

ARMY MATERIALS & MECHANICS RESEARCH CENTER
TECHNICAL INFORMATION SECTION
WATERTOWN, MASSACHUSETTS 02172

Cy 1



AD A033715

AMMRC CTR 76-39

MACHINE CASTING OF FERROUS ALLOYS

November 1976

by M.C. Flemings, K.P. Young, R.G. Riek, J.F. Boylan, R.L. Bye

MASSACHUSETTS INSTITUTE OF TECHNOLOGY
Department of Materials Science and Engineering
Cambridge, Massachusetts 02139

INTERIM TECHNICAL REPORT: ARPA CONTRACT NO. DAAG46-73-C-0110

Sponsored by: Defense Advanced Research Projects Agency ARPA Order No. 2267

Program Code No. 4010

Effective Date of Contract: January 1973

Contract Expiration Date: June 1976

Amount of Contract: \$1,069,846

Contract Period Covered by Report: 1 January 1976 - 30 June 1976

Approved for public release; distribution unlimited.

Prepared for

ARMY MATERIALS AND MECHANICS RESEARCH CENTER
Watertown, Massachusetts 02172

The views and conclusions contained in this document are those of the authors and should not be interpreted as necessarily representing the official policies, either expressed or implied, of the Advanced Research Projects Agency or the U. S. Government.

Mention of any trade names or manufacturers in this report shall not be construed as advertising nor as an official indorsement or approval of such products or companies by the United States Government.

DISPOSITION INSTRUCTIONS

**Destroy this report when it is no longer needed.
Do not return it to the originator.**

MACHINE CASTING OF FERROUS ALLOYS

Interim Technical Report

ARPA Contract No DAAG46-73-C-0110

June 1976

by

M. C. Flemings, K. P. Young, R. G. Riek,
J. F. Boylan, R. L. Bye

MASSACHUSETTS INSTITUTE OF TECHNOLOGY
Department of Materials Science and Engineering
Cambridge, Massachusetts 02139

Sponsored by: Defense Advanced Research Projects Agency ARPA Order No. 2267

Program Code No. 4010

Effective Date of Contract: January 1973

Contract Expiration Date: June 1976

Amount of Contract: \$1,069,846

Contract Period Covered by Report: 1 January 1976 - 30 June 1976

This research was supported by the Advanced Research Projects Agency of the Department of Defense and was monitored by the Army Materials and Mechanics Research Center under Contract No. DAAG46-73-C-0110.

TABLE OF CONTENTS

ABSTRACT	1
Introduction	3
Continuous Rheocasting	5
Thixocasting	7
Summary and Conclusions	10
References	11
Table I	12
Table II	13
Figures	14

ABSTRACT

This is the fifth interim report describing research conducted at the Massachusetts Institute of Technology as part of a joint university-industry research program on machine casting of ferrous alloys. It covers the period of the thirty-sixth to the forty-second month of this four-year program.

The basic system for Thixocasting ferrous alloys is fully and reliably operational. The Continuous Rheocaster works dependably in production runs in which typically up to 500 pounds of steel is produced at a rate of about 80 pounds per hour. Much longer runs could be produced if desired.

The Thixocast reheating process is completely automated. The two stage heating cycle employed delivers steel charges suitable for Thixocasting with a maximum temperature variation in the charge of $\pm 3^{\circ}\text{C}$. Work has been primary on 304 and 440C stainless steel.

Emphasis during this period has been on the production of a large amount of Rheocast stainless steel and the initiation of large scale Thixocasting runs to test actual die life. More than 3000 pounds of Rheocast stainless steel have been produced to date. Five hundred stainless steel Thixocastings have been produced in a hardened H-13 steel die with die life superior to results reported for H-13 dies used for liquid cast steel. The castings produced showed consistently good internal soundness. This Thixocasting work has been primarily on 304 stainless steel; additional work is planned on 440C.

Mechanical property evaluation of Thixocast 304 stainless steel indicates it possesses strength superior to the conventionally cast alloy with somewhat less ductility.

Introduction

In January, 1973, a joint university-industry research activity was undertaken to develop an economical method of machine casting ferrous alloys. A portion of this program was conducted at Massachusetts Institute of Technology primarily on machine casting of semi-solid alloys into reusable metal dies. A variety of casting concepts have been explored as reported in previous reports,^[1-4] but major emphasis of the work has been on two processes: Rheocasting and Thixocasting. In Rheocasting, a semi-solid slurry of a metal alloy is produced by vigorous agitation of a solidifying melt. This highly fluid slurry, typically the consistency of heavy machine oil at fractions solidified up to 0.5, is then cast directly to shape. In Thixocasting, fully solid ingots are first made from the semi-solid slurry and "charges" from these ingots are then reheated to the liquid-solid range and cast. Because the alloy slurries are thixotropic, these reheated charges retain their shape, behaving as soft solids, during transfer to the die casting machine. The high shear rates the charge undergoes within the gate entry and land area of the casting cavity reduce its viscosity to a level at which it flows smoothly into the cavity.

Previous reports in this series^[1-4] summarize the program through the first three years of activity (period ending December 31, 1975). At that point in the program the major thrust of effort had been on the development of a pilot plant scale system for Thixocasting ferrous alloys. This report summarizes the 6 month period January 1, to June 30, 1976 in which the system has been operated in essentially final form, and the emphasis has been placed on (1) the preparation of a

large amount of Rheocast steel for large scale Thixocasting runs to test actual die life in a variety of die materials, and (2) the initiation of those runs. The first such die study run has been completed in this period with encouraging results, both in terms of die life and casting quality.

Work has also continued during this period on the development of new forming processes utilizing a modified version of the Pb-Sn model alloy Continuous Rheocaster. Also, experimental and theoretical analysis of heat transfer in die casting is continuing.

Continuous Rheocaster

During this report period, the design of the Continuous Rheocaster for stainless steel production has been finalized. In total more than 3000 pounds of stainless steel have been produced together with smaller quantities of other alloys in runs of up to 500 pounds. Total production is detailed in Table 1.

A larger crucible size has been implemented. It is essentially similar to the previous design except that the upper chamber ferrous alloy capacity has been increased from 17 pounds to 40 pounds. A schematic of the larger furnace is shown in Figure 1. A high density alumina sheath has been incorporated outside the agitation zone to improve heat extraction efficiency. With this design the maximum AISI 304 stainless steel slurry output rate is about $300 \text{ pounds hour}^{-1}$ at about 0.5 volume fraction solid. In actual operation such high output is limited by the capacity of the upper reservoir chamber to intermittent bursts of about 40 pounds. During normal operation output and melting rate are balanced to give continuous uninterrupted production at a rate of about $80 \text{ pounds hour}^{-1}$. Typical runs now produce from 250 to 500 pounds. Furnace life is usually limited to 2 runs, but could be much greater. At the present time furnace life is dictated by failure of the internal alumina nozzle which has been traced to flaws in the as-received pieces. Erosion of the ceramics at nozzle failure is otherwise slight. Slag attack on the alumina components in the area of the slurry output nozzle has been eliminated by the incorporation of an Argon-4% Hydrogen protective gas shroud as shown in Figure 1.

Control of the Continuous Rheocaster is now almost exclusively by monitoring the amperage needed to drive the rotor in the agitation zone at constant speed. Thermocouples in the reservoir and stirring rotor remain for start up purposes but, save for monitoring reservoir chamber superheat, are not utilized in production. Continuous output of slurry of essentially constant fraction solid is achieved simply by regulating flow rate to stabilize the rotor drive amperage indication.

Considerable effort has also been developed to characterization of Continuously Rheocast AISI 304 stainless steel. A typical water quenched microstructure is shown in Figure 2. This shows the duplex structure of the primary solid particles consisting of δ ferrite partially transformed by peritectic reaction to austenite. The solute segregation throughout the microstructure of water quenched samples of the 304 stainless steel slurries has been determined by microprobe analysis. Figure 3 shows the typical measured variation in Fe, Cr, Ni, and Mn across a primary solid particle. The effect of heat treatment on the microsegregation in these structures is being investigated.

A program is also underway to characterize the inclusions found in Rheocast stainless steel.

Thixocasting

During this report period, the Thixocasting process for die casting partially solidified slurries of high temperature alloys has been radically improved by the introduction of a fully automatic reheat station (Figure 4). The new system incorporates a fully insulated induction furnace which has improved coil design to minimize end losses. This is coupled to a redesigned Softness Indicator^[4], which shuts off power to the induction coil and ejects the charge from the furnace when it has reached the desired casting condition (typically .45 to .55 fraction solid). The Softness Indicator now utilizes an adjustable air cylinder drive, while the actual probe has been changed to 1/8 inch diameter, flat bottom alumina rod which performs better at the higher operating temperatures experienced during the reheating of stainless steels. This system has the capacity for two stage heating, the initial stage being a high heating rate (typical 40 KW) step to quickly bring the charge up the alloy solidus temperature, while the second step reduces the heat input to a predetermined level which minimizes any temperature gradients through the ingot during final heating. This procedure has been refined to permit heating of 304 stainless steel charges to the liquid-solid region with a maximum measured temperature variation in the charge of $\pm 3^{\circ}\text{C}$. The resulting reheat cycles for both 440C and 304 stainless steel have been reduced to approximately ninety seconds. Further reductions could of course be effected with relatively simple, but time consuming modifications.

Die life studies for Thixocast stainless steel has continued through this report period using a variety of die materials. Identical

die inserts for the casting of the M16 rifle hammer have been machined in H-13 and H-21 die steels and hardened according to recommended industrial practices. To date, over 500 shots have been made into one set of hardened H-13 inserts operated at 275⁰C. No welding has been experienced, and die failure has been limited to fatigue cracking at localized hot spots on the die surface. A history of part finish is shown in Figure 5. This is a significant improvement over previously reported works on H-13 die life for casting steels^[5,6].

These parts were cast at about 0.5 volume fraction solid and a sample of 291 castings were rated radiographically for internal soundness according to a previously adopted scale^[3]. The results are shown in Figure 6 and because of the excellent internal soundness of the majority of the castings a new, stricter standard was adopted as illustrated in Figure 7. The histogram of Figure 8 shows the radiographic rating of the same sample of 291 castings according to this new scale.

Approximately 100 shots of Thixocast stainless steel have been made under the same conditions into the identical shape in H-21 die inserts. While results are still not complete at this time, the trend shows a marked improvement in die life for H-21 over that of H-13.

In addition to die life studies, work investigating the mechanical properties of Thixocast parts has been conducted^[7]. Tensile specimens were die cast in performed shapes under identical conditions, machined to final shape and tested. As Table II indicates, typical results for Thixocast 304 stainless steel show a significant improvement in strength over the conventionally cast alloy, with somewhat less ductility.

As part of some complimentary research done in the area of formability and mechanical property evaluation of Rheocast 304 stainless steel, ITT Harper Company has tested the mechanical properties of Rheocast ingots subsequently extruded^[8].

Rheocast ingots, supplied by M.I.T. were hydrostatically extruded (at 900-950⁰C, extrusion ratio 4.6:1), machined and tensile tested. The results, as shown in Figure 9, indicate that the tensile properties of extruded Rheocast 304 stainless steel are at least equivalent to extruded wrought material and superior to conventionally cold worked 304 stainless steel.

Summary Conclusions

1. The design of the Continuous Rheocaster has been finalized. It has produced stainless steel slurries at a continuous production rate of 80 pounds hour⁻¹ in runs as large as 500 pounds.
2. More than 3000 pounds of Rheocast stainless steel ingots have been produced, most of which will be used for large scale Thixocasting runs to study actual die life.
3. The reheating system for Thixocasting has been completely automated. Charges of stainless steel can be reheated for Thixocasting in 90 seconds with a maximum temperature variation within the charge of $\pm 3^{\circ}\text{C}$. Casting rate for stainless steel is 40 shots hour⁻¹ in the Thixocasting system.
4. A die life study in which 500 304 stainless steel Thixocastings have been made in a hardened H-13 die steel die indicates die life superior to that reported for H-13 dies when used for liquid cast steel. The castings from this study show consistently good internal soundness.
5. Initial mechanical property evaluation indicates that Thixocast 304 stainless steel is superior in strength to the conventionally cast alloy, with somewhat less ductility. In limited testing Extruded Rheocast 304 stainless steel possessed mechanical properties at least equivalent to those obtained for extruded wrought 304 stainless steel.

References

1. M. C. Flemings et al., "Machine Casting of Ferrous Alloys," Interim Technical Report AMMRC CTR 74-27, ARPA contract DAAG46-73-C-0110, 1 January - 30 December 1973, prepared for AMMRC, Watertown, Mass.
2. M. C. Flemings et al., "Machine Casting of Ferrous Alloys," Interim Technical Report AMMRC CTR 74-55, ARPA contract DAAG46-73-C-0110, 1 January - 30 December 1974, prepared for AMMRC, Watertown, Mass.
3. M. C. Flemings et al., "Machine Casting of Ferrous Alloys," Interim Technical Report AMMRC CTR 75-22, ARPA contract DAAG46-73-C-0110, 1 July - 30 June 1975, prepared for AMMRC, Watertown, Mass.
4. M. C. Flemings, K. P. Young, R. G. Riek, "Machine Casting of Ferrous Alloys," Interim Technical Report AMMRC CTR 76-15, ARPA contract DAAG46-73-C-0110, 1 July - 31 December 1975, prepared for AMMRC, Watertown, Mass.
5. G. D. Chandley, G. Scholl, Hitchner Manufacturing Corp., "Machine Casting of Ferrous Alloys," Interim Technical Report AMMRC CTR 75-9, ARPA contract DAAG46-73-C-0112, 1 July 1974 - 30 January 1975, prepared for AMMRC, Watertown, Mass.
6. A. B. Draper, E. E. Klans, J. H. Hoke, J. M. Samuels, G. Scholl, "Casting Ferrous Metals into Refractory Metal Dies," Final Report to The Pennsylvania Science and Engineering Foundation, August 1975.
7. F. E. Goodwin, "Structure and Properties of Thixocast High Temperature Alloys," S.M. Thesis, M.I.T., September 1976.
8. H. L. Andrews, J. S. Orlando, I.T.T. Harper Inc., Research and Development Case Report No. RD-7304-2.

TABLE I

TOTAL PRODUCTION OF CONTINUOUSLY RHEOCAST ALLOYS

<u>Alloy</u>	<u>Pounds Produced</u>
Copper Alloy 905	1050
AISI 440 C Stainless Steel	1080
AISI 304 Stainless Steel	1950
H.S. 31 Cobalt Base Superalloy	250

TABLE IIINITIAL MECHANICAL PROPERTY EVALUATION OF THIXOCAST
304 STAINLESS STEEL AT M.I.T.

	<u>Ultimate Tensile Strength psi</u>	<u>0.2% Offset (Yield) Stress psi</u>	<u>% Elongation at Rupture</u>
Typical Thixocast	91,000	41,000	25
Typical Investment Cast	70-80,000	35-40,000	30-40

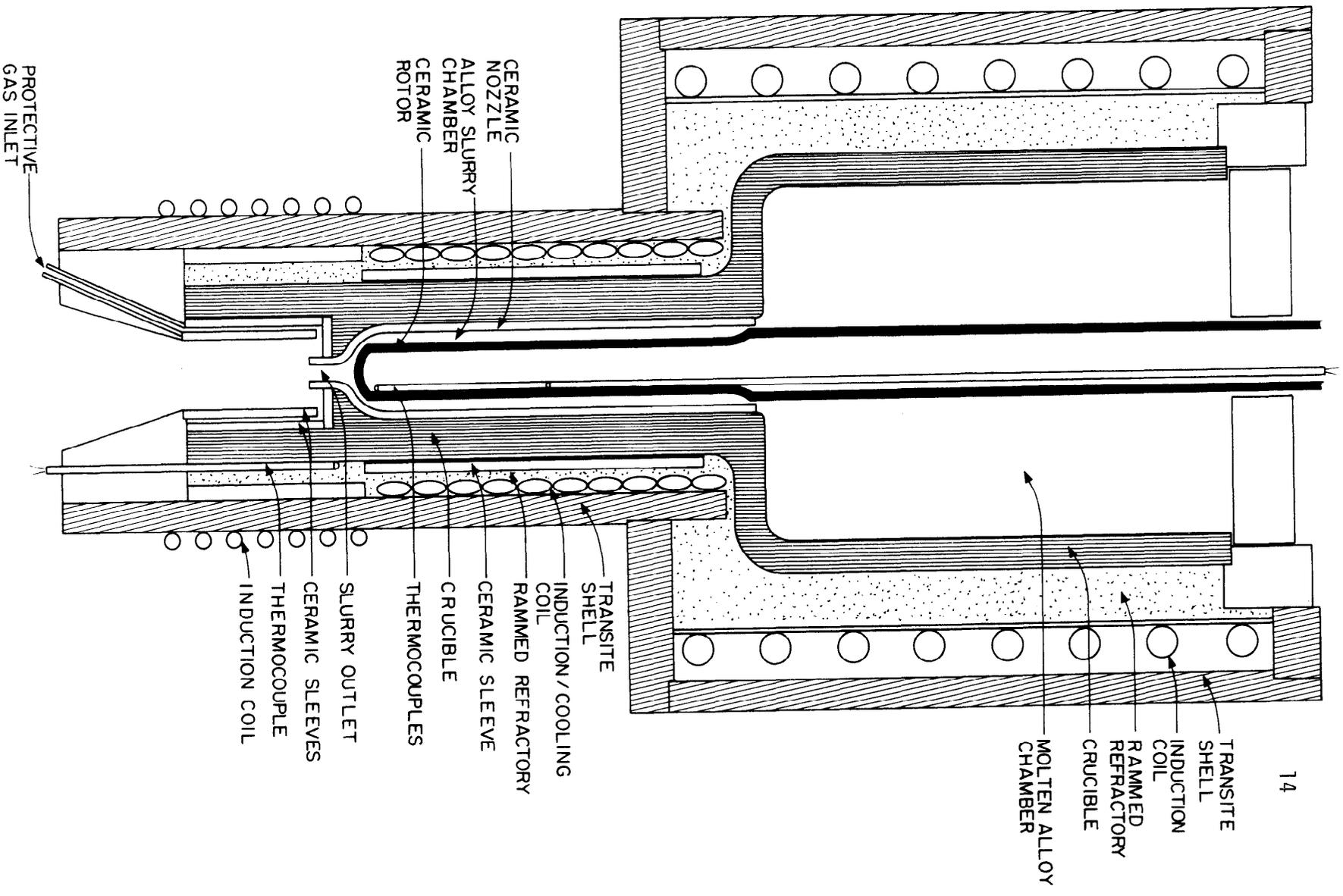
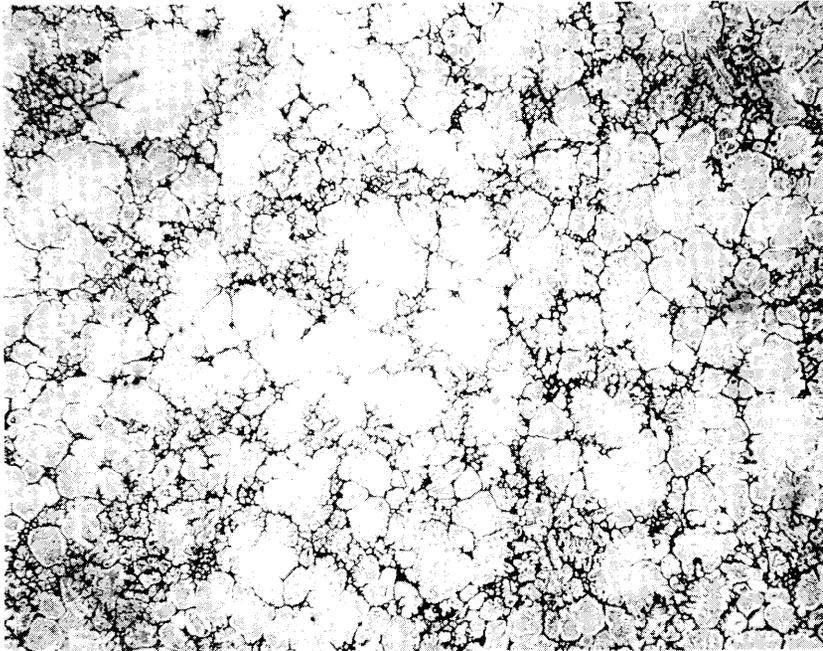
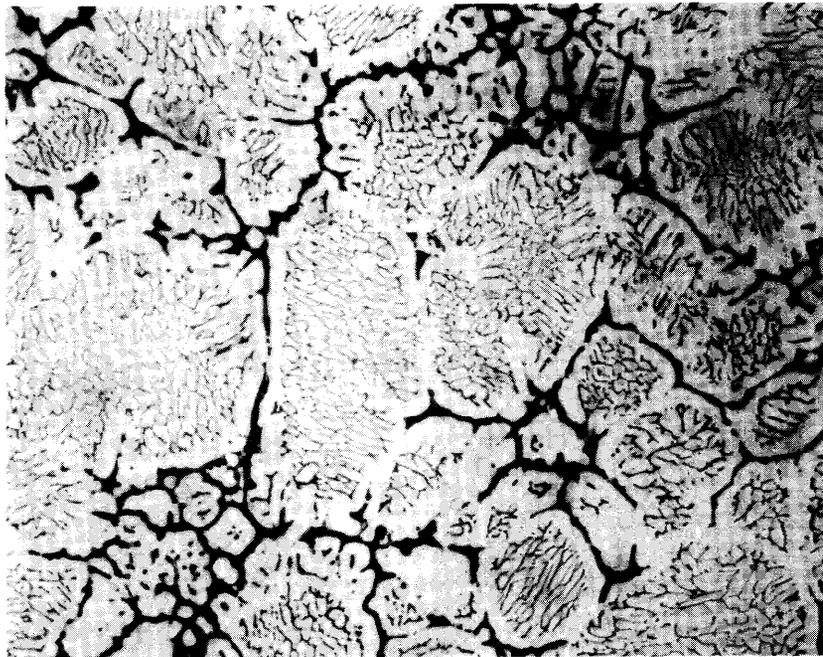


Figure 1: Schematic cross section of the Continuous Rheocasting furnace which has an upper chamber steel capacity of 40 pounds. Overall furnace height is 20-1/2 inches.



(a)



(b)

Figure 2: Photomicrographs of Continuously Rheocast AISI 304 stainless steel. KOH electrolytic etch. (a) 50X; (b) 200X.

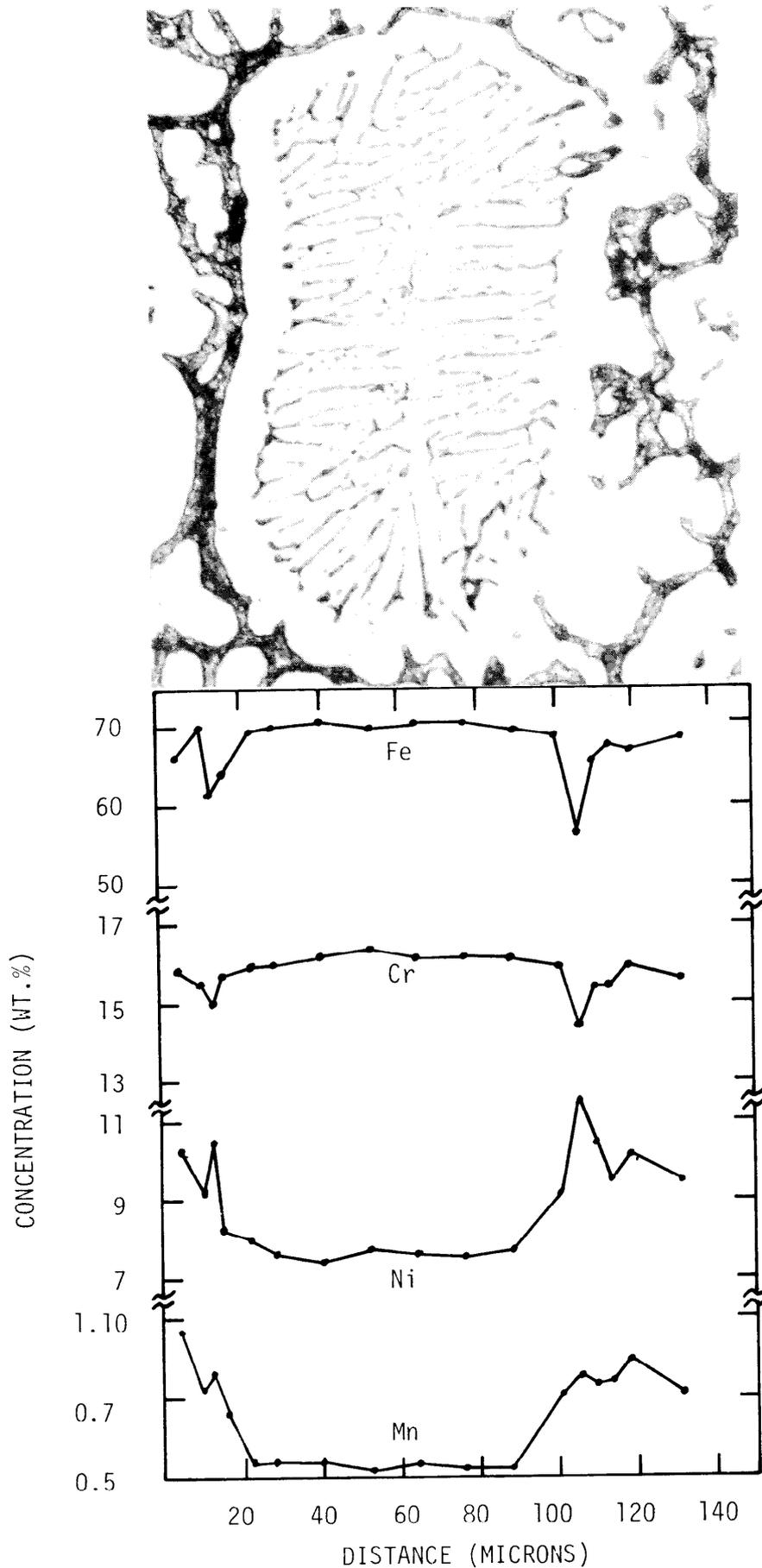


Figure 3: Microprobe data showing typical composition variations in AISI 304 stainless steel slurry. Sample was direct water quenched on removal from the Continuous Rheocaster.

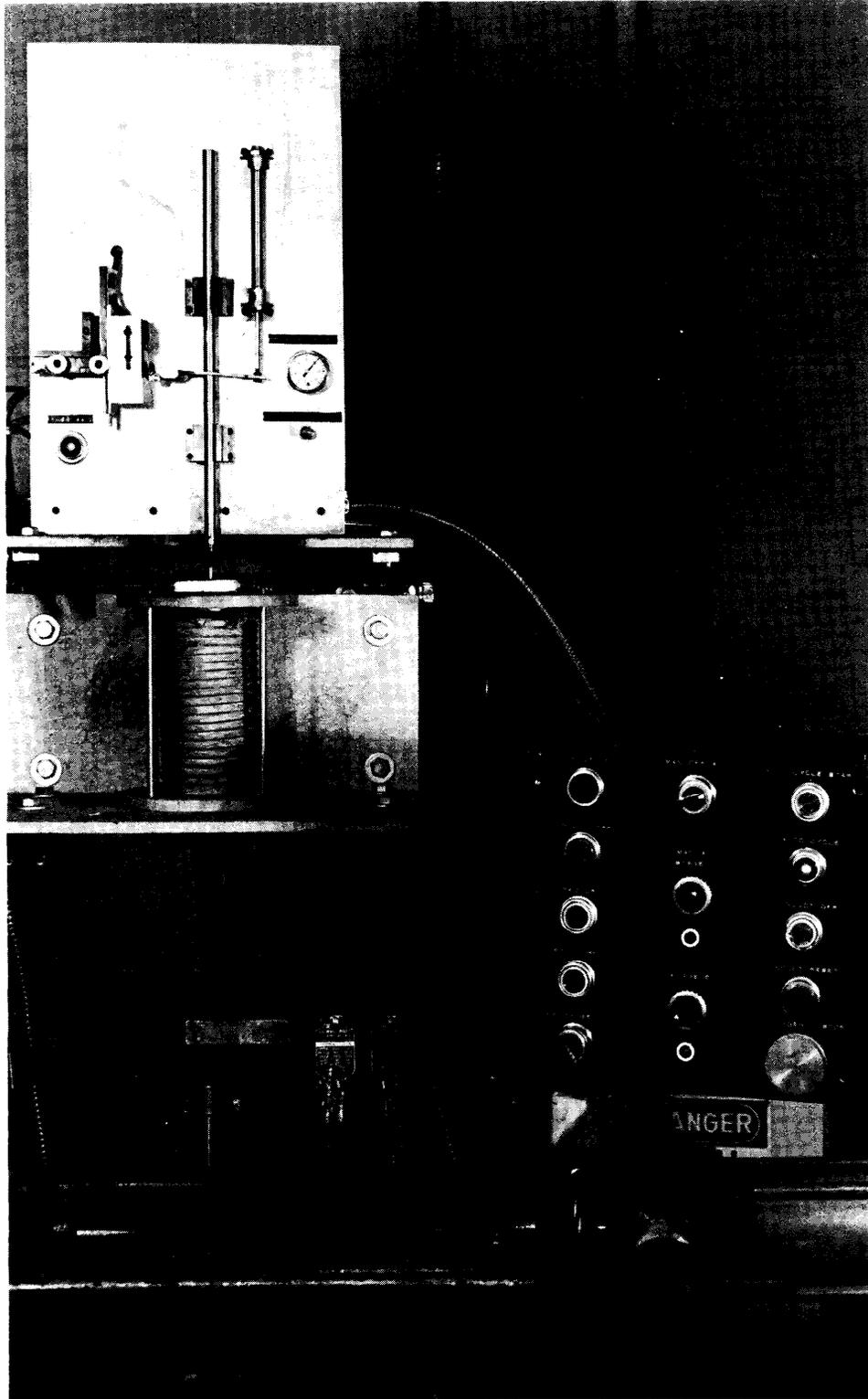
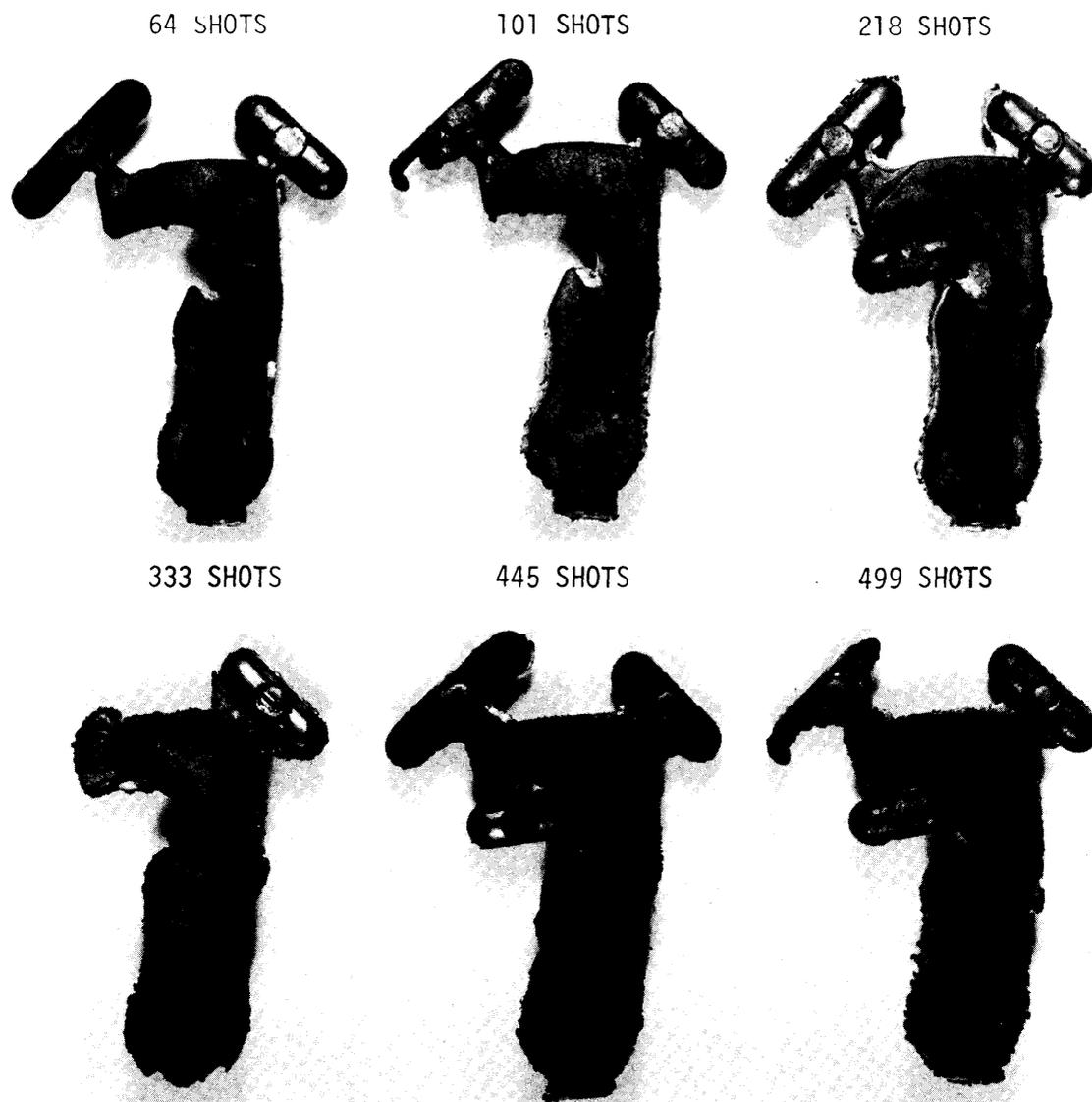


Figure 4: Overall view of the automated Thixocast reheating station.



THIXOCASTINGS OF M16 RIFLE HAMMER 304 STAINLESS/ H13 DIE STEEL

Figure 5: Sequence of 304 stainless steel Thixocastings produced at various intervals in the 500 shot die study run in H-13 die steel. 1X.

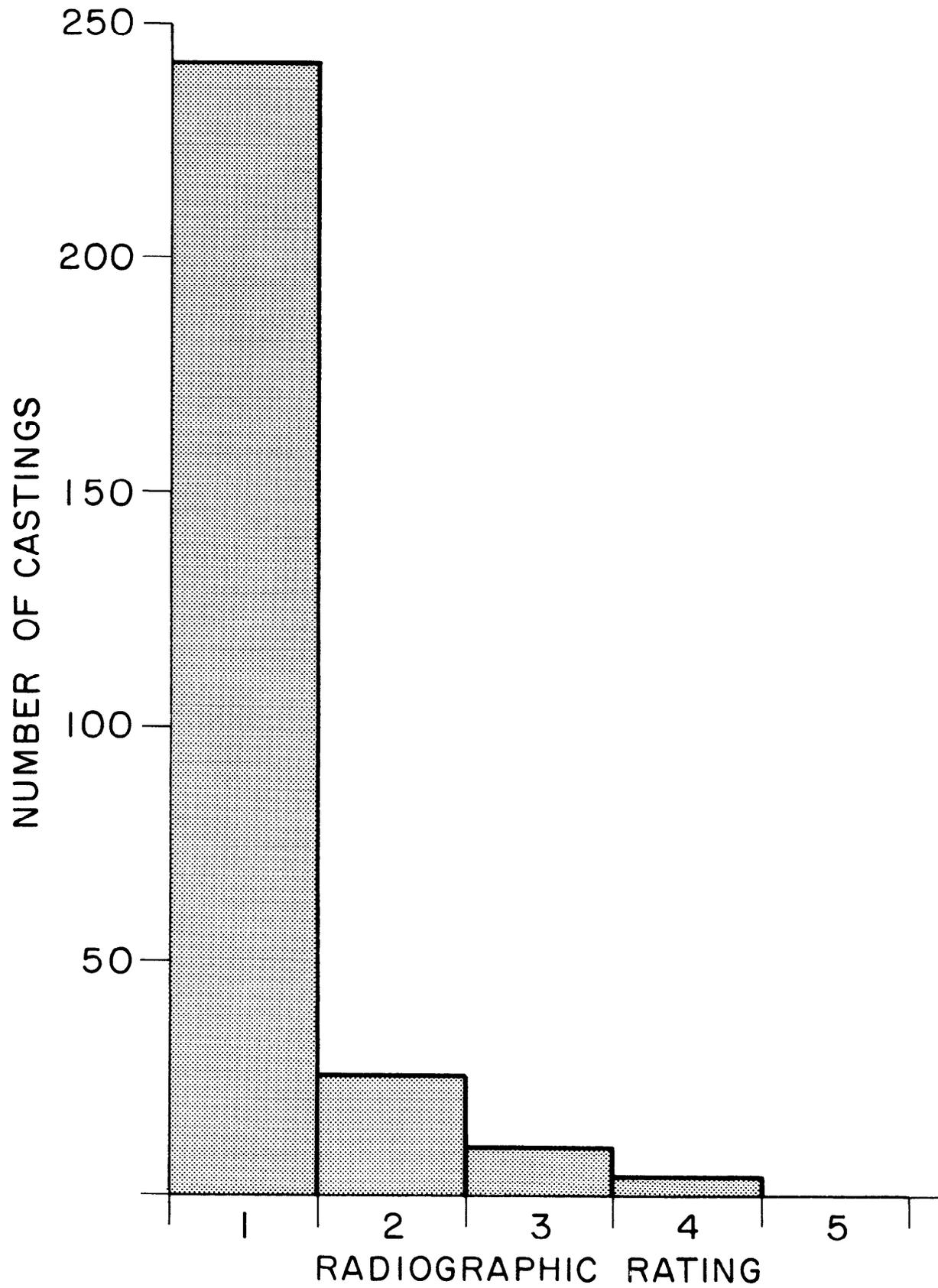
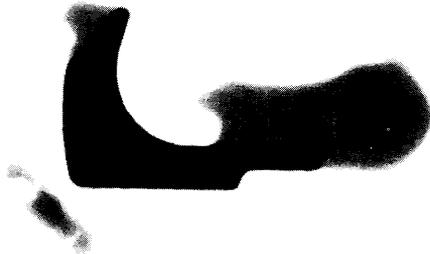
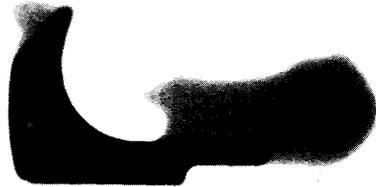


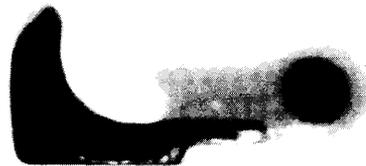
Figure 6: Distribution of radiographic ratings according to a previously adopted scale^[3] in a sample of 290 Thixocastings of 304 stainless steel. Castings were made at 0.5 volume fraction solid into a hardened H-13 steel die.



Rating 1



Rating 2



Rating 3



Rating 4



Rating 5

Figure 7: Examples of revised radiographic rating system.

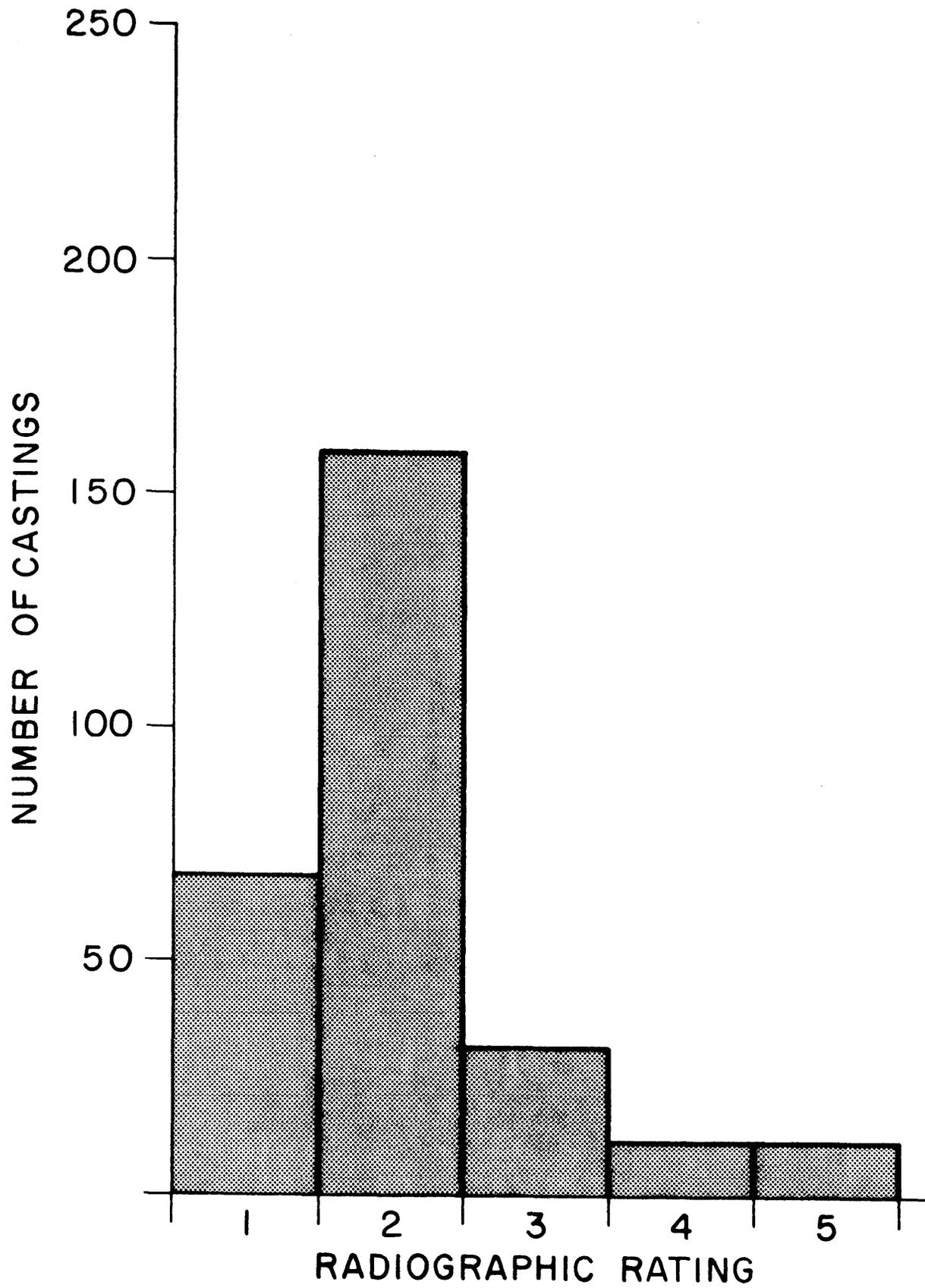


Figure 8: Distribution of radiographic ratings of the 291 Thixocastings of 304 stainless steel from Figure 6 according to the revised scale of Figure 7.

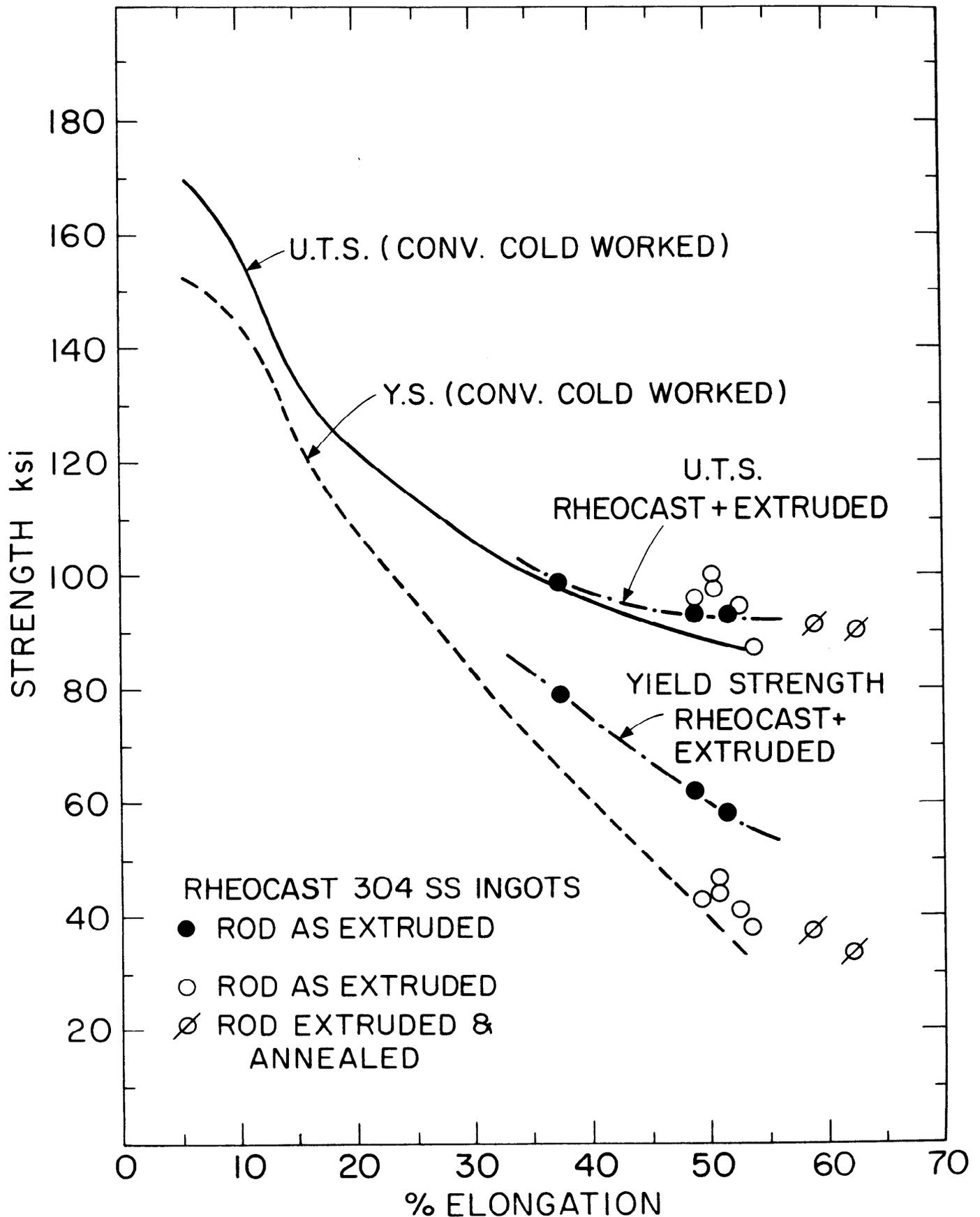


Figure 9: Mechanical properties of hydrostatically extruded Rheocast 304 stainless steel compared with the conventionally cold worked material and hydrostatically extruded wrought 304 stainless steel (open circles).

DISTRIBUTION LIST

No. of Copies	To
1	Office of the Director, Defense Research and Engineering, The Pentagon, Washington, D. C. 20301
12	Commander, Defense Documentation Center, Cameron Station, Building 5, 5010 Duke Street, Alexandria, Virginia 22314
1	Metals and Ceramics Information Center, Battelle Columbus Laboratories, 505 King Avenue, Columbus, Ohio 43201
	Chief of Research and Development, Department of the Army, Washington, D. C. 20310
2	ATTN: Physical and Engineering Sciences Division
	Commander, Army Research Office, P. O. Box 12211, Research Triangle Park, North Carolina 27709
1	ATTN: Information Processing Office
	Commander, U. S. Army Materiel Development and Readiness Command, 5001 Eisenhower Avenue, Alexandria, Virginia 22333
1	ATTN: DRCDE-TC
	Commander, U. S. Army Electronics Command, Fort Monmouth, New Jersey 07703
1	ATTN: DRSEL-GG-DD
1	DRSEL-GG-DM
	Commander, U. S. Army Missile Command, Redstone Arsenal, Alabama 35809
1	ATTN: Technical Library
1	DRSMI-RSM, Mr. E. J. Wheelahan
	Commander, U. S. Army Armament Command, Rock Island, Illinois 61201
2	ATTN: Technical Library
1	DRSAR-SC, Dr. C. M. Hudson
1	DRSAR-PPW-PB, Mr. Francis X. Walter
	Commander, U. S. Army Satellite Communications Agency, Fort Monmouth, New Jersey 07703
1	ATTN: Technical Document Center
	Commander, U. S. Army Tank-Automotive Research and Development Command, Warren, Michigan 48090
2	ATTN: DRDTA, Research Library Branch
	Commander, White Sands Missile Range, New Mexico 88002
1	ATTN: STEWS-WS-VT
	Commander, Aberdeen Proving Ground, Maryland 21005
1	ATTN: STEAP-TL, Bldg. 305

No. of Copies	To
1 1 1	Commander, Frankford Arsenal, Philadelphia, Pennsylvania 19137 ATTN: Library, H1300, Bl. 51-2 SARFA-L300, Mr. J. Corrie
1 1	Commander, Picatinny Arsenal, Dover, New Jersey 07801 ATTN: SARPA-RT-S
4	Commander, Redstone Scientific Information Center, U. S. Army Missile Command, Redstone Arsenal, Alabama 35809 ATTN: DRSMI-RBLD, Document Section
1	Commander, Watervliet Arsenal, Watervliet, New York 12189 ATTN: SARWV-RDT, Technical Information Services Office
1	Commander, U. S. Army Foreign Science and Technology Center, 220 7th Street, N. E., Charlottesville, Virginia 22901 ATTN: DRXST-SD2
1	Director, Eustis Directorate, U. S. Army Air Mobility Research and Development Laboratory, Fort Eustis, Virginia 23604 ATTN: Mr. J. Robinson, SAVDL-EU-SS
1	Librarian, U. S. Army Aviation School Library, Fort Rucker, Alabama 36360 ATTN: Building 5907
1	Naval Research Laboratory, Washington, D. C. 20375 ATTN: Dr. J. M. Krafft - Code 8430
1	Chief of Naval Research, Arlington, Virginia 22217 ATTN: Code 471
2 1 1 1	Air Force Materials Laboratory, Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFML/MXE/E. Morrissey AFML/LC AFML/LLP/D. M. Forney, Jr. AFML/MBC/Mr. Stanley Schulman
1 1	National Aeronautics and Space Administration, Washington, D. C. 20546 ATTN: Mr. B. G. Achhammer Mr. G. C. Deutsch - Code RR-1
1 1	National Aeronautics and Space Administration, Marshall Space Flight Center, Huntsville, Alabama 35812 ATTN: R-P&VE-M, R. J. Schwinghamer S&E-ME-MM, Mr. W. A. Wilson, Building 4720
1	Wyman-Gordon Company, Worcester, Massachusetts 01601 ATTN: Technical Library

No. of Copies	To
5	Defense Advanced Research Projects Agency, 1400 Wilson Boulevard, Arlington, Virginia 22209 ATTN: Dr. E. C. van Reuth
1	National Science Foundation, 1800 G Street, Washington, D. C. 20550 ATTN: Dr. Robert Reynik
5	General Electric Company, Corporate Research and Development, Schenectady, New York 12301 ATTN: Mr. F. X. Gigliotti, Jr.
5	Hitchiner Manufacturing Co., Inc., Elm Street, Milford, New Hampshire 03055 ATTN: Mr. G. D. Chandley
5	Abex Corporation, Research Center, Mahwah, New Jersey 07430 ATTN: H. R. Larson
5	Massachusetts Institute of Technology, Dept. of Metallurgy and Materials Science, Cambridge, Massachusetts 02139 ATTN: Dr. Merton C. Fleming
1	TRW Equipment, TRW Inc., 23555 Euclid Avenue, Cleveland, Ohio 44117 ATTN: Elizabeth Barrett, T/M 3417
1	Deposits & Composites Inc., 1821 Michael Faraday Drive, Reston, Virginia 22090 ATTN: Richard E. Engdahl, President
1	Dr. Maurice Sinnott, University of Michigan, Assoc. Dir. of Engineering, Ann Arbor, Michigan 48104
1	Fred E. Ziter, Adirondack Steel Casting Co., Shaker Road, Watervliet, New York 12189
1	Dr. Raymond J. Bratton, Westinghouse Electric Corporation Research Laboratory, Pittsburgh, Pennsylvania 15235
1	W. M. Spurgeon, Director, Mfg., Quality Control & Home Systems, Program Management Center, Bendix Research Laboratories, Bendix Center, Southfield, Michigan 48075
1	S. T. Wlodek, Director of Stellite R&D, Stellite Division, Cabot Corporation, 1020 West Park Avenue, Kokomo, Indiana 46901
1	Mr. William A. Butler, Contract Administrator, Microwave Associates, Inc., Burlington, Massachusetts 01803
1	Mr. John A. Ulrich, Sr. Vice-President, Chamberlain Manufacturing Corp., Waterloo, Iowa 50705

No. of Copies	To
1	A. V. Illyn, Technical Director, Babcock & Wilcox, Old Savannah Road, Augusta, Georgia 30903
1	Mr. W. J. Welsch (Code 224), Naval Materials Industry Resources Office, N.A.E.C., Building #537, Philadelphia, Pennsylvania 19112
1	Mr. R. E. Cross, Federal Die Casting Co., 2222 Elston Avenue, Chicago, Illinois 60614
1	Captain Ebenezer F. Porter, 2618 S. Lynn Street, Arlington, Virginia 22202
1	Mr. Charles E. Bates, Head, Metallurgy Section, Southern Research Institute, 2000 Ninth Avenue, South, Birmingham, Alabama 35205
1	Mr. R. F. Kirby, Chief, Materials Engineering Dept., Dept. 93-39M, Airesearch Manufacturing Company of Arizona, 402 South 36th Street, P. O. Box 5217, Phoenix, Arizona 85010
1	Dr. Mervin T. Rowley, American Foundry Men's Society, Golf & Wolf Roads, Des Plaines, Illinois 60016
1	William R. Freeman, Jr., Howmet Corporation, Vice President and Technical Director, Technical Center, Gas Turbine Components Group, 699 Benston Road, Whitehall, Michigan 49461
1	Dole A. Marek, General Motors Corporation, Detroit Diesel Allison, 4700 W 10th Street, Indianapolis, Indiana 46206
1	General Dynamics, Convair Aerospace Division, P. O. Box 748, Ft. Worth, Texas 76101
1	ATTN: Mfg. Engineering Technical Library
1	Dr. Robert Mehrabian, Dept. of Metallurgy & Mining Engineering, University of Illinois, Urbana, Illinois 61801
1	Robert McNally, Research Library, Special Metals Corporation, Middle Settlement Road, New Hartford, New York 13413
1	Director, Army Materials and Mechanics Research Center, Watertown, Massachusetts 02172
2	ATTN: DRXMR-PL
1	DRXMR-PR
1	DRXMR-AP
1	DRXMR-CT
1	DRXMR-X
1	DRXMR-ER

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER AMMRC CTR 76-39	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) MACHINE CASTING OF FERROUS ALLOYS		5. TYPE OF REPORT & PERIOD COVERED Interim Report 1 Jan 1976-30 June 1976
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) M. C. Flemings, K. P. Young, R. G. Riek, J. F. Boylan, R. L. Bye		8. CONTRACT OR GRANT NUMBER(s) DAAG46-73-C-0110
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS D/A Project: 2267 AMCMS Code: 4010 Agency Accession:
11. CONTROLLING OFFICE NAME AND ADDRESS Army Materials and Mechanics Research Center Watertown, Massachusetts 02172		12. REPORT DATE November 1976
		13. NUMBER OF PAGES 22
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Die casting Solidification Rheocasting Thixocasting		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This is the fifth interim report describing research conducted at the Massachusetts Institute of Technology as part of a joint university-industry research program on machine casting of ferrous alloys. It covers the period of the thirty-sixth to the forty-second month of this four-year program. The basic system for Thixocasting ferrous alloys is fully and reliably		

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

operational. The Continuous Rheocaster works dependably in production runs in which typically up to 500 pounds of steel is produced at a rate of about 80 pounds per hour. Much longer runs could be produced if desired.

The Thixocast reheating process is completely automated. The two stage heating cycle employed delivers steel charges suitable for Thixocasting with a maximum temperature variation in the charge of $\pm 3^{\circ}\text{C}$. Work has been primarily on 304 and 440C stainless steel.

Emphasis during this period has been on the production of a large amount of Rheocast stainless steel and the initiation of large scale Thixocasting runs to test actual die life. More than 3000 pounds of Rheocast stainless steel have been produced to date. Five hundred stainless steel Thixocastings have been produced in a hardened H-13 steel die with die life superior to results reported for H-13 dies used for liquid cast steel. The castings produced showed consistently good internal soundness. This Thixocasting work has been primarily on 304 stainless steel; additional work is planned on 440C.

Mechanical property evaluation of Thixocast 304 stainless steel indicates it possesses strength superior to the conventionally cast alloy with somewhat less ductility.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)