

AD-A 062 087

TECHNICAL LIBRARY

AD

AD-E400 215

TECHNICAL REPORT ARLCD-TR-78054

EFFECTS OF ADHESIVE AND PROCESSING PARAMETERS ON ADHESIVE BONDING OF POLYCARBONATE

DAVID W. LEVI
RAYMOND F. WEGMAN
MARIE C. ROSS
WILLIAM C. TANNER
MICHAEL J. BODNAR

AUGUST 1978



US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND
LARGE CALIBER
WEAPON SYSTEMS LABORATORY
DOVER, NEW JERSEY

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED.

The views, opinions, and/or findings contained in this report are those of the author(s) and should not be construed as an official Department of the Army position, policy or decision, unless so designated by other documentation.

Destroy this report when no longer needed. Do not return to the originator.

The citation in this report of the names of commercial firms or commercially available products or services does not constitute official endorsement or approval of such commercial firms, products, or services by the United States Government.

ERRATA

TECHNICAL REPORT ARLCD-TR-78054

EFFECTS OF ADHESIVE AND PROCESSING PARAMETERS
ON ADHESIVE BONDING OF POLYCARBONATE

David W. Levi
Raymond F. Wegman
Marie C. Ross
William C. Tanner
Michael J. Bodnar

Change item 3, page 5, in the basic publication to read as follows:

3. Whether ethanol wipe or sanding surface treatment is used appears to be immaterial as far as strength and durability of polycarbonate bonds is concerned.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER ARLCD-TR-78054	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) EFFECTS OF ADHESIVE AND PROCESSING PARAMETERS ON ADHESIVE BONDING OF POLYCARBONATE		5. TYPE OF REPORT & PERIOD COVERED
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) David W. Levi, Raymond F. Wegman, Marie C. Ross, William C. Tanner, Michael J. Bodnar		8. CONTRACT OR GRANT NUMBER(s) AMCMS Code No. 612105H840011
9. PERFORMING ORGANIZATION NAME AND ADDRESS ARRADCOM, LCWSL Applied Sciences Div, (DRDAR-LCA-OA) Dover, NJ 07801		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS ARRADCOM, TSD ATTN: DRDAR-TSS, STINFO Div Dover, NJ 07801		12. REPORT DATE AUGUST 1978
		13. NUMBER OF PAGES 21
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) ARRADCOM, LCWSL Applied Sciences Div, (DRDAR-LCA-OA) Dover, NJ 07801		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Adhesive bonding Mechanical properties Weibull distribution Polycarbonate		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The Weibull distribution was found to be quite useful in studying the effects of adhesive and processing parameters on adhesive bonding of polycarbonate. Adhesive selection is very important in satisfactorily bonding this polymer. Ethanol wipe and sanding as surface pretreatments of the polycarbonate appear to be equivalent. The humidity exposure of polycarbonate before and during bonding is briefly discussed. Surface exposure times (SET) of up to 30 days appear not to affect strength of either tested or aged specimens of urethane adhesive bonds. The lower-strength epoxy		

~~UNCLASSIFIED~~

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

20. (Cont'd)

bonds aged 30 days at 49°C (120°F) and 95% RH lose strength after the 30-day SET.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

TABLE OF CONTENTS

	Page No.
Introduction	1
Results and Discussion	1
Conclusions	5
References	5
Distribution List	13
Tables	
1 Correlation coefficients for linear Weibull distribution plots	7
2 Bond strengths at $F(X) = 0.50$	8
3 Test for significance of 30-day SET	9
Figures	
1 Comparison of adhesives and processing parameters for polycarbonate	10
2 Weibull distribution plot for all of the strength data for aged epoxy	

INTRODUCTION

The effects of processing parameters on adhesive bonding of metals, specifically aluminum (ref. 1, 2), titanium (ref. 3), and ferrous metals (ref. 4), have been the subject of continuing study by Picatinny/ARRADCOM Applied Science personnel. Particular emphasis has been placed on surface exposure times (SET), since these times can be significant in an assembly line operation. Generally, SET times of 10 to 30 days do not affect bond strengths, and treated metal parts can be wrapped and stored for a number of days before assembly is completed without adverse effect. The effects of other factors, such as surface treatment, adhesive characteristics, and aging, have also been investigated.

This report documents a more recent study of the effects of these parameters on the bonding of an important new organic structural polymer, polycarbonate (Lexan). Since the experimental procedures and the data used in this study were developed during the earlier work and are available in reference 5, they are not repeated in this report.

RESULTS AND DISCUSSION

Two adhesives were used in this study: a two-component urethane, Uralane 5738, and a two-component epoxy, Epon 828/Versamid 140.

To prepare the dry specimens, half of the Lexan panels were dried for 24 hours at 60°C (140°F) before the surfaces were treated; the other half (the wet specimens) were kept for 24 hours at 49°C (120°F) and 95% relative humidity (RH).

All of the panels were wiped with ethanol and air dried. The faying surfaces of one-half of the panels were sanded by hand (sanded specimens) before bonding while the other half were bonded directly after the ethanol wipe and air drying (ethanol wipe).

SET times of 0 to 4 hours, 15 days, and 30 days were obtained by conditioning the surface-prepared specimens at 23°C (73°F) and 50% RH for these times. The aged specimens were conditioned for 30 days at 49°C (120°F) and 95% RH before testing.

Since the data tended to show the usual adhesive-bond-strength scatter, it was quite difficult to draw firm conclusions visually as to the effect of the various parameters. The earlier work (refs. 1-4) indicated

that metal-bond-strength data could readily be fitted with a Weibull distribution function, which was also applicable to the present polycarbonate data.

The Weibull distribution function (ref. 6, 7) was used in the form

$$\log \log \left[\frac{1}{1-F(X)} \right] = -\log \alpha + \beta \log (X-\gamma) \quad (1)$$

where $F(X)$ is the distribution function, i.e., the fraction of samples failing at a strength (psi or Pa) of X or less, X corresponds to the strength values, and α , β , and γ are the parameters of the function. A plot of the left-hand side of equation (1) versus $\log (X - \gamma)$ should give a straight line. γ is selected on an iterative basis by making trial plots. α and β may be evaluated from the intercept and the slope.

In the application to the present data, all data points are tabulated in order of increasing bond strength and the data are plotted, according to equation (1), with $\gamma = 0$. The correlation coefficients (table 1) indicated that taking $\gamma = 0$ and using a two-parameter Weibull distribution appears to be satisfactory.

The linear Weibull distribution plots are shown in figure 1; correlation coefficients are given in table 1. It is immediately evident from these plots that the urethane adhesive (Uralane 5738) forms stronger bonds with polycarbonate than the epoxy (Epon 828/Versamid 140). Even the aged Uralane bonds are somewhat stronger than the unaged epoxy, although aging 30 days at 49°C (120°F) and 95% RH reduces bond strength in each case. A numerical comparison can readily be obtained from figure 1 at any value of $F(X)$. For example, taking $F(X) = 0.50$, we obtain the bond strength values in table 2 which enables us to compare actual bond strengths easily.

For both the Uralane tested at 23°C (73°F) and 50% RH and the aged specimens, a single line with correlation coefficient in the 0.99 region describes all of the data in each case. This would indicate that the ethanol wipe and sanding treatments are equivalent for the Uralane-bonded specimens. SET times of 0 to 4 hours, 15 days, and 30 days are also indistinguishable for these bonds.

Essentially the same results described for the urethane bonds were obtained for the epoxy bonds tested at 23°C (73°F) and 50% RH. A single Weibull line with correlation coefficient 0.994 described all of the data. Ethanol wipe and sanding of polycarbonate surfaces could not be distinguished. SET times of 0-4 hours, 15 days and 30 days gave essentially the same strengths.

The results for the aged epoxy are more complicated. Figure 1 and table 2 show that the bond strengths are quite low. The data scatter is also very troublesome, a fact that might be anticipated from the low bond strengths. The plot of all of the data is not satisfactory. Examination of the data indicated that values for the aged epoxy with dry, ethanol-wiped polycarbonate were much lower than for the other aged epoxy conditions. The plots in figure 1 thus give two distributions for aged epoxy and show that the data are much better represented by two distributions. The origin of the extraordinarily low strengths for the aged epoxy-dried, ethanol-wiped panels is obscure.

The distribution in figure 1 with only nine points was plotted with a table of plotting positions from which appropriate adjustments were made for the smallness of the sample size (ref. 7). This is only necessary where there are fewer than 20 points in the distribution.

Examination of the line in figure 1 for the aged epoxy as well as the correlation coefficients in table 1 indicated that results for this aged epoxy system are not as good as for the other systems studied. Further examination of the raw data revealed that the 30-day SET yielded lower strength bonds than 0 to 4 hours or 15 days. The Wilcoxon Sum of Ranks Test was used (ref. 8) to test the statistical significance of this visual observation. The data and appropriate tabulations are shown in table 3. In this table, the B tally represents 30-day SET while the A tally corresponds to the 0 to 4 hour and 15-day SET.

Since there were more than 20 measurements in the A samples, the significance of the B Ranks total (R) was found by

$$Z = \frac{n_B (n_A + n_B + 1) - 2R}{\left[\frac{(n_A)(n_B)(n_A + n_B + 1)}{3} \right]^{1/2}}$$

where n_A and n_B are the number of measurements in the A and B tally.
For the present case

$$Z = \frac{15 (29 + 15 + 1) - 2 (145.5)}{\frac{(29) (15) (29 + 15 + 1)}{3}}^{1/2}$$

$$Z = 4.75$$

The exact values of Z corresponding to important probability levels are (ref. 8)

$$P = 10\% \quad P = 5\% \quad P = 1\% \quad P = 0.2\%$$

$$Z = 1.64 \quad Z = 1.96 \quad Z = 2.58 \quad Z = 3.09$$

Since $Z = 4.75$, P is below 0.2%. This means that the observed difference between the 30-day SET and the other SET times could be expected as a result of chance less than once in 500 times. Since this possibility is remote, the difference can be considered quite significant. For the aged epoxy bonds, the 30-day SET leads to significantly weaker adhesive bonds.

Perhaps the most troublesome aspect of this work involves the question of the effect of moisture on bonded polycarbonate. Essentially equivalent results were obtained by pre-conditioning polycarbonate at 60°C (140°F) (dry) or at 49°C (120°F) and 95% RH (wet) (fig. 1, ref. 5). However, after the pre-conditioning step, the polycarbonate was prepared for bonding under ambient conditions, then conditioned at 23°C (73°F) and 50% RH for the SET period. The specimens were then bonded under ambient conditions, after which half were stored 7 days at 23°C (73°F) and 50% RH before testing and half were aged 30 days at 49°C (120°F) and 95% RH. Because of these subsequent treatments, it is questionable whether the terms "wet" and "dry", as defined above, are meaningful.

The strength of one group of epoxy-bonded specimens (ref. 5) after 15 days SET was abnormally low. These specimens, both "dry" and "wet", were bonded on an unusually humid day [89% RH and 21°C (70°F)]. Another otherwise identical group were prepared at 23°C (73°F) and 50% RH. In the latter case, the strengths were markedly higher and agreed with the other SET values.

CONCLUSIONS

1. The Weibull distribution is quite useful in comparing strengths of adhesive bonds to polycarbonate.
2. Selection of adhesive is important in bonding polycarbonate.
3. Ethanol wipe and sanding surface treatments do not, apparently, affect the strength and durability of polycarbonate bonds.
4. SET times of up to 30 days do not appear to affect the strength of ambient-tested and aged specimens of Uralane 5738. However, the strength of aged specimens of Epon 828/Versamide is reduced after 30 days SET.
5. The exact effect of moisture on polycarbonate bonding cannot be determined by the results of this study.

REFERENCES

1. D. W. Levi, W. C. Tanner, M. C. Ross, R. F. Wegman and M. J. Bodnar, "Effect of Surface Exposure Time on Bonds to Aluminum," *J. Appl. Polymer Sci.* 20, 1475 (1976)
2. D. W. Levi, "Durability of Adhesive Bonds to Aluminum," *Proc. Symp. on Durability of Adhesive Bonded Structures*, ARRADCOM, p. 283, October 1976
3. D. W. Levi, R. F. Wegman and M. J. Bodnar, "Effect of Titanium Surface Pretreatment and Surface Exposure Time on Peel Strength of Adhesive Bonds," *SAMPE J.* 1977, p. 32 (Mar/Apr)
4. D. W. Levi, M. C. Ross, W. C. Tanner, R. F. Wegman and M. J. Bodnar, "Effect of Processing Parameters on the Adhesive Bonding of Ferrous Metals," ARRADCOM Technical Report ARLCD-TR-77029, Dover, NJ, August 1977
5. M. C. Ross, W. C. Tanner, E. McAbee, and M. J. Bodnar, "Effect of Varying Processing Parameters in the Fabrication of Adhesive-Bonded Structures. Part X. Adhesive Bonding of Structural Plastics," Picatinny Arsenal Technical Report 4318, Dover, NJ, July 1972

6. F. H. Steiger, "Practical Applications of the Weibull Distribution Function," Chem. Tech. p. 225, 1971
7. C. A. Moyer, J. J. Bush, and B. T. Ruley, "The Weibull Distribution Function for Fatigue Life," Mater. Res. Stand. 2, p. 405 (1962)
8. R. Langley, Practical Statistics, Dover Pub., New York, 1971

Table 1. Correlation coefficients for linear Weibull distribution plots

System	Correlation coefficient
Uralane	0.996
Uralane, aged	0.990
Epoxy	0.994
Epoxy, aged	0.931
Epoxy, aged-dry, ethanol wiped	0.996

Table 2. Bond strengths at $F(X) = 0.50$

System	Bond strength
Uralane	720 psi (4.96×10^6 Pa)
Uralane, aged	560 psi (3.86×10^6 Pa)
Epoxy	390 psi (2.69×10^6 Pa)
Epoxy, aged	140 psi (9.65×10^5 Pa)

Table 3. Test for significance of 30-day SET

X	Tally	Rank value	B Ranks
66	B	1	1
68	B	2	2
70	A B	3,4	3.5
72	B	5	5
76	BB	6,7	13
80	BB	8,9	17
84	B	10	10
88	A BB	11,12,13	24
92	A B	14,15	14.5
98	B	16	16
100	A B	17,18	17.5
110	AAA	19,20,21	
130	B	22	22
140	A	23	
160	AA	24,25	
170	A	26	
180	AA	27,28	
190	AAAA	29,30,31,32	
200	AAA	33,34,35	
210	AA	36,37	
220	A	38	
250	AA	39,40	
290	A	41	
300	A	42	
310	AA	43,44	

R = 145.5

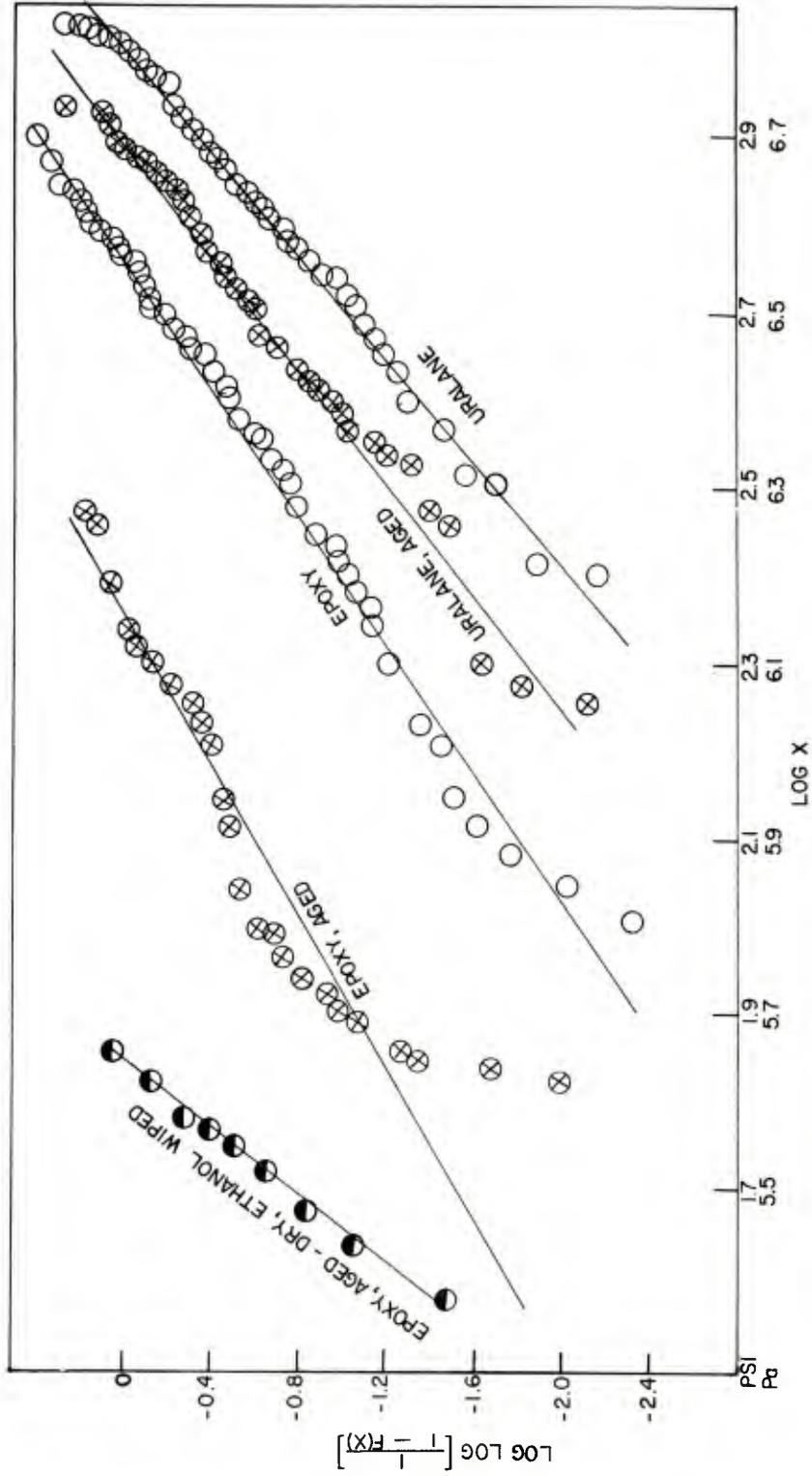


Figure 1. Comparison of adhesives and processing parameters for polycarbonate.

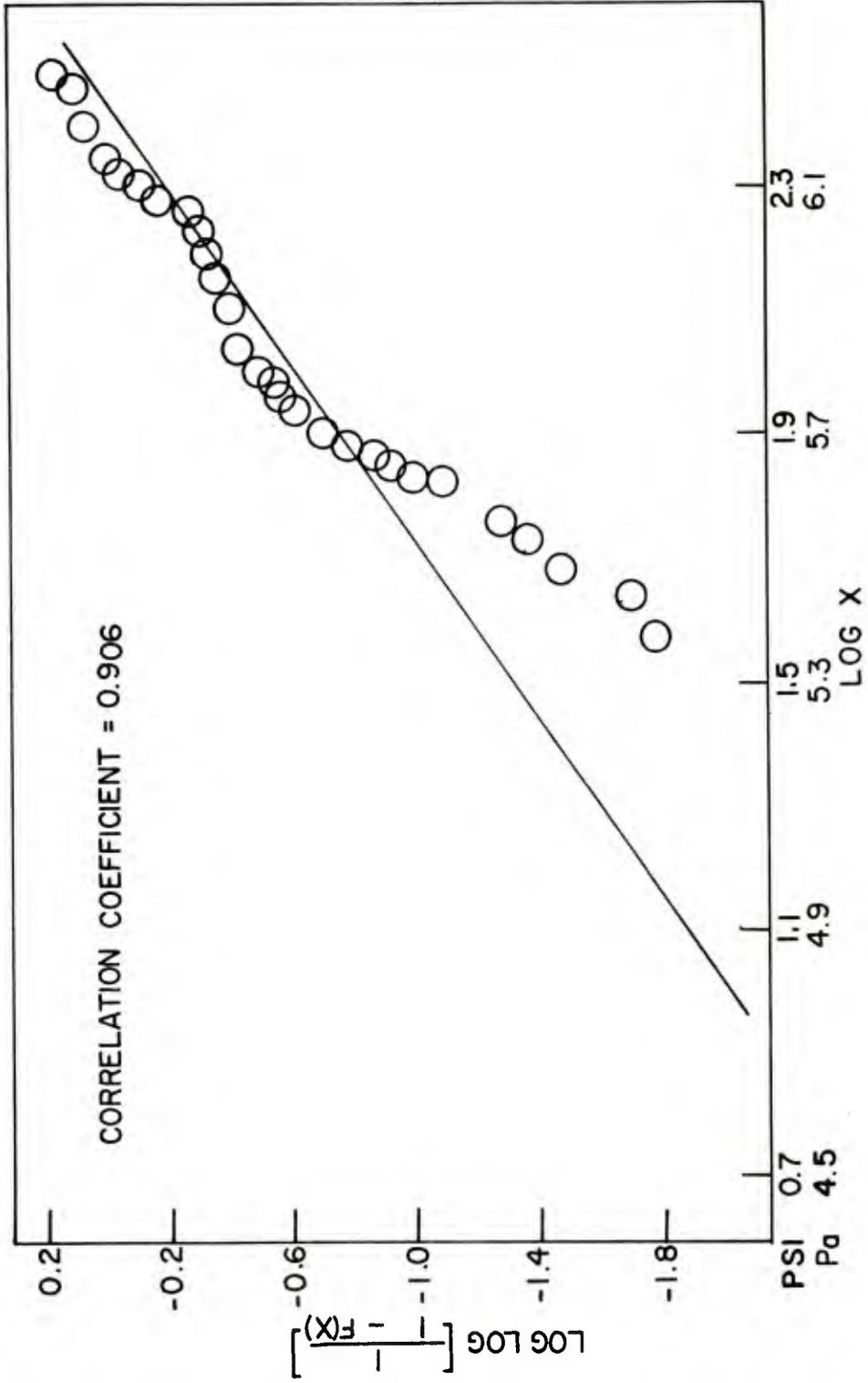


Figure 2. Weibull distribution plot for all of the strength data for aged epoxy.

DISTRIBUTION LIST

Commander
US Army Armament Research and
Development Command
ATTN: DRDAR-TSS (5)
DRDAR-LCA-OA (15)
DRDAR-LCN (5)
DRDAR-LCU (5)
DRDAR-QA (2)
DRDAR-TSF (2)
DRDAR-QAA
DRDAR-QAN
DRDAR-LCA-OK, Mr. H. Pebly
Mr. A. Landrock
Dover, NJ 07801

Commander
US Army Materiel Development and
Readiness Command
ATTN: DRCPP-PI
DRCQA
5001 Eisenhower Avenue
Alexandria, VA 22304

Commander
US Army Missile Research and
Development Command
ATTN: DRSMI-RLM, Mr. E. A. Verchot
Chief, Document Section
Redstone Arsenal, AL 35801

Commander
US Army Armament Materiel
Readiness Command
ATTN: DRSAR-ASF, Mr. H. Wohlferth
Rock Island, IL 61299

Commander
US Army Electronics Command
ATTN: DRSEL-TL-ME, Mr. Dan Lichenstein
DRSEL-TL-ME, Mr. A. J. Raffalovich
DRSEL-TL-ME, Mr. G. Platau
DRSEL-PP-EM2, Ms. Sarah Rosen
Fort Monmouth, NJ 07703

Director
US Army Tank-Automotive Research and
Development Command
ATTN: DRSTRA-KMD
Warren, MI 48090

Commander
US Army Materials & Mechanics
Research Center
ATTN: DRXMR-FR, Dr. G. Thomas
DRXMR-PL
Technical Information Section
Watertown, MA 02172

Director
US Army Production Equipment Agency
ATTN: DRXPE-MT, Mr. H. Holmes (2)
Rock Island Arsenal, IL 61299

Commander
Corpus Christi Army Depot
ATTN: DRSTS-MES, Stop 55 (2)
DRSTS-MESA, Mr. T. Tullos (2)
DRSTS-MESP, Mr. Bulloch
Corpus Christi, TX 78419

Commander/Director
Chemical Systems Laboratory
USA ARRADCOM, Bldg E5101
Aberdeen Proving Ground, MD 21010

Chief
Benet Weapons Laboratory
LCWSL, USA ARRADCOM
ATTN: DRDAR-LCB
Watervliet, NY 12189

Director
US Army Engineer Waterways
Experiment Station, P.O. Box 631
Corps of Engineers
ATTN: Mr. Hugh L. Green, WE SSS1
Vicksburg, MS 39180

Commander
US Army Medical Bio-Engineering
Research and Development Laboratories
Fort Detrick
ATTN: Dr. C. Wade
Frederick, MD 21701

Commander
Harry Diamond Laboratories
ATTN: Mr. N. Kaplan
Mr. J. M. Boyd
Library
Washington, DC 20438

Commander
Chemical Systems Laboratory
ATTN: DRDAR-CLE-PM, Mr. Dave Schneck
Aberdeen Proving Ground, MD 21010

Commander
Tobyhanna Army Depot
ATTN: Mr. A. Alfano
Tobyhanna, PA 18466

Director
US Army Ballistic Research Laboratory
US Army ARRADCOM, Bldg 328
Aberdeen Proving Ground, MD 21005

Commander
US Army Materiel Development and
Readiness Command
ATTN: DRCPM-UA, Mr. C. Musgrave
DRCPM-LH, Mr. C. Cioffi
DRCPM-HLS-T, Mr. R. E. Hahn
P.O. Box 209
St Louis, MO 63166

Commander
Natick Research & Development Command
Natick, MA 01760

Commander
US Army Engineer Research
and Development Laboratories
Fort Belvoir, VA 22060

Department of the Navy
Naval Air Systems Command
ATTN: Mr. John J. Gurtowski (AIR 52032C)
Washington, DC 20360

Naval Ordnance Station (NOSL)
ATTN: Mr. W. J. Ryan Code 5041
Southside Drive
Louisville, KY 40214

Naval Avionics Facility
ATTN: Mr. B. D. Tague, Code D/802
Mr. Paul H. Guhl, D/033.3
21st and Arlington
Indianapolis, IN 46218

Commander
US Naval Weapons Station
ATTN: Research and Development Division
Yorktown, VA 23491

Commander
Aeronautical Systems Division
ATTN: Mr. W. Scardino, APML/MXE
Mr. T. J. Aponyi
Composite and Fibrous Materials Br
Nonmetallic Materials Division
Wright-Patterson Air Force Base, OH 45433

Dr. Robert S. Shane, Staff Scientist
National Materials Advisory Board
National Academy of Sciences
2101 Constitution Avenue, NW
Washington, DC 20418

US Army Air Mobility
R&D Laboratory, Headquarters
ATTN: Mr. F. Immen, MS 207.5
Ames Research Center
Moffet Field, CA 94035

Naval Ship Engineering Center
ATTN: Mr. W. R. Graner, SEC 6101E
Prince George's Center
Hyattsville, MD 20782

Mare Island Naval Shipyard
Rubber Engineering Section
ATTN: Mr. Ross E. Morris, Code 134.04
Vallejo, CA 94592

Hanscom Air Force Base
ATTN: Mr. R. Karlson, ESD/DE, Stop 7
HQ, ESD
Bedford, MA 01731

Naval Air Development Center
Materials Laboratory
ATTN: Mr. Coleman Nadler, Code 30221
Div, AVTD
Warminster, PA 18974

Defense Documentation Center (12)
Cameron Station
Alexandria, VA 22314

Commander
USA Troop Support and
Aviation Materiel Readiness Command
ATTN: DRSTS-MEU (2), Mr. E. Dawson
DRSTS-ME (2), Mr. C. Sims
DRSTS-MEN (2), Mr. L. D. Brown
DRSTS-MEL (2), Mr. Bell
DRSTS-MET (2), Mr. Ceasar
P.O. Box 209, Main Office
St. Louis, MO 63166

Commander
USA Aviation R&D Command
ATTN: DRDAV-EQA, Mr. W. McClane
4300 Goodfellow Blvd.
St. Louis, MO 63120

US Army TRADOC Systems
Analysis Activity
ATTN: ATAA-SL (Tech Lib)
White Sands Missile Range, NM 88002

Commander
US Army Armament Materiel and
Readiness Command
ATTN: DRSAR-LEP-L
Rock Island, IL 61299

US Army Materiel Systems
Analysis Activity
ATTN: DRXSY-MP
Aberdeen Proving Ground, MD 21005

Weapon System Concept Team/CSL
ATTN: DRDAR-ACW
Aberdeen Proving Ground, MD 21010

Technical Library
ATTN: DRDAR-CLJ-L
Aberdeen Proving Ground, MD 21005

Technical Library
ATTN: DRDAR-TSB-S
Aberdeen Proving Ground, MD 21010

Technical Library
ATTN: DRDAR-LCB-TL
Benet Weapons Laboratory
Watervliet, NY 12189