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TECHNICAL REPORT ARTSD-TR-80001

**ELECTROSTATIC PROPENSITY OF GARMENTS
MADE OF NOMEX WITH
ONE PERCENT METAL FIBERS COMPARED
WITH FLAMEPROOF COTTON**

JOHN F. VAN SAVAGE

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**US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND
TECHNICAL SUPPORT DIRECTORATE
DOVER, NEW JERSEY**

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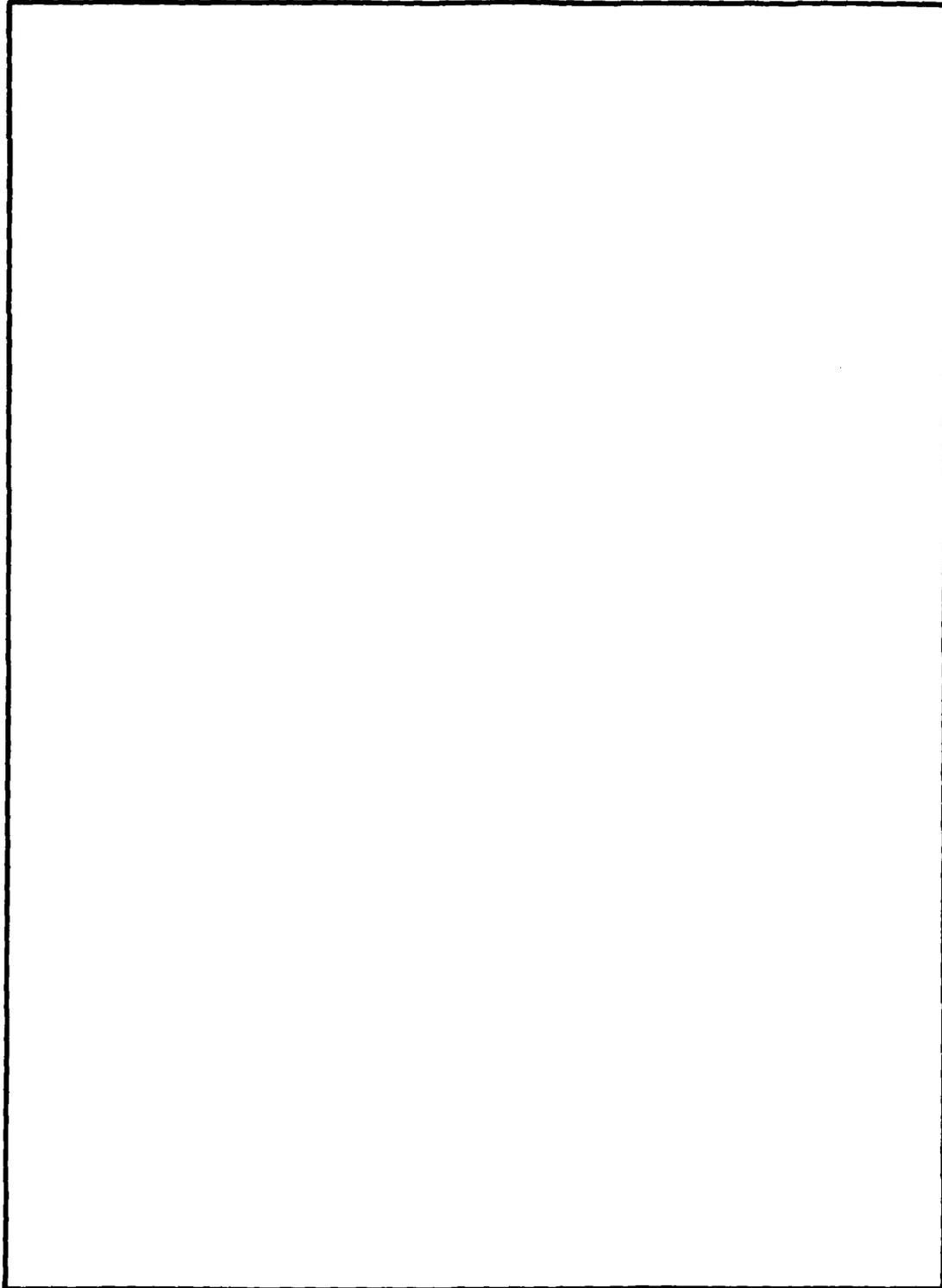
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Electrostatic hand discharge	Conductive linoleum																
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Garments which are worn by munitions handlers have a tendency to accumulate high electrostatic voltages depending on garment material, type of shoes worn, humidity, temperature, and composition of flooring. This test study compared garments made of flameproof cotton with garments made of two types of material woven from Nomex with 1% metal fibers. Electrostatic charge was measured using two methods: Hand discharge to an electrometer and a static meter gun held at 5, 15.25, and 30.5 cm (2, 6, and 12 in.).																	

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SUMMARY

Tests were performed to compare electrostatic charge developed on garments made of flameproof cotton with two types of material containing Nomex with metal fibers [Riegelstat F4X and Nomex with 1% stainless steel (Nomex SS)]. The data show:

1. Riegelstat F4X and Nomex SS were comparable to flameproof cotton in propensity to generate static charge. Nomex SS coveralls can be substituted for cotton coveralls now worn by explosive handlers.

2. Electrostatic voltages are negligible if Nomex SS or flameproof cotton coveralls are worn with conductive shoes and the floor is grounded.

3. Very high voltages can be generated which can prove hazardous if the explosives handler wears insulated shoes or the floor is insulated.

4. Generated electrostatic voltage levels are greater at lower humidities for test conditions of insulated shoes and/or insulated floor.

5. Static charge-generating propensity of Riegelstat F4X and of Nomex SS, after washing, was not conclusively determined.

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INTRODUCTION

A study was initiated to compare the static charges generated by cotton garments and by garments manufactured from two types of material containing Nomex with 1% metal fibers:

1. Ninety-nine percent Nomex and 1% Brumsmet fiber, manufactured by Riegel Textile Corporation (hereinafter referred to as Riegelstat F4X).

2. Ninety-nine percent Nomex and 1% stainless steel fibers (hereinafter referred to as Nomex SS).

The test plan included a general discussion on electrostatic charging, methods of measurements, and types of systems that could cause an electrostatic problem (app A).

The test plan also specified an evaluation of fabric surface resistance measurements that could be reliably used to observe the propensity of a garment to generate an electronic charge and its ability to dissipate that charge.

Tests were performed specifically to determine how Nomex with metal fibers (Riegelstat F4X and Nomex SS) compared with cotton, if either or both were an improvement over cotton, and if either or both could replace cotton fabric used in garments worn by explosive handlers and visitors to explosive areas. The following garments were tested:

1. Coat, Workrite Uniform Company, Riegelstat F4X
2. Coverall, Worklon Company, Nomex SS
3. Standard stock cotton coveralls
 - a. New without flameproofing
 - b. New with flameproofing
 - c. Old with flameproofing

Tests were performed in an atmospherically controlled chamber at 19% relative humidity, 21°C (70°F) and at 37% to 40% relative humidity, 24°C (75°F).

When the test subject wore conductive shoes, the static charge was minimal and, therefore, fewer tests were required. When the test subject wore insulated shoes, a minimum of three and a maximum of five readings were taken for each test:

1. Walking on copper plate
2. Walking on asbestos tile
3. Sliding about a plastic covered metal chair and then arising from it.
4. Sliding about on both a grounded and ungrounded metal chair and then arising from it.
5. Walking on conductive linoleum.

To record electrostatic propensity, the test subject, while standing on a conductive sheet (copper or conductive linoleum), grasped the probe of an electrometer with the fingers of his right hand. Electrostatic voltage measurements were taken while the subject wore both insulated spark-proof shoes and conductive shoes, with and without conductive sheet grounded. Sixteen separate tests were made on each garment; each test was performed three to five times, resulting in 48 to 80 separate readings for each relative humidity. The number of readings were again doubled because the copper measurement plate was either grounded or insulated.

The capacitance-to-ground of the test subject was measured with conductive and insulated spark-proof shoes. The following capacitance were recorded:

<u>Capacitance</u> <u>(picofarads)</u>	<u>Conditions</u>
120	Insulated shoes, copper measurement plate grounded
120	insulated shoes, copper measurement plate not grounded (insulated)
4600	conductive shoes, copper measurement plate grounded
3770	conductive shoes, copper measurement plate not grounded (insulated)

The energy available from hand discharge, dependent on the charge induced and the capacitance of the subject's body, can be calculated by

$$E = \frac{1}{2} CV^2 \text{ joules}$$

where E is the energy in joules, C is the capacitance in farads, and V is the maximum voltage as read on the electrometer.

Using representative values, a man wearing insulated shoes and charged to 10,000 volts has stored 60,000 ergs as electrical energy; whereas, if he were wearing conductive shoes which allow an electrostatic voltage of 100 volts, he has only stored 200 ergs of energy.

The ability of the human body to retain charge is determined by its leakage time constant which is the body's capacitance times its leakage resistance. The leakage resistance of the test subject from hand through shoes to ground was measured and found to be as follows:

1. With insulated shoes: 4×10^{11} ohms
2. With conductive shoes: 500,000 ohms

With conductive shoes, the leakage time constant is:

$$t = RC = 5 \times 10^5 \times 4600 \times 10^{-12} = 2.3 \text{ milliseconds}$$

Similarly, with insulated spark-proof shoes, the leakage time constant is 48 seconds.

The human body's discharge time constant is determined by the product of the body's capacitance in series with 5,000 ohms plus the external discharge resistance. Assuming a man is wearing insulated shoes and discharging into a low resistance, his discharge time constant is 0.6 microseconds.

TEST PROCEDURE

Measurement of Electrostatic Discharge from Hand

The test subject, attired in a Riegelstat F4X, Nomex SS or cotton garment, flameproof treated or untreated, performed body

movements simulating work conditions. The garments were first conditioned by being hung overnight in a test chamber at the desired temperature and relative humidity. After performing selected body movement, the test subject walked on a copper measurement plate and touched an electrometer probe. The body voltage was indicated on a Keithley 610B voltmeter and the maximum value was recorded. The body movements for which tests were performed were as follows:

1. Subject sliding about on a vinyl simulated leather covered metal chair and then arising from it.
2. Subject sliding about on a metal chair and then arising from it.
3. Subject walking on a metal plate.
4. Subject walking on asbestos tile.

The above tests were performed under the following conditions:

1. Relative humidity: 37-40%; temperature 24-26°C (75-79°F)
2. Relative humidity: 19%; temperature 21°C (70°F)
3. Metal plate: grounded and ungrounded
4. Metal chair: grounded and ungrounded
5. Footwear: conductive and insulated, spark-proof shoes
6. Clothing worn under the test garments: polyester knit trousers, combination polyester/cotton shirt, nylon or dacron socks and polyester tie.

When the subject wore insulated shoes, three to five tests were performed for each operation.

Appendix B delineates the raw data documented in testing of the following garments:

1. Coats, Riegelstat F4X, Workrite Uniform Company (Items 1, 2, 3 and A of app B)
2. Coveralls, Nomex SS, Worklon Company (Item B)
3. Coveralls, cotton, new, non-flameproof (Item C)

4. Coveralls, cotton, new, flameproof (Item D)
5. Coveralls, cotton, old, flameproof (Item E)
6. Coveralls, cotton, new, non-flameproof (Item F)
7. Coveralls, Nomex SS, Worklon Company (Item G)

After the above garments were tested, first at 40% and then at 19% relative humidities, they were washed ten times, using a standard washing procedure. Flameproof treatment was applied to the cotton garments after each washing. The Nomex-plus-metal-fiber garments received no flameproofing. Two garments (unwashed) were used as controls to compare electrostatic discharge with those garments washed.

Electrical Surface Resistance of Garment Fabric

Surface resistance measurements were made prior to the first washing and after the tenth. Three types of resistance measurements were made: voltage current type using a Keithley 610B Electrometer, resistance type using a Keithley 610B Electrometer, and a Simpson Voltmeter (VOM) which was used whenever the Keithley 610B Electrometer was overloaded due to Kiegelstat's low surface resistance. Figure 1 shows the test setup for the voltage/current method. Tests were performed on samples of specific size as determined by the dimensions of the concentric-ring electrodes. Based on the dimensions of the concentric-ring electrodes, ohms/square can be obtained by multiplying the resistance obtained by the constant 15.5.

The variable-voltage power supply is adjusted to any value up to 1,000 volts, taking care not to overload the current meter, a Keithley 610B Electrometer. Resistance is calculated by:

$$R = \frac{E}{I}$$

where E = power supply voltage (volts)
and I = current measured with the electrostatic voltage meter (amperes)

With a Keithley 610B Electrometer, resistance can also be measured directly. The power supply is not used in this mode.

When Nomex SS was tested, the test voltage caused a decrease in resistance, allowing current magnitudes to flow beyond the range

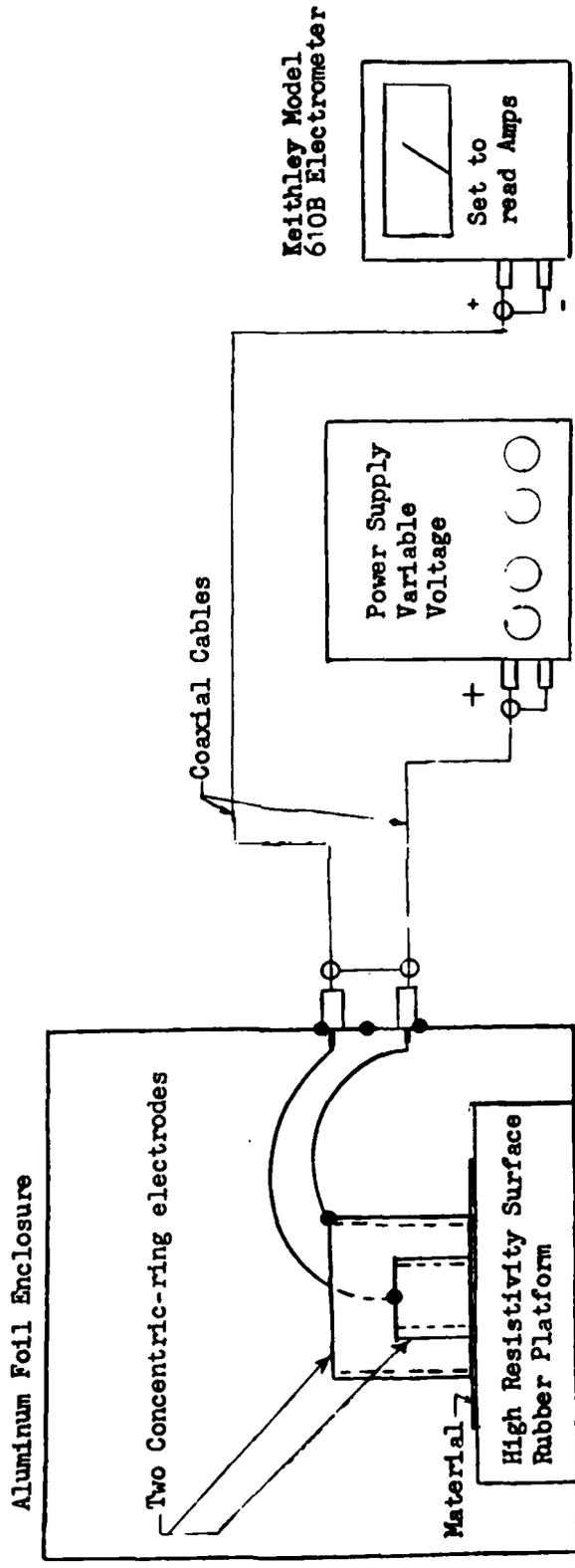


Figure 1. Voltage/current method of testing for surface resistance

of the Keithley 610B Electrometer. Therefore, an ohmmeter reading was made first of the material's resistance as received (app C).

Since Nomex with metal fibers developed low surface resistance after being washed ten times, an ohmmeter was used to obtain additional information.

Test Subject Capacitance

Capacitance during the electrostatic propensity tests was measured while the test subject was wearing both conductive and insulated shoes and standing on a copper plate (app D). The copper plate was either grounded or ungrounded to conform with the test requirement. The values of capacitance thus obtained made it possible to calculate energy stored on the test subject and to clarify the static charge phenomenon. The capacitance was obtained with the test subject's holding the capacitance measurement terminal of the General Radio Type 1650A Impedance Bridge while an operator adjusted its settings.

Test Subject Resistance to Ground

The resistance of the test subject to ground was obtained by his grasping the test probe of the Keithley 610B Electrometer. Resistance measurements were obtained using the voltage/current and the resistance method (app E). The resistance method was exclusively used for conductive shoes and only with the measurement plate grounded. For insulated shoes, the measurement plate was either grounded or ungrounded (insulated). With the voltage/current method, resistance is calculated by

$$R = \frac{V}{I}$$

Static Meter Gun Measurements

A static meter gun was held close to, but not touching, the garment being measured for electrostatic charge accumulation. Electric charge was not lost from the garment. The static meter was calibrated for distances of 5, 15.25, and 30.5 cm (2, 6, and 12 in.) away from the garment. Meter gun readings were made of the electrostatic potential on the garment's back, front, and coverall cuffs or polyester trouser cuffs (when coat rather than coverall was worn). The purpose of these tests was to measure the maximum electrostatic potential accumulation on each garment and compare the results with voltage measurements obtained with the electrometer. Repetitive tests were performed with the test subject's wearing either insulated or conductive shoes with the different types of garments, as was specified in the test plan.

Test equipment is listed in appendix F.

DISCUSSION

Comparison of Nomex Containing 1% Metal Fibers with Cotton

Nomex, a synthetic material manufactured by duPont Corporation, has superior properties of flame resistance compared with cotton. Garments of Nomex used by explosive handlers have the additional advantages of uniformity and reliability of flameproof properties as compared with flameproof-treated cotton garments. The superior wearability of Nomex over cotton significantly offsets increased cost.

Since Nomex is a synthetic material, it tends to generate static charge in use. For applications where it is important to minimize static charge, 1% metal fibers are woven into the material. Two such materials are evaluated in this report for comparison of static charge propensity as compared with cotton; one is Riegelstat F4X and the other is Nomex SS.

No attempt was made in this test program to generate the maximum possible static charge. Rather, the emphasis was to evaluate the comparative static-charge-generating propensity of the materials being evaluated over a range of test conditions considered realistic for the intended use of the garments. The total raw data that was generated is found in appendix B.

When the test subject wore conductive shoes rather than insulated shoes, the monitored static charges were considerably lower. However, even when the test subject wore conductive shoes, knee-length coat and polyester knit pants, the gun-type static meter registered voltages as high as 5,000 on the trouser cuffs. This was localized phenomenon and was present despite the fact that the data monitored with a hand on the electrometer probe indicated 160 volts (app B). Gun measurements on the coat were zero. For this same coat, when the test subject wore insulated shoes, his body voltage was nearly 9,000 volts; gun readings on the garment were as high as 8,000 volts; and gun readings on the trouser legs were as high as 10,000 volts. Similar measurements made with coveralls that did not allow the pant legs to be exposed had very low gun voltage readings (app B).

These data indicate the necessity of explosive handlers' wearing conductive shoes; also that static charge dissipative coveralls be worn in lieu of knee-length work coats which allow trouser legs to be exposed. If these protective measures are taken, clothing worn under the coveralls (that by themselves have static-charge-generating propensity) will not generate static charge voltages on the outside surface of the coveralls, thus averting static charge hazard for explosive handlers.

Whether the conductive plate is grounded or ungrounded, the static charge measured is the same (app G). The reason for this is the high capacitance-to-ground of the ungrounded plate. Had steps been taken to move the plate farther from ground (provide better isolation), the capacitance-to-ground would have been less and the voltage measured would have been greater. Similarly, measurements made with the test subject's standing on asbestos floor tile would have indicated greater voltages. These tests showed that conductive linoleum of the type normally used on table tops was equivalent to a metal plate for similar test conditions. A man arising from a metal chair generated considerable static charge independent of whether the chair was grounded or not. The test conditions that generated maximum voltage were those of a man sliding about on a plastic chair while wearing insulated shoes. Therefore, these are the conditions used for discussing the relative merits of the different garments, although the relative voltage levels measured amongst the test garments remain the same for the other test conditions.

Voltages monitored for the various test samples at 19% relative humidity, measured with the electrometer, are shown in app H. These data show that Nomex fabrics woven with metal fibers (both Riegelsat F4X and Nomex SS) are slightly superior to the untreated cotton; other data found in appendix B show that the untreated cotton generates up to 12,000 volts. Cotton with flameproofing is slightly superior to the others, with the older cotton garment being best. Data on similar tests at 35 to 39% relative humidity are presented in appendix B which also shows all voltage levels to be reduced approximately one order of magnitude due to the increased humidity. The average voltage levels for all of the Nomex-plus-metal-fiber materials is approximately equal to the average value of the cotton without flameproofing. However, the cotton with flameproofing is decidedly superior at the higher levels of humidity.

Electrostatic hand discharge voltage test data on test garments before washing and after 10 washings are shown in appendix H. The cotton garments were treated with flameproofing chemicals after each washing as is the normal custom. The object of this effort

was to determine whether the desirable properties of garments made from Nomex with metal fibers deteriorated after extensive washing. The cotton garments were used as a control.

The cotton garments without flameproofing decreased considerably in static-charge-generating propensity (app H). This is consistent with previous test data for cotton garments with added flameproofing chemicals as compared with new untreated cotton garments. The voltage level measured for the Nomex-with-metal-fiber garments also decreased dramatically following washing. These results for the Nomex with metal fibers were not considered consistent with theory. The expectation was that the static charge propensity of the Nomex with metal fibers was expected to remain the same at best and, if there were mechanical deterioration of the metal fibers, the voltage levels were expected to increase. It is suspected that the decrease in voltage levels occurred during handling in the laundry room by inadvertent contamination from the flameproofing used for the cotton. These data, therefore, do not provide the required information concerning the effect of many washings of the Nomex with metal fibers.

Carefully controlled, standard wash tests are recommended to evaluate possible change in static charge propensity of Nomex with metal fibers. To avoid postponing use of this material, spot checks should be performed on a man wearing a garment of this material, after each actual use, and after extended washings to assure that physical deterioration due to washing has not created a static charge problem.

The techniques for monitoring electrostatic voltages as presented in this report, do not record possible transient voltage levels that could be considerably higher than the steady state levels monitored. If these high level voltages exist under certain circumstances, they should be ascertained inasmuch as dangerous detonation of explosives, presently unpredictable, could occur.

One could represent a condition where a man, sitting in a chair and wearing conductive shoes, could generate a high voltage. However, on arising from the chair and stepping on a conductive floor, he could decrease the voltage to a safe level. Under these circumstances, if the man touched a detonator as he was arising from the chair (while at his peak voltage level), he could deliver sufficient voltage and energy to fire the detonator. The charging time constant is much less than the discharge time constant. This phenomenon might explain the reason for some explosions, the causes of which are presently unknown. Therefore, transient-type tests to evaluate this effect are recommended.

Relative Resistivity Measurements of the Garment Fabrics

Relative resistivity measurements recorded on the various garment materials are presented in appendix C. These data do not allow one to predict the static charge propensity of Nomex with metal fibers as compared to cotton. Although the Nomex with metal fibers showed very low relative resistivity as compared to cotton, the static charge generated was comparable. The reason for this apparent discrepancy is believed to be the inhomogeneity of the Nomex-with-metal-fiber material because a low percentage of metal fibers may not completely neutralize the charge generated in the high resistance Nomex threads, but yet show low resistance in direct readings. It is possible, however, to develop a relationship for a homogeneous material, such as pure cotton, between resistivity and static charge-generating propensity, although additional work is required to make this relationship more definitive.

CONCLUSIONS

1. At relative humidity levels of 19% to 39%, an explosives handler, standing on a conductive floor, will generate the same static charge voltage levels when wearing coveralls made of Nomex SS as he would if he were wearing flameproof-treated coveralls.

2. To minimize static charge voltage buildup, an explosives handler should work on a conductive floor, and should wear conductive shoes and a coverall, rather than a work coat which would expose his pant legs. Under these conditions, garments worn under the coveralls, including underwear, will not adversely affect static charge energy generated by the man to his environment.

3. Observations showed that at the relative humidity levels tested, a man wearing insulated shoes will generate lower electrostatic voltage levels if he is wearing a flameproof-treated cotton garment, rather than an untreated cotton or Nomex-with-metal-fibers garment (either Riegelsat F4X or Nomex SS).

4. Even if a man is wearing conductive shoes and a knee-length work coat made of Nomex with metal fibers, the voltage levels on the portion of his pants exposed beneath his knees could generate dangerous levels of voltage.

5. Data obtained on the performance of Nomex with metal fibers after washing are questionable because of suspected inadvertent contamination. These tests should be rerun.

6. Where test conditions include insulated shoes or insulated floor, static charge voltages induced on garments increase in magnitude when the ambient relative humidity is decreased from 39% to 19%. Relative humidity as low as 5% can exist in a loading area under extreme conditions; tests should be performed at low humidities on both Nomex with metal fibers and on cotton to evaluate potential hazards.

7. Under special circumstances, transient static-charge-induced voltages of very high levels, not recorded with normal measurement techniques, may present a safety hazard.

RECOMMENDATIONS

1. Coveralls made from Nomex with 1% metal fibers may safely be used as uniforms for explosives handlers providing conditions include conductive floor and conductive shoes. Additional electrostatic tests should be performed on Nomex with metal fibers after washing. In the interim, static charge gun tests should be performed on garments of this material in use after washing.

2. It is not necessary to control the clothing the explosives handler wears under his coveralls providing the conditions described above are met.

3. Additional tests are recommended to evaluate static-charge-induced voltages on both Nomex with metal fibers and on cotton at low temperatures and low relative humidities.

4. Static charge tests should be performed to evaluate the safety hazards from possible large amplitude transient voltages generated during the charging process even where conductive shoes are worn.

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APPENDIX A

TEST PLAN FOR EVALUATION OF ELECTROSTATIC
PROPENSITY OF VARIOUS FABRICS

TEST PLAN FOR EVALUATION OF ELECTROSTATIC PROPENSITY OF VARIOUS FABRICS

by

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Evaluation Branch, ID, TSD

MAY 1974

OBJECTIVE

The Evaluation Branch, Instrumentation Division, Technical Support Directorate was requested by Messrs W. Field and B. Perlmutter of Methods Engineering Division and Mr. J. Lippian of the Safety Office, to prepare a test plan to compare the electrostatic properties of various garments to determine if they can be safely worn by explosive handlers and visitors to explosive areas. The following materials are to be tested:

- a. Sager Glove Company, shirt, 100% Cotton-Roxel (washable fire retardant treatment)
- b. Sager Glove Company, trousers, 100% Cotton-Lynrus (washable fire retardant treatment)
- c. Worklon Company, coveralls, 99% Nomex, 1% stainless steel fiber
- d. Standard stock cotton coveralls
 1. New, with flame proofing
 2. New, without flame proofing
 3. Old, with flame proofing
- e. Workrite Uniform Company, 99% Nomex Aramid, 1% Brunsmet fiber

BACKGROUND

Garments Used in Explosive Environments at Picatinny Arsenal

Cotton has long been recognized as the best material for control of static electricity. This control comes about because of the material's ability to absorb moisture from the air which reduces surface resistivity (the lower the surface resistivity the less the material's propensity for storing charge). It must, however, be recognized that cotton's unique charge dissipation characteristic is associated with the moisture content of the surrounding air; below 35% relative humidity even cotton becomes material to be concerned with in the control of static electricity.

Cotton coveralls used at Picatinny Arsenal are treated with flame proofing material during one phase of the laundering cycle. There have been problems in obtaining consistency in obtaining flame retardancy in the process. This Arsenal is considering using garments manufactured from Nomex, DuPont's flame retardant nylon. Uniforms of Nomex solve many of problems associated with flame retardant cotton; however, its reported propensity for electrostatic charging renders the material useless in an explosive environment, except where additional anti-static treatment is provided. Riegel Textile Corporation manufactures a fabric sold under the trade name Riegelstat Flx which combines a metal fiber, Brunsmet, with Nomex. This fabric is reported to have properties which compete with cotton as an anti-static fabric.

General Discussion on Static Electricity

Although the field of electrostatics has been known for years, many of the phenomena associated with it are still not understood. This has led many authors to state that electrostatics is both a science and an art.

It is well known that when two different materials are brought in contact and then separated, equal and opposite charges are produced on each material. If one of these charged materials comes in proximity to a conductor, without touching it, free electronics are either attracted toward the charged body or repelled, depending on the polarity of the charging source. If the conductor is isolated from ground while in the presence of the charging body and is then grounded, electrons will either flow from or to earth, depending on the polarity of the charging source. Also, during the process of grounding the conductor a spark discharge often occurs.

The conductor referred to in the previous discussion is very often a human. Charging of the body can occur, for example, during the removal of clothing or when a person rises from a chair. It also occurs when a person walks across an ungrounded floor, especially if non-conductive shoes are worn. If a charged person touches a large object or ground, a spark discharge results. The most obvious danger of a spark discharge is its ability to initiate explosives or volatile gas and air mixtures. It is because of this danger that the control of static charge is of utmost importance in explosive environments.

Control of Static

The common methods used to control the generation and safe dissipation of electrostatic charge, include the use of anti-static materials or finishes, increasing the relative humidity, by ionization or by providing a low resistance path to ground for all items of equipment including flooring and footwear.

Measurement of Static Propensity

There are many schools of thought as regards to the proper way to test for static proneness. Of the many test procedures found in the literature the methods which are most used include the measurement of:

- a. Surface resistivity
- b. Total charge generated
- c. Charge decay rate

The technical manual of The American Association of Textile Chemists and Colorists (AATCC) specifies four different tests for testing for static accumulation. Test Methods AATCC 84-1969 and 76-1969 test respectively for electrical resistivity of yarns and fabrics. Test Method AATCC 15-1969 is a fabric-to-metal cling test. Test Method AATCC 134-1969 is used to measure carpet static (human body potential is measured using an electrostatic voltmeter).

Federal test method Standard 101B, Method 4046 is used to determine the properties of materials in film and sheet form. This procedure utilizes a high voltage power supply and special fixtures to charge and discharge a test specimen. The time required to induce a charge on the surface, the intensity and polarity of the charge, and the time required for complete dissipation of the charge are measured.

A practice that has been followed by this organization is assessing electrostatic problems is to develop a test procedure based on the specific system being evaluated. In this case we are dealing with a clothing-man system. Hence, the procedures developed for the evaluation of various fabrics specified in the Objective will include in addition to evaluation of surface resistivity specific tests that reflect the real system.

PROCEDURE

Surface Resistivity

The measurement of resistivity will be in accordance with the AATCC test method 76-1969.

Three test specimens will be cut from each of the test materials (as received) to be evaluated. Each specimen will be conditioned in a test chamber at three different relative humidity conditions (25, 40 and 65%) at 24°C (75°F) for a period of four hours. The size of each test specimen will be selected to suit the dimensions of the electrodes of the test fixture. Resistance measurements will be made using the Keithley 610B voltmeter.

The above tests will also be conducted after the test specimens have been washed ten times. The exact laundering process is to be specified. Cotton coveralls are presently laundered in accordance with D/M 21-7-1.1, Operation of Laundry.

Man-Clothing Test

For this test an individual attired in the test garments, will perform specific operations which will evaluate the fabric's static propensity.

These operations will include:

- a. Person sliding about on a vinyl simulated leather covered metal chair and then rising from it.
- b. Person sliding about on a metal chair and then rising from it.
- c. Person removing garment; this will be simulated by rubbing test fabrics across the person's back and shoulders.
- d. Person walking on conductive surface which is insulated.

The above tests will be conducted under the following conditions:

- a. Temperature - 24°C (75°F)
- b. Relative humidity - 25 and 50%
- c. Floor and Chair - conductive and non-conductive
- d. Footwear - conductive and non-conductive
- e. Undergarments - cotton, nylon, knit polyester trousers, etc
- f. Number of tests - ten for each operation

When the person completes each operation he touches a probe which connects to an electrostatic voltmeter.

TEST REPORT

Resistivity data on each test specimen will be provided. A comparison will be made between the resistivity of each specimen and the body voltage generated during each operation. From the results a material safety criteria will be developed.

APPENDIX B

ELECTROSTATIC PROPENSITY OF GARMENTS

ICRT OPERATIONAL DATA
 TA ILLUSTRATION SHEET

TESTED BY	GARMET TYPE	TRFH NO.	DATE	ALUMINUM CO	BA. GUN	VOLTMETER TYPE	STATIC CHARGE (Volts)	INDEXES		RESISTANCE	TYPE OF OPERATION	ADDITIONAL READINGS (Volts)	NOTES
								INDEX	INDEX				
W. S. Smith	Coat	1	1/13	24	33	100	100 135 95	✓	✓	✓	WALKING ON PLATE		
	Coat						40 130 100 90	✓	✓	✓	WALKING ON PLATE		
	PVA						550 570 150 148 800	✓	✓	✓	PLASTIC CHAIR		
							150 220 50 350 670	✓	✓	✓	PLASTIC CHAIR		
							350 80 50 250	✓	✓	✓	METAL CHAIR, GROUND		
							250 107 90 150	✓	✓	✓	METAL CHAIR, GROUND		
								✓	✓	✓	METAL CHAIR		
								✓	✓	✓	METAL CHAIR		
			7/6				47 2 6 42 10	✓	✓	✓	WALKING ON PLATE	0.7	
							-7 -8 -6 -7 -8	✓	✓	✓	WALKING ON PLATE		
							5 8.3 -2 7 7.5	✓	✓	✓	PLASTIC CHAIR		
							-8 -8 -7 -8 -7	✓	✓	✓	PLASTIC CHAIR		
							-5 -6.2 -2.3 -2.4 -2.7	✓	✓	✓	METAL CHAIR, GROUND		
							4 -7 -7 -8 -7	✓	✓	✓	METAL CHAIR, GROUND		
								✓	✓	✓	METAL CHAIR		
								✓	✓	✓	METAL CHAIR		
	Revelite	2	7/13	245	36		92 30 58 10 37	✓	✓	✓	WALKING ON PLATE		
	Coat						6 8 31 50 91	✓	✓	✓	WALKING ON PLATE	600	
	PVA						300 270 700 600 900	✓	✓	✓	PLASTIC CHAIR	1,300 600	
							150 330 550 400 550	✓	✓	✓	PLASTIC CHAIR		
							490 390 390	✓	✓	✓	METAL CHAIR, GROUND		
							550 275 220	✓	✓	✓	METAL CHAIR, GROUND		
							100 370 520 520 495	✓	✓	✓	METAL CHAIR		
							190 340 340 480	✓	✓	✓	METAL CHAIR		
			7/13	26	36		-11 -9.5	✓	✓	✓	WALKING ON PLATE		
							-2.5	✓	✓	✓	WALKING ON PLATE		
							5	✓	✓	✓	PLASTIC CHAIR		
							-8 -2.4	✓	✓	✓	PLASTIC CHAIR		
								✓	✓	✓	METAL CHAIR, GROUND		
							-7	✓	✓	✓	METAL CHAIR, GROUND		
							-2.4	✓	✓	✓	METAL CHAIR		

ENVIRONMENTAL DATA
RELATION SHEET

TESTER	GARMET	ITEM NO.	DATE	RELATIVE HUMIDITY	TEMP	R.H.	GUN	STATIC CHARGE (VOLTS)		SHOES	FLOOR SURFACE RESISTANCE		TYPE OF OPERATION	NOTES	ADDITIONAL READINGS (VOLTS)	BEFORE WASHING
								VOLTMETER TYPE	TYPE		MOHS	COND				
1	Woolen	3	9/13	33.3	37.5			15 20 19	7 5	✓	✓	WALKING ON PLATE				
2	Coat							8 34 74		✓	✓	WALKING ON PLATE				
3	FOX							500 330 1K	845	✓	✓	PLASTIC CHAIR				
4								1K 350 450 930		✓	✓	PLASTIC CHAIR				
5								220 300 390		✓	✓	METAL CHAIR, GROUND				
6								550 300 350		✓	✓	METAL CHAIR, GROUND				
7								270 300 1K 440		✓	✓	METAL CHAIR				
8								450 180 420 240		✓	✓	METAL CHAIR				
9										✓	✓	WALKING ON PLATE				
10			9/18	23.3	35			-8		✓	✓	WALKING ON PLATE				
11								1.7		✓	✓	WALKING ON PLATE				
12								2.6		✓	✓	PLASTIC CHAIR				
13								-8		✓	✓	PLASTIC CHAIR				
14										✓	✓	METAL CHAIR, GROUND				
15								5		✓	✓	METAL CHAIR, GROUND				
16								-8		✓	✓	METAL CHAIR				
17										✓	✓	METAL CHAIR				
18										✓	✓	WALKING ON PLATE				
19	Registat	A	9/14	23.3	38			-39 46 -5 31		✓	✓	WALKING ON PLATE				
20	Coat							-13 55 48 57		✓	✓	WALKING ON PLATE				
21	FOX							520 650 350 250		✓	✓	PLASTIC CHAIR				
22								520 1K 14K 1.3K		✓	✓	PLASTIC CHAIR				
23								50 30 40 130		✓	✓	METAL CHAIR, GROUND				
24								180 115 260 210		✓	✓	METAL CHAIR, GROUND				
25								130 20 -50 380		✓	✓	METAL CHAIR				
26								440 -110 -30 15 110		✓	✓	METAL CHAIR				
27										✓	✓	WALKING ON PLATE				
28			9/14	22.8	39			2.2 2.8 -0.8 1.4		✓	✓	WALKING ON PLATE				
29								-9 -8 -8 -8		✓	✓	WALKING ON PLATE				
30								11.5 -3 14.5 14.5 -5		✓	✓	PLASTIC CHAIR				
31								-8 -8 -8 -8		✓	✓	PLASTIC CHAIR				
32								1.7 9 .6 1.4		✓	✓	METAL CHAIR, GROUND				
33								-8 -8 -8 -8		✓	✓	METAL CHAIR, GROUND				
34								93 -3 -8 -2		✓	✓	METAL CHAIR				
35								-8 -8 -8 -8		✓	✓	METAL CHAIR				
36										✓	✓	METAL CHAIR				

TEST DOCUMENTATION DATA
TRANSLATION SHEET

TESTED BY	GARMENT TYPE	ITEM NO.	DATE	WEIGHING C. %	1971 TEMP R.H.	GUN	STATIC CHARGE (VOLTS)			SHOES	FLOOR SURFACE RESISTANCE		TYPE OF OPERATION	NOTES	ADDITIONAL READINGS (VOLTS)	BEFORE WASHING TESTS IN 833.08
							VOLTMETER	TYPE	CIR		RESISTANCE	RESISTANCE				
	COVERALS	8	1/11/71	22.2	36		40	17	39	-50	-31	✓	WALKING ON PLATE			
	WOOLWOL						110	550	300	500		✓	WALKING ON PLATE			
							600	750	730	300	1.6K	✓	PLASTIC CHAIR			
							600	330	100	200		✓	METAL CHAIR			
							570	600	630	300	350	✓	METAL CHAIR, GROUNDED			
							550	800	700			✓	METAL CHAIR, GROUNDED			
							-14					✓	WALKING ON PLATE			
							-8					✓	WALKING ON PLATE			
							1.5					✓	PLASTIC CHAIR			
							-6					✓	PLASTIC CHAIR			
							-34					✓	METAL CHAIR, GROUNDED			
							-7					✓	METAL CHAIR			
												✓	METAL CHAIR			
	Woolblend Cotton	C	1/11/71	25	37		38	14	19	14	34	✓	WALKING ON PLATE			
	COVERALS						36	36	70	8	18	✓	WALKING ON PLATE			
	New, No Flame Proof						400	470	370	580	350	✓	PLASTIC CHAIR			580
							180	350	1,028	450	450	✓	PLASTIC CHAIR			
							650	350	800			✓	METAL CHAIR, GROUNDED			
							700	1K	1.1K			✓	METAL CHAIR, GROUNDED			
							680	500	450	150	600	✓	METAL CHAIR			
							600	600	1,380K	1.4K	500	✓	METAL CHAIR			495
			1/11/71	21	38		3	-1				✓	WALKING ON PLATE			
							-8					✓	WALKING ON PLATE			
							1.9					✓	PLASTIC CHAIR			
							-8					✓	PLASTIC CHAIR			
							-8					✓	METAL CHAIR, GROUNDED			
							-8					✓	METAL CHAIR, GROUNDED			
							-8					✓	METAL CHAIR			
							-8					✓	METAL CHAIR			

INSTRUMENTATION DATA
TABULATION SHEET

TESTED BY	GARMENT TYPE	ITEM NO.	DATE	INSTRUMENTATION		STATIC CHARGE (VOLTS)		SHOES		FLOOR SURFACE RESISTANCE		TYPE OF OPERATION	NOTES
				1974	1975	1976	1977	1978	1979	1980	1981		
W. SUMNER	COTTON COVERALS	D	1/10/74	233	38	-70	-20	35	80	100	✓	WALKING ON PLATE	Hours of BEFORE WASHING minutes (before) TESTS IN B3208
						-50	-100	-50	✓	WALKING ON PLATE			
						100	-100	-120	-60	✓	PLASTIC CHAIR		
						20	45	45	✓	PLASTIC CHAIR			
						-40	-10	+33	+30	✓	METAL CHAIR, OUNDED		
						14	30	5	40	✓	METAL CHAIR		
						100	25	0	✓	METAL CHAIR			
						-2.8	✓	WALKING ON PLATE					
						-1.8	✓	WALKING ON PLATE					
						3	✓	PLASTIC CHAIR					
W. SUMNER	COTTON COVERALS	E	1/10/74	245	37	30	-25	-36	-5	5	✓	WALKING ON PLATE	52-61
						-14	-28	-17	10	30	✓	WALKING ON PLATE	
						80	52	120	160	100	✓	PLASTIC CHAIR	
						150	94	320	540	400	✓	PLASTIC CHAIR	
						-15	-28	-31	-22	✓	METAL CHAIR, OUNDED		
						-100	-30	-40	-60	✓	METAL CHAIR, OUNDED		
						130	-8	-8	2	-12	✓	METAL CHAIR	
						40	-15	-2	-8	-4	✓	METAL CHAIR	
						-13	✓	WALKING ON PLATE					
						-2.4	✓	WALKING ON PLATE					
10	✓	PLASTIC CHAIR											
-2.4	✓	PLASTIC CHAIR											
-8	✓	METAL CHAIR, OUNDED											
-15	✓	METAL CHAIR, OUNDED											
-7	✓	METAL CHAIR											
-2.4	✓	METAL CHAIR											
W. SUMNER	COTTON COVERALS	E	1/10/74	245	37	30	-25	-36	-5	5	✓	WALKING ON PLATE	52-61
						-14	-28	-17	10	30	✓	WALKING ON PLATE	
						80	52	120	160	100	✓	PLASTIC CHAIR	
						150	94	320	540	400	✓	PLASTIC CHAIR	
						-15	-28	-31	-22	✓	METAL CHAIR, OUNDED		
						-100	-30	-40	-60	✓	METAL CHAIR, OUNDED		
						130	-8	-8	2	-12	✓	METAL CHAIR	
						40	-15	-2	-8	-4	✓	METAL CHAIR	
						-13	✓	WALKING ON PLATE					
						-2.4	✓	WALKING ON PLATE					
10	✓	PLASTIC CHAIR											
-2.4	✓	PLASTIC CHAIR											
-8	✓	METAL CHAIR, OUNDED											
-15	✓	METAL CHAIR, OUNDED											
-7	✓	METAL CHAIR											
-2.4	✓	METAL CHAIR											

INSTIGMENTATION DATA
TAMULATION SHEET

Tested By	SABRANT TYPE	ITEM NO.	DATE	WINDMILL		GUN	STATIC CHARGE (VOLTS)		TYPE OF OPERATION	NOTES
				1974	1975		HPMD DISCHARGE	ELECTROMETER TYPE		
			Temp	RH	Trouser	Gun	Gun	Electrometer		
1	Coat FXR	1	9/20	41	19			0 -36 -40 -32 -15 -30	WALKING ON PLATE	ADDITIONAL PLATE WASHING TESTS IN B109
2	Workrate							0 -30 -120 +50 +50	WALKING ON PLATE	
3								0 BK 7.5K 7.5K	PLASTIC CHAIR	
4								0 BK 3.7K BK	PLASTIC CHAIR	
5								0 300 300 200	METAL CHAIR, GROUND	
6								0 350 450 300	METAL CHAIR, GROUND	
7								0 1.5 1.0 2.0	WALKING ON PLATE	
8								0 -8 -8	WALKING ON PLATE	
9								0 37 70 70 55	PLASTIC CHAIR	
10								0 -8 -8	PLASTIC CHAIR	
11								40 4.5 16.0 2.0	METAL CHAIR, GROUND	
12								-8 -8 -8	METAL CHAIR, GROUND	
13								0 40 -18 -14	WALKING ON PLATE	
14	Resquist	2	9/30	21	19			0 38 30 50	WALKING ON PLATE	
15	Coat FXR							5.5K 5.5K 6 K 5.2K	PLASTIC CHAIR	
16	Workrate							0 2K 2.8K 6 K 5.5K	PLASTIC CHAIR	
17								0 500 750 530	METAL CHAIR, GROUND	
18								0 530 600 750	METAL CHAIR, GROUND	
19								0 -8 -1.5 -8	WALKING ON PLATE	
20								0 100 70 50 60	WALKING ON PLATE	
21								C -6 3 15 8.5	PLASTIC CHAIR	
22								0 -8 -8 -8	PLASTIC CHAIR	
23								0 10 22 28	METAL CHAIR, GROUND	
24								C -8 -8 -8	METAL CHAIR, GROUND	
25										
26										
27										
28										
29										
30										
31										
32										
33										
34										
35										
36										
37										

EXPERIMENTAL DATA
CALCULATION SHEET

TESTED BY	GARRISKY	ITEM NO.	DATE APPROVED		GUN	STATIC CHARGE (VOLTS)				SHOES	WEAR MADE ON	TYPE OF OPERATION	NOTES	
			C %	Temp		RH	TRIGGER	GAUZE	ELECTROMETER					TYPE
		A	10/1	21.1	19	-10K	0	55	100	160	95	WALKING ON PLATE		
						-2K	0	-370	200	65	200	PLASTIC CHAIR		
						-3K-2K	5K-5K	5.5K	6.5K	7.8K		PLASTIC CHAIR		
						-1K	8K	6.7K	7.3K			METAL CHAIR, GROUNDED		
						-5K	0.5K	940	1230	41K		METAL CHAIR, GROUNDED		
						4K	0.5K	930	720	930		METAL CHAIR, GROUNDED		
						-4K	0	23	-3	-12	2	WALKING ON PLATE		
						-5K	0	-2	0	0		WALKING ON PLATE		
						-5K-4K	0	70	120	100	160	PLASTIC CHAIR		
						-5K	0	-8	-8	-8		PLASTIC CHAIR		
						-5K	0	20	12	20		METAL CHAIR, GROUNDED		
						-5K	0	-8	-8	-8		METAL CHAIR, GROUNDED		
		B	7/30	21.1	19		0	260	80	120	130	WALKING ON PLATE		
							0	-33	28	72	52	WALKING ON PLATE		
							5K	6K	7.2K	7.8K		PLASTIC CHAIR		
							3K-4K	7.9K	3K	5K		PLASTIC CHAIR		
							260	850	950	1K		METAL CHAIR, GROUNDED		
							500	950	850	100		METAL CHAIR, GROUNDED		
							0	16	.8	.8		WALKING ON PLATE		
							0	-8	.8	-8		WALKING ON PLATE		
							0	50	98	100	76	97	PLASTIC CHAIR	
							0	-8	-8	-8		PLASTIC CHAIR		
							0	19	12	15		METAL CHAIR, GROUNDED		
							0	-8	-8	-8		METAL CHAIR, GROUNDED		

INSTRUMENTATION DATA
TABULATION SHEET

ITEM NO.	ELEMENT TYPE	TEMP. HUMIDITY		STATIC CHARGE (VOLTS)		SHOES		MEAS. MADE ON	TYPE OF OPERATION	NOTES
		Temp	Humidity	Hand Discharge	Electrometer Type	Shoe	Shoe			
1	COVERALLS	1/30	21.1	19	0	-200	550-1K	-650-800	WALKING ON PLATE	ADDITIONAL B-PURE W-RING READINGS TESTS IN B309
2	COVERALLS				0	-220	100-160		WALKING ON PLATE	
3	COVERALLS				5K	6K	6.7K	8.2K	7K	6.5K
4	COVERALLS				10K	6K	4.5K	10K	12K	
5	COVERALLS				2K	1.8K	3.4K	2.7K	2.6K	
6	COVERALLS				5K	2.5K	4.0K	3.4K	2.8K	
7	COVERALLS				0	17	.5	1.0	1.8	
8	COVERALLS				0	-8	-8	-8		
9	COVERALLS				0	92	110	140	100	180
10	COVERALLS				0	-8	-8	-8		
11	COVERALLS				0	61	60	64		
12	COVERALLS				0	-	-	-8	-8	
13	COVERALLS				0	32	110	100	180	180
14	COVERALLS				500	3K	1.1K	1K		
15	COVERALLS				3.15K	6.5K	7K	3.8K	5.7K	
16	COVERALLS				5K	5K	3.7K	5K	5K	
17	COVERALLS				0	550	650	550		
18	COVERALLS				0	250	300	450		
19	COVERALLS				0	.8	10.5	7	3.5	
20	COVERALLS				0	-8	-8	-8		
21	COVERALLS				0	45	42	76	98	57
22	COVERALLS				0	-8	-8	-8		
23	COVERALLS				0	23	20	25	19	
24	COVERALLS				0	-8	-8	-8		
25	COVERALLS				0	-8	-8	-8		
26	COVERALLS				0	-8	-8	-8		
27	COVERALLS				0	-8	-8	-8		
28	COVERALLS				0	-8	-8	-8		
29	COVERALLS				0	-8	-8	-8		
30	COVERALLS				0	-8	-8	-8		
31	COVERALLS				0	-8	-8	-8		
32	COVERALLS				0	-8	-8	-8		
33	COVERALLS				0	-8	-8	-8		
34	COVERALLS				0	-8	-8	-8		
35	COVERALLS				0	-8	-8	-8		
36	COVERALLS				0	-8	-8	-8		
37	COVERALLS				0	-8	-8	-8		
38	COVERALLS				0	-8	-8	-8		
39	COVERALLS				0	-8	-8	-8		
40	COVERALLS				0	-8	-8	-8		
41	COVERALLS				0	-8	-8	-8		
42	COVERALLS				0	-8	-8	-8		
43	COVERALLS				0	-8	-8	-8		
44	COVERALLS				0	-8	-8	-8		
45	COVERALLS				0	-8	-8	-8		
46	COVERALLS				0	-8	-8	-8		
47	COVERALLS				0	-8	-8	-8		
48	COVERALLS				0	-8	-8	-8		
49	COVERALLS				0	-8	-8	-8		
50	COVERALLS				0	-8	-8	-8		
51	COVERALLS				0	-8	-8	-8		
52	COVERALLS				0	-8	-8	-8		
53	COVERALLS				0	-8	-8	-8		
54	COVERALLS				0	-8	-8	-8		
55	COVERALLS				0	-8	-8	-8		
56	COVERALLS				0	-8	-8	-8		
57	COVERALLS				0	-8	-8	-8		
58	COVERALLS				0	-8	-8	-8		
59	COVERALLS				0	-8	-8	-8		
60	COVERALLS				0	-8	-8	-8		
61	COVERALLS				0	-8	-8	-8		
62	COVERALLS				0	-8	-8	-8		
63	COVERALLS				0	-8	-8	-8		
64	COVERALLS				0	-8	-8	-8		
65	COVERALLS				0	-8	-8	-8		
66	COVERALLS				0	-8	-8	-8		
67	COVERALLS				0	-8	-8	-8		
68	COVERALLS				0	-8	-8	-8		
69	COVERALLS				0	-8	-8	-8		
70	COVERALLS				0	-8	-8	-8		
71	COVERALLS				0	-8	-8	-8		
72	COVERALLS				0	-8	-8	-8		
73	COVERALLS				0	-8	-8	-8		
74	COVERALLS				0	-8	-8	-8		
75	COVERALLS				0	-8	-8	-8		
76	COVERALLS				0	-8	-8	-8		
77	COVERALLS				0	-8	-8	-8		
78	COVERALLS				0	-8	-8	-8		
79	COVERALLS				0	-8	-8	-8		
80	COVERALLS				0	-8	-8	-8		
81	COVERALLS				0	-8	-8	-8		
82	COVERALLS				0	-8	-8	-8		
83	COVERALLS				0	-8	-8	-8		
84	COVERALLS				0	-8	-8	-8		
85	COVERALLS				0	-8	-8	-8		
86	COVERALLS				0	-8	-8	-8		
87	COVERALLS				0	-8	-8	-8		
88	COVERALLS				0	-8	-8	-8		
89	COVERALLS				0	-8	-8	-8		
90	COVERALLS				0	-8	-8	-8		
91	COVERALLS				0	-8	-8	-8		
92	COVERALLS				0	-8	-8	-8		
93	COVERALLS				0	-8	-8	-8		
94	COVERALLS				0	-8	-8	-8		
95	COVERALLS				0	-8	-8	-8		
96	COVERALLS				0	-8	-8	-8		
97	COVERALLS				0	-8	-8	-8		
98	COVERALLS				0	-8	-8	-8		
99	COVERALLS				0	-8	-8	-8		
100	COVERALLS				0	-8	-8	-8		

INSTRUMENTATION DATA
TABULATION SHEET

TEST #	GARRONT	DATE	TEMPERATURE		STATIC CHARGE (VOLTS)		HAND DISCHARGE ELECTROMETER TYPE & I/O	SHOES		TYPE OF OPERATION	NOTES
			C°	F°	RESISTANCE	RESISTANCE		SOLE COND.	SOLE COND.		
1	E	10/21	19	0	0	500	550	100	100	WALKING ON PLATE	
2	Coveralls			0	0	70	100	100		WALKING ON PLATE	
3	Old. W. T. E			4K	4K	5K	4.8K	4.2K		PLASTIC CHAIR	
4	FLAME PROOF			4K	4K	4K	4K	5.2K		PLASTIC CHAIR	
5				0	0	60	380	240		METAL CHAIR, GROUND	
6				0	0	600	600	50		METAL CHAIR, GROUND	
7				0	0	5	5	4		WALKING ON PLATE	
8				0	0	0	0	0		WALKING ON PLATE	
9				0	0	100	130	60	45	PLASTIC CHAIR	
10				0	0	0	0	0		PLASTIC CHAIR	
11				0	0	5	9	11		METAL CHAIR, GROUND	
12				0	0	C	-8	-8	-8	METAL CHAIR, GROUND	
13										WALKING ON PLATE	
14										WALKING ON PLATE	
15										PLASTIC CHAIR	
16										METAL CHAIR, GROUND	
17										METAL CHAIR, GROUND	
18										WALKING ON PLATE	
19										WALKING ON PLATE	
20										PLASTIC CHAIR	
21										METAL CHAIR, GROUND	
22										METAL CHAIR, GROUND	
23										WALKING ON PLATE	
24										WALKING ON PLATE	
25										PLASTIC CHAIR	
26										METAL CHAIR, GROUND	
27										METAL CHAIR, GROUND	
28										METAL CHAIR, GROUND	
29										METAL CHAIR, GROUND	
30										METAL CHAIR, GROUND	
31										METAL CHAIR, GROUND	
32										METAL CHAIR, GROUND	
33										METAL CHAIR, GROUND	
34										METAL CHAIR, GROUND	
35										METAL CHAIR, GROUND	
36										METAL CHAIR, GROUND	
37										METAL CHAIR, GROUND	
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43										METAL CHAIR, GROUND	
44										METAL CHAIR, GROUND	
45										METAL CHAIR, GROUND	
46										METAL CHAIR, GROUND	
47										METAL CHAIR, GROUND	
48										METAL CHAIR, GROUND	
49										METAL CHAIR, GROUND	
50										METAL CHAIR, GROUND	

1. IDENTIFICATION DATA
IN RADIATION SHEET

TEST NO.	GARMENT	DATE	BY	ITEM NO.	TYPE	DATE		STATIC CHARGE (VOLTS)		INDEXES		FLOOR SURFACE	TESTS PERFORMED IN	NOTES
						TEST	TEMP	TYPE	TYPE	INDEX	INDEX			
1	Wool Sweater	10/2	22.8	27	CUN	200	100-210	0	✓	✓	✓	WALKING ON LINOLINUM	PRIOR TO 10 WASHINGS 83208	
2	Wool Sweater	10/2	22.8	27	CUN	250	390	0	✓	✓	✓	WALKING ON LINOLINUM	All measurements were made on light conductive linoleum which was either powdered or impregnated (unlisted).	
3	Cashmere Sweater	10/2	22.8	27	CUN	200	140	60	✓	✓	✓	WALKING ON ASBESTOS FLOOR		
4	Cashmere Sweater	10/2	22.8	27	CUN	150	240	70	✓	✓	✓	WALKING ON ASBESTOS FLOOR		
5	Cashmere Sweater	10/2	22.8	27	CUN	200	3K	3K	✓	✓	✓	PLASTIC CHAIR		
6	Cashmere Sweater	10/2	22.8	27	CUN	200	700	700	✓	✓	✓	PLASTIC CHAIR	First reading was 9 FT.	
7	Cashmere Sweater	10/2	22.8	27	CUN	42	3.9		✓	✓	✓	WALKING ON LINOLINUM		
8	Cashmere Sweater	10/2	22.8	27	CUN	8	.8		✓	✓	✓	WALKING ON LINOLINUM		
9	Cashmere Sweater	10/2	22.8	27	CUN	3.1	4.6		✓	✓	✓	WALKING ON ASBESTOS FLOOR		
10	Cashmere Sweater	10/2	22.8	27	CUN	2.3	2.3		✓	✓	✓	WALKING ON ASBESTOS FLOOR		
11	Cashmere Sweater	10/2	22.8	27	CUN	2	7	12	✓	✓	✓	PLASTIC CHAIR		
12	Cashmere Sweater	10/2	22.8	27	CUN	6.5	4.5		✓	✓	✓	PLASTIC CHAIR		
13	Cashmere Sweater	10/2	22.8	27	CUN									
14	Cashmere Sweater	10/2	22.8	27	CUN									
15	Cashmere Sweater	10/2	22.8	27	CUN									
16	Cashmere Sweater	10/2	22.8	27	CUN									
17	Cashmere Sweater	10/2	22.8	27	CUN									
18	Cashmere Sweater	10/2	22.8	27	CUN									
19	Cashmere Sweater	10/2	22.8	27	CUN									
20	Cashmere Sweater	10/2	22.8	27	CUN									
21	Cashmere Sweater	10/2	22.8	27	CUN									
22	Cashmere Sweater	10/2	22.8	27	CUN									
23	Cashmere Sweater	10/2	22.8	27	CUN									
24	Cashmere Sweater	10/2	22.8	27	CUN									
25	Cashmere Sweater	10/2	22.8	27	CUN									
26	Cashmere Sweater	10/2	22.8	27	CUN									
27	Cashmere Sweater	10/2	22.8	27	CUN									
28	Cashmere Sweater	10/2	22.8	27	CUN									
29	Cashmere Sweater	10/2	22.8	27	CUN									
30	Cashmere Sweater	10/2	22.8	27	CUN									
31	Cashmere Sweater	10/2	22.8	27	CUN									
32	Cashmere Sweater	10/2	22.8	27	CUN									
33	Cashmere Sweater	10/2	22.8	27	CUN									
34	Cashmere Sweater	10/2	22.8	27	CUN									
35	Cashmere Sweater	10/2	22.8	27	CUN									
36	Cashmere Sweater	10/2	22.8	27	CUN									
37	Cashmere Sweater	10/2	22.8	27	CUN									
38	Cashmere Sweater	10/2	22.8	27	CUN									
39	Cashmere Sweater	10/2	22.8	27	CUN									
40	Cashmere Sweater	10/2	22.8	27	CUN									
41	Cashmere Sweater	10/2	22.8	27	CUN									
42	Cashmere Sweater	10/2	22.8	27	CUN									
43	Cashmere Sweater	10/2	22.8	27	CUN									
44	Cashmere Sweater	10/2	22.8	27	CUN									
45	Cashmere Sweater	10/2	22.8	27	CUN									
46	Cashmere Sweater	10/2	22.8	27	CUN									
47	Cashmere Sweater	10/2	22.8	27	CUN									
48	Cashmere Sweater	10/2	22.8	27	CUN									
49	Cashmere Sweater	10/2	22.8	27	CUN									
50	Cashmere Sweater	10/2	22.8	27	CUN									

INSTRUMENTATION DATA
TABULATION SHEET

TESTED BY	GARGUMENT TYPE	ITEM NO	DATE	TEMP RH	% RH	GUM TRANSFER	STATIC CHARGE (VOLTS)	HAND DISCHARGE ELECTROMETER	TYPE OF OPERATION	NOTES	ADDITIONAL WASHINGS	AFTER 10 MINUTES
VanSonne	Respirator	1	10/18	26.7	26.5				WALKING ON PLATE			
	Coat, FXX						2.8K 1.2K 1.25K		PLASTIC CHAIR			
	WASHBITE						700 600 700		PLASTIC CHAIR			
							210 200 320		METAL CHAIR, GROUNDED			
							120 110 0		METAL CHAIR, GROUNDED			
							-2.5 -2 -1.0		WALKING ON PLATE			
							-4 -4 -4		WALKING ON PLATE			
							13 2 3		PLASTIC CHAIR			
							2 2 5		PLASTIC CHAIR			
							-4 -5 +4 1		METAL CHAIR, GROUNDED			
							3 2 -2		METAL CHAIR, GROUNDED			
VanSonne	Respirator	2	10/18	26.7	26.5		70 110 110		WALKING ON PLATE			
	Coat, FXX						320 200		WALKING ON PLATE			
	WASHBITE						630 580 830		PLASTIC CHAIR			
							500 1.2K 750		PLASTIC CHAIR			
							-70 100 250		METAL CHAIR, GROUNDED			
							70 140 110		METAL CHAIR, GROUNDED			
							2 0 2		WALKING ON PLATE			
							-5 4.5 6		WALKING ON PLATE			
							-1 -1 -1 -1		PLASTIC CHAIR			
							-7 -7 -7		METAL CHAIR, GROUNDED			
							-2.2 +1.5 -3.8		METAL CHAIR, GROUNDED			

INSTRUMENTATION DATA
TABULATION SHEET

TESTED BY	GARMENT TYPE	ITEM NO	DATE	STATIC CHARGE (VOLTS)		SHOES	TYPE OF OPERATION	NOTES	AFTER IO
				Co % RH	Hand Disc Mark 64				
1	99% WARE B	B	10/17	25.5	29.5				ADDITIONAL WASHINGS (10 MIN)
2	1% S.S								
3	COVERALS								
4	WASHES								
5									
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BIORADIATION DATA
IRRADIATION SHEET

INVEST BY	GARMENT TYPE	ITEM NO.	DATE	ATMOSPHERIC C	RH	GUM	STATIC CHARGE (VOLTS)			INDEXES		FLOOR SURFACE RESISTANCE MERS PER CM	TYPE OF OPERATION	NOTES ADDITIONAL READINGS (MITS)	APRER TEN WASHING TESTS IN B 3109
							VALUETER	TYPE	TYPE	TYPE	TYPE				
1	99% Cotton Control	F	2300	21.1	19		-200	100	200	350	✓		PLASTIC CHAIR	350	
2	99% Cotton Control	B	2100	21.1	19		-200	300	400		✓		PLASTIC CHAIR		
3	99% Cotton Control	F	2300	21.1	19		9K	6K	75K		✓		PLASTIC CHAIR		CONTROL UNWASHED
4	99% Cotton Control	C	2100	21.1	19		2.9K	1.9K	1.9K	20K	✓		PLASTIC CHAIR		
5	99% Cotton Control	G	2300	21.1	19		3.5K	2.5K	3K		✓		PLASTIC CHAIR		CONTROL UNWASHED

APPENDIX C

RELATIVE RESISTIVITY OF TEST GARMENTS

INSTRUMENTAL DATA
FABRICATION SHEET

MATERIAL OR GARMENT	24°C		PRIOR TO TEN WASHINGS - OHMS		19 1/2 RH 70°F		21.1°C		AFTER TEN WASHINGS 24 TO 26°C			
	NO	VOLT/CURRENT RESISTANCE	SIMPSON VOM	19 1/2 RH 70°F	RESISTANCE	SIMPSON VOM	21.1°C	OHMS	24 TO 26°C	RESISTANCE	SIMPSON VOM	NOTES
HIGH RESISTANT RUBBER PLATFORM	1	6 x 10 ⁸	---	---	---	---	---	---	---	---	---	---
Rieselstat Coat Fyx 1	1	---	20K	---	---	---	---	---	---	---	---	---
Rieselstat Coat Fyx 2	2	1.41 x 10 ⁸	---	2.0 Meg	---	---	---	---	---	---	---	---
Rieselstat Coat Fyx 3	3	---	100K	---	---	---	---	---	---	---	---	---
Rieselstat Coat Fyx A	A	---	---	---	---	---	---	---	---	---	---	---
NOVEX plus 1 1/2 G.S. COVERALLS	B	---	---	20 Meg	---	---	---	---	---	---	---	---
COTTON COVERALLS NEW NO FLAME PROOF	C	1.15 x 10 ⁸	---	---	---	---	---	---	---	---	---	---
COTTON COVERALLS NEW WITH FLAME PROOF	D	1.46 x 10 ⁸	---	---	---	---	---	---	---	---	---	---
COTTON COVERALLS OLD WITH FLAME PROOF	E	1.91K	---	---	---	---	---	---	---	---	---	---

NOTE: THE COTTON COVERALLS WERE TREATED WITH FLAME PROOFING AFTER EACH WASHING

THE RIEGELSTAT SAMPLE PATCHES WERE NOT WASHED

APPENDIX D

CAPACITANCE MEASUREMENTS OF TEST SUBJECT

CAPACITANCE MEASUREMENTS OF TEST SUBJECT

1. Insulated Spark Proof Shoes

Capacitance (Picofarads)		Test Performed	
Measurement Plate was		in Building	
Grounded	Ungrounded	3208	3109
110	108	x	-
120	120	-	x
110	110	-	x

2. Conductive Shoes

Capacitance (Picofarads)		Test Performed	
Measurement Plate was		in Building	
Grounded	Ungrounded	3208	3109
1380	-	x	-
1520	-	x	-
4600	3770	-	x
3470	-	-	x

3. Test Subject Capacitance Standing on Asbestos Floor Tile

Capacitance (Picofarads)		Test Performed
Shoes		
Insulated	Conductive	in Building
100	140	3208

4. Capacitance Measurement Plate

The measurement plate is a copper sheet 91.4 x 244 cm (3 x 8 ft) which lays on, and is insulated from, two sheets of polyethylene. For this test the copper sheet is ungrounded (insulated). Test performed in Bldg. 3109.

C = 12,300 picofarads

5. Capacitance of Test Subject Standing on Polyethylene Sheet

A polyethylene sheet was placed over the copper plate on which test subject stood and a capacitance measurement was taken. Test performed in Bldg. 3208.

C = 1200 picofarads

APPENDIX E

HAND TO GROUND THROUGH SHOE RESISTANCE
MEASUREMENT OF TEST SUBJECT

HAND TO GROUND THROUGH SHOE RESISTANCE MEASUREMENT OF TEST SUBJECT

1. Insulated, Spark Proof Shoes

Metal Floor Grounded	Insulated from Ground
4×10^{11} ohms	10^{12} to 10^{13} ohms

2. Conductive Shoes

Metal Floor	
Grounded	Ungrounded
500K ohms 700K ohms 900K ohms	n/a

APPENDIX F

EQUIPMENT

EQUIPMENT

1. Electrical

a. Electrometer, Model 610B, including probe Model 6103A (1000:1) and probe model 6101A (1:1). Manufactured by Keithley Instruments.

b. High Voltage Power Supply Model 240A, manufactured by Keithley Instruments

c. Impedance Bridge, Type No. 1650A, manufactured by General Radio Co.

d. VOM, Simpson Model 260

e. Static Meter, Model CMI-7777, manufactured by Custom Materials, Inc., Chelmsford, Massachusetts

2. Accessories

a. Conductive shoes, Government issue

b. Insulated shoes, spark proof, Government issue

c. Copper plate 8.128 mm (.032 in.) thick, 91.4 x 244 cm (3 x 8 ft)

d. Two each polyethylene sheets 5.08 mm (.020 in.) thick, 122 x 274 cm (4 x 9 ft)

APPENDIX G

ELECTROSTATIC HAND DISCHARGE

APPENDIX H

COMPARISON OF ELECTROSTATIC HAND DISCHARGE OF TEST GARMENTS

DISTRIBUTION LIST

Commander
U.S. Naval Sea Systems Command
ATTN: SEA-04H2, G. Heimer
Washington, DC 20362

Commander
U.S. Naval Air Systems Command
ATTN: AIR-5162, P. Yurcisin
Washington, DC 20361

Headquarters
U.S. Army Materiel Development and
Readiness Command
ATTN: DRCSF
AMCRD-GI
AMCRD-T
5001 Eisenhower Avenue
Alexandria, VA 22333

Commander
U.S. Army Armament Materiel
Readiness Command
ATTN: DRSAR-SF
DRSAR-LEP-L
Rock Island, IL 61299

Commander
U.S. Army Test and Evaluation Command
ATTN: AMSTE-TAA
Aberdeen Proving Ground, MD 21005

Commander
U.S. Army Armament Research and
Development Command
ATTN: DRDAR-TSE-M (10)
DRDAR-TSE-M, J. Van Savage (3)
DRDAR-TSS (5)
Dover, NJ 07801

Administrator
Defense Technical Information Center
ATTN: Accessions Division (12)
Cameron Station
Alexandria, VA 22314

Weapon System Concept Team/CSL
ATTN: DRDAR-ACW
Aberdeen Proving Ground, MD 21010

Technical Library
ATTN: DRDAR-CLJ-L
APG, Edgewood Area, MD 21010

Director
U.S. Army Ballistic Research Laboratory
ATTN: DRDAR-TSB-S
Aberdeen Proving Ground, MD 21005

U.S. Army Materiel Systems
Analysis Activity
ATTN: DRXSY-MP
Aberdeen Proving Ground, MD 21005

Chief, Bureau of Medicine and Surgery
Department of the Navy
ATTN: BUMED-4A
Washington, DC 20372

Scientific Director
Biomedical Research Laboratory
Walter Reed Army Medical Center
Washington, DC 20012

Library of Congress
Science and Technology Division
Washington, DC 20540

Director
Development Center
Marine Corps Development and
Education Command
Quantico, VA 22134

Naval Research Laboratory
Technical Information Division
ATTN: Code 6214, Mr. W. Ferguson
Washington, DC 20370

Benet Weapons Laboratory
Technical Library
ATTN: DRDAR-LCB-TL
Watervliet, NY 12189

Director
U.S. Army TRADOC Systems Analysis Activity
ATTN: ATAA-SL (Technical Library)
White Sands Missile Range, NM 88002

Commander
Defense Personnel Support Center
ATTN: NLABS Representative
2800 South 20th Street
Philadelphia, PA 19101

School of Textiles
North Carolina State University
ATTN: Library
P.O. Box 5006
Raleigh, NC 27607

Commander
Air Force Materials Laboratory
ATTN: Mr. J. Ross, Technical Area Manager
Fibrous Materials, Composite and
Fibrous Materials Branch
Wright Patterson AFB, OH 45433

Commandant
U.S. Army Quartermaster School
ATTN: Quartermaster Library (2)
Fort Lee, VA 23801

Commander
U.S. Army Research Office, Durham
ATTN: CRD-AA-IP
Box CM, Lake Station
Durham, NC 27706

Commander
Arctic Aeromedical Laboratory
ATTN: Librarian
APO 731, Seattle, Washington 98733

Commander
U.S. Army Electronics R&D Laboratories
ATTN: Technical Information Division
Fort Monmouth, NJ 07003

Director
U.S. Army Mechanics & Materials
Research Center
ATTN: Technical Library
Watertown, MA 02172

Commander
U.S. Army Arctic Test Center
APO Seattle, Washington 98733