	$35 \times 10^{-9}$
	$85 \times 10^9$	$75 \times 10^{-9}$
	$106 \times 10^9$	$150 \times 10^{-9}$
	$54 \times 10^9$	$250 \times 10^{-9}$
	$24 \times 10^9$	$350 \times 10^{-9}$
	$11 \times 10^9$	$450 \times 10^{-9}$
	$5 \times 10^9$	$550 \times 10^{-9}$
	$2 \times 10^9$	$650 \times 10^{-9}$
	$1 \times 10^9$	$750 \times 10^{-9}$
	$.4 \times 10^9$	$850 \times 10^{-9}$
	$.2 \times 10^9$	$950 \times 10^{-9}$
	$.3 \times 10^9$	$1250 \times 10^{-9}$

TABLE 5 Moderate Rain Particles

PARTICLE SIZE AND NUMBER CONCENTRATION DISTRIBUTION

WEATHER TYPE	PARTICLE NUMBER DENSITY ( $\text{Km}^{-3}$ )	PARTICLE RADIUS ( $\text{Km}$ )
<u>MODERATE RAIN</u>		
(4 mm/hr)	$6 \times 10^9$	$6.5 \times 10^{-9}$
	$13 \times 10^9$	$15 \times 10^{-9}$
	$51 \times 10^9$	$35 \times 10^{-9}$
	$90 \times 10^9$	$75 \times 10^{-9}$
	$146 \times 10^9$	$150 \times 10^{-9}$
	$87 \times 10^9$	$250 \times 10^{-9}$
	$49 \times 10^9$	$350 \times 10^{-9}$
	$27 \times 10^9$	$450 \times 10^{-9}$
	$15 \times 10^9$	$550 \times 10^{-9}$
	$8 \times 10^9$	$650 \times 10^{-9}$
	$4 \times 10^9$	$750 \times 10^{-9}$
	$2 \times 10^9$	$850 \times 10^{-9}$
	$1 \times 10^9$	$950 \times 10^{-9}$
	$.2 \times 10^9$	$1250 \times 10^{-9}$
	$.1 \times 10^9$	$1750 \times 10^{-9}$

TABLE 6 Heavy Rain Particles

PARTICLE SIZE AND NUMBER CONCENTRATION DISTRIBUTION

WEATHER TYPE	PARTICLE NUMBER DENSITY ( $\text{Km}^{-3}$ )	PARTICLE RADIUS (Km)
<u>HEAVY RAIN</u>  (16 mm/hr)	$6 \times 10^9$	$6.5 \times 10^{-9}$
	$13 \times 10^9$	$15 \times 10^{-9}$
	$51 \times 10^9$	$35 \times 10^{-9}$
	$92 \times 10^9$	$75 \times 10^{-9}$
	$160 \times 10^9$	$150 \times 10^{-9}$
	$110 \times 10^9$	$250 \times 10^{-9}$
	$75 \times 10^9$	$350 \times 10^{-9}$
	$50 \times 10^9$	$450 \times 10^{-9}$
	$32 \times 10^9$	$550 \times 10^{-9}$
	$20 \times 10^9$	$650 \times 10^{-9}$
	$13 \times 10^9$	$750 \times 10^{-9}$
	$8 \times 10^9$	$850 \times 10^{-9}$
	$6 \times 10^9$	$950 \times 10^{-9}$
	$13 \times 10^9$	$1250 \times 10^{-9}$
	$2 \times 10^9$	$1750 \times 10^{-9}$
$.1 \times 10^9$	$2250 \times 10^{-9}$	

We have developed models to represent the simultaneous vertical variations in rain rate and liquid cloud content from the earth's surface to cloud top. Shown in Table 7 and 8 is our summer mid-latitude moderate (6 mm/hr) and heavy (15 mm/hr) rain model which provides air pressure, temperature, relative humidity, cloud content, and rain rate as a function of height in the atmosphere. Notice that they both have the same cloud base and top but differ significantly in cloud liquid water content and rain rate outside and within the cloud. The rain rate decreases rather slowly (at about 0.5 mm/hr/.25 km) from the surface to about midway through the cloud where it drops to near zero very rapidly. This same vertical variation in rain rate was found to also prevail at tropical latitudes for the same heavy rain situation, Fig. 9, but where the cloud top extends to far greater heights.

The general form of the exponential function, as given in our Eq. (4), has been simplified and used by Bent, Deirmendjian, and Khrgian and Mazin to specify static models of rain. If we take our Eq. (17) and insert the difference in velocity between the updraft ( $V_u$ ) and terminal fall ( $V_T$ ) velocity, ( $V_T - V_u$ ), in the integrand it transposes the left hand side of the equation from the total mass concentration of liquid water into the rainfall rate. When the updraft is small relative to droplet terminal fall velocities then the equation simplifies, and, as shown in Fig. 21, remains

TABLE 7 Moderate Rain (6 mm/hr) For Summer Mid-Latitudes

RAIN MODEL ATMOSPHERE - MODERATE RAIN - 6 MM/HR			45 N MODEL - MID-LATITUDE		
HEIGHT (KM)	PRESSURE (MB)	TEMPERATURE (DEG C)	RELATIVE HUMIDITY	CLOUD CONTENT (GM/CU M)	RAIN RATE (MM/HR)
0.000	1013.00	287.20	1.000	0.0000	6.000
.250	983.00	286.20	1.000	.2000	5.500
.500	954.00	285.10	1.000	.2000	4.400
.750	926.00	284.00	1.000	.3200	3.500
1.000	899.00	282.70	1.000	.3300	3.000
1.250	872.00	281.20	1.000	.3400	2.400
1.500	846.00	280.00	1.000	.3500	1.900
1.750	820.00	278.50	1.000	.3500	1.500
2.000	795.00	277.30	1.000	.3500	1.100
2.500	747.00	274.40	1.000	.3500	.600
3.000	701.00	271.20	1.000	.3500	.200
3.500	658.00	268.50	1.000	.3100	-0.000
4.000	616.00	265.00	1.000	.2500	-0.000
4.500	577.00	261.00	1.000	.1800	-0.000
5.000	540.00	258.00	1.000	.1300	-0.000
5.500	505.00	254.50	1.000	.0900	-0.000
6.000	472.00	251.50	1.000	.0500	-0.000
6.500	440.00	246.70	1.000	.0300	-0.000
7.000	410.00	242.20	1.000	.0100	-0.000
7.500	382.00	238.00	1.000	-0.0000	-0.000
8.000	356.00	234.50	1.000	-0.0000	-0.000
8.500	330.00	229.00	1.000	-0.0000	-0.000
9.000	307.00	225.00	.900	-0.0000	-0.000
9.500	285.00	220.00	.850	-0.0000	-0.000
10.000	264.00	223.20	.800	-0.0000	-0.000
11.000	226.00	216.70	.400	-0.0000	-0.000
12.000	193.00	216.70	.160	-0.0000	-0.000
13.000	165.00	216.70	.060	-0.0000	-0.000
14.000	141.00	216.70	.041	-0.0000	-0.000
15.000	120.00	216.70	.031	-0.0000	-0.900
16.000	103.00	216.70	.023	-0.0000	-0.000
17.000	87.00	216.70	.019	-0.0000	-0.000
18.000	75.00	216.70	.016	-0.0000	-0.000
19.000	66.10	216.70	.014	-0.0000	-0.000
20.000	58.70	216.70	.012	-0.0000	-0.000
22.000	48.00	210.70	.007	-0.0000	-0.000
24.000	39.00	220.70	.004	-0.0000	-0.000
26.000	31.50	222.70	.002	-0.0000	-0.000
28.000	25.00	224.70	.001	-0.0000	-0.000
30.000	19.70	226.70	-0.000	-0.0000	-0.000
35.000	5.00	237.00	-0.000	-0.0000	-0.000
40.000	2.00	251.00	-0.000	-0.0000	-0.000
45.000	1.40	265.00	-0.000	-0.0000	-0.000
50.000	.80	270.70	-0.000	-0.0000	-0.000

TABLE 8 Heavy Rain (15 mm/hr) For Mid-Latitudes

RAIN MODEL ATMOSPHERE - HEAVY RAIN - 15 MM/HR			US N MODEL - MID-LATITUDE		
HEIGHT (KM)	PRESSURE (MB)	TEMPERATURE (DEG K)	RELATIVE HUMIDITY	CLOUD CONTENT (G/GU M)	RAIN RATE (MM/HR)
0.000	1013.02	287.20	1.000	0.0000	15.000
0.250	983.00	286.20	1.000	0.3000	14.600
0.500	954.00	285.10	1.000	0.4000	14.100
0.750	926.00	284.00	1.000	0.5000	13.600
1.000	899.00	282.70	1.000	0.5000	13.200
1.250	873.00	281.20	1.000	0.5000	12.800
1.500	848.00	279.60	1.000	0.5000	12.400
1.750	824.00	277.90	1.000	0.5000	12.000
2.000	800.00	277.00	1.000	0.5000	11.600
2.250	777.00	276.00	1.000	0.5000	11.200
2.500	754.00	274.90	1.000	0.5000	10.800
2.750	731.00	273.70	1.000	0.5000	10.400
3.000	709.00	272.40	1.000	0.5000	10.000
3.250	687.00	271.00	1.000	0.5000	9.600
3.500	666.00	269.50	1.000	0.5000	9.200
3.750	645.00	268.00	1.000	0.5000	8.800
4.000	625.00	266.40	1.000	0.5000	8.400
4.250	605.00	264.80	1.000	0.5000	8.000
4.500	586.00	263.10	1.000	0.5000	7.600
4.750	567.00	261.40	1.000	0.5000	7.200
5.000	549.00	259.60	1.000	0.5000	6.800
5.250	531.00	257.80	1.000	0.5000	6.400
5.500	514.00	256.00	1.000	0.5000	6.000
5.750	497.00	254.10	1.000	0.5000	5.600
6.000	481.00	252.20	1.000	0.5000	5.200
6.250	465.00	250.30	1.000	0.5000	4.800
6.500	449.00	248.40	1.000	0.5000	4.400
6.750	434.00	246.50	1.000	0.5000	4.000
7.000	419.00	244.60	1.000	0.5000	3.600
7.250	404.00	242.70	1.000	0.5000	3.200
7.500	389.00	240.80	1.000	0.5000	2.800
7.750	374.00	238.90	1.000	0.5000	2.400
8.000	359.00	237.00	1.000	0.5000	2.000
8.250	344.00	235.10	1.000	0.5000	1.600
8.500	329.00	233.20	1.000	0.5000	1.200
8.750	314.00	231.30	1.000	0.5000	0.800
9.000	299.00	229.40	1.000	0.5000	0.400
9.250	284.00	227.50	1.000	0.5000	0.000
9.500	269.00	225.60	1.000	0.5000	0.000
9.750	254.00	223.70	1.000	0.5000	0.000
10.000	239.00	221.80	1.000	0.5000	0.000
10.250	224.00	219.90	1.000	0.5000	0.000
10.500	209.00	218.00	1.000	0.5000	0.000
10.750	194.00	216.10	1.000	0.5000	0.000
11.000	179.00	214.20	1.000	0.5000	0.000
11.250	164.00	212.30	1.000	0.5000	0.000
11.500	149.00	210.40	1.000	0.5000	0.000
11.750	134.00	208.50	1.000	0.5000	0.000
12.000	119.00	206.60	1.000	0.5000	0.000
12.250	104.00	204.70	1.000	0.5000	0.000
12.500	89.00	202.80	1.000	0.5000	0.000
12.750	74.00	200.90	1.000	0.5000	0.000
13.000	59.00	199.00	1.000	0.5000	0.000
13.250	44.00	197.10	1.000	0.5000	0.000
13.500	29.00	195.20	1.000	0.5000	0.000
13.750	14.00	193.30	1.000	0.5000	0.000
14.000	0.00	191.40	1.000	0.5000	0.000
14.250	0.00	189.50	1.000	0.5000	0.000
14.500	0.00	187.60	1.000	0.5000	0.000
14.750	0.00	185.70	1.000	0.5000	0.000
15.000	0.00	183.80	1.000	0.5000	0.000
15.250	0.00	181.90	1.000	0.5000	0.000
15.500	0.00	180.00	1.000	0.5000	0.000
15.750	0.00	178.10	1.000	0.5000	0.000
16.000	0.00	176.20	1.000	0.5000	0.000
16.250	0.00	174.30	1.000	0.5000	0.000
16.500	0.00	172.40	1.000	0.5000	0.000
16.750	0.00	170.50	1.000	0.5000	0.000
17.000	0.00	168.60	1.000	0.5000	0.000
17.250	0.00	166.70	1.000	0.5000	0.000
17.500	0.00	164.80	1.000	0.5000	0.000
17.750	0.00	162.90	1.000	0.5000	0.000
18.000	0.00	161.00	1.000	0.5000	0.000
18.250	0.00	159.10	1.000	0.5000	0.000
18.500	0.00	157.20	1.000	0.5000	0.000
18.750	0.00	155.30	1.000	0.5000	0.000
19.000	0.00	153.40	1.000	0.5000	0.000
19.250	0.00	151.50	1.000	0.5000	0.000
19.500	0.00	149.60	1.000	0.5000	0.000
19.750	0.00	147.70	1.000	0.5000	0.000
20.000	0.00	145.80	1.000	0.5000	0.000
20.250	0.00	143.90	1.000	0.5000	0.000
20.500	0.00	142.00	1.000	0.5000	0.000
20.750	0.00	140.10	1.000	0.5000	0.000
21.000	0.00	138.20	1.000	0.5000	0.000
21.250	0.00	136.30	1.000	0.5000	0.000
21.500	0.00	134.40	1.000	0.5000	0.000
21.750	0.00	132.50	1.000	0.5000	0.000
22.000	0.00	130.60	1.000	0.5000	0.000
22.250	0.00	128.70	1.000	0.5000	0.000
22.500	0.00	126.80	1.000	0.5000	0.000
22.750	0.00	124.90	1.000	0.5000	0.000
23.000	0.00	123.00	1.000	0.5000	0.000
23.250	0.00	121.10	1.000	0.5000	0.000
23.500	0.00	119.20	1.000	0.5000	0.000
23.750	0.00	117.30	1.000	0.5000	0.000
24.000	0.00	115.40	1.000	0.5000	0.000
24.250	0.00	113.50	1.000	0.5000	0.000
24.500	0.00	111.60	1.000	0.5000	0.000
24.750	0.00	109.70	1.000	0.5000	0.000
25.000	0.00	107.80	1.000	0.5000	0.000
25.250	0.00	105.90	1.000	0.5000	0.000
25.500	0.00	104.00	1.000	0.5000	0.000
25.750	0.00	102.10	1.000	0.5000	0.000
26.000	0.00	100.20	1.000	0.5000	0.000
26.250	0.00	98.30	1.000	0.5000	0.000
26.500	0.00	96.40	1.000	0.5000	0.000
26.750	0.00	94.50	1.000	0.5000	0.000
27.000	0.00	92.60	1.000	0.5000	0.000
27.250	0.00	90.70	1.000	0.5000	0.000
27.500	0.00	88.80	1.000	0.5000	0.000
27.750	0.00	86.90	1.000	0.5000	0.000
28.000	0.00	85.00	1.000	0.5000	0.000
28.250	0.00	83.10	1.000	0.5000	0.000
28.500	0.00	81.20	1.000	0.5000	0.000
28.750	0.00	79.30	1.000	0.5000	0.000
29.000	0.00	77.40	1.000	0.5000	0.000
29.250	0.00	75.50	1.000	0.5000	0.000
29.500	0.00	73.60	1.000	0.5000	0.000
29.750	0.00	71.70	1.000	0.5000	0.000
30.000	0.00	69.80	1.000	0.5000	0.000
30.250	0.00	67.90	1.000	0.5000	0.000
30.500	0.00	66.00	1.000	0.5000	0.000
30.750	0.00	64.10	1.000	0.5000	0.000
31.000	0.00	62.20	1.000	0.5000	0.000
31.250	0.00	60.30	1.000	0.5000	0.000
31.500	0.00	58.40	1.000	0.5000	0.000
31.750	0.00	56.50	1.000	0.5000	0.000
32.000	0.00	54.60	1.000	0.5000	0.000
32.250	0.00	52.70	1.000	0.5000	0.000
32.500	0.00	50.80	1.000	0.5000	0.000
32.750	0.00	48.90	1.000	0.5000	0.000
33.000	0.00	47.00	1.000	0.5000	0.000
33.250	0.00	45.10	1.000	0.5000	0.000
33.500	0.00	43.20	1.000	0.5000	0.000
33.750	0.00	41.30	1.000	0.5000	0.000
34.000	0.00	39.40	1.000	0.5000	0.000
34.250	0.00	37.50	1.000	0.5000	0.000
34.500	0.00	35.60	1.000	0.5000	0.000
34.750	0.00	33.70	1.000	0.5000	0.000
35.000	0.00	31.80	1.000	0.5000	0.000
35.250	0.00	29.90	1.000	0.5000	0.000
35.500	0.00	28.00	1.000	0.5000	0.000
35.750	0.00	26.10	1.000	0.5000	0.000
36.000	0.00	24.20	1.000	0.5000	0.000
36.250	0.00	22.30	1.000	0.5000	0.000
36.500	0.00	20.40	1.000	0.5000	0.000
36.750	0.00	18.50	1.000	0.5000	0.000
37.000	0.00	16.60	1.000	0.5000	0.000
37.250	0.00	14.70	1.000	0.5000	0.000
37.500	0.00	12.80	1.000	0.5000	0.000
37.750	0.00	10.90	1.000	0.5000	0.000
38.000	0.00	9.00	1.000	0.5000	0.000
38.250	0.00	7.10	1.000	0.5000	0.000
38.500	0.00	5.20	1.000	0.5000	0.000
38.750	0.00	3.30	1.000	0.5000	0.000
39.000	0.00	1.40	1.000	0.5000	0.000
39.250	0.00	-0.50	1.000	0.5000	0.000
39.500	0.00	-2.40	1.000	0.5000	0.000
39.750	0.00	-4.30	1.000	0.5000	0.000
40.000	0.00	-6.20	1.000	0.5000	0.000
40.250	0.00	-8.10	1.000	0.5000	0.000
40.500	0.00	-10.00	1.000	0.5000	0.000
40.750	0.00	-11.90	1.000	0.5000	0.000
41.000	0.00	-13.80	1.000	0.5000	0.000
41.250	0.00	-15.70	1.000	0.5000	0.000
41.500	0.00	-17.60	1.000	0.5000	0.000
41.750	0.00	-19.50	1.000	0.5000	0.000
42.000	0.00	-21.40	1.000	0.5000	0.000
42.250	0.00	-23.30	1.000	0.5000	0.000
42.500	0.00	-25.20	1.000	0.5000	0.000
42.750	0.00	-27.10	1.000	0.5000	0.000
43.000	0.00	-29.00	1.000	0.5000	0.000
43.250	0.00	-30.90	1.000	0.5000	0.000
43.500	0.00	-32.80	1.000	0.5000	0.000
43.750	0.00	-34.70	1.000	0.5000	0.000
44.000	0.00	-36.60	1.000	0.5000	0.000
44.250	0.00	-38.50	1.000	0.5000	0.000
44.500	0.00	-40.40	1.000	0.5000	0.000
44.750	0.00	-42.30	1.000	0.5000	0.000
45.000	0.00	-44.20	1.000	0.5000	0.000
45.250	0.00	-46.10	1.0		

TABLE 9 Heav Rain (15 mm/hr) For Tropical Latitudes

TROPICAL - 15 N	HEAVY RAIN OF 15 MM/HR		RELATIVE	CLOUD CONTENT	RAIN RATE
HEIGHT (KM)	PRESSURE (MB)	TEMPERATURE (DEG K)	HUMIDITY	(GM/CM <sup>3</sup> )	(MM/HR)
0.000	1013.00	298.00	1.000	-0.0000	15.000
0.250	1008.00	297.20	1.000	.2000	14.500
0.500	1003.00	296.40	1.000	.4000	14.000
0.750	998.00	295.60	1.000	.6000	13.500
1.000	993.00	294.80	1.000	.8000	13.000
1.250	988.00	294.00	1.000	1.0000	12.500
1.500	983.00	293.20	1.000	1.2000	12.000
1.750	978.00	292.40	1.000	1.4000	11.500
2.000	973.00	291.60	1.000	1.6000	11.000
2.250	968.00	290.80	1.000	1.8000	10.500
2.500	963.00	290.00	1.000	2.0000	10.000
2.750	958.00	289.20	1.000	2.2000	9.500
3.000	953.00	288.40	1.000	2.4000	9.000
3.250	948.00	287.60	1.000	2.6000	8.500
3.500	943.00	286.80	1.000	2.8000	8.000
3.750	938.00	286.00	1.000	3.0000	7.500
4.000	933.00	285.20	1.000	3.2000	7.000
4.250	928.00	284.40	1.000	3.4000	6.500
4.500	923.00	283.60	1.000	3.6000	6.000
4.750	918.00	282.80	1.000	3.8000	5.500
5.000	913.00	282.00	1.000	4.0000	5.000
5.250	908.00	281.20	1.000	4.2000	4.500
5.500	903.00	280.40	1.000	4.4000	4.000
5.750	898.00	279.60	1.000	4.6000	3.500
6.000	893.00	278.80	1.000	4.8000	3.000
6.250	888.00	278.00	1.000	5.0000	2.500
6.500	883.00	277.20	1.000	5.2000	2.000
6.750	878.00	276.40	1.000	5.4000	1.500
7.000	873.00	275.60	1.000	5.6000	1.000
7.250	868.00	274.80	1.000	5.8000	.500
7.500	863.00	274.00	1.000	6.0000	.200
7.750	858.00	273.20	1.000	6.2000	.100
8.000	853.00	272.40	1.000	6.4000	-.000
8.250	848.00	271.60	1.000	6.6000	-.000
8.500	843.00	270.80	1.000	6.8000	-.000
8.750	838.00	270.00	1.000	7.0000	-.000
9.000	833.00	269.20	1.000	7.2000	-.000
9.250	828.00	268.40	1.000	7.4000	-.000
9.500	823.00	267.60	1.000	7.6000	-.000
9.750	818.00	266.80	1.000	7.8000	-.000
10.000	813.00	266.00	1.000	8.0000	-.000
10.250	808.00	265.20	1.000	8.2000	-.000
10.500	803.00	264.40	1.000	8.4000	-.000
10.750	798.00	263.60	1.000	8.6000	-.000
11.000	793.00	262.80	1.000	8.8000	-.000
11.250	788.00	262.00	1.000	9.0000	-.000
11.500	783.00	261.20	1.000	9.2000	-.000
11.750	778.00	260.40	1.000	9.4000	-.000
12.000	773.00	259.60	1.000	9.6000	-.000
12.250	768.00	258.80	1.000	9.8000	-.000
12.500	763.00	258.00	1.000	10.0000	-.000
12.750	758.00	257.20	1.000	10.2000	-.000
13.000	753.00	256.40	1.000	10.4000	-.000
13.250	748.00	255.60	1.000	10.6000	-.000
13.500	743.00	254.80	1.000	10.8000	-.000
13.750	738.00	254.00	1.000	11.0000	-.000
14.000	733.00	253.20	1.000	11.2000	-.000
14.250	728.00	252.40	1.000	11.4000	-.000
14.500	723.00	251.60	1.000	11.6000	-.000
14.750	718.00	250.80	1.000	11.8000	-.000
15.000	713.00	250.00	1.000	12.0000	-.000
15.250	708.00	249.20	1.000	12.2000	-.000
15.500	703.00	248.40	1.000	12.4000	-.000
15.750	698.00	247.60	1.000	12.6000	-.000
16.000	693.00	246.80	1.000	12.8000	-.000
16.250	688.00	246.00	1.000	13.0000	-.000
16.500	683.00	245.20	1.000	13.2000	-.000
16.750	678.00	244.40	1.000	13.4000	-.000
17.000	673.00	243.60	1.000	13.6000	-.000
17.250	668.00	242.80	1.000	13.8000	-.000
17.500	663.00	242.00	1.000	14.0000	-.000
17.750	658.00	241.20	1.000	14.2000	-.000
18.000	653.00	240.40	1.000	14.4000	-.000
18.250	648.00	239.60	1.000	14.6000	-.000
18.500	643.00	238.80	1.000	14.8000	-.000
18.750	638.00	238.00	1.000	15.0000	-.000
19.000	633.00	237.20	1.000	15.2000	-.000
19.250	628.00	236.40	1.000	15.4000	-.000
19.500	623.00	235.60	1.000	15.6000	-.000
19.750	618.00	234.80	1.000	15.8000	-.000
20.000	613.00	234.00	1.000	16.0000	-.000
20.250	608.00	233.20	1.000	16.2000	-.000
20.500	603.00	232.40	1.000	16.4000	-.000
20.750	598.00	231.60	1.000	16.6000	-.000
21.000	593.00	230.80	1.000	16.8000	-.000
21.250	588.00	230.00	1.000	17.0000	-.000
21.500	583.00	229.20	1.000	17.2000	-.000
21.750	578.00	228.40	1.000	17.4000	-.000
22.000	573.00	227.60	1.000	17.6000	-.000
22.250	568.00	226.80	1.000	17.8000	-.000
22.500	563.00	226.00	1.000	18.0000	-.000
22.750	558.00	225.20	1.000	18.2000	-.000
23.000	553.00	224.40	1.000	18.4000	-.000
23.250	548.00	223.60	1.000	18.6000	-.000
23.500	543.00	222.80	1.000	18.8000	-.000
23.750	538.00	222.00	1.000	19.0000	-.000
24.000	533.00	221.20	1.000	19.2000	-.000
24.250	528.00	220.40	1.000	19.4000	-.000
24.500	523.00	219.60	1.000	19.6000	-.000
24.750	518.00	218.80	1.000	19.8000	-.000
25.000	513.00	218.00	1.000	20.0000	-.000
25.250	508.00	217.20	1.000	20.2000	-.000
25.500	503.00	216.40	1.000	20.4000	-.000
25.750	498.00	215.60	1.000	20.6000	-.000
26.000	493.00	214.80	1.000	20.8000	-.000
26.250	488.00	214.00	1.000	21.0000	-.000
26.500	483.00	213.20	1.000	21.2000	-.000
26.750	478.00	212.40	1.000	21.4000	-.000
27.000	473.00	211.60	1.000	21.6000	-.000
27.250	468.00	210.80	1.000	21.8000	-.000
27.500	463.00	210.00	1.000	22.0000	-.000
27.750	458.00	209.20	1.000	22.2000	-.000
28.000	453.00	208.40	1.000	22.4000	-.000
28.250	448.00	207.60	1.000	22.6000	-.000
28.500	443.00	206.80	1.000	22.8000	-.000
28.750	438.00	206.00	1.000	23.0000	-.000
29.000	433.00	205.20	1.000	23.2000	-.000
29.250	428.00	204.40	1.000	23.4000	-.000
29.500	423.00	203.60	1.000	23.6000	-.000
29.750	418.00	202.80	1.000	23.8000	-.000
30.000	413.00	202.00	1.000	24.0000	-.000
30.250	408.00	201.20	1.000	24.2000	-.000
30.500	403.00	200.40	1.000	24.4000	-.000
30.750	398.00	199.60	1.000	24.6000	-.000
31.000	393.00	198.80	1.000	24.8000	-.000
31.250	388.00	198.00	1.000	25.0000	-.000
31.500	383.00	197.20	1.000	25.2000	-.000
31.750	378.00	196.40	1.000	25.4000	-.000
32.000	373.00	195.60	1.000	25.6000	-.000
32.250	368.00	194.80	1.000	25.8000	-.000
32.500	363.00	194.00	1.000	26.0000	-.000
32.750	358.00	193.20	1.000	26.2000	-.000
33.000	353.00	192.40	1.000	26.4000	-.000
33.250	348.00	191.60	1.000	26.6000	-.000
33.500	343.00	190.80	1.000	26.8000	-.000
33.750	338.00	190.00	1.000	27.0000	-.000
34.000	333.00	189.20	1.000	27.2000	-.000
34.250	328.00	188.40	1.000	27.4000	-.000
34.500	323.00	187.60	1.000	27.6000	-.000
34.750	318.00	186.80	1.000	27.8000	-.000
35.000	313.00	186.00	1.000	28.0000	-.000
35.250	308.00	185.20	1.000	28.2000	-.000
35.500	303.00	184.40	1.000	28.4000	-.000
35.750	298.00	183.60	1.000	28.6000	-.000
36.000	293.00	182.80	1.000	28.8000	-.000
36.250	288.00	182.00	1.000	29.0000	-.000
36.500	283.00	181.20	1.000	29.2000	-.000
36.750	278.00	180.40	1.000	29.4000	-.000
37.000	273.00	179.60	1.000	29.6000	-.000
37.250	268.00	178.80	1.000	29.8000	-.000
37.500	263.00	178.00	1.000	30.0000	-.000
37.750	258.00	177.20	1.000	30.2000	-.000
38.000	253.00	176.40	1.000	30.4000	-.000
38.250	248.00	175.60	1.000	30.6000	-.000
38.500	243.00	174.80	1.000	30.8000	-.000
38.750	238.00	174.00	1.000	31.0000	-.000
39.000	233.00	173.20	1.000	31.2000	-.000
39.250	228.00	172.40	1.000	31.4000	-.000
39.500	223.00	171.60	1.000	31.6000	-.000
39.750	218.00	170.80	1.000	31.8000	-.000
40.000	213.00	170.00	1.000	32.0000	-.000
40.250	208.00	169.20	1.000	32.2000	-.000
40.500	203.00	168.40	1.000	32.4000	-.000
40.750	198.00	167.60	1.000	32.6000	-.000
41.000	193.00	166.80	1.000	32.8000	-.000
41.250	188.00	166.00	1.000	33.0000	-.000
41.500	183.00	165.20	1.000	33.2000	-.000
41.750	178.00	164.40	1.000	33.4000	-.000
42.000	173.00	163.60	1.000	33.6000	-.000
42.250	168.00	162.80	1.000	33.8000	-.000
42.500	163.00	162.00	1.000	34.0000	-.000
42.750	158.00	161.20	1.000	34.2000	-.000
43.000	153.00	160.40	1.000	34.4000	-.000
43.250	148.00	159.60	1.000	34.6000	-.000
43.500	143.00	158.80	1.000	34.8000	-.000
43.750	138.00	158.00	1.000	35.0000	-.000
44.000	133.00	157.20	1.000	35.2000	

only dependent upon raindrop size. This rain rate equation could be used as a feedback mechanism and iterate between it and the assumed form of the  $n(r)$  equation. That is to say, for the Marshall-Palmer equation one could assume an initial value for  $N_0$ , solve the integral to obtain a first guess value for  $R$ , compare the first  $R$  value with that observed, select a new value for  $N_0$  to reduce the difference between observed and computed  $R$ , and iterate to obtain the most applicable  $N_0$  for that rain. A similar approach can be used with the exponential or modified gamma function as an aid in modifying one of the parameters such as the shape factor and/or the coefficient  $A$  which is related to the liquid water content. Fig. 22 shows the log log relation that exists between rainfall rate  $R$  ( $\text{mm hr}^{-1}$ ) and liquid water content  $W_L$  ( $\text{g m}^{-3}$ ) of raindrop. Two equations express this analytically as

$$W_L = 0.072 R^{.88} \quad (1)$$

for Marshall-Palmer rain and

$$W_L = 0.11 R^{.88} \quad (2)$$

for Joss drizzle.

In fact, for many obscuration problems it is possible to infer sensor attenuation directly by meteorological measurement of rainfall rate on liquid water content. This is especially noticeable in the microwave portion of the spectrum as shown in Fig. 23 as well as in the visible and infrared (Low 1979) for other weather features such as fog. Here, however, we are interested

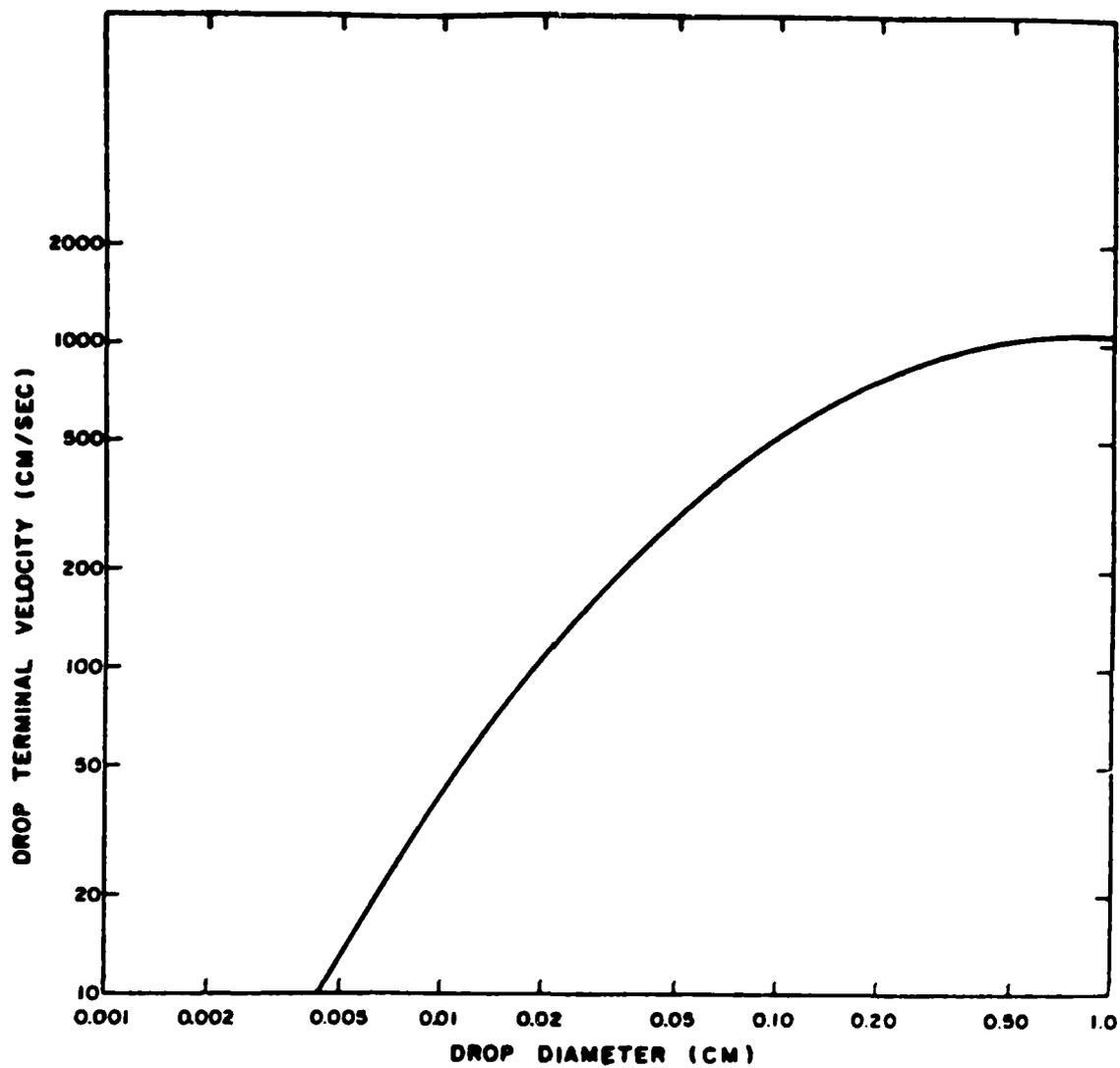


Fig. 21 Terminal Velocity Vs. Raindrop Size

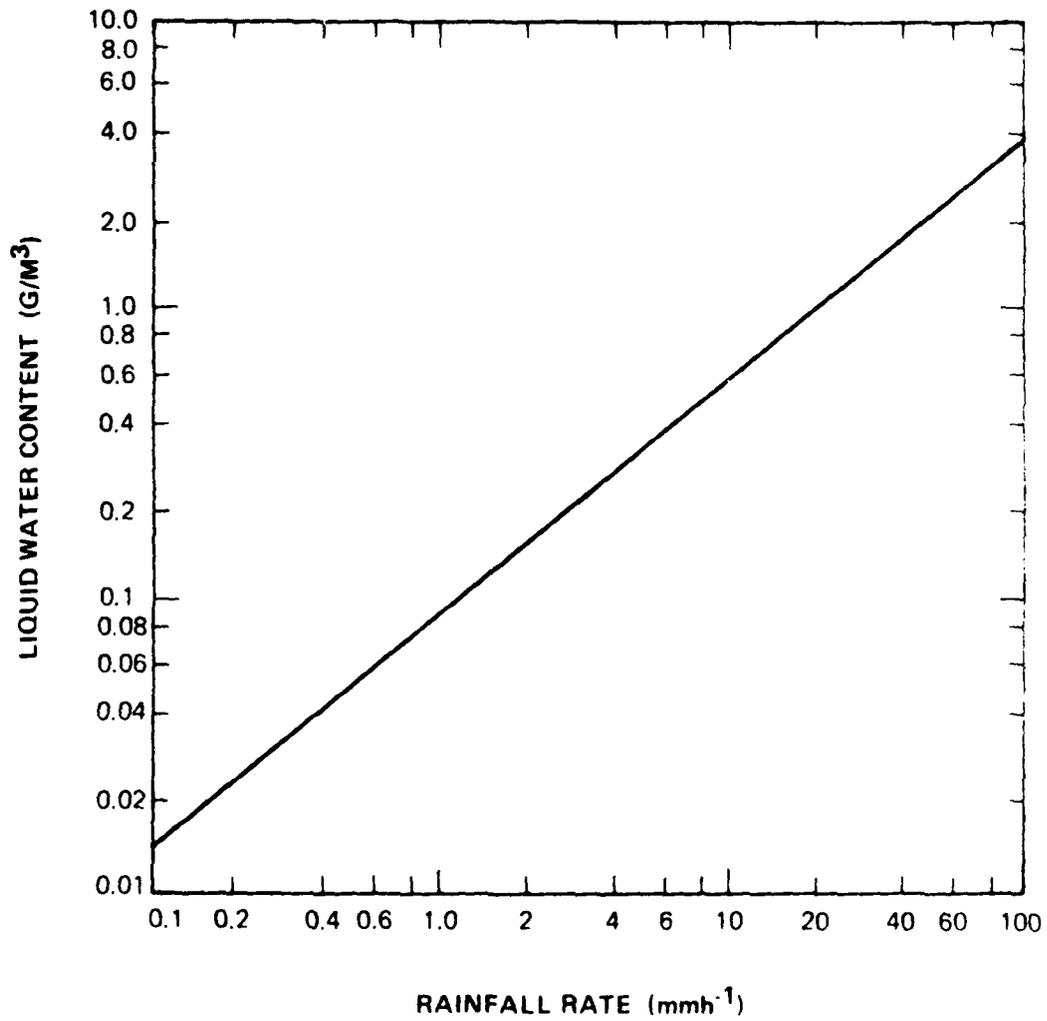


Fig. 22 Liquid Water Content of Precipitation Versus Rainfall Rate

in specification of raindrop size distributions and we have two strong candidates, the exponential approach that we previously used for fogs and clouds, and the Marshall-Palmer method. During the course of analyzing both approaches, we analyzed Marshall-Palmer type data from several sources, geographical locations, and rainfall types and was able to obtain a best fit equation that solves the coefficient  $N_0$  problem previously discussed. Figure 24 shows our plot of the variation of  $N_0$  coefficient relative to rainfall rate with best fit equation being

$$N_0 = 12000 R^{-.72} \quad (41)$$

This equation alters the raindrop size distribution properly by increasing the population of small droplets in drizzle while decreasing the population of raindrops associated with showers and thunderstorms. By combining Equations (37), (38), and (41) it is now possible to have a single analytical expression for deriving raindrop particle size distributions for all rain/drizzle/mist type environments and geographical locations using only routinely measured rate of rainfall.

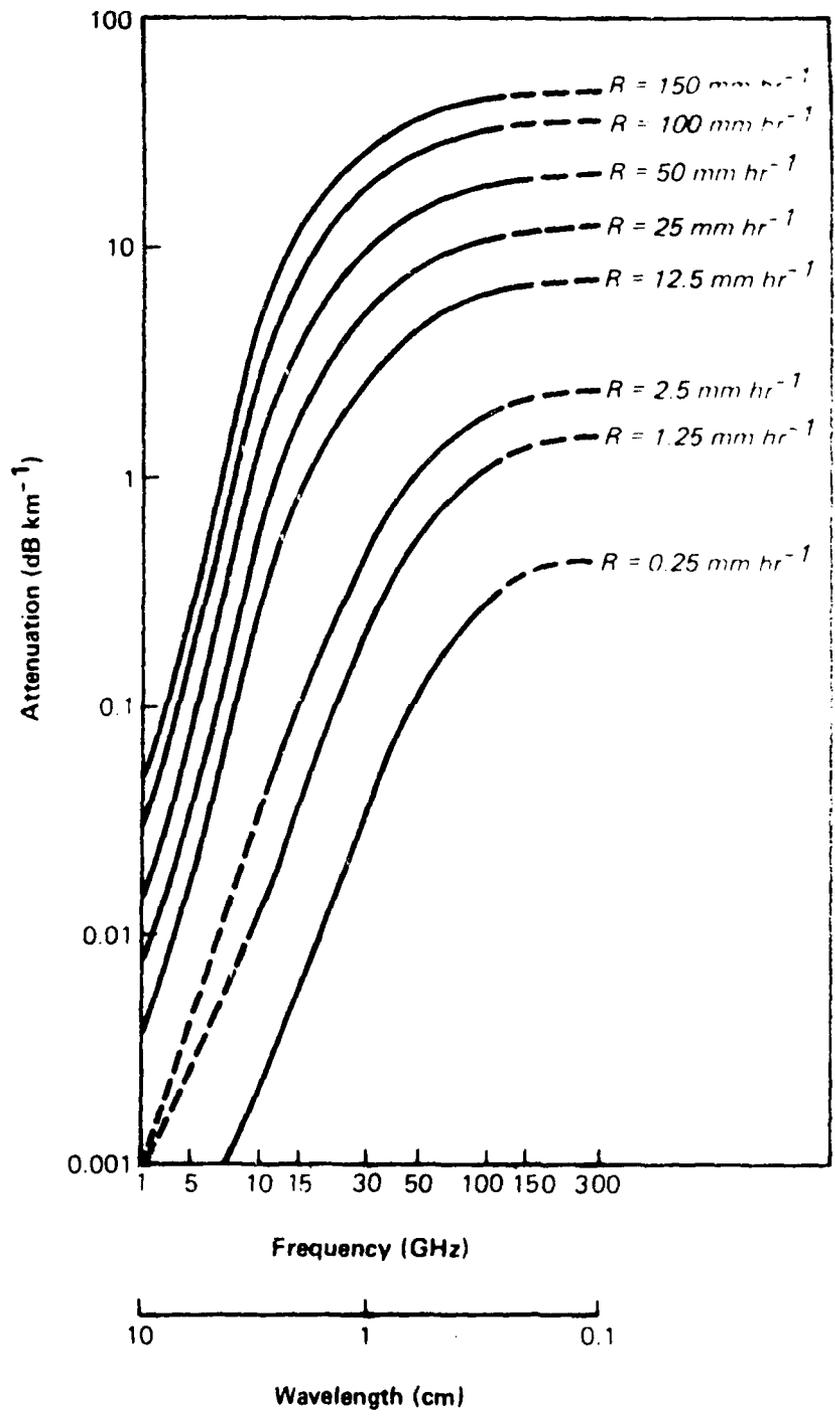


Fig. 23 Attenuation vs. Frequency for Various Rainfall Rates

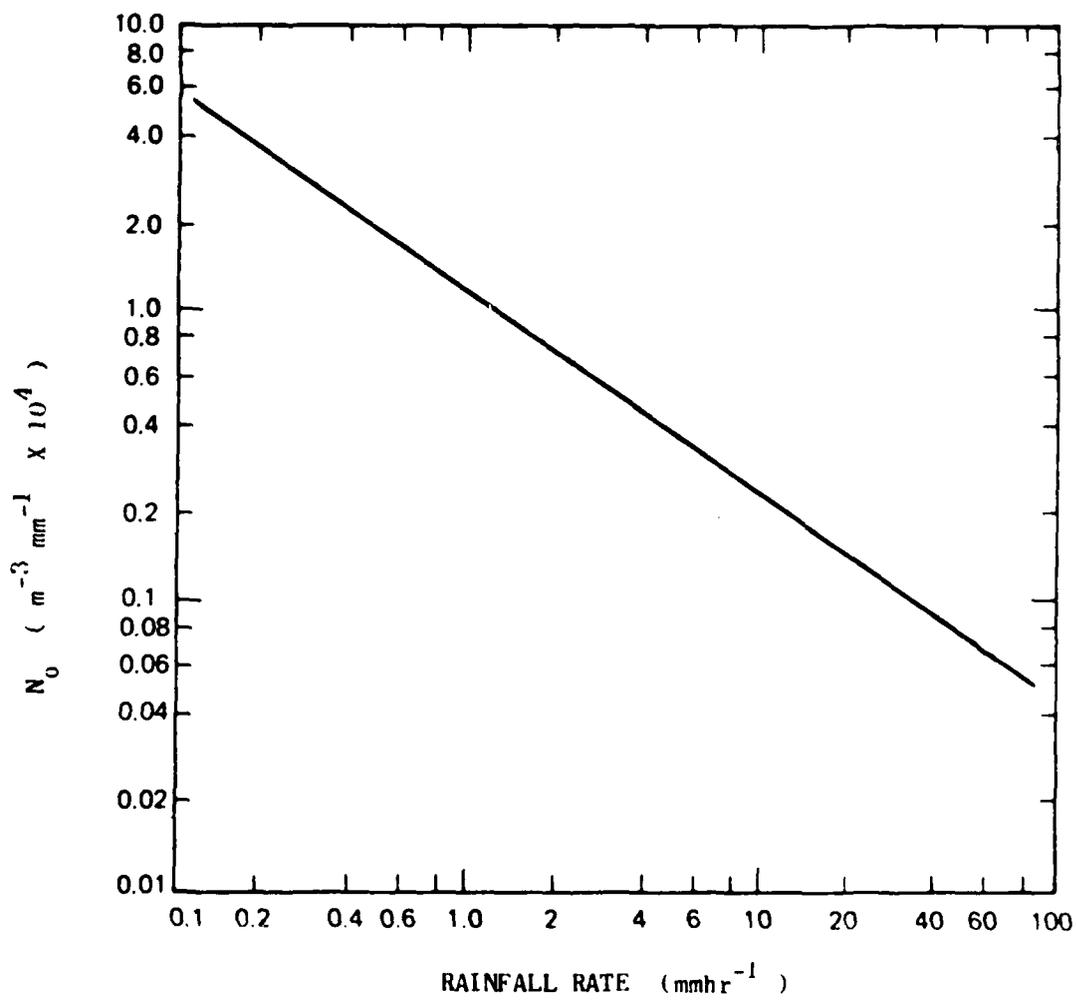


Fig. 24 Coefficient  $N_0$  Versus Rainfall Rate

#### 2.2.3.2 Dynamic Procedure

1. Using objective surface and upper air analysis techniques, such as CIVAS, obtain rainfall rate, height of cloud base and top, and horizontal changes in precipitation and cloud features.
2. Solve Equations (38) and (41) to obtain applicable values of  $\beta$  and  $N_0$  given the observed rainfall rate at the earth's surface.
3. Solve Eq. (37) to obtain raindrop size distributions over a selected range of raindrop diameters from 0.75 to 2.25 mm for rainrates equal to or less than 1 mm/hr, from 1.25 to 3 mm for rainrates greater than 1 mm/hr but less than 25 mm/hr, and from 1.5 to 4.5 mm for rainrates equal to or greater than 25 mm/hr.
4. Obtain the vertical distribution of rainfall rate by decreasing the surface value by 0.5 mm/hr per 0.25 km height in the atmosphere up to the mid-point height in the cloud at which the rainrate drops to zero.
5. Use the above derived rainrate distribution in the horizontal and vertical to derive changes in raindrop particle size distributions in the cloud-free air and cloud environment.

### 3. CONCLUSIONS AND RECOMMENDATIONS

1. Dynamic models are presented for specifying particle size distributions in horizontal and vertical directions for haze, fog, cloud and rain conditions given only routinely available meteorological data. Case studies showed these models performed well individually and when used together. This effort should be viewed as the first step in developing dynamic models that are responsive to observed and forecast weather changes. These models need to be applied, tested, modified, and improved.
2. More complete microphysical observations are needed not only to better understand atmospheric processes but also to provide better inputs to such meso- and synoptic scale models as developed here. Efforts should be made to incorporate and combine these dynamic models with such Army Cloud Fog Analysis System (CFAS) and Cloud/Ice/Visibility Analysis System (CIVAS) to depict natural obscurants at any desired time or location.
3. A more cooperative working environment must be created between the micro- and macro- atmospheric physicist. The micro-physicist feels threatened to think that Army users could be satisfied with only macro- scale data. In turn, the macro- physicist feels threatened when told only extensive microphysical observations

can provide necessary details. We have a lot to accomplish if we are to someday be in a position to help our Army provide day to day and hour by hour assessments of defensive and offensive weapon effectiveness. This requires all talents operating collectively with realistic guidelines on what meteorological data will be available for use in specifying and predicting obscuration for a Field Army.

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