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STRUCTURAL DYNAMIC PROPERTIES OF TACTICAL MISSILE JOINTS-PHASE 3

George Lasker, et al

General Dynamics

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ABSTRACT The results of a third and final phase in a general study of the structural dynamic properties of tactical missile airframe joints are presented. The overall objectives of the study were to provide a better understanding of mechanical joint effects on missile dynamic response and to improve methods for predicting and representing their characteristics in system simulation and response studies.

Finite element structural analysis techniques started in Phase 1 are shown to be capable of providing reliable estimates of joint compliance in complex actual missile structures. A technique for extracting joint compliance values from missile model test data started in Phase 1 is refined to improve convergence and user convenience. A user's manual for the joint compliance extraction digital computer code is included as an appendix to the report. An exploratory study of missile joint self-induced vibration is presented together with an initial evaluation of some promising methods for suppression and control. The report concludes with a proposed rating system for joints intended to integrate the many design considerations such as strength, weight, producibility, and maintainability, in addition to structural dynamic considerations, into overall system requirements.

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Final Report

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By

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for the

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FOREWORD

This study has been conducted by the Pomona Division of General Dynamics Corporation for the Naval Air Systems Command under Contract N00019-72-C-0507.

The principal investigator for the study has been Mr. John G. Maloney. Dr. George Lasker has performed the finite element analysis presented in Section 3. The joint compliance extraction technique and computer code work was performed by Mr. M. T. Shelton. The direct technical supervisor has been Mr. David A. Underhill, Structural Dynamics Section Head.

Mr. George P. Maggos has been the Naval Air Systems Command technical monitor.

The authors wish to acknowledge the contributions of Messrs David O. Rife, James B. Samonte and Donald G. VandeGriff for providing assistance in various portions of the study.

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Section 1.0

SUMMARY

Results of a third and final phase in a general study of the structural dynamic properties of tactical missile joints are presented. This effort, undertaken by the Pomona Division of General Dynamics for the Naval Air Systems Command, has been intended to provide a better understanding of mechanical joint effects on missile dynamic response and improved methods for predicting and representing their characteristics in system simulation and response studies.

Highlights of the results obtained in the first two study phases (References 1 and 2) are reviewed, covering an industry survey, classification scheme, and parametric evaluation of joint compliance effects. Finite element structural analysis techniques started in Phase 1 and completed in this final study phase are shown to be capable of providing reliable estimates of joint compliance in complex actual missile structures.

Experimental methods are reviewed and a joint compliance extraction code designed to solve for joint properties from modal test data is described in some detail. This method, also started in the Phase 1 study, has been refined during the present phase to improve convergence and user convenience. A user's manual for this code is included as an Appendix.

An exploratory study of missile joint self-induced vibration is presented together with an initial evaluation of some promising methods for suppression and control. The report concludes with a discussion of a proposed rating system for tactical missile joints with the objective of offering the designer some perspective on integrating the many considerations such as strength, producibility, and maintainability, in addition to compliance, into overall system requirements.

Section 2.0

INTRODUCTION

The structural dynamic properties of tactical missile joints can play an extraordinarily important role in weapon system structural response characteristics. This report deals with the third and final phase of an exploratory study of the primary structural dynamic characteristics of missile mechanical joints and the analytical and experimental tools identified and developed for predicting their behavior.

The most conspicuous attribute of the average tactical missile joint is flexural compliance under applied bending moment. The first phase study was largely devoted to an examination of this characteristic starting with a literature search and an industry survey to sample others' experience followed by a parametric study of joint compliance effects, elastic coupling, the significance of stiffness discontinuities and the importance of considering actual load paths through joint elements. Based on the industry survey, it was concluded that investigators generally represent missile joints in analytical modeling by flexural springs selected by trial and error to match measured response characteristics. Joint compliance effects were typically found to account for more than 30 percent of the total elastic deformation of a missile in its primary bending modes.

A joint classification scheme proposed in a NASA study reported in Reference 3 suggested factors of ten increase in compliance progressing from each level - Excellent, Good, Moderate, and Loose. Thus, a "Moderate" joint would be 10 times as compliant as a "Good" joint and 100 times as compliant as an "Excellent" joint. Viewed in terms of stiffness loss in a typical missile airframe, a "Good" joint represents a local reduction in section properties of approximately 60 percent over a span of one half body diameter. A "Moderate" joint would correspondingly reduce local section properties 95 percent. Such gross structural inefficiencies are attributed to poor distribution of load paths through joint interfaces. Figure 2-1 shows the powerful influence of joint compliance on the first mode frequency of a missile idealized as a uniform beam.

From the standpoint of the structural dynamic analyst charged with the responsibility for developing adequate math models in developmental studies, methods for accurately estimating joint compliance are of paramount importance. The advent of finite element structural analysis techniques has offered some very promising tools for realistically representing detailed elastic behavior with joint elements. Finite element modeling of idealized joints was started in an exploratory effort

during Phase 1 and - based on encouraging results - considerably expanded during Phase 2 to encompass an actual missile joint design for which accurate compliance test data were available for correlation purposes. This effort has been continued during the present and final study phase with emphasis on computational economy and is presented in Section 3.0.

Experimental methods when test hardware is available offer another important approach to the determination of missile joint structural dynamic properties. An ideal test configuration for evaluating joint properties is considered to be a simple uniform structure on a free-free suspension to avoid external constraints and with the subject joint located at mid-span. The joint bending compliance then has a dominant effect on odd numbered modes (1, 3, . . .) and the joint shear compliance is exposed by even numbered modes (2, 4, . . .). Simple tests were performed during Phase 1 on tubular models to illustrate the basic test approach and to explore the effects of load path discontinuities. Actual missile joint hardware was employed in a series of four similar tests during the Phase 2 study, with data on two joint configurations being provided in a colloborative effort by Naval Weapon Center, China Lake personnel. One joint test of particular interest involved a shear joint with 18 radial screws. Joint compliance was evaluated parametrically as a function of number of fasteners, producing the surprisingly consistent and well ordered results shown in Figure 2-2. An exploratory generalization of this shear joint behavior is shown in Figure 2-3 with the cautionary comment that the derived compliance expression must be viewed with some skepticism since it considers only joint diameter and number of fasteners. Test data for two unrelated specimens are compared with the empirical compliance expression in the figure, however, and show better agreement than might be expected. The 8 fastener data point is taken from the 8-inch diameter shear joint tested at the Naval Weapons Center, China Lake and reported in the Phase 2 study. The 3 and 6 fastener data points are taken from the segmented tube test data in Phase 1 extrapolated to a "fastener" arc length of 2 degrees in order to correspond to the 1/4 inch bolts used with the 13.5 inch diameter data source.

The opportunity to test single joints in the "ideal" configuration is the exception rather than the rule, however, and more generally dynamic testing is performed on total airframes with many joints. The traditional approach consists of hand tuning compliance values to produce matching results between the mathematical model and measured mode shapes and frequencies. Since this is a laborious, time consuming, and often frustrating task, an automated and systematic approach is desirable. To these ends, an exploratory effort based on the optimization method of steepest descent was developed in Phase 1 of the study. This method of extracting joint compliance values from a set of measured missile elastic mode frequencies and shapes was shown to be feasible. However,

various limitations in the implemented method precluded full development. A more general approach developed by Hall, Calkin and Sholar, Reference 4, appeared in the literature and in Phase 2 their method was applied to the problem of extracting joint compliances. The result is a digital computer code. In Phase 3 refinements were added to the joint compliance extraction technique code to increase its utility and a user's manual was prepared for the code. Section 4 and the Appendix of the present report present the Phase 3 efforts on the joint compliance extraction technique.

Another important characteristic of missile airframe joints is that of self-induced vibration. This behavior is most usually associated with joint designs having inherently low interface preloads, and its presence can create unnecessarily severe environments in laboratory testing as well as in both captive and free-flight. Section 5 of this report describes an investigation of this phenomena covering both full scale and model exploratory testing.

The final section of this report, Section 6, illustrates a method of integrating the structural dynamic properties of joints with other important mechanical attributes that airframe joints must possess to meet overall system requirements.

FIGURE 2-1

FREQUENCY RATIO VS. JOINT STIFFNESS RATIO
UNIFORM BEAM - MIDSPAN JOINT

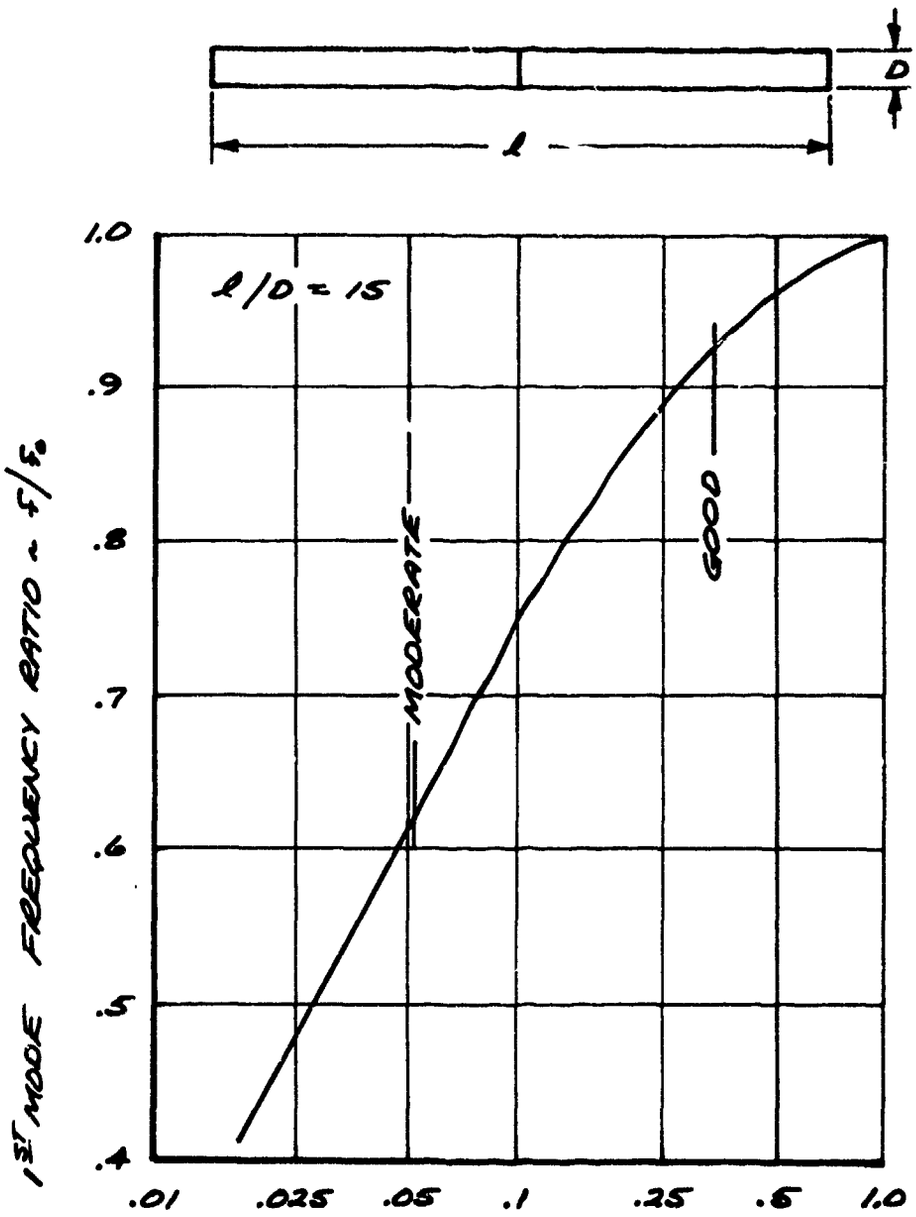


FIGURE 2-2

13.5 INCH DIAMETER SHEAR BOLT JOINT
FLEXURAL COMPLIANCE VS. NUMBER OF FASTENERS

$C_\theta = 12.71 (10)^{-8} / n^{1.404}$ RAD./IN-LB.

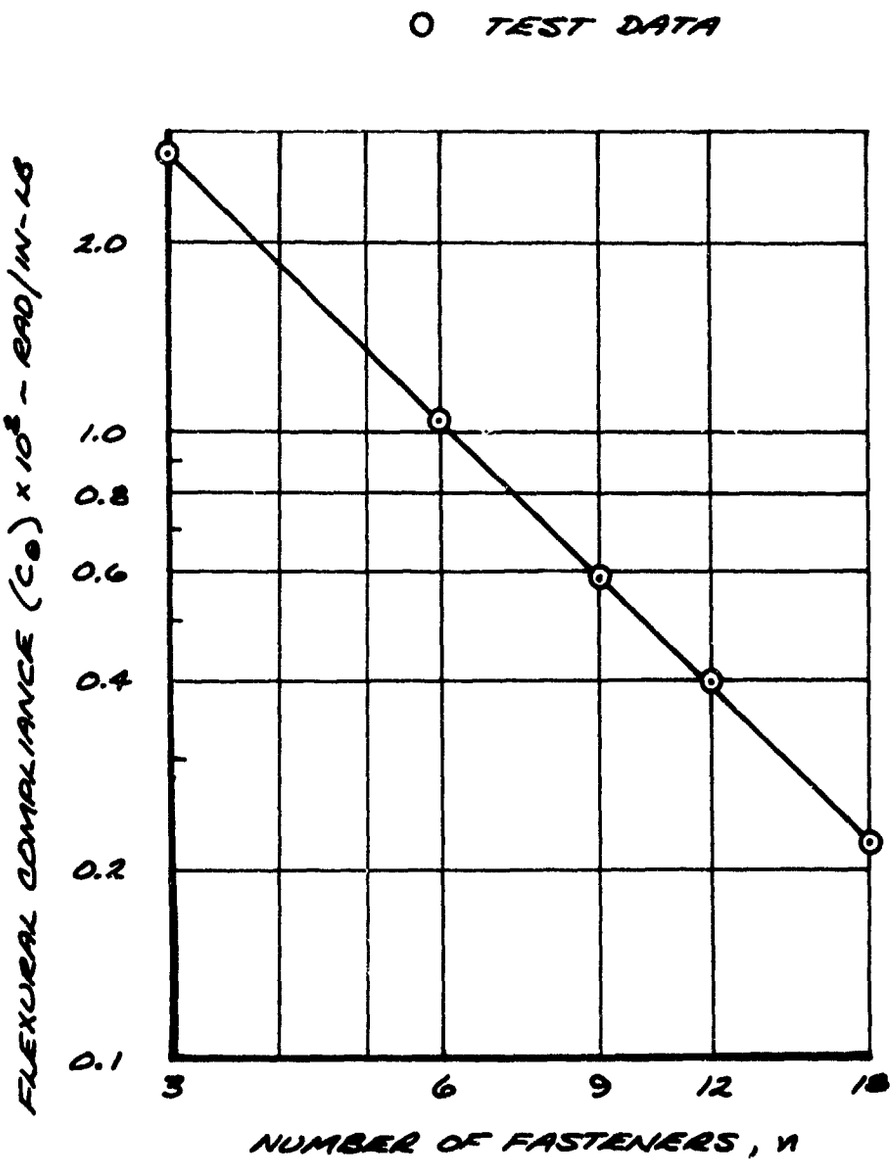


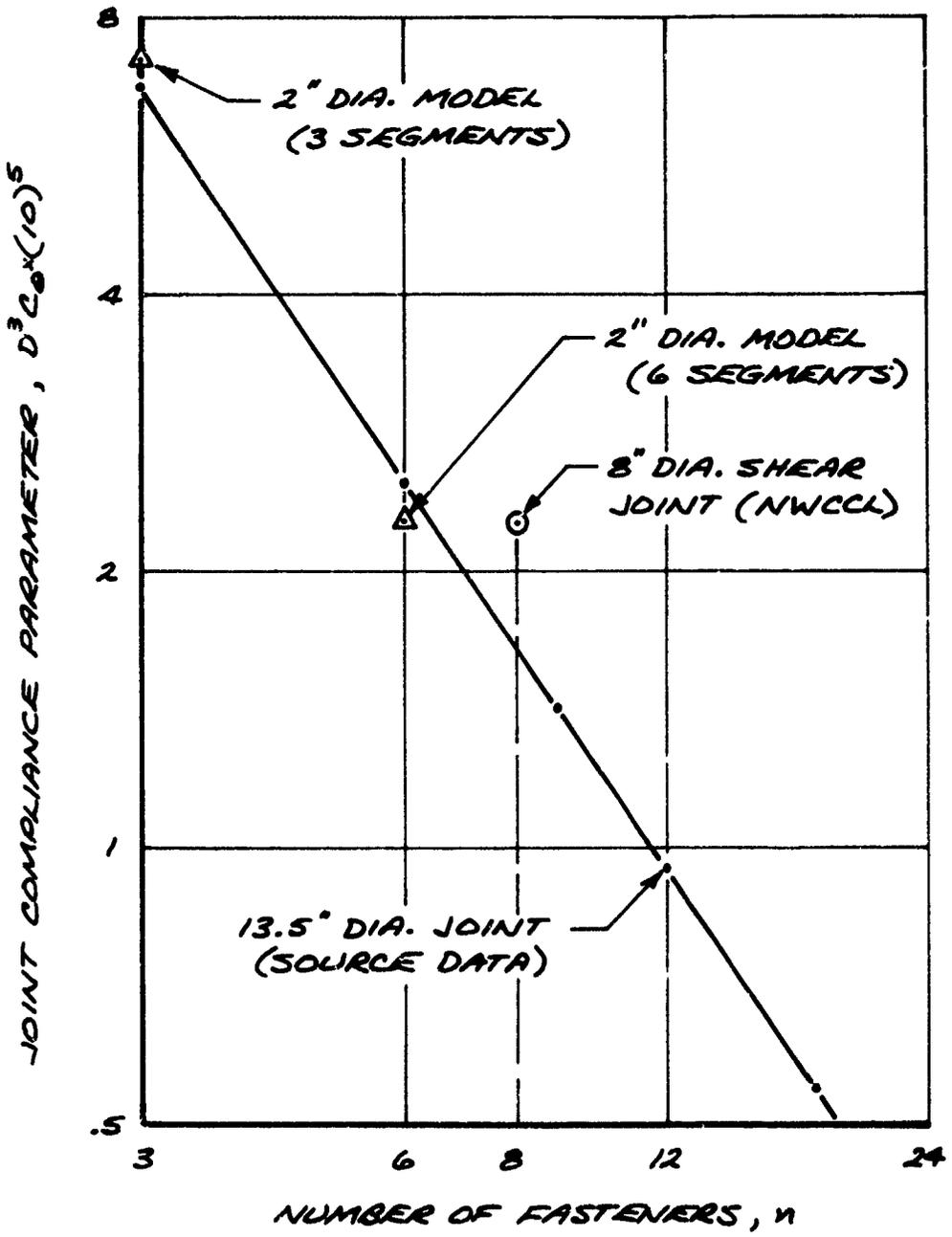
FIGURE 2-3

GENERALIZED SHEAR JOINT COMPLIANCE VERSUS NUMBER OF FASTENERS

$$D^3 C_\bullet = 31.3\,(10)^{-5}/n^{1.404}$$

WHERE D = JOINT DIA. IN INCHES

$C_\bullet$ = COMPLIANCE, RAD/IN-LB.



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Section 3.0

JOINT COMPLIANCE ANALYSIS

Finite element structural analysis methods have been shown in earlier study phases to offer considerable promise as means of predicting tactical missile mechanical joint properties. In the Phase 2 portion of the investigation a finite element type of analysis was performed on an eighteen fastener shear joint. The analysis made use of the NASTRAN computer program. The math model used described the structure on each side of the joint by means of a set of conical shell elements. Bolts were then described by discrete springs. Each spring constrains two corresponding points on each side of the joint. The solution process is based on a Fourier series expansion about the circumference. Thus forces and displacements are determined by summing a set of harmonic components. The compliance associated with various harmonics can be zero. The zero compliance harmonics are well defined for uniform bolt patterns. Thus for a joint with n bolts, the compliance associated with all harmonics are zero except for harmonics 0, 1, n-1, n + 1, 2 n-1, 2 n + 1, ...

In Phase 2 the problem was formulated and computations were performed entirely on NASTRAN. The cost per computer run was quite high even though only twelve harmonics were used. Two effects played a role in the high cost. If the structure was geometrically axisymmetric the stiffness matrix for each harmonic would be uncoupled from all others, however, due to the bolts the structure is asymmetric. Thus a coupling between harmonics results with a corresponding high computer solution time. The problem is aggravated to a considerable degree by the fact that the zero harmonics cannot be excluded from the solution process. Thus to solve this problem using say 50 harmonics is almost prohibitive.

On examining this problem it became apparent that it was not inherently expensive but rather due to limitations within the NASTRAN program. It also became apparent that a small efficient computer program could be written which used certain NASTRAN outputs. This was done as part of the Phase 3 finite element analysis effort.

The new computer program uses NASTRAN generated stiffness coefficients associated with each harmonic and the structure on each side of the joint.

3.1 PROBLEM FORMULATION

Consider two axisymmetric shells with a common axis of symmetry which are attached together with respect to a discrete set of points around the circumference as shown in Figure 3-1.

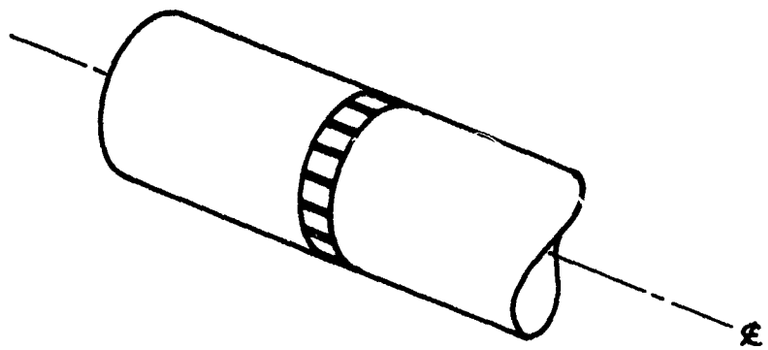


Figure 3-1. Sketch Showing Two Axisymmetric Shells Attached at a Discrete Set of Points

We require the attachments to be positioned so that they are symmetric with respect to a plane of symmetry which includes the missile longitudinal axis. The attachment forces do not act at points but rather over a small area defined by the thickness of the shell and an arc length defined by the enclosed angle ϵ as shown in Figure 3-2.

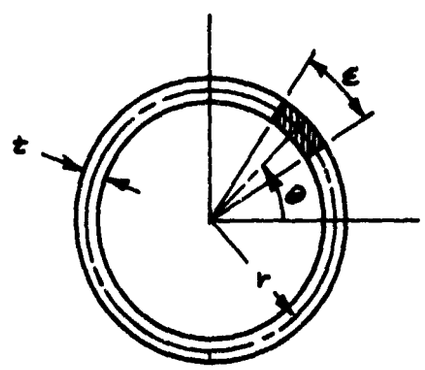


Figure 3-2. Area Over Which Bolt Acts as Defined in Math Model

Also the distribution of the load over the area is taken as uniform. Let P be the resultant bolt force acting on the area. The stress $\sigma(\theta)$ can then be expanded into a cosine series in the form

$$\sigma(\theta) = \frac{1}{t} \sum a_n \cos n\theta \tag{3.1}$$

On doing so we obtain

$$\sigma(\theta) = \frac{2p}{t\epsilon} \sum_{n=1}^{\infty} \frac{\sin(n\epsilon/2)}{n} \cos(n\theta) \tag{3.2}$$

or

$$a_n = \frac{2p}{n\epsilon} \sin(n\epsilon/2) \tag{3.3}$$

The use of the cosine series imposes the requirement that the horizontal plane be a plane of symmetry The quantity $t\sigma(\theta)$ has units of load per unit arc length. The quantity $f(\theta) = t\sigma(\theta)$ can be expressed in the form

$$f(\theta) = f_1 \cos(\theta) + f_2 \cos(2\theta) + f_3 \cos(3\theta) + \cdots \tag{3.4}$$

where

$$f_n = \frac{2p}{n\epsilon} \sin(n\epsilon/2) \tag{3.5}$$

It can be interpreted as a generalized force associated with the n th harmonic. Let f_{ni} be the generalized force associated with the n th harmonic and the i th bolt. Let the joint have b bolts and let p_i be the force resultant for the i th bolt acting at θ_i. Then the harmonic generalized forces f_n associated with the set of bolts used on the joint are

$$f_n = \sum_{i=1}^{b} f_{ni} = \sum_{i=1}^{b} \frac{2p_i}{n\epsilon} \sin(n\epsilon/2) \cos(n\theta_i) \tag{3.6}$$

Let us define a matrix with elements a_{ij}

$$a_{ij} = \frac{2}{i\epsilon} \sin(i\epsilon/2) \cos(n\theta_j) \tag{3.7}$$

Let f_i and p_j respectively be elements of column vectors $\{f_i\}$ and $\{p_j\}$. Then from (3.6) and (3.7) one can see that the following relationship holds

$$\{f_i\} = [a_{ij}]\{p_j\} \tag{3.8}$$

Let $[s_{ij}]$ be a diagonal matrix where element s_{ij} is a spring stiffness constant associated with the i th bolt and let $\{v_j\}$ be a column matrix associated with bolt elongations. Then the following relationship holds.

$$\{p_j\} = [s_{jk}]\{v_k\} \tag{3.9}$$

If we could assign a point on the circumference to each bolt then bolt elongation could be expressed by a set of generalized displacements u_n as follows:

$$v_i = \sum_{n=1}^{\infty} u_n \cos(n\theta_i) \tag{3.10}$$

Since the bolt load is associated with an area as shown in Figure 3-2 we cannot associate the bolt displacement with only one point. We will give an indirect definition which will implicitly contain an averaging over this area. Let the problem be limited to m harmonics and let $[c_{ij}]$ be an m by b matrix which relates bolt elongations $\{v_i\}$ to generalized harmonic displacements $\{u_j\}$ as follows

$$\{v_i\} = [c_{ij}]\{u_j\} \tag{3.11}$$

Then virtual bolt elongations $\{\delta v_i\}$ and virtual generalized displacements $\{\delta u_j\}$ are related by

$$\{\delta v_i\} = [c_{ij}]\{\delta u_j\} \tag{3.12}$$

We require the following to hold

$$\{p_i\}^T\{\delta v_i\} = \{f_j\}^T\{\delta u_j\} \tag{3.13}$$

That is, we require the virtual work associated with virtual elongation $\{\delta v_i\}$ to be equal to the virtual work associated with the corresponding generalized variables. On substituting from (3.8) and (3.12) into (3.13) we obtain

$$\{p_i\}^T [c_{ij}] \{\delta u_j\} = \{p_i\}^T [a_{ij}]^T \{\delta u_j\} \tag{3.14}$$

Equation (3.14) can hold for all virtual displacements $\{\delta u_j\}$ and all loads $\{p_i\}$ if and only if

$$[c_{ij}] = [a_{ij}]^T \tag{3.15}$$

Therefore from (3.7) and (3.15) it follows that

$$c_{ij} = \frac{2}{j\epsilon} \sin\left(\frac{j\epsilon}{2}\right) \cos(n\theta_i) \tag{3.16}$$

From (3.8), (3.9), (3.11), and (3.15) it follows that

$$\begin{aligned} \{f_i\} &= [a_{ij}] \{p_j\} \\ &= [a_{ij}] [s_{jk}] \{v_k\} \\ &= [a_{ij}] [s_{jk}] [a_{k\ell}]^T \{u_\ell\} \end{aligned} \tag{3.17}$$

Let

$$[\bar{s}_{i\ell}] = [a_{ij}] [s_{jk}] [a_{k\ell}]^T \tag{3.18}$$

Thus $[\bar{s}_{i\ell}]$ is a stiffness matrix which describes the stiffness of the set of joint bolts with respect to the generalized (harmonic) variables $\{f_i\}$ and $\{u_\ell\}$. Then (3.17) has the form

$$\{f_i\} = [\bar{s}_{ij}] \{u_j\} \tag{3.19}$$

We will now define the variables associated with the axisymmetric structures on each side of the joint. These structures will be interpreted as two free structures whose relative displacements are constrained by the bolt attachments. We will assume that there is no relative radial or circumferential motion across the joint. Since the two structures are unconstrained except by the joint it follows that the zero and first

harmonics of longitudinal relative displacements are respectively associated with relative longitudinal translation and pitch rigid body motions. The higher harmonics on the other hand are associated with shell deformation.

Using NASTRAN we can compute the displacement u_n associated with each higher harmonic load f_n acting on the joint. We can then compute two sets of stiffness coefficients associated with each of the structures as follows:

$$K_{ii}' = \frac{f_i'}{u_i'}$$
$$K_{ii}'' = \frac{f_i''}{u_i''} \tag{3.20}$$

where the single and double primes are used to distinguish the two structures. From the above discussion it follows that

$$K_{11}' = K_{11}'' = 0 \tag{3.21}$$

The joint displacements can be described by relative generalized (harmonic) displacement parameters $\{u_i\}$ described earlier. They are related to the harmonic displacement parameters for the two structures as follows:

$$u_i = u_i' - u_i'' \tag{3.22}$$

Then from (3.17) and (3.19) it follows that

$$u_i = \frac{f_i'}{K_{ii}'} - \frac{f_i''}{K_{ii}''} \tag{3.23}$$

This is a consequence of the orthogonality of the set of cosine functions. Similarly joint equilibrium and harmonic function orthogonality requires

$$f_i' = - f_i'' = f_i \tag{3.24}$$

where f_i indicates that the prime will not be required below. Substituting (3.24) into (3.23) and simplifying we obtain

$$u_i = \left(\frac{K_{ii}' + K_{ii}''}{K_{ii}' K_{ii}''} \right) f_i \tag{3.25}$$

or

$$f_i = K_{ii} u_i \tag{3.26}$$

where

$$K_{ii} = \frac{K_{ii}' K_{ii}''}{K_{ii}' + K_{ii}''} \tag{3.27}$$

The parameters K_{ii} describe the effective stiffness associated with the set of harmonics for the axisymmetric structure on both sides of the joint. Let $[K_{ij}]$ be a diagonal matrix with diagonal elements K_{ii}. Then (3.26) can be expressed in the following matrix form

$$\{f_i\} = [K_{ij}] \{u_j\} \tag{3.28}$$

Note that

$$K_{11} = 0 \tag{3.29}$$

Partition equation (3.19) and (3.28) as follows

$$\begin{Bmatrix} f_1 \\ \{f_i\}_2 \end{Bmatrix} = \begin{bmatrix} \bar{S}_{11} & [\bar{S}_{ij}]_{12} \\ [\bar{S}_{ij}]_{21} & [\bar{S}_{ij}]_{22} \end{bmatrix} \begin{Bmatrix} u_1 \\ \{u_j\}_2 \end{Bmatrix} \tag{3.30}$$

$$\begin{Bmatrix} f_1 \\ \{f_i\}_2 \end{Bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & [K_{ij}]_{22} \end{bmatrix} \begin{Bmatrix} u_1 \\ \{u_j\}_2 \end{Bmatrix} \tag{3.31}$$

From (3.30) and (3.31) we obtain

$$f_1 = \bar{S}_{11} u_1 + [\bar{S}_{ij}]_{12} \{u_j\}_2 \tag{3.32}$$

$$\{f_i\}_2 = [\bar{S}_{ij}]_{21} u_1 + [\bar{S}_{ij}]_{22} \{u_j\}_2 \tag{3.33}$$

$$\{f_i\}_2 = [K_{ij}]_{22} \{u_j\}_2 \tag{3.34}$$

From (3.33) and (3.34) we obtain

$$\{u_j\}_2 = \left[[K_{ij}]_{22} - [\bar{S}_{ij}]_{22} \right]^{-1} [\bar{S}_{jk}]_{21} u_1 \tag{3.35}$$

On substituting (3.35) into (3.32) we obtain

$$f_1 = \left(\bar{S}_{11} + [\bar{S}_{ij}]_{12} \left[[K_{jk}]_{22} - [\bar{S}_{jk}]_{22} \right]^{-1} [\bar{S}_{k1}]_{21} \right) u_1 \tag{3.36}$$

Let A_{11} equal the quantity in brackets. Then (3.36) has the form

$$f_1 = A_{11} u_1 \tag{3.37}$$

The parameter u_1 is a measure of the maximum relative displacement around the circumference. We wish to relate the joint stiffness to more common parameters M and ϕ which correspond to joint bending moment and joint relative rotation. Now u_1 and ϕ are related by

$$u_1 = r\phi \tag{3.38}$$

where r is defined in Figure 3-2. We will define the relationship between M and f_1 by requiring that the following hold for all virtual displacements δu_1 and $\delta\phi$.

$$M\delta\phi = f_1 \delta u_1 \tag{3.39}$$

On substituting (3.38) into (3.39) we obtain

$$M\delta\phi = f r \delta\phi \tag{3.40}$$

For the above to hold for all virtual changes it follows that

$$M = rf \tag{3.41}$$

On substituting (3.38) into (3.37) and the resultant into (3.41) we obtain

$$M = r^2 A_{11} \phi \tag{3.42}$$

The equivalent joint stiffness designated by H is related by

$$H = r^2 \left(\bar{S}_{11} + [\bar{S}_{ij}]_{12} \left[[K_{jk}]_{22} - [\bar{S}_{jk}]_{22} \right]^{-1} [\bar{S}_{kl}]_{21} \right) \tag{3.43}$$

3.2 TEST CASE AND RESULTS

A computer program which can compute the effective joint stiffness as described above was written. The structural configuration used in the Phase 2 study was used in this study since comparative test data were available. Figure 3-3 describes the joint and Figure 3-4 describes the finite element model of shell elements used in all the NASTRAN analyses.

The NASTRAN computer program was used to compute the longitudinal harmonic stiffness coefficient designated by K'_{ii} and K''_{ii} for the first 108 harmonics. These stiffness coefficients are given in Table 3-1 and a log-log plot of the stiffness coefficient versus harmonic number is given in Figure 3-5.

As can be seen from Figure 3-5 the value of stiffness appears to approach a straight line for higher values of harmonic number. A straight line on a log-log plot implies the following continuous function relationship

$$\frac{K}{K_1} = \left(\frac{n}{n_1}\right)^{\alpha} \tag{3.44}$$

where K is the dependent stiffness variable, n is the independent harmonic number variable, (K_1, n_1) is a point on the line and α is a coefficient related by

$$\alpha = \frac{LOG\left(\frac{K_2}{K_1}\right)}{LOG\left(\frac{n_2}{n_1}\right)} \tag{3.45}$$

where (K_2, n_2) is a point on the line. For the two lines in Figure 3-5 associated with the two structures connected by the joint, the data used to compute higher harmonic stiffness coefficients are given in Table 3-2.

Table 3-2

Data Used in Equation (3.44) to Compute Stiffness Coefficients for Harmonics Greater than 108

	Structure 1	Structure 2
K_1	1.57×10^7	4.35×10^7
K_2	3.32×10^8	9.90×10^8
n_1	10	10
n_2	100	100

As pointed out earlier many harmonics do not influence the computation. Table 3-3 shows the harmonics which influence the computations as a function of number of fasteners.

Each bolt has an effective arc length over which it acts. As noted earlier this arc length is defined by the enclosed angle ϵ. Let us define the quantity R as the ratio of ϵ over the angle subtended by the bolt. The R can be interpreted as the effective number of bolt diameters over which the bolt load distributes at the joint.

The larger the value of R the higher the joint stiffness will be. To establish correct values of R computed values of stiffness were compared to measured results obtained in the Phase 2 study. Table 3-4 summarizes the Phase 2 measured values of stiffness.

Table 3-4

Phase 2 Measured Values of Stiffness for Various Numbers of Fasteners ($\times 10^8$ Inch Pounds per Radian)

Number of Fasteners	Stiffness
3	0.358
6	0.971
9	1.680
12	2.575 (interpolated)
18	4.440

Table 3-5 gives computed values of joint stiffness for the three fastener joint, for various values of R and for different values of the highest harmonic used in the calculations. The value of R equal to 6.24 gives results which are almost equal to the measured values. Table 3-6 shows results for 3, 6, 9 and 18 fastener cases using R equal to 6.24. Although the results match the experimental values for the three fastener case, they are quite in error for the 18 fastener case. The compliances of the 18 fastener case for various values of R are given in Table 3-7. As can be seen a value of R close to 1.5 is required if the 18 fastener case is to match measured results. Using a linear interpolation between the compliance values for R equal to 1.5 and 2.0 we conclude that a value of R equal to 1.544 will give a value very close to the measured compliance. Table 3-8 gives results for R equal to 1.544. Since R equal to 6.24 gives correct values for the 3 fastener case and R equal to 1.544 gives correct values for the 18 fastener case, we used a linear interpolation to establish values of R for the 6, 9 and 12 fastener case. Computed joint stiffness for these cases are given in Table 3-9. Figure 3-6 gives curves of stiffness versus number of fasteners of the measured results and of the computed results for R equal to 1.544 and 6.24.

As can be seen from the results described above there does not appear to be a simple way of describing bolt shell interaction. For the joint in question one shell surface overlaps the other and the bolt load acts on the two contacting surfaces. The above results imply that the fewer the bolts the more compliant the joint but the larger the effective contact area between the shells becomes. The results suggest that a more detailed analytical description of the bolt area is required.

Figure 3-7 shows the curve of joint stiffness versus R for the three fastener case. A dashed straight line referred to as the "reference line" is also shown in this figure. Before continuing our discussion of this curve note Figure 3-8 which shows curves of stiffness versus highest harmonic used in the computation for various values of R. In essence these curves show the way in which the cosine series converges. Note that the cosine series converges slower for smaller values of R and that all curves are monotonically decreasing. Now re-examine Figure 3-7. The separation of the curve for low values of R can partly be explained by the slow convergence, i.e., the values shown for the lower values of R are somewhat separated from the values at the point of convergence. The separation from the reference line associated with higher values of R can be explained in a different way. The assumption was made in the derivation that the load distribution along the arc length associated with the bolt load is uniform. This does not introduce very much error for small R however for large R the error is significant.

3.3 CONCLUSIONS

The analysis described here was motivated by the fact that comparable analyses performed using the NASTRAN computer program would have been prohibitive. A joint stiffness analysis performed entirely on NASTRAN during the Phase 2 study cost approximately $300.00 per run for a case which used 12 harmonics. In the present analysis the determination of K' and K" were made once for 109 harmonics using NASTRAN at a cost of $2000.00 and all subsequent runs cost from $0.10 to $0.30. The relatively high cost in generating the K's motivated use of formulas (3.44) for generating higher K values.

One of the problems with using NASTRAN to solve the complete problem is that one would have to use all the harmonics up to the highest one used. One could not exclude harmonics. Thus a run using the present method which used up to harmonic number 400 and costing $0.30 would have cost in excess of $5000.00 if done directly on NASTRAN. In the present study over 100 runs were made at a modest cost.

An unexpected problem was the one associated with selecting an appropriate bolt load distribution parameter (R). The effective load path area for each fastener in the shear bolt joint analyzed appears to decrease as the number of fasteners increases. It should be noted, however, that joint compliance estimates within 10 to 20 percent will in most cases be more than adequate for missile modal analysis purposes. Accuracy in compliance estimates is more important for compliant joints which have a greater influence on airframe modal characteristics than for stiff joints which have little effect on airframe response characteristics.

A useful effort which was not attempted in this study would be to develop a simple expression for estimating K_1, n_1, and α used in equation (3.44). Such an expression would allow the determination of joint compliance for shells of revolution.

TABLE 3-1 NASTRAN Computed Stiffness Coefficients for the Structure on Each Side of the Joint for 108 Harmonics (amts x 10^8 pounds per inch)

	Structure 1	Structure 2		Structure 1	Structure 2		Structure 1	Structure 2
1	0.04291	0.06535	37	0.95935	2.66935	73	2.12083	6.30799
2	0.04239	0.08109	38	0.98724	2.75904	74	2.15987	6.42760
3	0.04219	0.11913	39	1.01513	2.84877	75	2.19932	6.54837
4	0.04415	0.06769	40	1.04307	2.93862	76	2.23918	6.67031
5	0.05090	0.21266	41	1.07109	3.02867	77	2.27945	6.79342
6	0.06247	0.24588	42	1.09974	3.11901	78	2.32014	6.91770
7	0.07684	0.48946	43	1.12753	3.20969	79	2.36125	7.04316
8	0.08313	0.30330	44	1.15600	3.30079	80	2.40277	7.16979
9	0.11140	0.33731	45	1.18467	3.39238	81	2.44471	7.29760
10	0.13189	0.37756	46	1.21356	3.48451	82	2.48706	7.42659
11	0.15477	0.42459	47	1.24271	3.57724	83	2.52984	7.55677
12	0.18000	0.47815	48	1.27211	3.67062	84	2.57303	7.68813
13	0.20748	0.53858	49	1.30180	3.76470	85	2.61664	7.82067
14	0.23698	0.60538	50	1.33178	3.85953	86	2.66068	7.95439
15	0.26821	0.67771	51	1.36207	3.95515	87	2.70513	8.08928
16	0.33244	0.75520	52	1.39268	4.05158	88	2.75000	8.22535
17	0.33442	0.83705	53	1.42362	4.14888	89	2.79530	8.36258
18	0.36869	0.92249	54	1.45490	4.24706	90	2.84102	8.50097
19	0.40330	1.01082	55	1.48653	4.34616	91	2.88716	8.64049
20	0.43800	1.10136	56	1.51851	4.44621	92	2.93373	8.78115
21	0.47251	1.19358	57	1.55085	4.54722	93	2.98072	8.92287
22	0.50669	1.28663	58	1.58356	4.64922	94	3.02810	9.06563
23	0.54040	1.38028	59	1.61664	4.75223	95	3.07597	9.20931
24	0.57356	1.47360	60	1.65010	4.85627	96	3.12423	9.35370
25	0.60612	1.37804	61	1.68394	4.96135	97	3.17292	9.49853
26	0.63806	1.66562	62	1.71816	5.06749	98	3.22203	9.64273
27	0.66940	1.75835	63	1.75278	5.17471	99	3.27157	9.78316
28	0.70015	1.85126	64	1.78778	5.04321	100	3.32153	9.89900
29	0.73036	1.94382	65	1.82318	5.39240	101	3.37193	10.26364
30	0.76009	2.03090	66	1.85898	5.50289	102	3.42274	10.29839
31	0.78938	2.12750	67	1.89517	5.61450	103	3.47399	10.43826
32	0.81829	2.21863	68	1.93102	5.72724	104	3.52566	10.58834
33	0.84690	2.30934	69	1.96877	5.84112	105	3.57776	10.74234
34	0.70160	2.39970	70	2.00617	5.95611	106	3.63029	10.89874
35	0.90340	2.48976	71	2.04398	6.07225	107	3.68329	11.05698
36	0.93142	2.07962	72	2.08220	6.18955	108	3.73663	11.21680

TABLE 3-3 Harmonics Having Non Zero Stiffness Coefficients for the Various Fastener Arrangements

Number Of Fasteners									
3		6		9		12		18	
2	40	5	79	8	118	11	157	17	235
4	41	7	83	10	125	13	167	19	251
5	43	11	85	17	127	23	169	35	253
7	44	13	89	19	134	25	179	37	269
8	46	17	91	26	136	35	181	53	271
10	47	19	95	28	143	37	191	55	287
11	49	23	97	35	145	47	193	71	289
13	50	25	101	37	152	49	203	73	305
14	52	29	103	44	154	59	205	89	307
16	53	31	107	46	161	61	215	91	323
17	55	35	109	53	163	71	217	107	325
19	56	37	113	55	170	73	227	109	341
20	58	41	115	62	172	83	229	125	343
22	59	43	119	64	179	85	239	127	359
23	61	47	121	71	181	95	241	143	361
25	62	49	125	73	188	97	251	145	377
26	64	53	127	80	190	107	253	161	379
28	65	55	131	82	197	109	263	163	395
29	67	59	133	89	199	119	265	179	397
31	68	61	137	91	206	121	275	181	413
32	70	65	139	98	208	131	277	197	415
34	71	67	143	100	215	133	287	199	431
35	73	71	145	107	217	143	289	215	433
37	74	73	149	109	224	145	299	217	449
38	76	77	151	116	226	155	301	233	451

TABLE 3-5 Computed Joint Stiffness for Three Fasteners and Various Values of the Ratio of ϵ over the Bolt Diameter Enclosed Angle ($\times 10^7$ inch pound per radian)

Highest Harmonic	R(Values of ϵ Over Bolt Diameter Enclosed Angle)							
	½	1	3	5	6	6.2	6.24	10
1	10388.0	10387.0	10378.0	10359.0	10345.0	10342.7	10342.2	10270.0
3	12.6700	12.6730	12.7050	12.7760	12.8372	12.8372	12.8851	13.1129
6	5.1253	5.1308	5.1905	5.3076	5.3955	5.4142	5.4183	5.9090
9	3.8632	3.8708	3.9532	4.1160	4.2386	4.2347	4.2703	4.9572
12	3.3277	3.3374	3.4449	3.6567	3.8157	3.8496	3.8567	4.7262
15	3.0494	3.0618	3.1941	3.4531	3.6449	3.6855	3.6941	4.6893
18	2.8862	2.9009	3.0572	3.3584	3.5769	3.6225	3.6321	4.6884
36	2.4698	2.5013	2.8092	3.2721	3.5359	3.5865	3.5971	4.6569
64	2.2466	2.3132	2.7897	3.2592	3.5231	3.5741	3.5848	4.6497

Table 3-6

Computed Equivalent Joint Stiffness (x 10^8 inch pound per radian) for 3, 6, 9, 18 Fasteners. All Computations Use 6.24 for the Value of ϵ Over the Bolt Diameter Enclosed Angle

Highest Harmonic	3	6	9	18
1	1034.22	2068.40	3102.62	6205.2
3	1.28851	- -	- -	- -
6	.54183	2.0828	- -	- -
9	.42703	- -	4.3292	- -
12	.38567	1.1690	- -	- -
15	.36941	- -	- -	- -
18	.36321	1.0632	2.5469	48.734
36	.35971	1.0470	2.4721	31.067
54	- -	- -	2.4547	29.7569
64	.35848	- -	- -	- -
72	- -	1.0412	2.4509	29.589
109	- -	1.0406	2.4486	29.356

Table 3-7

Computed Joint Stiffness for Eighteen Fasteners and Various Values of the Ratio of ϵ over the Bolt Diameter Enclosed Angle (x 10^8 inch pounds per radian)

Highest Harmonic	Values of ϵ Over Bolt Diameter Enclosed Angle			
	0.5	1.0	1.5	2.0
1	6232.9	6232.0	6230.2	6230.2
17	10.9580	11.2330	-	-
35	5.0374	5.2411	-	-
53	4.0392	4.3071	-	-
71	3.5954	3.9403	-	-
109	3.1513	3.6822	-	-
181	2.9575	-	4.4163	5.2684
253	2.9178	-	4.4128	5.2620
325	2.9140	-	4.4092	5.2597

Table 3-8

Computed and Measured Equivalent Joint Stiffness ($\times 10^8$ Inch Pounds per Radian) for 3, 6, 9, 12, and 18 Fasteners. All computations use 1.544 for the value of R.

Number of Fasteners	Highest Harmonic Number	Computed Joint Stiffness	Measured Joint Stiffness
3	55	.2445	.358
6	109	.6089	.971
9	163	1.163	1.680
12	217	1.962	2.573*
18	325	4.480	4.440

*Interpolated

Table 3-9

Computed Equivalent Joint Stiffness
($\times 10^8$ Inch Pounds per Radian)

Number of Fasteners	Highest Harmonic Number	R	Computed Stiffness	Test Data
3	55	6.240	0.3585	0.358
6	109	5.301	0.9430	0.971
9	163	4.361	1.8306	1.680
12	217	3.422	2.9524	2.573*
18	325	1.544	4.4798	4.440

*Interpolated

FIGURE 3-3

SHEAR BOLT JOINT

TEST SPECIMEN AND SECTION MODELED USING FINITE ELEMENTS

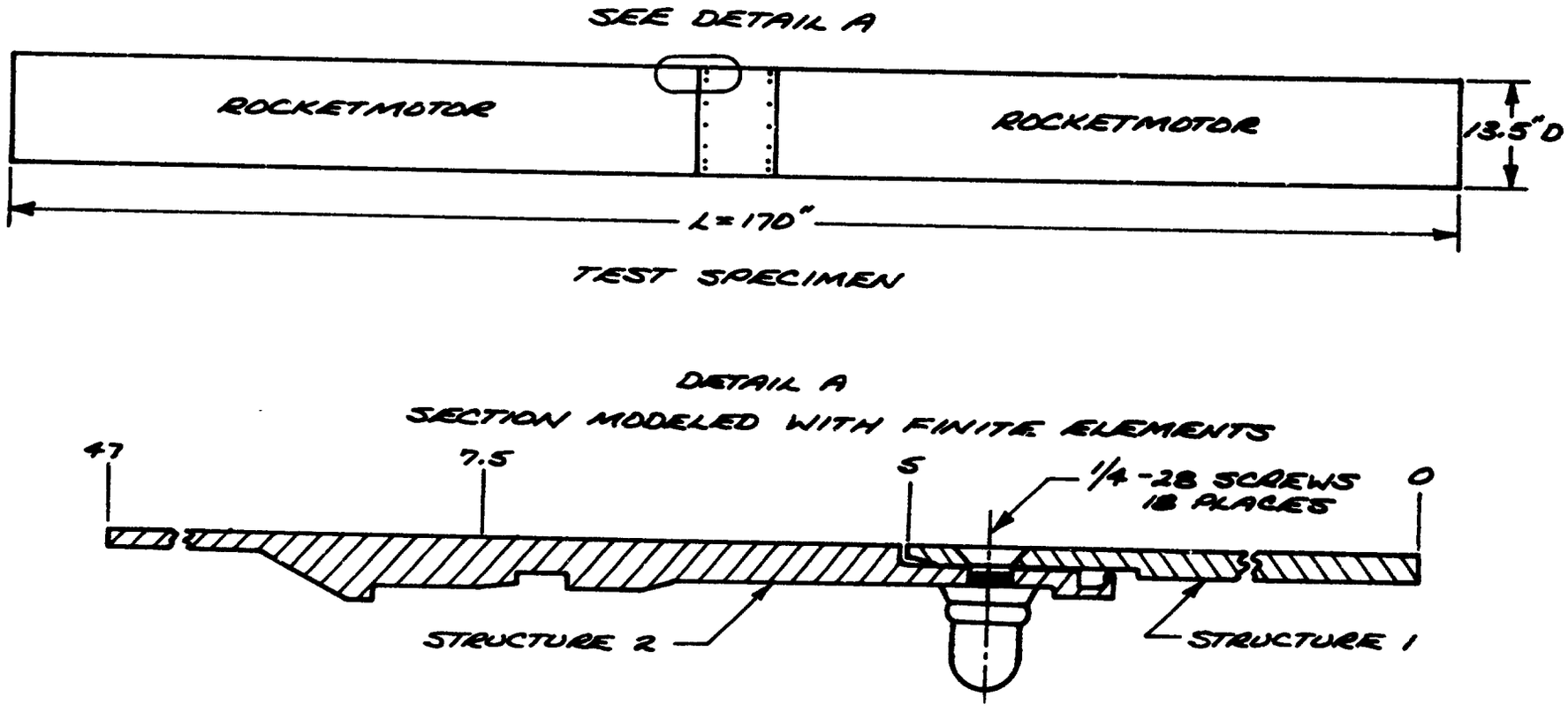
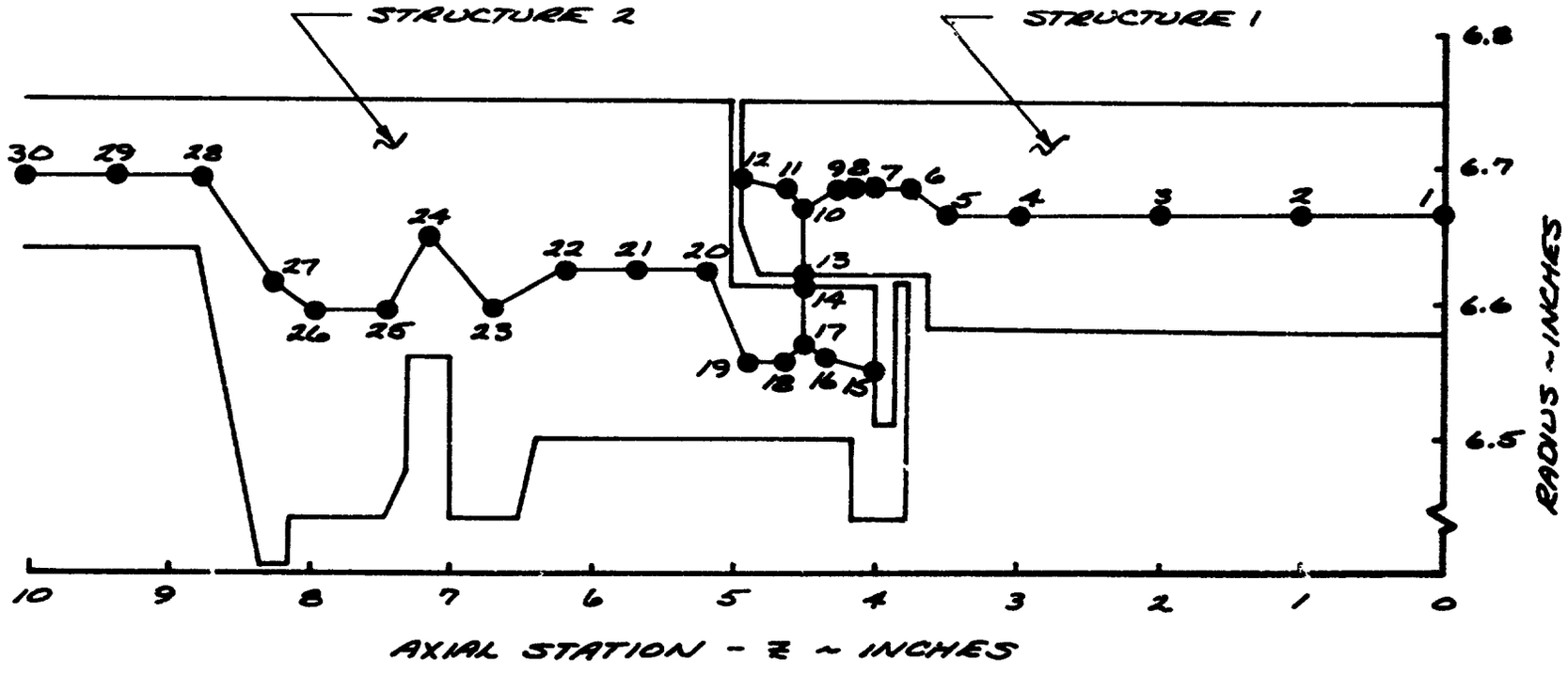


FIGURE 3-4

SHELL ELEMENT MODEL IN THE REGION OF THE SHEAR BOLT JOINT



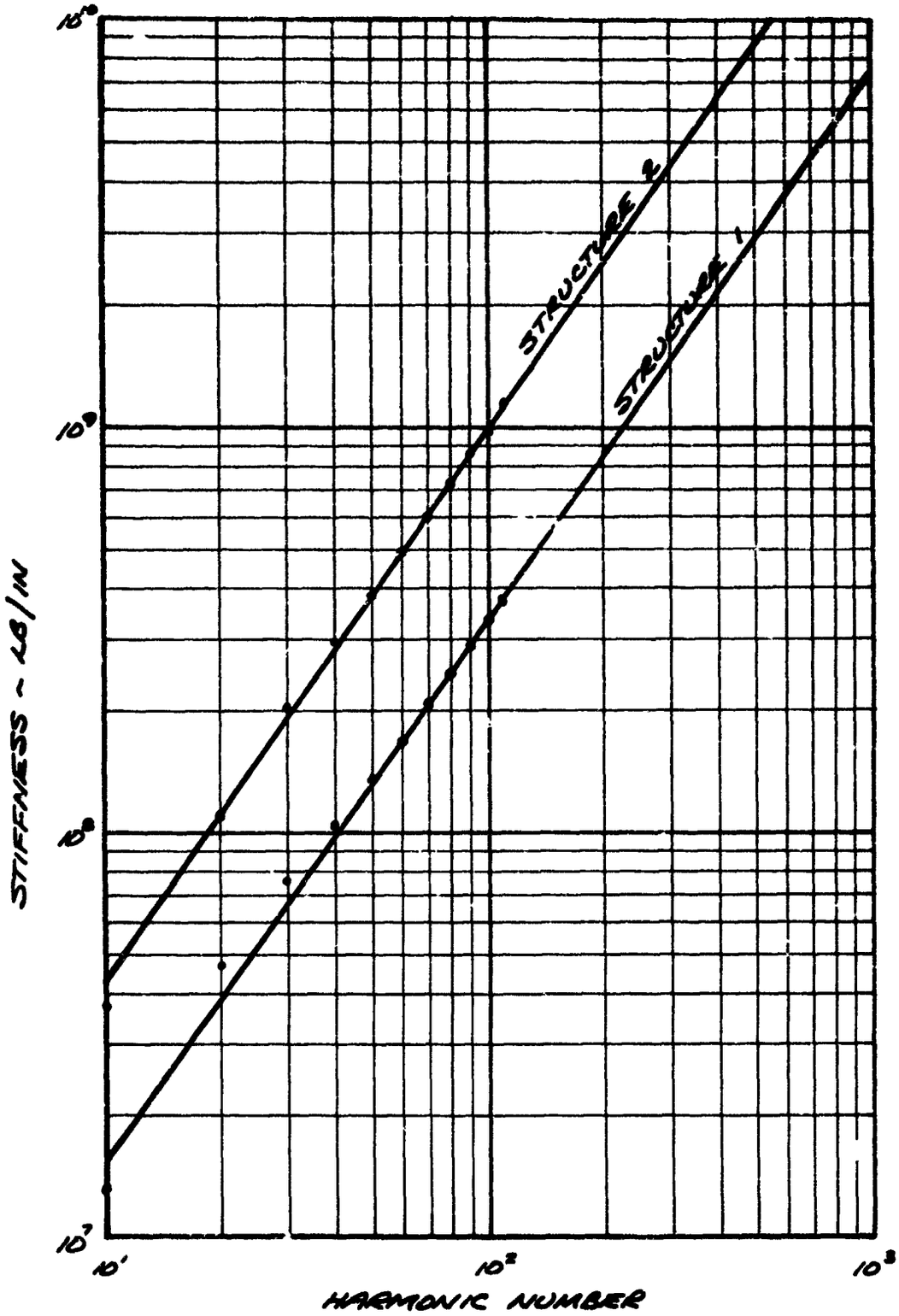


FIGURE 3-5 LOG-LOG PLOTS OF NASTRAN COMPUTED STIFFNESS COEFFICIENTS VERSUS HARMONIC NUMBER FOR THE TWO STRUCTURES

FIGURE 3-6

CURVE OF STIFFNESS VERSUS NUMBER OF FASTENERS FOR R = 1.544, R = 6.24 AND MEASURED RESULTS

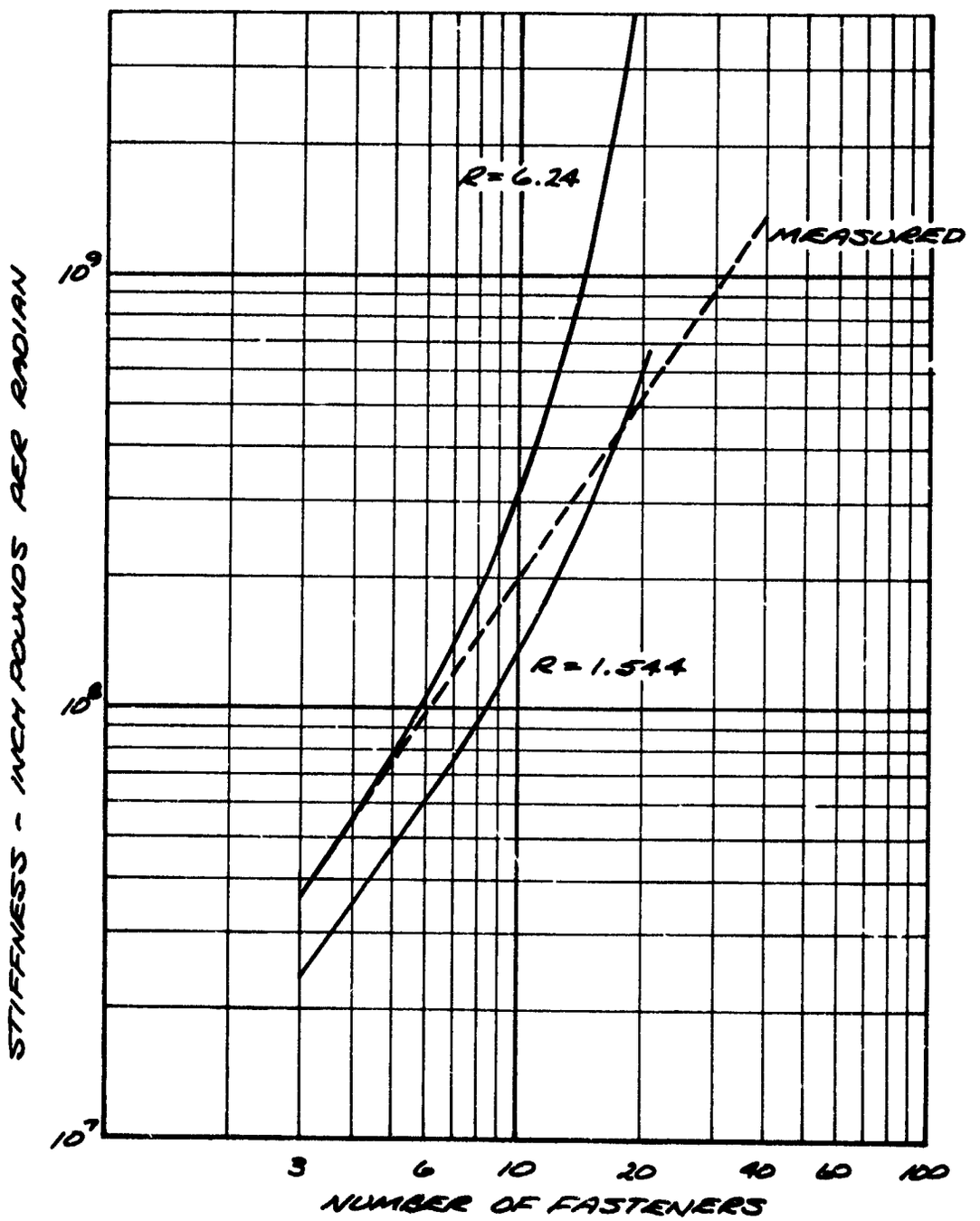


FIGURE 3-7

CURVE OF JOINT STIFFNESS VERSUS R (RATIO OF ε OVER THE BOLT DIAMETER ENCLOSED ANGLE) FOR THE THREE FASTENER CASE.

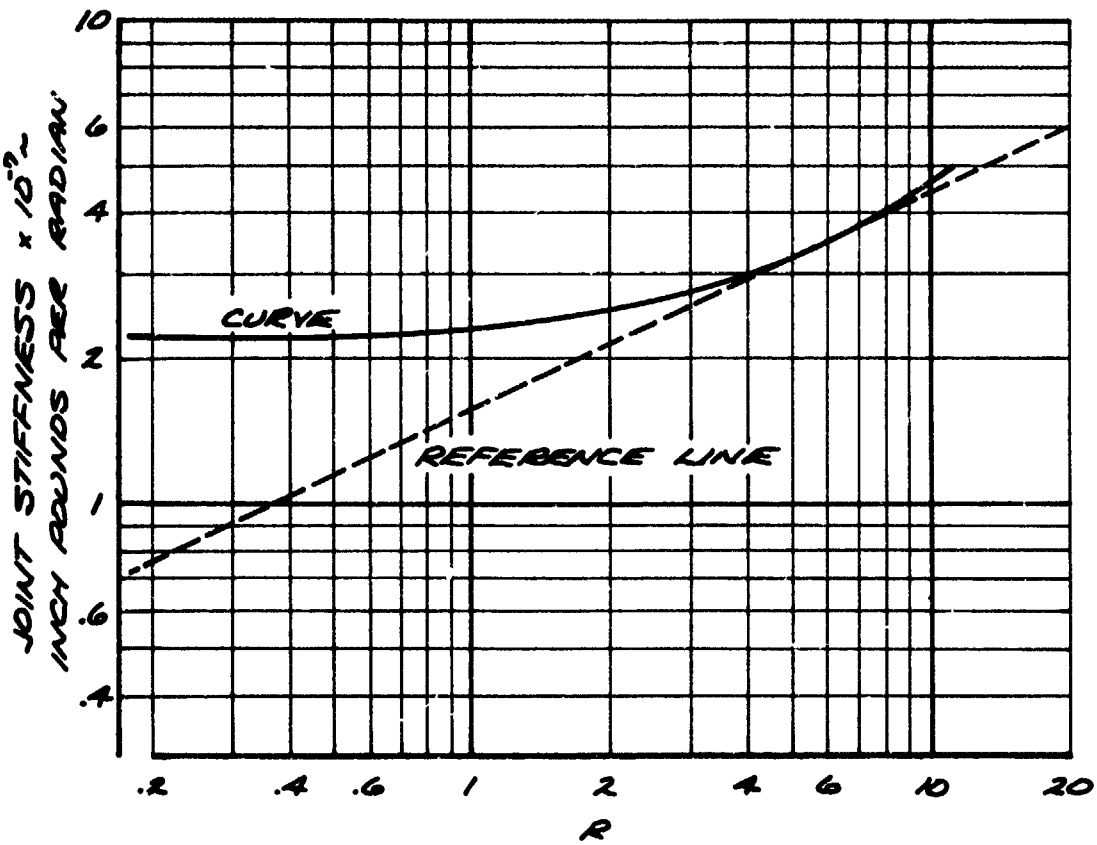
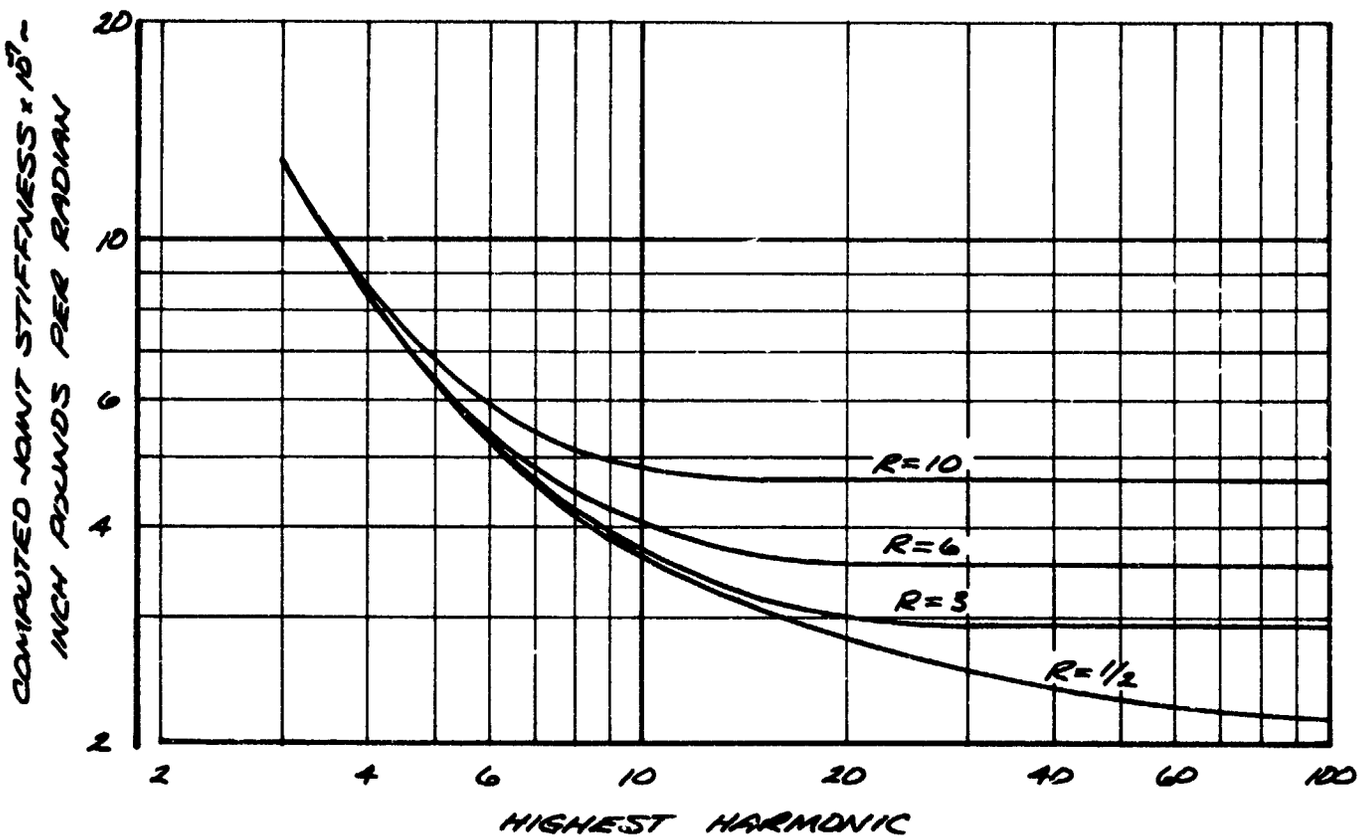


FIGURE 3-8

CURVES OF COMPUTED JOINT STIFFNESS VERSUS HIGHEST HARMONIC FOR THREE FASTENER JOINT AND VARIOUS VALUES OF R (RATIO OF E OVER BOLT DIAMETER ENCLOSED ANGLE.)



Section 4.0

JOINT COMPLIANCE EXTRACTION TECHNIQUE DEVELOPMENT

Tactical missile joint compliances often represent one of the major uncertainties in developing an acceptable analytical model for dynamic response studies. This uncertainty tends to be reinforced if large differences are discovered between theoretical and experimental mode shapes and frequencies. If one assumes that errors in assumed joint compliances are totally responsible for the theory/test mismatch, then a method of solution for effective joint compliances is suggested through an iterative "best fit" between modal analysis and modal test data. Since distributed mass and missile airframe stiffness parameters are generally well defined, the assumption that all errors lie in the effective joint compliances is not usually unreasonable. For many years at the Pomona Division of General Dynamics a somewhat arbitrary trial and error "hand tuning" procedure was employed to arrive at a set of joint compliances which would yield an acceptable fit between analysis and test data. This procedure can become quite time consuming and cumbersome, however, when more than two or three unknown joint compliances are involved.

A joint compliance extraction technique was developed during Phase 1 of the study of structural dynamic properties of tactical missile joints (Reference 1). It utilized a steepest-descent method to solve for variable unknown spring rates based upon a weighted best fit match between experimental and theoretical mode shapes and natural frequencies. The method was tailored specifically to beam representations of missile structures. Unfortunately, the method as implemented had several limitations. One of the restrictions was that the number of modes used had to equal or exceed the number of unknown joints to obtain meaningful results. Also, only bending cases with free-free boundary conditions could be run, and no method of handling appendages had been devised.

Late in the Phase 1 study, a general method for estimating structural parameters from dynamic test data appeared in Reference 4 which looked promising for use in the extraction of missile airframe joint compliances. Subsequently this method was applied in Phase 2 to simple test cases with encouraging results. As confidence was gained in the optimization method, the method was programmed for use with a Control Data Corporation 6400 computer. Originally only first order gradient terms were used. The first order gradient method worked well with a small (two degree of freedom) system, but was inadequate for larger systems. Next a second order gradient method in which the second order terms were approximated by differences was tried and techniques developed to improve convergence of the method. The resulting computer program is called program JOINTS.

During the present and final phase of this study (Phase 3) a number of program refinements and improvements have been introduced and evaluated. These program additions include the following:

1. A time saving option is provided for generation of "Standard" weighting factors which weights all test mode shapes and frequencies equally. Provision still exists, of course, for input of alternate weighting factors if preferred.

2. Program logic has been added to preclude missing or skipping over needed theoretical modes by assuring theoretical/test mode correspondence both in number of nodes and polarity. This prevents sizable errors which can result from mode mismatching and avoids numerous program restarts, thus saving turn around time between computer runs.

3. An option is offered to use a greater number of theoretical modes than experimental modes in the calculation of the gradients of the cost function. This feature aids solution convergence when only a few experimental modes are available.

4. An interpolation/extrapolation program called FILLIN has been added which takes experimental modal data at any arbitrary set of test missile stations and generates modal displacement and slope data at missile stations consistent with the lumped parameter modal analysis model. This operation offers a substantial labor savings in the preparation of input data for the joint compliance extraction program.

Section 4.1 presents the theory that program JOINTS is based upon. Rationale in selecting iteration bite size and the considerations involved in choosing experimental mode shape and frequency weighting factors are discussed in Section 4.2 together with a review of some of the results obtained with a hypothetical test case during the Phase 2 study. Section 4.3 presents a discussion and summary of the new program features added during the present phase and Section 4.4 offers a program application test case based on a set of actual tactical missile modal test data. The joint compliance extraction technique user's manual, including a listing of the programs, and appropriate test cases are presented in the Appendix.

4.1 METHOD OF ANALYSIS

The joint compliance extraction technique is designed to determine mechanical joint compliances of an elastic missile structure by generating the "best" least square fit between a linear lumped parameter mathematical model and a given set of experimental modal data. A major assumption in the method is that the joint compliances constitute the principal unknowns in the lumped parameter system, with both distributed

mass and stiffness being precisely defined. Weighting factors which involve mode number, shape, and frequency acknowledge the existence of accuracy limitations in the test data. The joint compliances yielding a best fit are found by minimizing a quadratic function of the differences between corresponding theoretical and experimental eigenvalues and eigenvectors. This function, referred to as the cost function, is expressed as follows:

$$F = \frac{1}{2} \sum_{i=1}^{N_t} \left\{ W_{if} \left(\omega_{ie}^2 - \omega_{it}^2 \right)^2 + \left(\underline{X}_{ie} - \underline{X}_{it} \right)^T W_{ix} \left(\underline{X}_{ie} - \underline{X}_{it} \right) \right\} \quad (4.1)$$

The frequencies and mode shapes are denoted by ω and $\underline{X}$, respectively. The weighting factor matrix is W and the index i is the mode number. If the mode shape slopes are used, they are treated as additional components of the $\underline{X}$'s. The subscripts e and t denote experimental and theoretical values, respectively. The minimization of the cost function constitutes a nonlinear programming problem which is the subject of this section. Optimization problems not amenable to standard methods are more the rule than the exception. In this case the optimization is accomplished by a steepest descent method especially developed for this study. The basic concept originally appeared in Reference 4. Before proceeding with a detailed discussion of the method, the structural mathematical model utilized will be described.

4.1.1 System Model. The fundamental structural dynamic considerations of a tactical missile are often handled with a linear lumped parameter mathematical model. The one used in this study is typical. More expressly, the mathematical model simulates a beam-like body with a series of lumped masses connected by weightless beams. Discrete shear, compressive; torsional, and flexural springs may be included at any point in the model. The model can be used to analyze bending, torsion, and longitudinal motion. The model contains provisions for including appendages attached to the main body at arbitrary angles with arbitrary attachment springs. The appendages are modeled similarly to the main body. The boundary value problem that results from this representation can be expressed as an eigenvalue problem:

$$\left[K - \omega_{it}^2 M \right] X_{it} = 0 \qquad i = 1, 2, \cdots N \quad (4.2)$$

where M and K are mass and stiffness matrices, respectively. The subroutine within the computer program which solves the eigenvalue problem uses the Holzer-Myklestad method. This numerical method utilizes transfer matrices from point to point on the model and finds the eigenvalues by satisfying the boundary conditions using an iterative procedure. A

complete description of the method is found in Reference 5. Limitations of the method and economy preclude extraction of all N modes where N is typically 50 to 200. It will be seen later that the lack of a complete set of modes introduces approximations into the optimization method and necessitates modifications.

4.1.2 Solution Method. The "best fit" values of the joint compliances, defined in a least square error sense, are determined by minimizing the cost function which is accomplished with a modified steepest descent method. Steepest descent or gradient methods as they are also known, iteratively converge on the location of the minimum, since an analytical solution of the condition for an extremum, $\nabla F = 0$, is not possible. The successive estimates of the minimizing values of the independent variables, in this case a vector the components of which are the unknown spring rates of the structural joints $\underline{k}$, are

$$\underline{k}^{(n+1)} = \underline{k}^{(n)} - \theta \nabla F \Big|_{\underline{k}^{(n)}} \tag{4.3}$$

The superscript indicates the number of the estimate. If the quantity θ is a constant, the algorithm is a first order method commonly referred to as the steepest descent method. It is based on the intuitive notion that if one proceeds in the direction of the steepest descent, which Equation 4.3 does, in small steps one must arrive at a local minimum. It can also be proven rigorously (Reference 6). A very efficient second order method may be derived by applying the Newton-Raphson algorithm to the gradient of the cost function which yields the successive approximation,

$$\underline{k}^{(n+1)} = \underline{k}^{(n)} - S \left[\frac{\partial^2 F}{\partial k_i \, \partial k_j} \right] \nabla F \Big|_{\underline{k}^{(n)}} \tag{4.4}$$

The matrix of second partial derivatives must be non-singular. Theoretically, the step size, S, is a scalar. However, in this study, it was necessary to generalize its definition. Equation 4.4 serves as the basis for the algorithm developed. The reasons for the modifications that were necessary will be explained as they are encountered.

The jth component of the gradient of the cost function is

$$\frac{\partial F}{\partial k_j} = \sum_{i=1}^{N_1} \left\{ W_{if} \left(\omega_{it}^2 - \omega_{ie}^2 \right) \frac{\partial \omega_{it}^2}{\partial k_j} + \left(\underline{X}_{it} - \underline{X}_{ie} \right)^T W_{ix} \frac{\partial \underline{X}_{it}}{\partial k_j} \right\} \tag{4.5}$$

where k_j is the jth unknown spring rate. In order to calculate the partial derivatives of the eigenvalues and eigenvectors with respect to

the k_j's, a departure was made from Reference 4. Here the modes were normalized to unity with respect to the generalized mass M,

$$\underline{X}_{it}^{T} M \underline{X}_{jt} = \delta_{ij} \tag{4.6}$$

Also a joint compliance positioning matrix, K^j, is introduced which locates the unknown spring rates within the full spring matrix -

$$K = \bar{K} + \sum_{j=1}^{N_J} K^j k_j \tag{4.7}$$

$\bar{K}$ is the matrix of known spring elements. Because of the peculiarities of the method used to solve the eigenvalue problem, the spring matrix, K, is not directly available and so neither are the variable spring positioning matrices, the K^j's. However, they can be derived by considering the strain energy stored in the jth spring. For simplicity, assume that a separate spring rate is assigned to each joint. Then the strain energy associated with the jth spring is:

$$U_j = \frac{1}{2} k_j \left({}'x_j - x_j' \right)^2 \tag{4.8}$$

where $'x_j$ and x_j' are the slopes to the left and to the right of the joint for the case of a rotational spring. The strain energy is also $U_j = 1/2 k_j \underline{x}'^T K^j \underline{x}'$. Equating the two expressions and then the coefficients of like terms, it can be deduced that the matrix, Kj, must be the null matrix except for a submatrix,

$$\begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix} \tag{4.9}$$

corresponding to the coordinates on either side of the joint. Then according to Reference 7 the partial derivatives are

$$\frac{\partial \omega_{it}^2}{\partial k_j} = \underline{X}_{it}^{T} K^j \underline{X}_{it} \tag{4.10a}$$

$$\frac{\partial \underline{X}_{it}}{\partial k_j} = \sum_{\ell \neq i}^{N} \frac{\underline{X}_{\ell t}^{T} K^j \underline{X}_{it}}{\omega_{it}^2 - \omega_{\ell t}^2} \underline{X}_{\ell t} \tag{4.10b}$$

Equations (4.10a) and (4.10b) can be expanded in terms of components of the normal coordinates by utilizing the strain energy relationship for each joint.

$$\frac{\partial \omega_{it}^2}{\partial K_j} = x_{it,mj}\left(x_{it,mj} - x_{it,mj+1}\right) + x_{it,mj+1}\left(-x_{it,mj} + x_{it,mj+1}\right)$$

$$= \left(x_{it,mj} - x_{it,mj+1}\right)^2 \tag{4.11a}$$

$$\frac{\partial \underline{X}_{it}}{\partial K_j} = \sum_{\ell \neq i}^{N} \left(\omega_{it}^2 - \omega_{\ell t}^2\right)^{-1} \left\{x_{\ell t,mj}\left(x_{it,mj} - x_{it,mj+1}\right)\right.$$

$$\left. + x_{\ell t,mj+1}\left(-x_{it,mj} + x_{it,mj+1}\right)\right\} \underline{X}_{\ell t} \tag{4.11b}$$

where the indices mj and $mj+1$ refer to the components of the normal coordinates to the left and right of the jth joint respectively. The partial derivatives of the mode shapes were derived using the second formulation of Reference 7 which requires a complete set of theoretical modes. As pointed out previously the sum has to be truncated for reasons of accuracy and economy. This is usually the case in dynamic problems. Here the justification is a posteriori. The number of theroetical modes used in the computation of their derivatives is an option to be selected by the user.

$$\frac{\partial \underline{X}_{it}}{\partial K_j} \cong \sum_{\ell \neq i}^{N_1} \frac{\underline{X}_{\ell t}^T K^j \underline{X}_{it}}{\omega_{it}^2 - \omega_{\ell t}^2} \underline{X}_{\ell t} \tag{4.12}$$

The second partial derivative of the cost function with respect to the unknown spring rates, k_q and k_j, is

$$\frac{\partial^2 F}{\partial K_q \partial K_j} = \sum_{i=1}^{N_1} \left\{ W_{if}\left[\frac{\partial \omega_{it}^2}{\partial K_q}\frac{\partial \omega_{it}^2}{\partial K_j} + \left(\omega_{it}^2 - \omega_{ie}^2\right)\frac{\partial^2 \omega_{it}^2}{\partial K_q \partial K_j}\right]\right.$$

$$\left. + \frac{\partial \underline{X}_{it}^T}{\partial K_q} W_{ix} \frac{\partial \underline{X}_{it}}{\partial K_j} + \left(\underline{X}_{it} - \underline{X}_{ie}\right)^T W_{ix} \frac{\partial^2 \underline{X}_{it}}{\partial K_q \partial K_j}\right\} \tag{4.13}$$

The second partials of the eigenvalues and mode shapes are

$$\frac{\partial^2 \omega_{it}^2}{\partial K_q \partial K_j} = \frac{\partial X_{it}^T}{\partial K_q} K^j \underline{X}_{it} + X_{it}^T K^j \frac{\partial \underline{X}_{it}}{\partial K_q} \tag{4.14a}$$

$$\begin{aligned}\frac{\partial^2 \underline{X}_{it}}{\partial K_q \partial K_j} \cong \sum_{\ell \neq i}^{N_i} (\omega_{it}^2 - \omega_{\ell t}^2)^{-1} \Bigg\{ \Bigg[& -(\omega_{it}^2 - \omega_{\ell t}^2)^{-1} \left(\frac{\partial \omega_{it}^2}{\partial K_q} - \frac{\partial \omega_{\ell t}^2}{\partial K_q} \right) \underline{X}_{\ell t}^T K^j \underline{X}_{it} \\ & + \frac{\partial \underline{X}_{\ell t}^T}{\partial K_q} K^j \underline{X}_{it} + \underline{X}_{\ell t}^T K^j \frac{\partial \underline{X}_{it}}{\partial K_q} \Bigg] \underline{X}_{\ell t} \\ & + \underline{X}_{\ell t}^T K^j \underline{X}_{it} \frac{\partial \underline{X}_{\ell t}}{\partial K_q} \Bigg\}\end{aligned} \tag{4.14b}$$

During Phase 2 it was felt that direct calculation of the second partial derivatives of the eigenvalues and eigenvectors using the above equations were prohibitive because of computer memory size limits. It was subsequently realized that direct calculation of the second partial derivatives is very likely economically feasible since many of the terms are zero. However, since only a small number of unknown missile joints are assumed, the method employed in program JOINTS approximates the second partials by taking differences of the first partials. Such a numerical process tends to be accuracy sensitive and demands careful monitoring. Without resorting to double precision arithmetic, the step size must be large enough to yield a sufficient number of significant figures . On the other hand, too large a step size may enclose a region too large for the cost function to be represented by a quadratic. The procedure settled upon was the following. Using the current estimate $\underline{k}^{(n)}$, the gradient of the cost function is computed with Equations (4.5), (4.11a) and (4.12). The current estimates of the unknown springs are successively incremented one at a time in the direction dictated by the corresponding component of the gradient:

$$K_j'^{(n)} = K_j^{(n)} \left[1 - r \cdot SGN\left(\frac{\partial F}{\partial K_j} \bigg|_{K^{(n)}} \right) \right] \tag{4.15}$$

The relative increment, r, is the same for all the unknown spring rates and fixed for a particular problem. The gradient is calculated at $\underline{k}'^{(n)}$ and the ratios of the differences of the respective components and the spring rate increments are computed. In order to improve the estimates of the second partial derivatives, corresponding off-diagonal estimates which theoretically should be equal are averaged as indicated below.

$$\frac{\partial^2 F^{(n)}}{\partial K_i \partial K_j} = \frac{\partial^2 F^{(n)}}{\partial K_j \partial K_i} \approx \frac{1}{2} \left\{ \left(K_i'^{(n)} - K_i^{(n)} \right)^{-1} \left[\frac{\partial F^{(n)}}{\partial K_j} \right]_{K_i}^{K_i'} \right. \tag{4.16}$$

$$\left. + \left(K_j'^{(n)} - K_j^{(n)} \right)^{-1} \left[\frac{\partial F^{(n)}}{\partial K_i} \right]_{K_j}^{K_j'} \right\}$$

The Hessian, the matrix of second partial derivatives, is then inverted. The correction terms in Equation (4.4) are computed using a value of 1.0 for S. The sign and magnitude of each correction component are compared to those of the increment used to estimate the second partials. If the signs agree or if the magnitude is less than 2-1/2% of the current spring rate, the second order correction is utilized. If not, equation (4.15) is used. If the new spring rates, $\underline{k}^{(n+1)}$, result in an increase in the cost function, the correction terms to $\underline{k}^{(n)}$ are halved repeatedly until a decrease in the cost function is obtained. In any case, each variable spring rate is kept within prespecified limits. These procedures which taken together may be considered a complicated method of selecting a varying step size, S, evolved heuristicly. Modifications which can be made to improve them and put them on a more rigorous basis are possible.

4.2 SPECIAL PARAMETERS

This section discusses two of the parameters important to the proper functioning of the method of solution. Both of these parameters are input quantities in the present version of Program JOINTS. These parameters are the set of weighting factors and the step size - r.

4.2.1 Weighting Factors. Ideally the weighting in the cost function should reflect both the relative accuracy of the experimental data and the relative importance of the information to be obtained from applications of the mathematical model. Often for missiles constructed with thin cylindrical shells, the experimental data will diverge from beam behavior in progressively higher modes. For many dynamic analyses (such as dynamic loads analyses and autopilot elastic mode coupling analyses), the contribution of the higher modes is less significant than the lower modes. If the above conditions hold for any given problem, then the weighting factors should decrease in some way with increasing mode number.

A derivation of the weighting factors is now developed. The cost function (Equation 4.1) may be broken down into two terms (mode shape and frequency) for each mode

$$F_i = F_{if} + F_{ix} \tag{4.17}$$

where

$$F_{if} = \frac{1}{2} W_{if} \left(\omega_{ie}^2 - \omega_{it}^2 \right)^2 \tag{4.18}$$

$$F_{ix} = \frac{1}{2} \left(\underline{X}_{ie} - \underline{X}_{it} \right)^T W_{ix} \left(\underline{X}_{ie} - \underline{X}_{it} \right) \tag{4.19}$$

Rewriting F_{ix} as a summation yields

$$F_{ix} = \frac{1}{2} W_{ix} \sum_k \left(\underline{X}_{ie_k} - \underline{X}_{it_k} \right)^2 \tag{4.19a}$$

To see the size of terms produced in the cost function by an error in the eigenvalue or eigenvector, a relative error of size ϵ is assumed in each of the measured quantities. Then the cost function terms will be equated by proper selection of weighting factors. That is, an error of ϵ will be assumed in both ω^2 and X, and weighting factors will then be found which give equal size terms in the cost function. If the theoretical eigenvalues and eigenvectors are assumed correct, then an error of ϵ in the eigenvalue can be written as

$$\omega_{it}^2 = (1+\epsilon)\, \omega_{ie}^2 \tag{4.20}$$

The frequency terms in the cost function become

$$F_{if} = \frac{1}{2} W_{if} \left[\omega_{ie}^2 - (1+\epsilon)\, \omega_{ie}^2 \right]^2$$

$$F_{if} = \frac{1}{2} W_{if} \left[-\epsilon\, \omega_{ie}^2 \right]^2$$

$$F_{if} = \frac{1}{2} W_{if}\, \epsilon^2 \omega_{ie}^4 . \tag{4.21}$$

This means that an error of ϵ in the eigenvalue will produce a residual term in the cost function proportional to the product of the fourth power of the frequency and the square of the error. Considering the same error applied to the mode shape contribution to the cost function yields

$$F_{ix} = \frac{1}{2} W_{ix} \sum_{\ell} \left[X_{ie_\ell} - (1+\epsilon) X_{ie_\ell} \right]^2$$

$$F_{ix} = \frac{1}{2} W_{ix} \sum_{\ell} \epsilon^2 X_{ie_\ell}^2 \tag{4.22}$$

The above equation shows that an error of ϵ in the eigenvector will produce a residual term in the cost function proportional to the product of the square of the eigenvector and the square of the error. Since the mode shapes are normalized to a unity generalized mass, then

$$1 = \sum_{\ell} m_\ell X_{ie_\ell}^2 \tag{4.23}$$

If assumptions are made that the test specimen is a slender beam with uniform mass and station distributions, then the above equation may be rewritten as

$$1 = \bar{m} \sum_{\ell} X_{ie_\ell}^2$$

$$\sum_{\ell} X_{ie_\ell}^2 = 1/\bar{m} \tag{4.23a}$$

and the mode shape portion of the cost function becomes inversely proportional to the mass

$$F_{ix} = \frac{1}{2} W_{ix} \epsilon^2 \frac{1}{\bar{m}} \tag{4.24}$$

where $\bar{m} = \dfrac{\text{mass of beam}}{\text{Number of stations}}$

F_{ix} is independent of frequency, and is dependent upon the mass, number of beam stations, and the square of the error.

To equate the size of the frequency terms in the cost function with each other, the following weighting factors were selected

$$W_{if} = \frac{\omega_{Nie}^4}{\omega_{ie}^4} \tag{4.25}$$

where

ω_{Nie} = highest experimental mode frequency

Equating the mode shape and frequency terms of the cost function yields

$$W_{ix} \frac{1}{\bar{m}} = \frac{\omega_{N1e}^4}{\omega_{ie}^4} \omega_{ie}^4 = \omega_{N1e}^4$$

$$W_{ix} = \omega_{N1e}^4 \bar{m}$$

$$W_{ix} = \frac{\omega_{N1e}^4 m}{N} \tag{4.26}$$

where m = mass of the missile (Lb-Sec^2/In)

N = number of internal stations

The above weighting factors then approximately weight the mode shape and frequency errors equally. These factors have been built into Program JOINTS along with a set of adjustable weighting factor coefficients. If unequal weights are desired, weighting factor coefficients are input to the program and these coefficients are multiplied by the above factors to obtain the new weighting factors used by the program. That is

$$W_{if} = WFC_{if} \left(\frac{\omega_{N1e}^4}{\omega_{ie}^4} \right) \tag{4.27}$$

$$W_{ix} = WFC_{ix} \left(\frac{\omega_{N1e}^4}{N} m \right) \tag{4.28}$$

where WFC_{if} and WFC_{ix} are input separately for each mode.

Some consideration was given to including provisions for weighting some mode components more than others, but this was concluded to be an impractical and unwarranted complexity in the operation of the program.

4.2.2 "Bite" Size Selection. The bite size being discussed in this section is r in equation (4.15), the increment each spring is altered during the intermediate calculation in the computation of the second order partials. The choice of the spring increment size, r, can cause a problem unless care is taken in its selection. The step size must be large enough to prevent incurring numerical accuracy problems, yet small enough to give an adequate estimate of the second order gradients of the cost function.

The present tolerance ratio on the frequency solution in the modal analysis routine in Program JOINTS is 1×10^{-5}. That is, the theoretical

frequency solutions will be no worse than .001 percent. In selecting a value of r to be used in Program JOINTS, a change in each individual spring equal to r times the spring rate should produce frequency changes greater than .01 percent in the theoretical modes. This change in frequency is dependent upon the joint locations and magnitude of compliances. Reference 1 (Phase 1 Report) provides an extensive discussion of these parameters. Another constraint on the step size to be considered is that if the originally assumed joint compliances are 'far from convergence' a first order gradient method is used rather than the second order gradient method. If the first order method is used, r is the amount the compliance is altered each iteration. If r is small, the solution time may be very large. The phrase 'far from convergence' is defined as a region which is determined by the directions indicated for changes in individual spring rates from the first order and the second order gradient methods. If the two methods indicate opposite directions should be taken for the change in spring rate, the first order method is used. As the cost function minimum is approached, the first and second order terms agree in sign for the change in spring rate so the magnitude determined from the second order method is used. This choice of either the first or second order method is made independently for each spring.

To illustrate the effect of the step size r, consider the non-uniform bending beam model shown in Figure 4-1. It consists of five beam sections connected by four flexural joints, each of "moderate" to "good" stiffness for the assumed test airframe. The Holzer Myklestad method (identical to what is used in Program JOINTS) was used to generate the required modal data for this test case. Since the modal data are "exact" for the lumped parameter model, a precise means for judging the accuracy of the JOINTS program solution is provided. Selected flexural joints were then assumed to be unknown, and arbitrary (incorrect) initial values selected.

Figure 4-2 shows the results obtained with Program JOINTS by using two modes to solve for three joint compliances. For this case, the compliance of the first of the four joints was assumed to be known correctly and the compliance of the last three were assumed high by a factor of two. The value of the intermediate step size, r, used in this case was 25%. Figure 4-2 shows the result of eighteen iterations. The convergence is seen to be quite slow. Other values of r have been considered with interesting results. Figure 4-3 shows the same example as Figure 4-2, except the value of r was changed from 25% to 1%. Here convergence to the three correct joint flexural compliances is achieved in four iteration cycles or about four times as fast. This points out the importance of the intermediate step size, r, used in approximating the second partial derivatives. In both of these examples, three unknown spring rates were solved using only two modes.

Figure 4-4 illustrates further the importance of the intermediate step size, r, in the convergence of the method. Values of r considered

in Figure 4-4 range from 25% to 1%. Very little difference is seen between 1% and 5%, suggesting that both approximate the second order gradients well. For this case, it can be seen that 25%, 20%, and 15% were all too large a value for r. All three values of r will produce the correct joint compliances but the run time is much longer for the larger values of r. The value of r for best convergence will not be the same for all cases. In fact, for some problems it might be more efficient to make two computer runs using two different values of r. In the beginning, use of a larger value of r may be required if the program employs the first order gradient method. However, the solution may be speeded up by using a smaller value of r as the cost function minimum is approached and the program uses the second order gradient method.

4.3 PROGRAM FEATURES ADDED

This section discusses some of the techniques developed during the Phase 3 study to increase the efficiency of Program JOINTS and to decrease the work required by the user. Covered in this discussion are the program generation of weighting factors, logic in JOINTS to correct for modes being missed by the eigenvalue extraction subroutine, and the benefits of using the input parameter 'CLOSE'. In addition, this section introduces the computer program (Program FILLIN) written as an aid for the user of Program JOINTS. Program FILLIN accepts measured modal data in a general format and interpolates between those data points to obtain a new set of data in the format appropriate for use in Program JOINTS. The changes to the input data are necessitated because Program JOINTS compares the experimental and theoretical modal data at identical missile stations.

4.3.1 Weighting Factor Generation. In the original program format, the weighting factors required to use Program JOINTS had to be calculated by the user. As an added convenience, it was decided to accomplish the major portion of the weighting factor computation within the program. Equations 4.25 and 4.26 of section 4.2.1 present the equations of the weighting factors now used in the program. The option is retained to input weighting factor coefficients desired by the user, but these weighting factor coefficients (WFC_{if} and WFC_{ix} in equations 4.27 and 4.28) modify the factors computed by the program and do not replace them. If no values are input for WFC_{if} and WFC_{ix} , these coefficients are each assumed equal to 1.0. If the user, for example, wishes to weight the first mode shape and frequency a factor of two more than the other modes, he simply inputs the value 2.0 for WFC_{1f} and WFC_{1x} and 1.0 for all other modes.

4.3.2 'Missing' Mode Logic. Another option built into Program JOINTS during Phase 3 is a check to guard against missing modes in the eigenvalue extraction routine. This is accomplished by checking the computed modes against the experimental modes. For bending cases, the number

of slope sign changes in each theoretical mode shape is compared with each measured mode. Like modes are matched and if any modes are missing the program will go back and compute the missing modes. Because of the way the Myklestad subroutine treates redundant appendages, this check should not be used with a model that has redundant appendages.

4.3.3 Number of Theoretical Modes. Another improvement introduced to Program JOINTS is to allow the calculation and inclusion of more theoretical modes than experimental modes in the partial derivatives of the mode shape given in equation (4.11b) The partial derivative of the eigenvector for the ith mode is expressed as the sum of contributions from all modes except the ith mode. This sum is truncated at however many modes are available for the calculation. If only one mode is available, then the partial is approximated by zero. If two modes are available, then the partial is approximated by contributions from one mode. For a distributed system, the partial derivative would be computed from an infinite sum. The larger the number of modes, the closer the sum should approximate the partial derivatives. Using more modes in approximating the partial derivatives can be expected to produce more accurate values, aid in the problem solution, and accelerate the rate of convergence. The amount of computer time used per iteration cycle, however. is directly proportional to the number of theoretical modes used in the solution. Because of this cost consideration, the user would be advised to use an equal number of theoretical modes in the solution when three or more measured modes are available.

4.3.4 Input Parameter 'CLOSE'. The input parameter 'CLOSE', Table A-3,used in Program JOINTS is another parameter designed to save computer time. If a value is not input for 'CLOSE' into Program JOINTS, a continuous search is made for the required number of modes between specified frequency limits. Computer time may be saved by eliminating as much of the searching as possible. A way of eliminating the unnecessary searching is to start below but very near the answer. The reason for starting just below the answer is that the frequency search is done in an increasing order. For a model which matches the experimental data fairly closely, the search starting frequency for each mode may be selected close to the experimental frequencies. If a value of 'CLOSE' is input, the search for the ith mode starts at the frequency equal to 'CLOSE' times the experimental frequency for the ith mode.

Starting the search for the modes near the required solution has saved considerable computer time in several of the test cases. Using the tactical missile application of Section 4.4 as an example, a value of 'CLOSE' equal to 0.9 cost approximately 30% less than an identical run where a continuous search was used. However, care must be taken that 'CLOSE' times the experimental frequency for the ith mode will not be less than the theoretical frequency for the $(i-1)^{th}$ mode, in which case the $(i-1)^{th}$ mode will be repeated for the ith mode.

4.3.5 Test Data Preparation. One of the goals of the Phase 3 study was to simplify the tasks of the person using Program JOINTS. During the Phase 2 study, it became obvious that for Program JOINTS to be easily useable, a scheme was needed to reduce the amount of work required to get the experimental data in the format necessary for the program. As the cost function is formulated, the mode shape deflection and slope at every internal station are compared with a measured mode shape deflection and slope at that station. However, seldom are the measurements made at the station locations required by the mathematical model. In addition, the quantities most usually measured during test are the modal deflections and not the slopes. One way of handling this problem is to plot the measured deflection data. From these plots, a new set of modal deflections and slopes are read at the desired stations and key punched on cards. As an example of the size of this problem, the tactical missile test case discussed in Section 4.4 has a total of 78 stations. The number of data points read per mode is 156, and three modes were used for that case. It was for this reason that Program FILLIN was written.

Program FILLIN accepts modal data measured at a set of missile stations and the mathematical model data to be used in Program JOINTS. The program then interpolates using several simple curve fitting techniques. The program is primarily designed for bending mode cases. The method of interpolation to be used at a particular station is determined by the station type and the relative locations of stations at which experimental values are available The types of stations considered include those not at a joint, those immediately to the right or left of joints, and those at the ends of the main beam or an appendage. The first class of stations includes the majority of stations. For these stations interpolation was accomplished with a sliding parabolic least square curve fit to four experimental values. That is the two nearest experimental values on either side of the station are used for the least square fit. If two experimental values are not available on both sides of the station, linear interpolation or if necessary extrapolation is resorted to. This also applies to stations at ends of appendages and to modal slopes at stations immediately to the right or left of rotational spring joints and to modal displacements at stations immediately to the right or left of shear spring joints. Modal slopes at a shear joint are the average of the two straight line slopes on each side of the joint.

One of the limitations of Program FILLIN is that appendages with 180° attachment angles will have slope values with the sign opposite to the Myklestad subroutine. This occurs because the Myklestad routine uses a different coordinate systems on appendages than it does on the main beam while FILLIN uses only one coordinate system. Another limitation of

FILLIN is that inaccuracies can occur at stations near joints and in slopes at roots of appendages. However, one of the advantages of the least square curve fit is that the method will smooth the experimental data.

4.4 TACTICAL MISSILE TEST CASE

To show the utility of Programs FILLIN and JOINTS, a set of measured bending modal data for an actual tactical missile were selected as a test case. The set of modal data had previously been matched with a mathematical modal by a trial and error method. This method took approximately sixty computer runs. Previous test cases based on hypothetical models had shown that the method arrives at the correct joint compliances rapidly when an exact math model is used with no errors in the input data. The results obtained with this test case illustrate how well the program works when matching a lumped parameter model to actual measured data with its inherent experimental errors.

Figures 4-5, 4-6, and 4-7 present the three experimental modes and the curve fit values obtained from Program FILLIN for the tactical missile. There are slight discrepancies between the measured data points and the curve fit values, especially near the front end of the missile where few data points exist. The forward end of the missile is a radome shell and quite stiff for the weight it supports. It therefore bends very little in the lower bending modes. When the program fits the data points with a quadratic equation, the match is not perfect. Nevertheless the interpolated modal displacements and slopes are believed to be reasonable representations of the measured modes. Since the method tends to smooth the data, a test case with larger experimental errors in the measured modes would look more impressive.

The output displacements and slopes from Program FILLIN are punched on cards in the format for Program JOINTS. However, the punched output must be checked and corrected as 180 degree appendages will have the sign of the slopes out of phase with the Myklestad program. This is due to a different sign convention in the Myklestad subroutine for 180 degree appendages.

The data output from Program FILLIN was then used as the input modal data for Program JOINTS. The set of weighting factors selected for this application were chosen to equate all three modes (both frequencies and mode shapes) equally. The first three joint compliances (which represented airframe joints) were started approximately 300% higher than the hand tuned values. The fourth joint compliance represented the attachment compliance for an internal appendage. The originally assumed value of the fourth compliance was started high by 30% over the hand tuned value.

Figure 4-8 shows the rate of convergence obtained by Program JOINTS for the tactical missile application. The program was run for a total of eight iteration cycles. However, the cost function did not improve significantly after the third cycle. The final (iteration cycle eight) joint compliances obtained agree quite well with the hand tuned values. Figures 4-9, 4-10, and 4-11 present a comparison of the experimental and theoretical modes. It is apparent from the figures that a good match has been obtained between the two sets of data.

Next, a new set of weighting factors was chosen to see what effect different weighting factors had on the solution. It should also be noted that the test data was represented well by the beam model in the above solution. The set of frequency weighting factor coefficients selected were 100, 10, and 1 for the first, second, and third modes respectively. The corresponding mode shape weighting factor coefficients were 1, 0.1, and 0.01. Figure 4-12 shows the solution (No. 2) obtained for this condition. Comparison of Figures 4-8 and 4-12 shows that both sets of compliances obtained are close to the hand tuned values. The following is a comparison of the experimental frequencies and the frequencies obtained for the two sets of weighting factors.

Mode No.	Experimental Frequency (Hz)	Theoretical Frequency (Hz)	
		Solution No. 1	Solution No. 2
1	59.3	59.5	59.3
2	116.	114.4	116.0
3	153.	154.2	153.6

As shown above, the case where the frequencies are weighted more heavily than the mode shapes (solution number 2) does in fact exhibit a better match between the experimental and theoretical frequencies.

4.5 STATUS OF THE EXTRACTION TECHNIQUE

The joint compliance extraction technique in its present format is believed to offer a useful, convenient, and reliable method for estimating effective compliances of missile joints from modal test data. The method presumes that the missile airframe distributed stiffness and mass properties are known, the modal characteristics can be adequately modeled as a lumped parameter beam, and that all discrepancies between modal analysis and modal test data can be attributed to uncertainties in the joint compliance values. As in any analytical method, additional refinements and areas for improvement will become evident as applications are further explored with actual test data.

LIST OF SYMBOLS FOR SECTION 4.0

F = Cost Function of Error Terms

N_1 = Number of Experimental Modes

$\sum_i$ = Summation on Index i

ω = Mode Frequency

X = Mode Shape

W = Weighting Factor

$(\ )^T$ = Transpose of $(\ )$

K = Stiffness Matrix

M = Mass Matrix

N = Number of Internal Stations in Model

K = Unknown Spring Components

n = Iteration Number

θ = Step Size

∇F = $\frac{\partial F}{\partial K}$ = Gradient of F

S = Step Size

$[\ ]^{-1}$ = Inverse of $[\ ]$

δ_{ij} = Kronecker Delta $\begin{cases} = 1 & i = j \\ = 0 & i \neq j \end{cases}$

$\bar{K}$ = Matrix of Known Spring Elements

N_J = Number of Joints

U = Strain Energy

X_j', X_j' = Slope to the Left and Right of Joint j

K' = Intermediate Spring Rate Used in Computing the Second Order Derivatives of F

LIST OF SYMBOLS FOR SECTION 4.0 (Cont'd.)

r = Intermediate Step Size Used to Obtain K'

$SGN(\ )$ = The Sign of ( )

ϵ = Relative Error Size

λ = ω^2 = Eigenvalue

m = Mass of Missile

WFC = Weighting Factor Coefficients

SUBSCRIPTS

e = Experimental

t = Theoretical

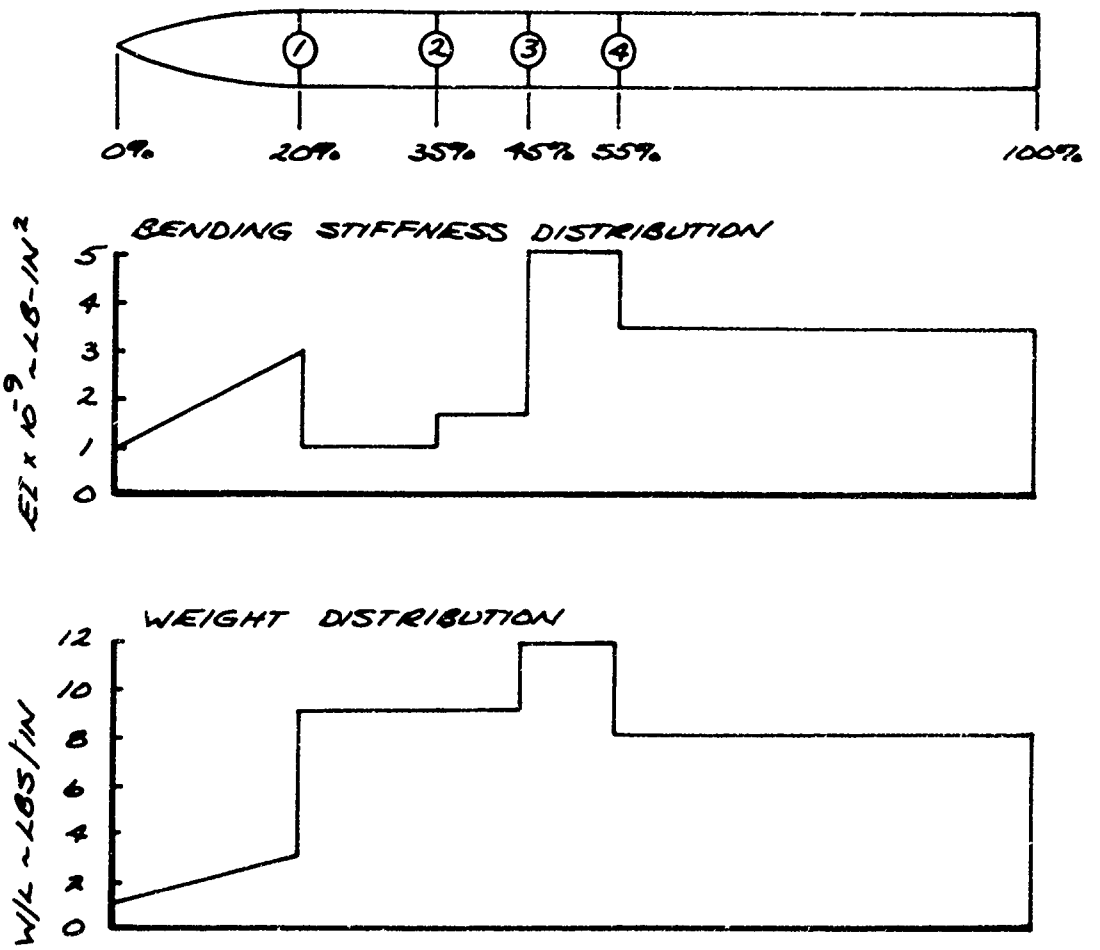
x = Mode Shape

f = Frequency

i, j, ℓ, m, q = Indices or Counters

FIGURE 4-1

NON-UNIFORM BENDING BEAM PROPERTIES



MODE NO.	FREQUENCY WITH JOINTS (HZ)	FREQUENCY W/O JOINTS (HZ)
1	35.9	50.4
2	100.7	118.3

JOINT NO.	COMPLIANCE RAD/IN-LB
1	.1 -7
2	.1 -7
3	.1 -7
4	.1 -7

FIGURE 4-2
NON-UNIFORM BENDING BEAM
SOLUTION FOR THREE JOINT COMPLIANCES
USING TWO MODES, r = 25%

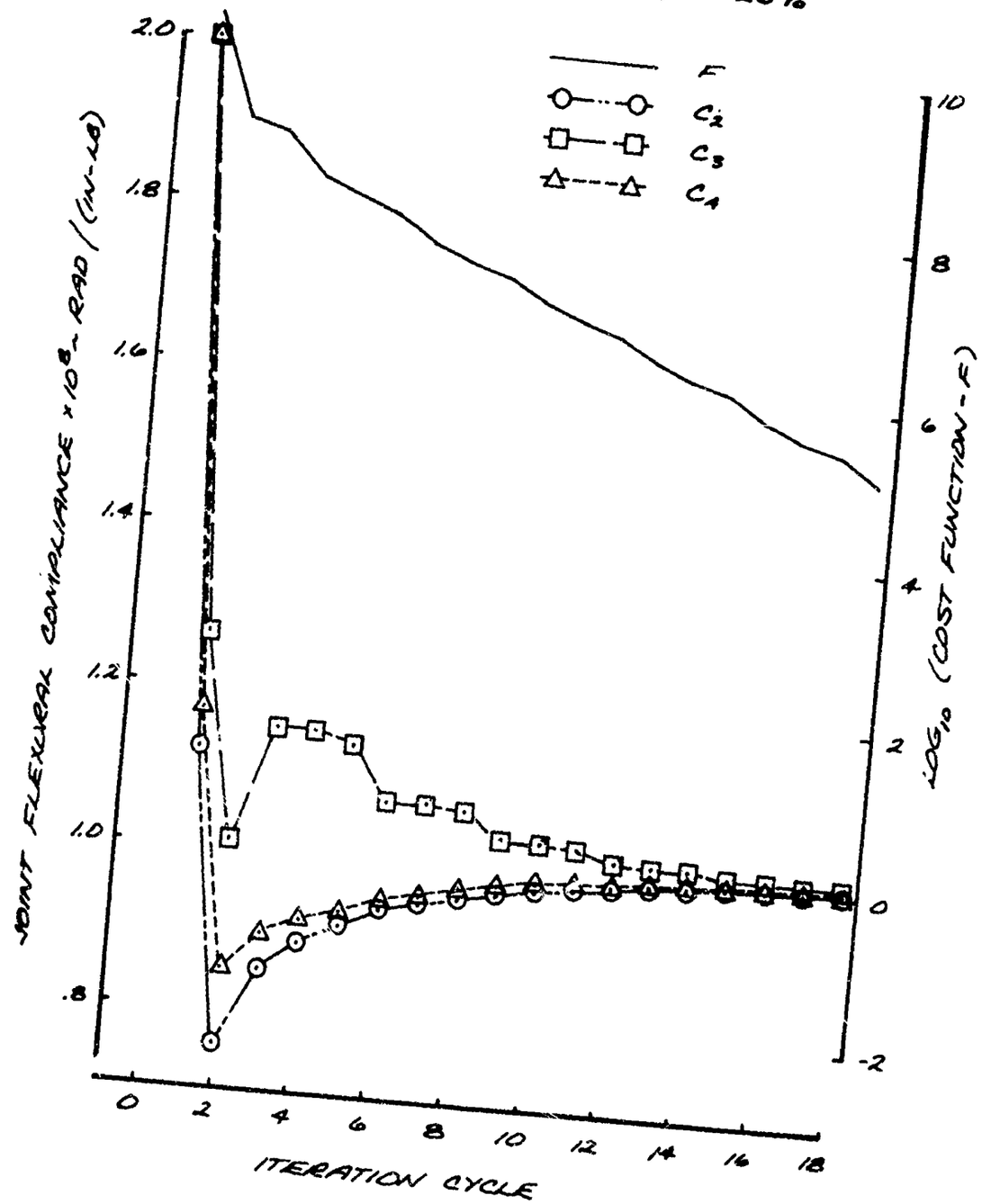


FIGURE 4-3

NON-UNIFORM BENDING BEAM
SOLUTION FOR THREE JOINT COMPLIANCES
USING TWO MODES, r = 1%

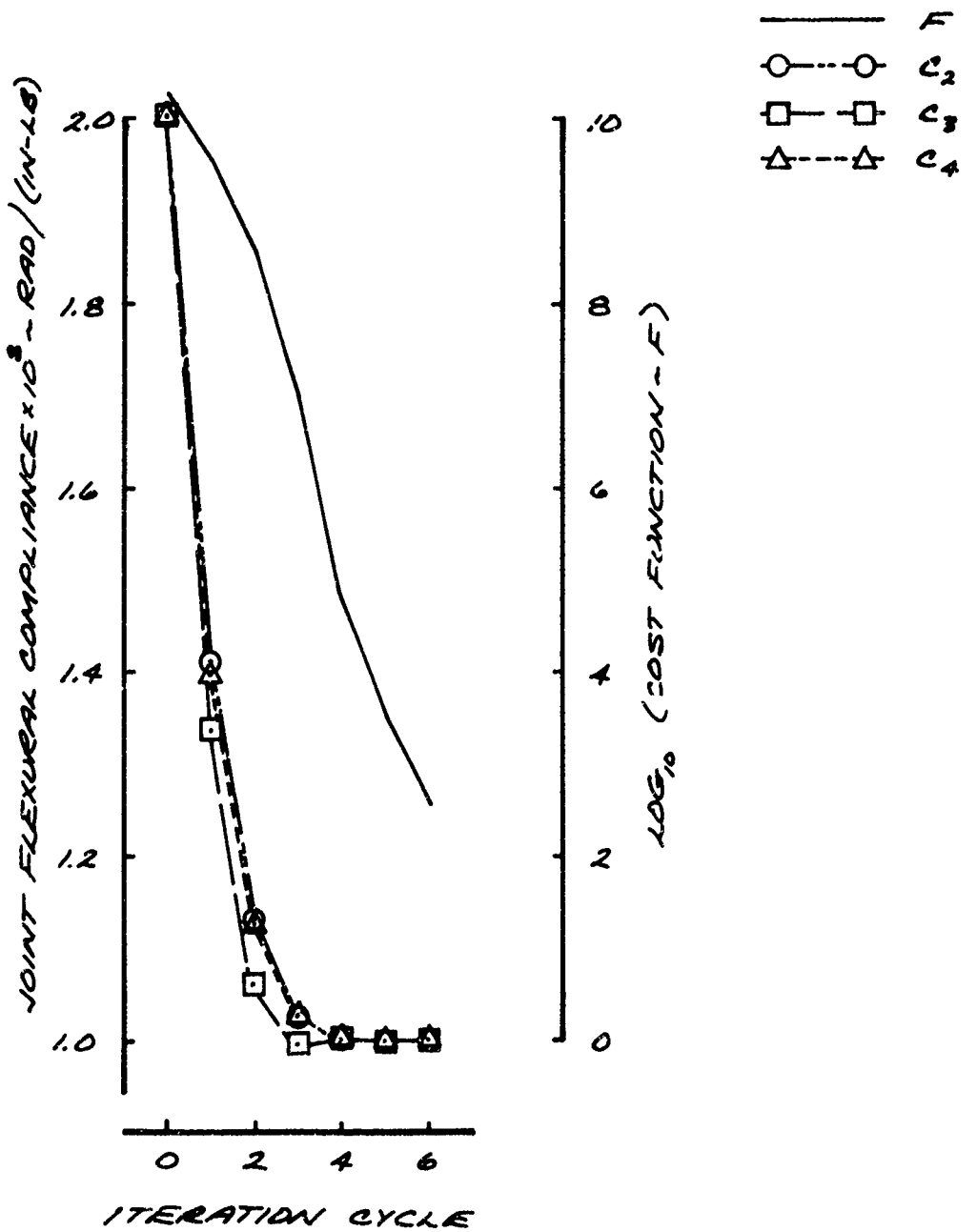


FIGURE 4-4

NON-UNIFORM BENDING BEAM
CONVERGENCE VS. INTERMEDIATE STEP SIZE - r
SOLVING FOR THREE JOINT COMPLIANCES
USING TWO MODES

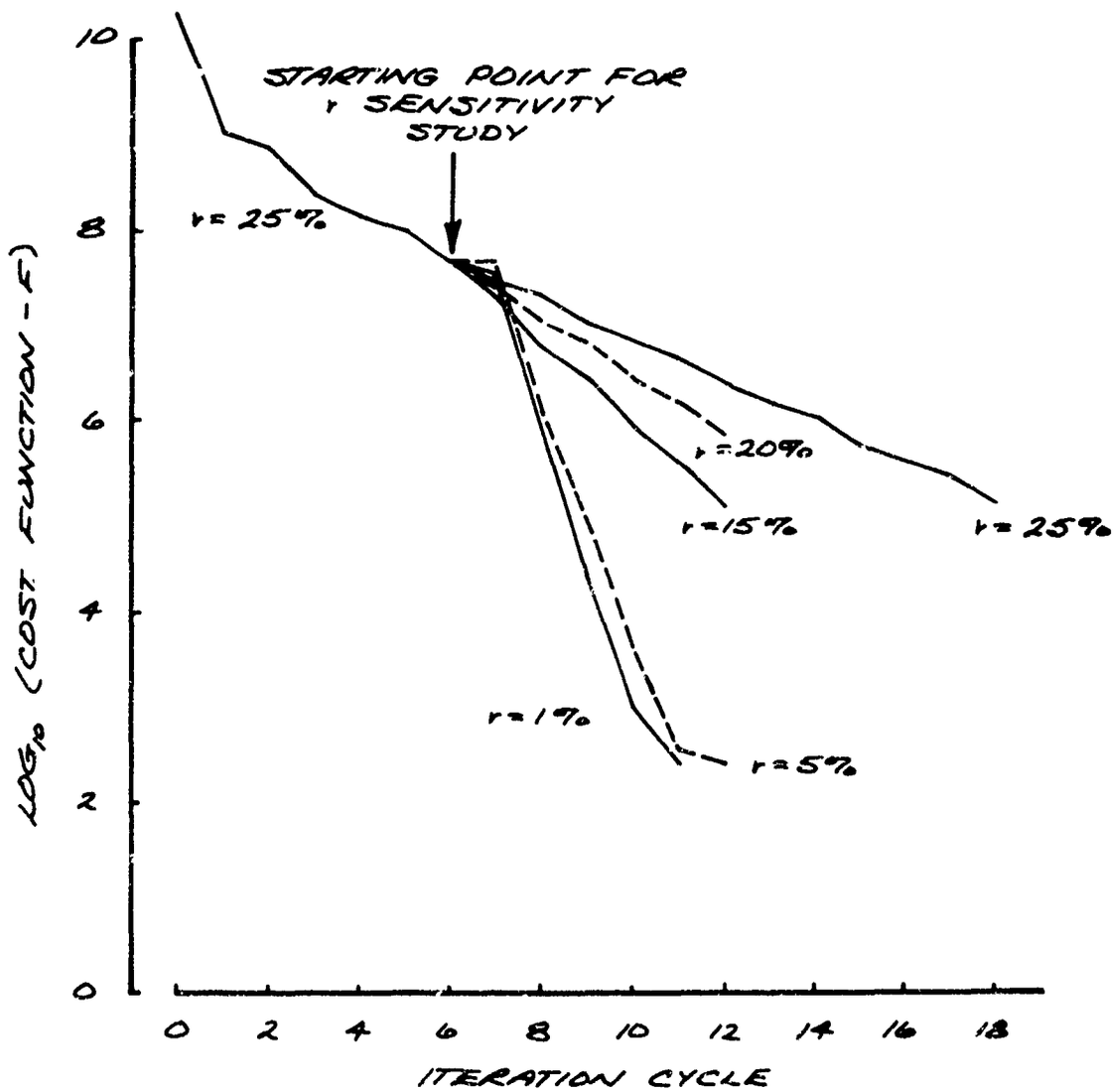


FIGURE 4-5

TACTICAL MISSILE MEASURED BENDING MODES
FIRST MODE $f_E = 59.3$ Hz

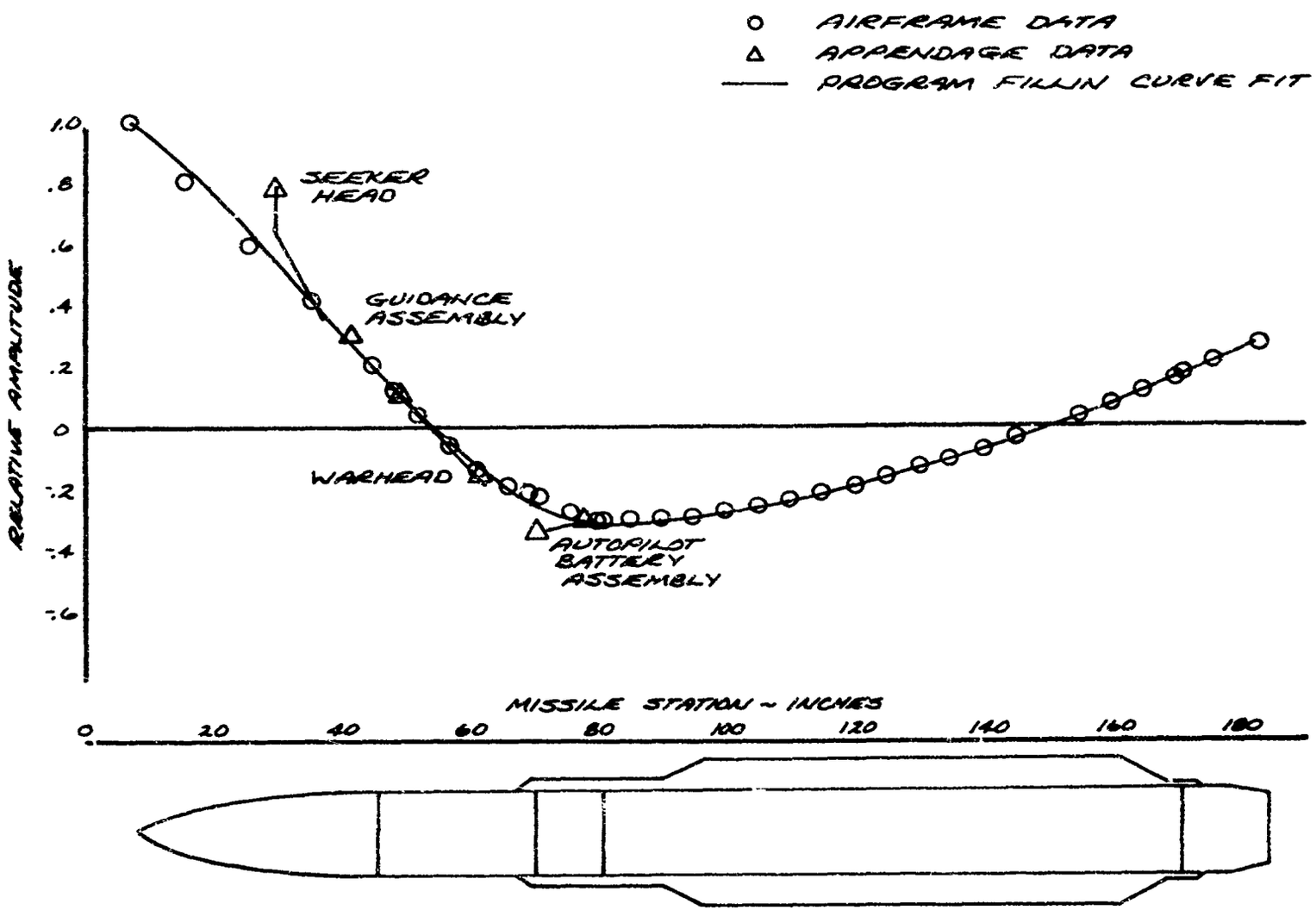


FIGURE 4-6

TACTICAL MISSILE MEASURED BENDING MODES
SECOND MODE $f_E = 116$ HZ

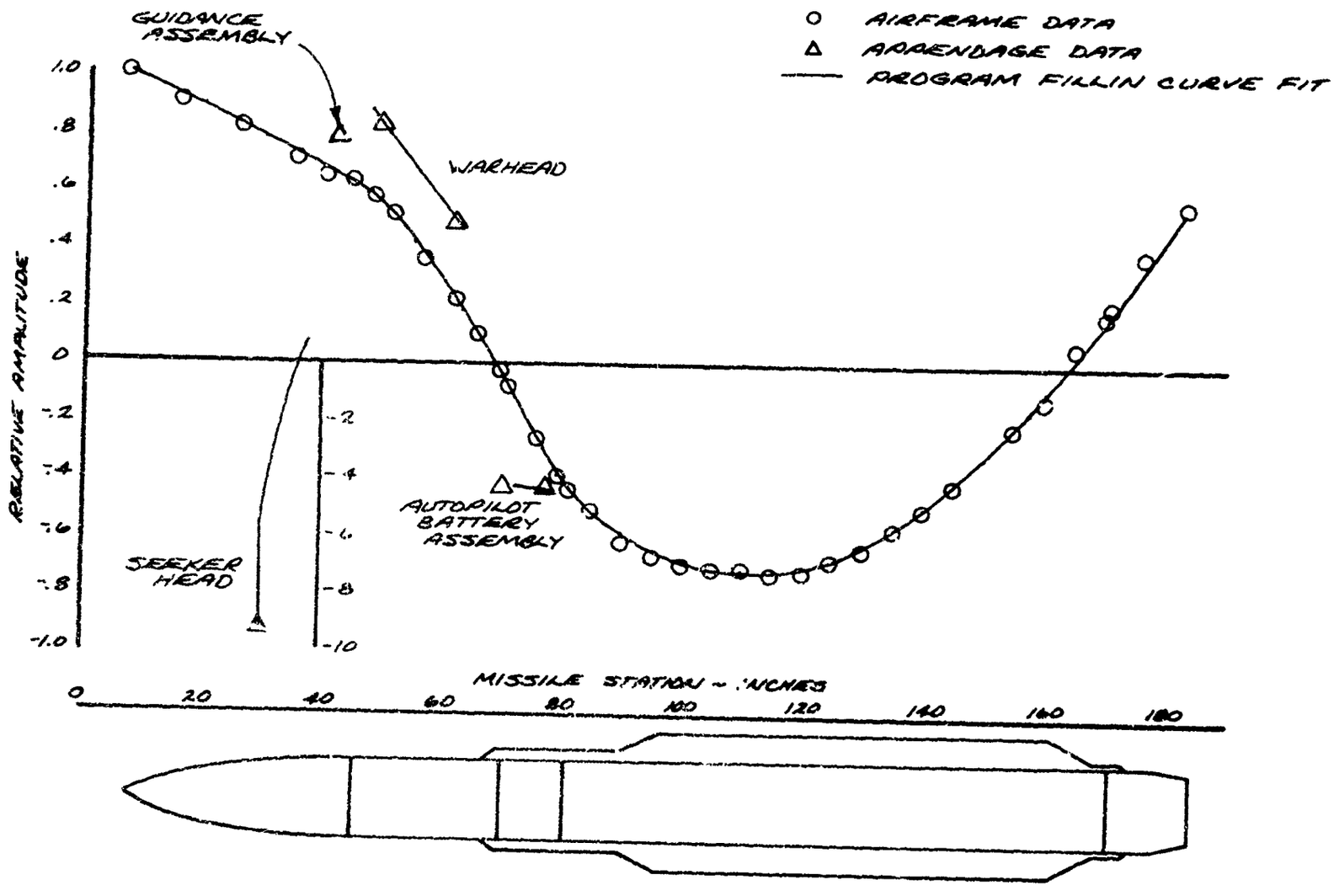


FIGURE 4-7

TACTICAL MISSILE MEASURED BENDING MODES
THIRD MODE f_E = 153 HZ

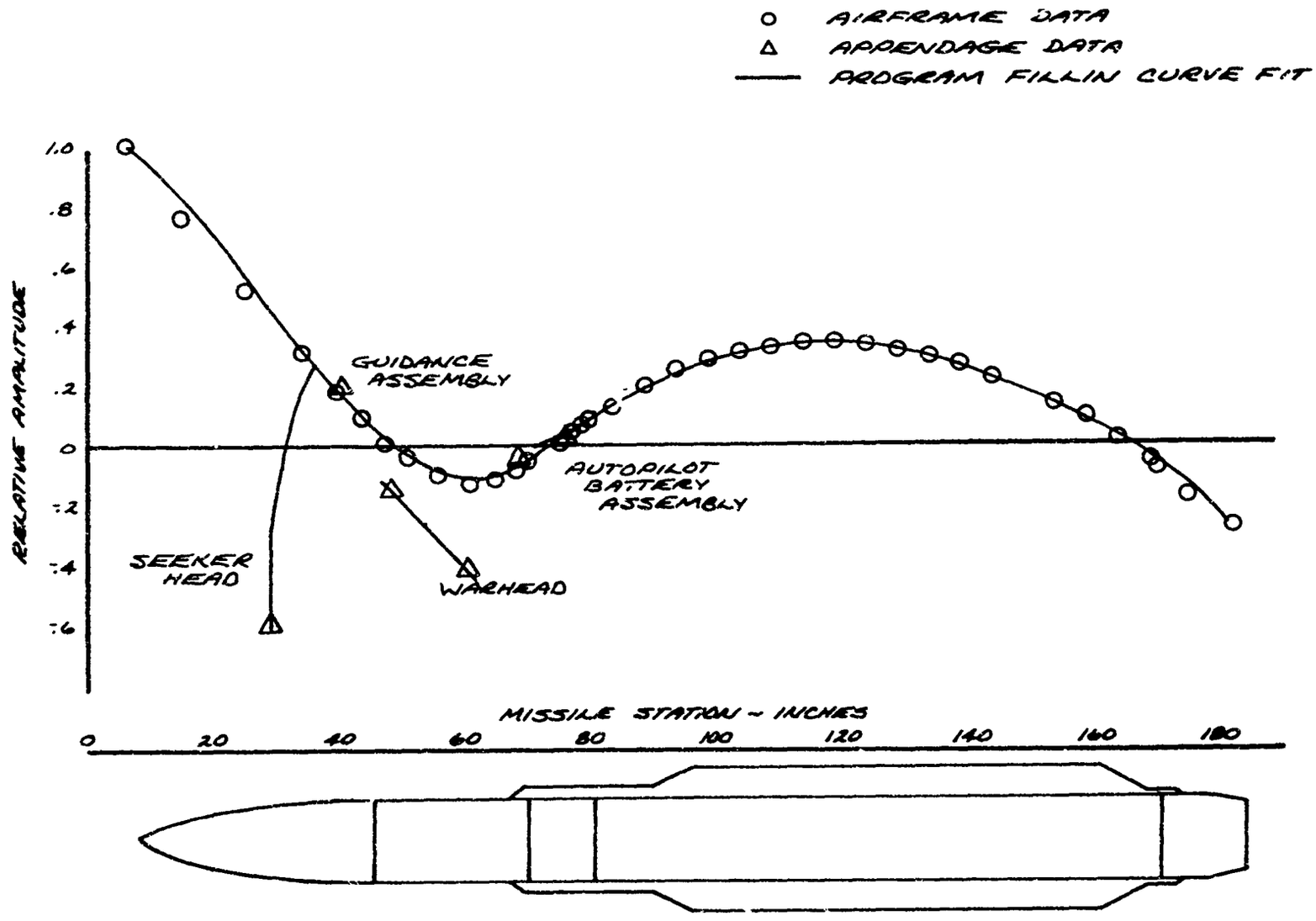


FIGURE 4-8

TACTICAL MISSILE APPLICATION
SOLUTION NO. 1
EQUAL WEIGHTING FACTORS

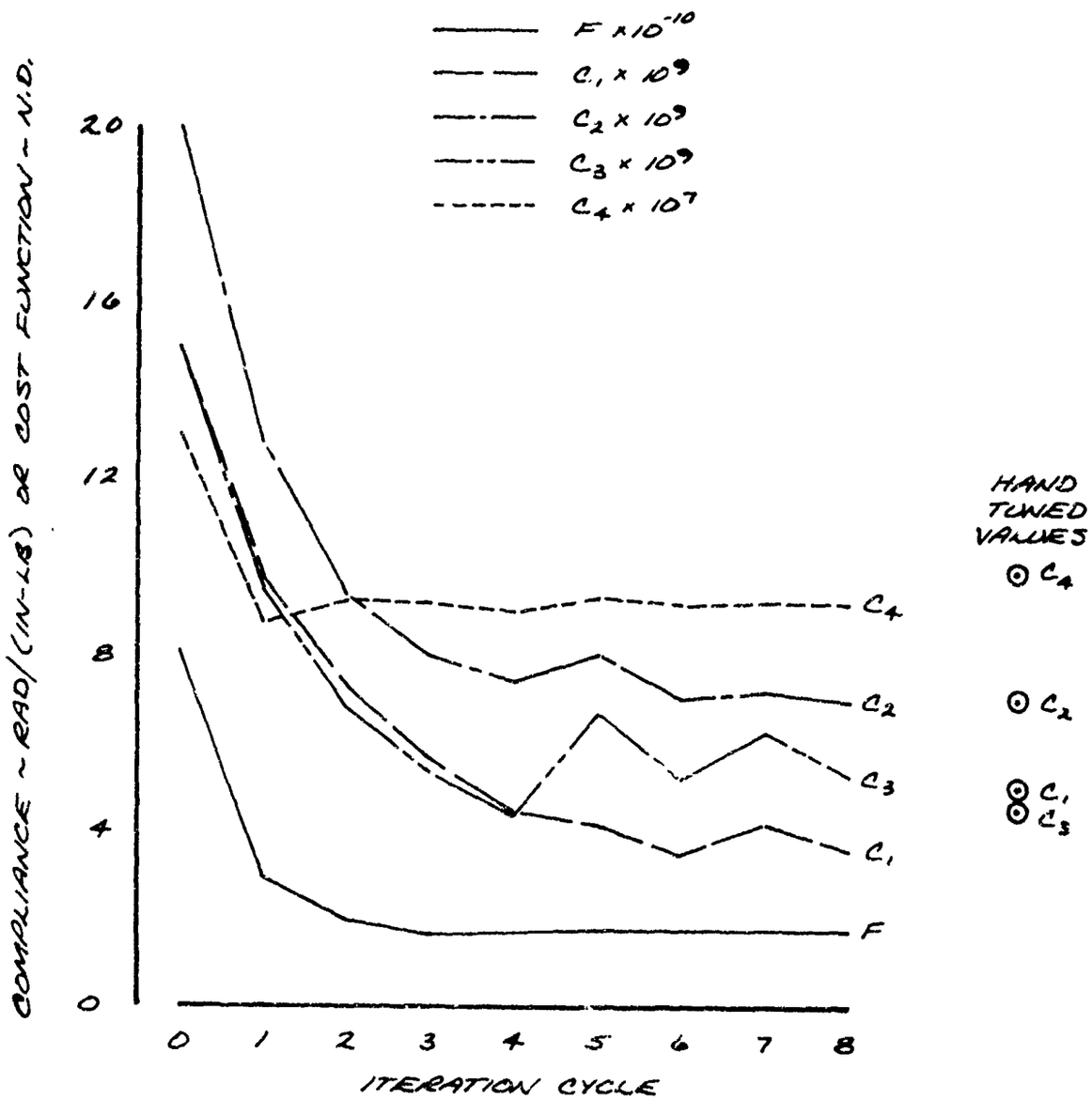


FIGURE 4-9

TACTICAL MISSILE APPLICATION
COMPARISON OF EXPERIMENTAL AND THEORETICAL FIRST MODES

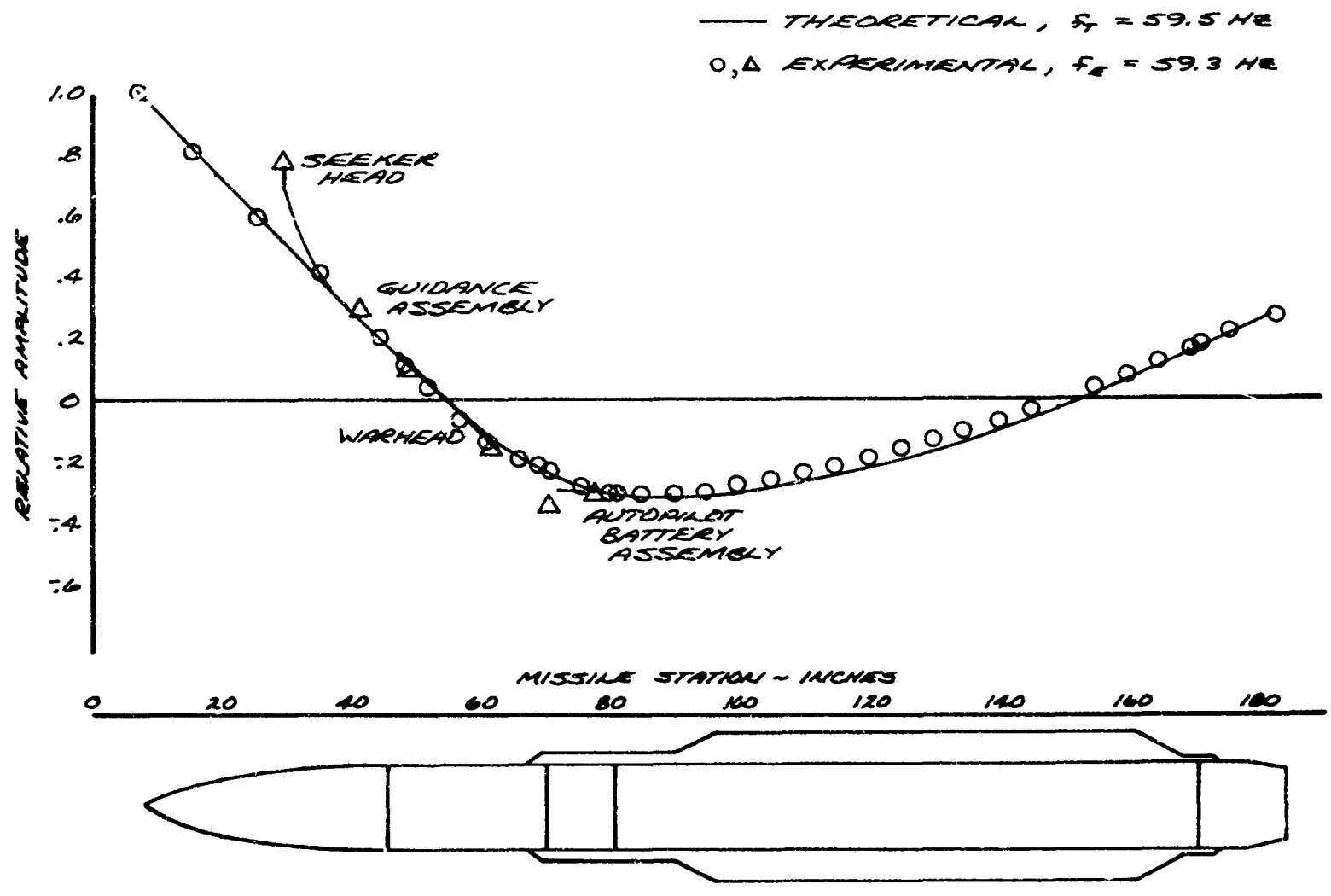


FIGURE 4-10

TACTICAL MISSILE APPLICATION
COMPARISON OF EXPERIMENTAL AND THEORETICAL SECOND MODES

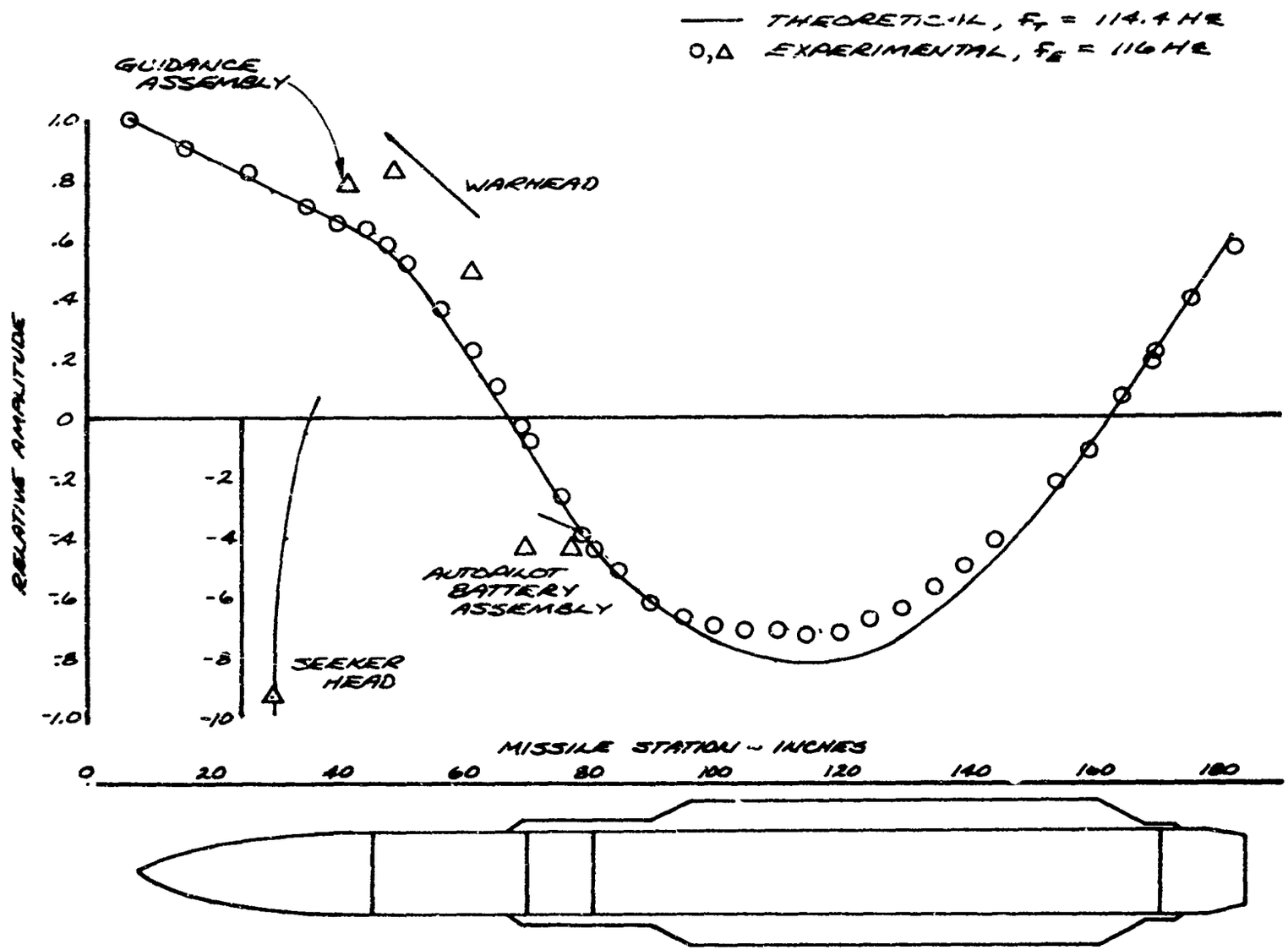


FIGURE 4-11

TACTICAL MISSILE APPLICATION

COMPARISON OF EXPERIMENTAL AND THEORETICAL THIRD MODES

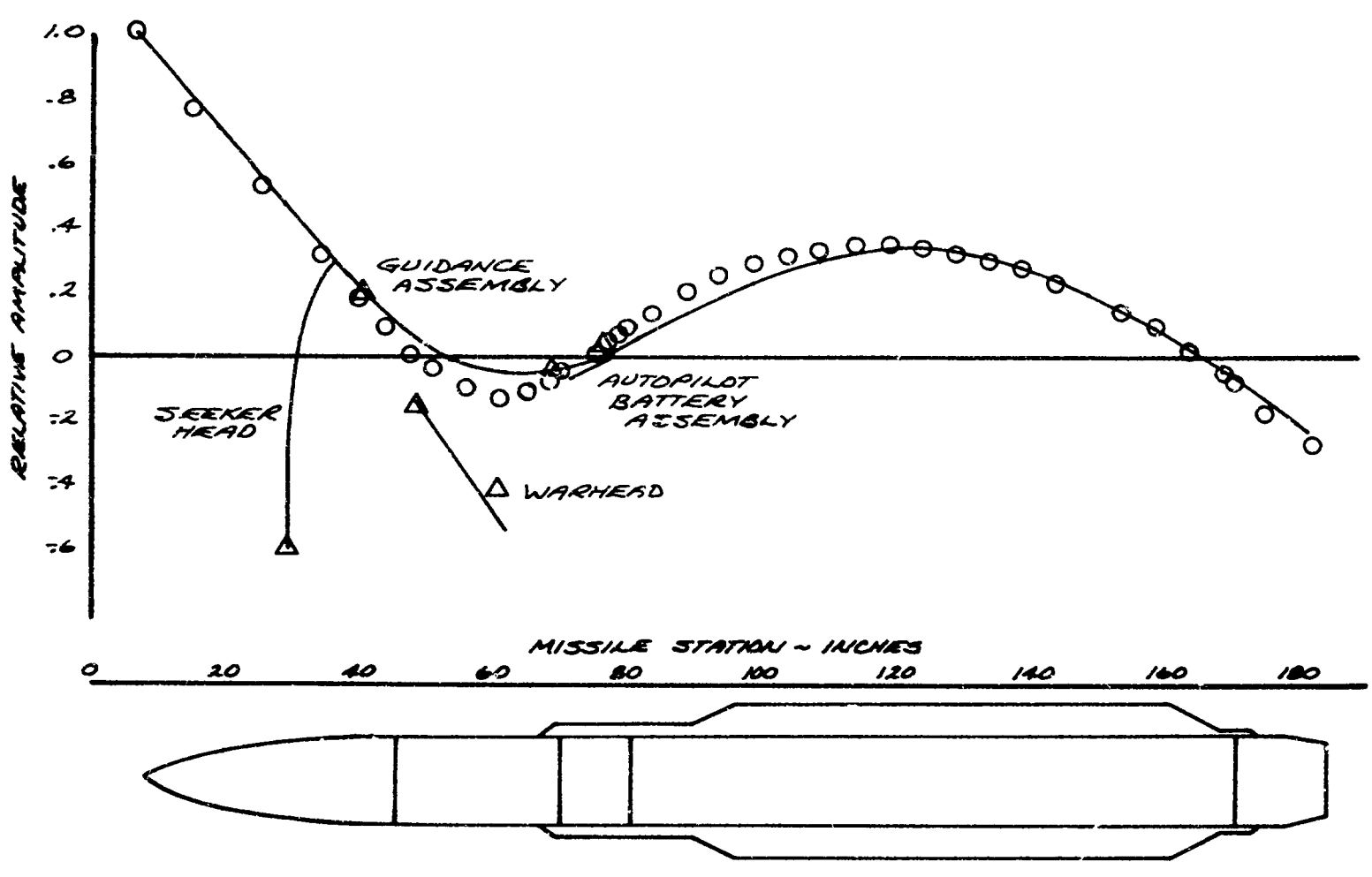
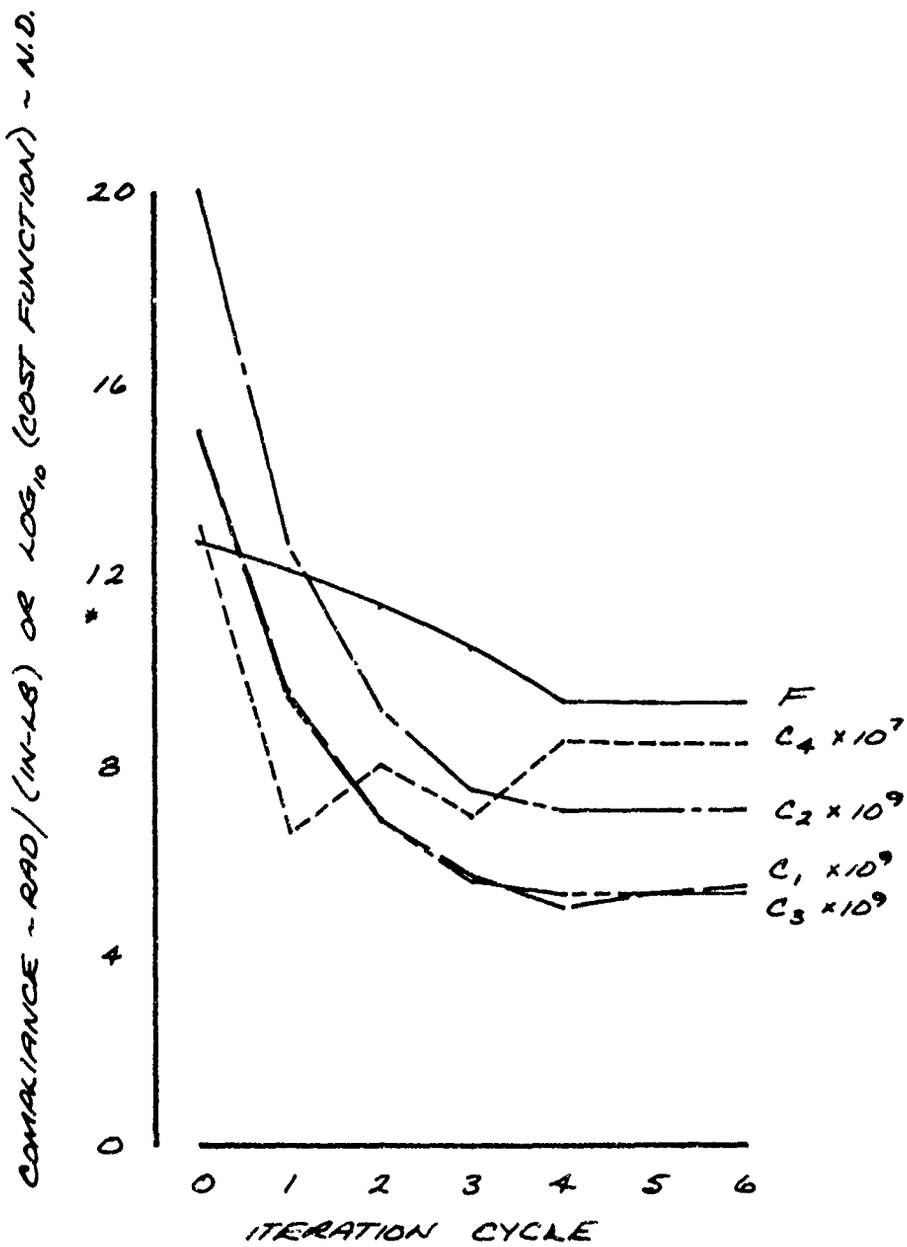


FIGURE 4-12

TACTICAL MISSILE APPLICATION
SOLUTION NO. 2
UNEQUAL WEIGHTING FACTORS



Section 5.0

MISSILE JOINT SELF INDUCED VIBRATION

Tactical missile airframe joints can become significant sources of mechanical shock and vibration under transient loading conditions which exceed mating surface interface preloads. If mating surface separation and impact occurs, shock transients generated at the interface will propagate from the airframe joints throughout the missile structure. Under oscillatory loading conditions, the repetitive shock transients - modified by strain wave reflections - often assume the appearance of broadband vibration when monitored at missile components.

One obvious potential problem area with noisy joints can occur in laboratory sinusoidal vibration testing where the test conditions are specified in terms of displacement or acceleration input at the test fixture/specimen interface. Since only the fundamental input levels at the excitation frequency are usually controlled, a significant overtest can result from uncontrolled broadband vibration induced by mechanical joint interface impact.

The vibration environment source characteristic can also be of concern in the case of air launched missiles which are often exposed to many captive flight hours. Excitation of comparatively low frequency aircraft and missile modes by aerodynamic turbulence and/or buffet may result in the secondary generation of high frequency vibration due to mechanical interface impact within missile airframe joints and in some instances at aircraft interface contact points such as sway brace pads and lugs.

Recent tactical missile flight vibration measurements, furthermore, provide suspicious evidence that for some current missile designs the joints may be a prime contributor to missile flight vibration and shock environments. If this premise is valid, then improvements in missile joint design may yield significant reductions in environmental exposure and support cost saving relaxations in environmental specifications.

This section presents the results of an exploratory investigation of the mechanism of joint self induced vibration and an initial evaluation of possible methods for control and suppression. The scope of the investigation has included tests of both full scale actual missile joints and an idealized subscale joint model. A design concept for a joint interface treatment to suppress self induced vibration involving flame deposited teflon was developed in missile section level testing with sufficient promise to warrant missile round level flight test evaluation. Test results from both laboratory section level (encouraging) and flight missile level (inconclusive) are reviewed and discussed. Due to the inconclusive results obtained in the missile level testing, a sub-scale

idealized joint model was designed with the objective of isolating and controlling some of the more elusive full scale test parameters. The model test results, while exhibiting some scatter, do show consistent trends and a significant improvement in joint preload, damping, and mechanical noise reduction when a teflon coating is present at the model joint interfaces.

More work clearly remains to be done in this area. The investigation thus far has shown that joint interface impact can be a powerful source of broadband vibration and that interface coatings can effect a substantial improvement in joints exhibiting these characteristics.

5.1 FULL SCALE LAB TESTS

The full scale joint designs selected for consideration in this study include a discontinuous land ring joint shown in Figure 5-1 and a continuous split ring joint shown in Figure 5-2. Both of these joints are highly compliant (rated about "moderate' under the classification basis discussed in Section 2.0) with comparatively low interface contact preload (estimated to be approximately 12 pounds/inch) under design assembly torques. The low preload is best illustrated by the fact that in one tactical missile application, with the discontinuous land ring joint, the assembly preload is well exceeded in a one g environment; i.e. the static moment produced by the missile structure forward of the joint is nearly twice the preload induced moment.

Ring joints of this type have consistently demonstrated a capacity for generating joint interface impact vibration in section level vibration testing. In one instance of sinusoidal vibration testing of a missile guidance section, a 3g sweep was observed to produce 20g broadband when the fundamental passed through a joint impact resonance.

The initial hypothesis in searching for a fix for this behavior was that compliant material placed on the contacting surfaces of the joint would inhibit metal to metal impact and thus materially reduce the resulting vibration. It was further conjectured that any adverse effect of this compliant material on joint stiffness could be offset by a general improvement in load distribution resulting from filling voids and irregularities in the mating surfaces. Each of the ring joint designs has 3 contacting surfaces - two associated with the ring nut and subject to abrasion as the surfaces slide in contact during assembly, and one where the missile shroud sections butt together. With practical manufacturing tolerances, a perfect fit on the mating surfaces is virtually never achieved. The uncertain and variable load paths due to this feature are viewed as a major contributing factor to both high compliance and noise generation characteristics. Another obviously important parameter is the joint preload, with any increase achieved either through higher assembly torques or reduced friction in the sliding surfaces (threads) being beneficial.

A variety of candidate joint interface materials including epoxy, RTV, plastics, elastomers, and soft metals such as lead and aluminum were selected for evaluation. These materials, in general, were only introduced on the non-sliding surfaces of the joint. Epoxy and RTV were applied also to the sliding surfaces with the expectation that most of the coating would be wiped off points of contact but that some of the voids in the mating surfaces might be filled. The test set-up used to determine the effect on joint self induced vibration, shown in Figure 5-3, consisted of a missile nose section cantilevered from a discontinuous ring joint attached through a test fixture to an oil slide table. The basic test specimen when driven at resonance would exhibit an abrupt increase in broadband vibration when the joint preload was exceeded with the ratio of broadband to fundamental response at the joint exceeding a factor of 8 for one test point. The test was then repeated with each of the joint interface materials using a constant assembly torque and recording broadband (20 5000 Hz) response at the joint for several reference fundamental response levels. Table 5-1 presents the results obtained with the different interface coatings for two dynamic bending moment levels at the ring joint interface. These data should be considered qualitative at best with the test results generally showing poor repeatability with large variations for small changes in test conditions. The exception to this was the Teflon configuration which showed not only the best performance from the standpoint of minimum impact noise but also good repeatability and consistency in subsequent re-tests.

It should be noted that the teflon configuration represented the first effort to coat the sliding surfaces of the joint. Flame deposited teflon has sufficient bond strength on the coupling ring and low friction on the sliding surfaces to remain intact and not be wiped off the contacting surfaces during joint assembly. The low friction on the sliding surfaces in fact undoubtedly accounts for a major portion of the substantial improvement shown for this configuration by producing a large increase in joint interface preload for the same torque. The teflon coating was applied only to the coupling ring, rather than all joint contacting surfaces, not by choice but by expedience since the coating process was performed out of plant. One other potentially important characteristic of the teflon was observed to be an apparent significant increase in effective structural damping for the test specimen, with larger shaker output required for the same bending moment response. Based on these admittedly limited but encouraging results, the use of teflon on ring joint interfaces was concluded to have shown sufficient promise to warrant missile level evaluation.

5.2 MISSILE LEVEL QUALIFICATION AND FLIGHT TEST

A continuing series of test firings for an advanced version of a surface launched missile planned for the Spring of 1973 offered an opportunity for missile level flight evaluation of the effect of teflon coated joints on missile flight vibration. Environmental data obtained

on earlier flights of essentially the same missile airframe with unmodified joints provided a direct basis for comparison. The missile configuration in question employs six primary joints. Three of which are ring joints, two being of the discontinuous land type and one of the continuous split ring type. The remaining three joints are of the tension bolt type, considered to be very stiff and sufficiently preloaded under assembly torques to preclude any separation under flight loads. The missile profile and joint locations are shown in Figure 5-4.

A decision was made to treat only the ring joints and furthermore to confine the teflon coating to the coupling rings, recognizing that one of the interfaces for each joint, as was the case in the lab test configuration, would not be teflon coated. Prior to design release and acceptance for flight of this missile joint modification, several possible issues needed to be resolved in securing a design requalification. This effort included:

1. Proof load tests of the modified joints to demonstrate that the teflon coating had not compromised structural integrity.

2. Creep tests to provide assurance that missile assembly preloads (albeit low in the case of the ring joints) would not be seriously degraded.

3. Further lab evaluation to confirm the expected noise suppression characteristics of the teflon.

One facet of this phase of the investigation was a concerted attempt to devise a means for measuring the interface preload - both for the basic and teflon coated joints. This effort, unfortunately, was largely unsuccessful, precluding definition of this important parameter which would have been particularly useful in interpreting dynamic response and creep characteristics. Proof loads were successfully applied to the joints in question without incident, and the creep issue was qualitatively resolved by retorqueing control joints after suitable aging and noting that no relative motion of the joint coupling ring occurred.

Joint impact noise suppression tests were carried out using essentially the same test set-up shown in Figure 5-3. In this case, however, three different test fixtures were required to represent the three different joint locations on the missile airframe. The test results for the three joints are plotted in Figure 5-5 in terms of noise suppression achieved by the teflon coating versus the basic joint noise factor, with these parameters defined as follows:

g_F = in-plane fundamental response at the joint

g_{BB} = in-plane broadband response at the joint (20-5000 Hz)

$g_N = \vec{g}_{BB} - \vec{g}_F$ = in-plane noise at the joint

(g_N/g_F) = joint noise factor

$(g_N/g_F)_T/(g_N/g_F)_B$ = joint noise suppression factor - a ratio of teflon coated joint noise factor to basic joint noise factor.

The test results obtained in this series showed considerably less improvement in joint noise characteristics with teflon coated coupling rings than had been observed in the earlier testing. Previous lab data for Joint 1 are shown for comparison. Joint 3 at low response levels was "quieter" in the basic configuration than with teflon for the one specimen tested, although the performance of the teflon configuration improved rapidly as the excitation level was increased. Data points connected by straight lines in Figure 5-5 reflect the two different response levels for the same joint. These data would appear to indicate that "quiet" joints do not admit much improvement while considerable benefit from the teflon coating might be expected with "noisy" joints.

Since the teflon coated rings had satisfactorily passed all design qualification requirements, the configuration was released for flight test evaluation. A total of four instrumented test flights were made with complete data acquisition. From the standpoint of showing an improvement attributable to the teflon coated coupling rings, however, the flights were uniformly disappointing being virtually indistinguishable from the earlier flight series with the basic unmodified joints.

Possible interpretations of this test outcome include:

1. The importance of coating all three joint interface surfaces rather than just two may have been underestimated. Lab testing could have been misleading in this respect if excitation levels relative to joint preloads were not representative of the flight conditions.

2. Joint impact may not be a significant contributor to the flight vibration environment for this missile configuration. In this case, improvements in the joint response characteristics would not have been noticed.

In hopes of answering some of the questions associated with joint self induced vibration, an idealized ring joint model which would admit more precise measurements of the critical parameters was designed and tested.

5.3 JOINT IMPACT MODEL DESIGN AND TEST

The ideal test specimen for joint impact modeling was visualized (as in previous joint investigations) as a simple uniform structure with a single ring joint replica at the mid-span. Free-free boundary conditions would be used to avoid uncertainties in support constraints. As a result, the primary joint characteristics of interest (compliance, damping, impact noise generation) would dominate and be deducible from the test specimen dynamic response. The model joint replica design, while permitting considerable simplification, was required to simulate all of the important properties of a typical full scale missile ring joint including compliance, low interface preload, and similar assembly and interface contact characteristics. Additionally, the joint replica design approach must provide accurate and reliable means for measuring joint interface preload versus applied torque during assembly and as a function of time during creep investigations.

The joint replica designed to satisfy these requirements is illustrated in Figure 5-6. Joint preload is accomplished through a single strain gaged bolt on the center line of the aluminum test specimen, with this preload reacted circumferentially through a separate joint ring representing multiple joint interface contact surfaces. Interchangeable stainless steel "joint rings" provide a convenient means for investigating the effects of various joint interface materials. The model joint compliance is assumed to be provided primarily by the extensional elasticity of the center axis bolt estimated as follows:

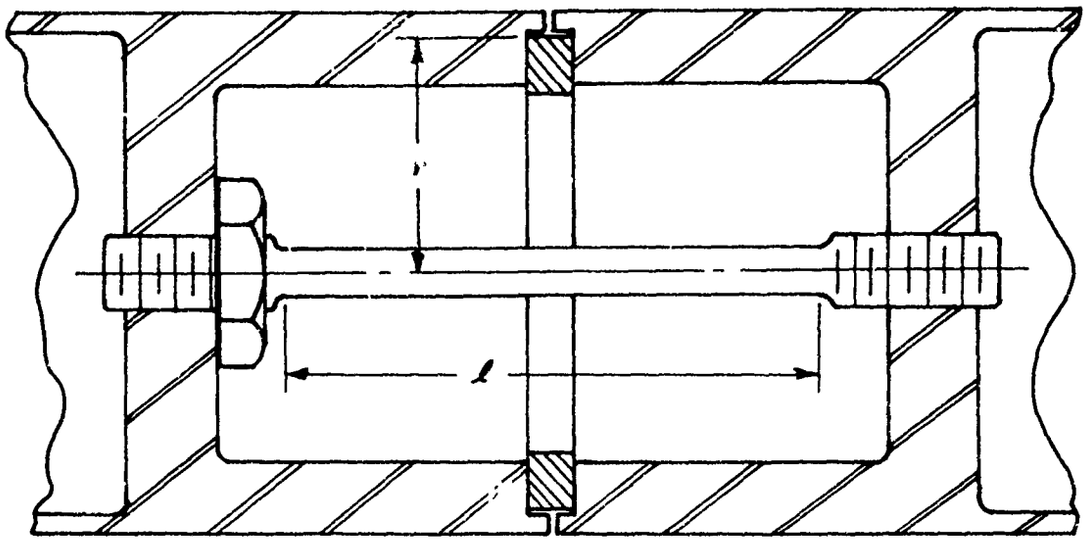
$$C_{\theta} = \frac{\ell}{r^2 A E} \tag{5.1}$$

where: ℓ = effective spring length, 3".

r = effective radius, 1.265 inches.

E = modulus of elasticity, 30 $(10)^6$ #/in^2.

A = cross sectional area of spring elements, in^2.



The center axis bolt is locked to one half of the model with a locking nut and the model assembled by applying preselected torques to the other half of the test specimen. The threads on the center axis bolt are lubricated to insure that the primary frictional torques in the joint assembly are associated with the contacting surfaces on the interface ring. The full scale ring joints described in Section 5.2 have estimated compliances ranging from $0.75(10)^{-8}$ to $2.7(10)^{-8}$ rad/in # and fall in the moderate to good joint compliance classification scale. A corresponding range for the model joint compliance was provided by making three center axis couplers with diameters from 1/8 to 3/8 inches. A direct comparison between model and full scale joint compliance is obtained by multiplying the full scale values by the cube of the full scale to model diameter ratio as follows:

CONFIGURATION	$C_\theta(10)^6$ Rad/In #
Full Scale X $(D_F/D_M)^3$	.88 - 3.2
Model	.57 - 5.1

Where: D_F = Full scale Missile Diameter, 13.5 inches

D_M = Model Diameter, 2.75 inches

5.3.1 Model Joint Preload. The relationship between joint preload - measured by strain gages on the center axis tension bolt - and applied torque was investigated for three joint interface coatings in addition to the basic clean dry joint. The results of these measurements are shown in Figure 5-7. The teflon coating, approximately 3 mils thick,

was flame deposited by an application process identical to that used on the full scale rings discussed in Section 5.2. The Molybdenum Disulfide (MDS) Dry Film was applied using an aerosol spray; and the Silicon Grease, DC-4, was directly wiped on the joint interface surfaces. A thorough cleaning of the joint interfaces with solvent was performed between each test of a different coating material.

Both of the lubricants, MDS and DC-4, resulted, as might be expected, in a fairly significant increase in joint preload, ranging from 60 to 100 percent. The teflon coating, however, produced the largest increase in joint preload with a consistent and repeatable gain of greater than 5 over the basic unlubricated joint.

Teflon has a well recognized tendency to cold flow under load. To assess the implications of this behavior on the preload of a joint with teflon on the interface surfaces, a preload of 600 pounds was applied to the model joint and found to have been maintained with virtually no change after 64 hours. The estimated loading on the teflon for this condition was 318 psi, assuming uniform distribution over the joint interface.

5.3.2 Model Vibration Test Setup and Results. A sketch of the test setup used to evaluate the dynamic response characteristics of the ring joint model is shown in Figure 5-8. A free-free suspension was employed with the model oriented vertically to avoid any gravity moment bias on the joint. Force excitation was provided by an MB Electrodynamic Shaker, rated at 50 pounds peak force capability, monitored by a force gage at the input station on the test specimen. Triaxial response (acceleration) was monitored at the top end of the specimen to establish a total response reference, and both force and in-plane acceleration at the input station were monitored to provide a basis for estimating system damping. Although vibration induced by joint interface impact is propagated in all response coordinates, the longitudinal response ($\ddot{x}$) was concluded to provide the primary and most sensitive measure of joint impact induced response. The impact forcing function is assumed to be impulsive in nature with primary excitation at twice the transverse mode frequency with the response distributed over a broad frequency spectrum. Total impact induced noise was interpreted as the rms vibration over a 20-5000 K hz bandwidth measured in thelongitudinal coordinate (x) at the response station on the test specimen. This broadband vibration level was then normalized by the vector sum of the inplane and crossplane transverse response at the excitation frequency to establish a noise ratio for the particular test condition.

Table 5-2 presents response data for the basic configuration with uncoated metalic surfaces at the joint interface. Test parameters include variations in both joint preload and excitation level. Estimates of system damping shown are based on calculated generalized mass and

generalized force in the model response. The general trend is for frequency to increase with response level. Corresponding data for the test specimen with teflon at the joint interface is presented in Table 5-3. Considerable scatter in the response parameters is shown for both configurations at the lower preload and excitation levels, reflecting the nonlinearities and cross coupling in the test specimen response. The two higher values for joint preload used with the teflon configuration (200 and 400 pounds) are intended to represent a conservative estimate of the preload increase which would be realized over the basic configuration (50 to 100 pounds) for the same assembly torque. Particularly noteworthy is the fact that the teflon configuration at the higher preload levels exhibits pronounced decreases in impact noise ratio accompanied by significant increases in resonant frequency. The predicted relationship between test specimen 1st mode frequency and effective joint compliance is shown in Figure 5-9. Upper bound frequency test points are shown for the basic configuration assembled with 50 to 100 pounds for comparison with the teflon configuration assembled first with equal preload (50 to 100 pounds) and then with "equal" torque (200 to 400 pounds preload). Table 5-4 presents a comparison of the basic and teflon configuration response based on an arithmetic average of all test data with the following conclusions:

1. For comparable preloads, the teflon coating on the model joint interface reduced joint impact vibration by an average factor of greater than 2 while increasing mode damping by an average factor of greater than 2.

2. For comparable assembly torques, the teflon configuration reduced joint impact vibration by an average factor of nearly ten while maintaining and slightly increasing the improved damping attributed to the teflon. Additionally, the effective joint stiffness was found to be nearly a factor of 3 greater than the basic joint for the same torque, presumably because of the significantly higher joint preload realized with teflon.

5.4 FULL SCALE IMPLICATIONS OF MODEL TEST RESULTS

1. Joint interface impact can be a significant source of self-induced vibration.

2. The vibration generation mechanism requires physical separation at the joint interface for impact to occur.

3. Corrective measures would appear to include increasing preload to avoid interface separation and/or coating the impacting surfaces with a compliant material to attenuate the response.

4. Teflon as a candidate material for joint interface treatment has been shown in idealized model tests to produce a

substantial improvement in joint preload, reduction in self-induced vibration, and increase in joint contribution to structural damping.

5. Conflicting and mixed results obtained with partial teflon treatment of full scale noise susceptible joints are suspected to have been caused by neglecting to coat all of the primary joint interface surfaces.

6. The results to date in exploring joint interface coatings have shown some encouraging trends. Many questions remain unanswered, however, and more work is clearly needed before practical applications can be considered in actual missile structure.

Table 5-1
Measured Noise Ratios for Discontinuous Land Joint with Different Surface Treatments
Constant Assembly Torque 4500 in #

Config.	Application	Response Level (1)	Noise Ratio (2)
Basic	Dry Film Lube (MDS) on All Surfaces	1 2	3.37 8.30
Epoxy	All Surfaces (with parting agent) to Fill Voids	1 2	1.36 5.45
RTV	All Surfaces	1 2	1.19 2.62
Lead	Foil Tape on Non-Sliding Surfaces Only	1 2	1.35 2.52
Aluminum	Foil Tape on Non-Sliding Surfaces Only	1 2	1.70 1.98
Silicone	Thin Sheet Non-Sliding Surfaces Only	1 2	2.10 2.01
Teflon	Flame Deposited on Coupling Ring Only	1 2	1.12 1.14

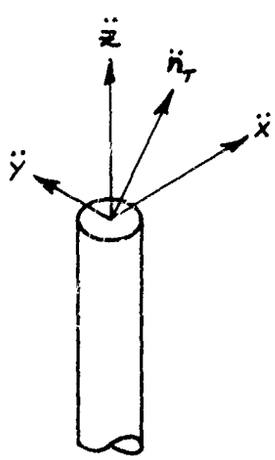
(1)

Response Level	Dynamic Bending Moment Induced at Joint
1	3000 in #
2	5000 in #

(2) Noise ratio defined as ratio of broadband response to fundamental response (g_{BB}/g_F)

Table 5-2
Basic Joint Model Dynamic Response

Preload #	Freq f_1 hz	$\ddot{n}_T$ g's	% Cross Plane	Noise Ratio	Damping ζ
50	101	9.9	110	.19	.0078
50	106	16.7	117	.66	.0077
50	103	22.2	119	72	.0049
75	107	7.4	93	.11	.022
75	108	18.6	124	.78	.0095
75	108	24.7	116	.63	.0079
100	110	9.9	108	1.42	.046
100	113	11.5	86	.45	.017
100	109	20.3	109	.84	.0098



Where:

$\ddot{x}$ = inplane response at f_i

$\ddot{y}$ = crossplane response at f_i

$\ddot{n}_T$ = vector sum $\vec{\ddot{x}} + \vec{\ddot{y}}$

$\ddot{z}$ = broadband (20-5000 hz) response

Noise Ratio = $\ddot{z} / \ddot{n}_T$

Table 5-3
Teflon Coated Joint Model Dynamic Response

Preload Comparable to Basic Joint

Preload #	Freq. Hz	g's	% Cross Plane	Noise Ratio	Damping
50	111	8.5	138	.088	.094
	110	18.7	124	.69	.0072
	111	21.0	107	.86	.0055
75	137	7.7	116	.072	.014
	134	8.1	127	.11	.013
	97	11.8	30	.13	.073
	101	18.8	20	.38	.060
100	94	6.1	35	.033	.042
	122	16.3	129	.41	.007
	101	13.5	27	.096	.059
	104	20.4	19	.27	.058

"Torque" Comparable to Basic Joint

Preload #	Freq. Hz	g's	% Cross Plane	Noise Ratio	Damping
200	114	7.9	51	.026	.031
	150	15.2	114	.19	.013
	119	12.4	45	.039	.037
	120	18.5	43	.092	.048
400	153	8.1	19	.031	.034
	151	15.9	22	.063	.053
	143	33.2	27	.048	.049

Table 5-4
Basic/Teflon Joint Model
Dynamic Response Comparison

Configuration	Comparison Basis	Preload Range #	Average Noise Factor	Average Damping %
Basic	Reference	50-100	.644	.015
Teflon	Equal Preload	50-100	.285	.032
Teflon	Equal Torque	200-400	.070	.038

Noise Factor Reduction:

Equal Preload .285/.644 = .44

Equal Torque .070/.644 = .11

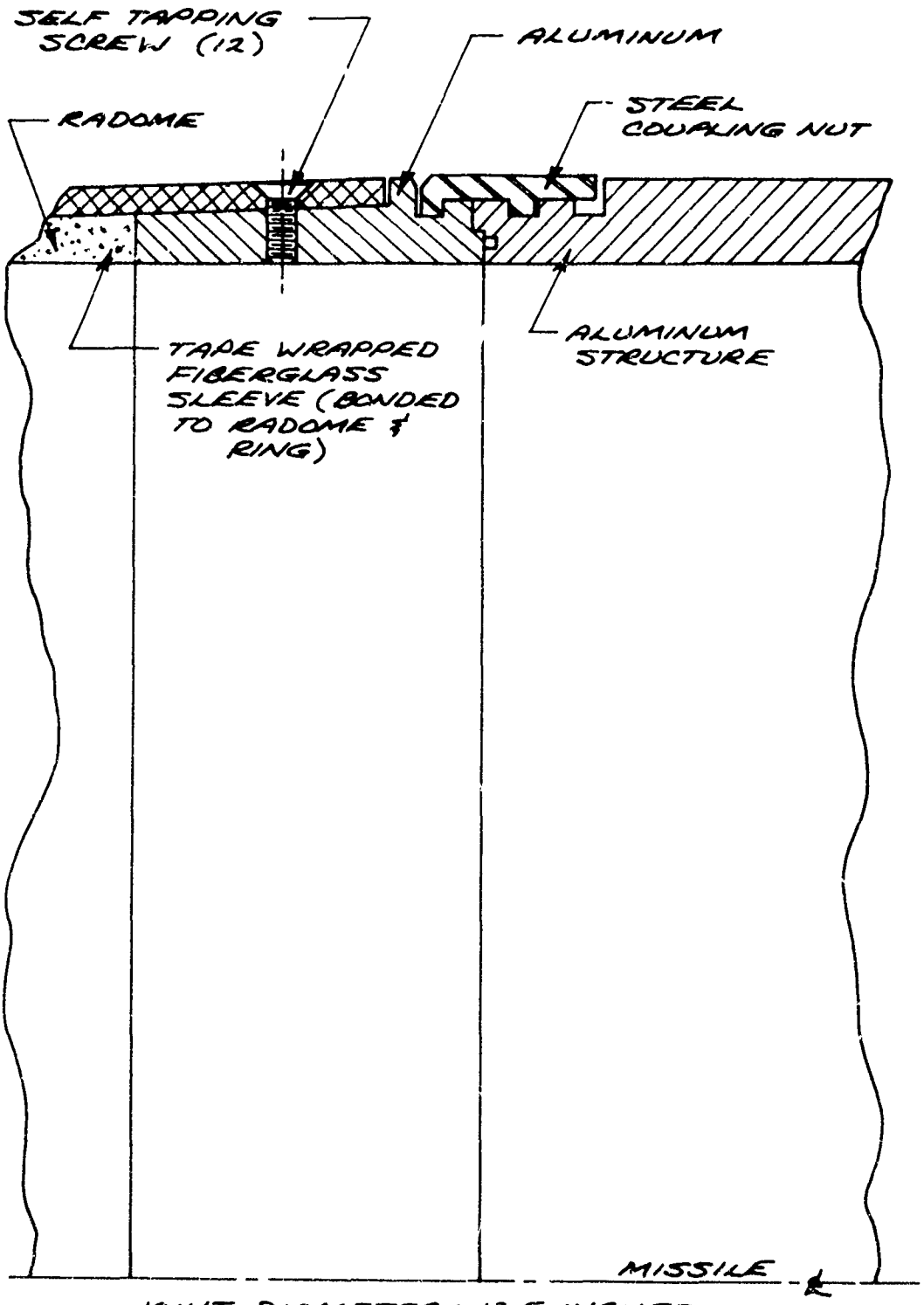
Damping Increase:

Equal Preload .032/.015 = 2.1

Equal Torque .038/.015 = 2.5

FIGURE 5-1

DISCONTINUOUS LAND RING JOINT

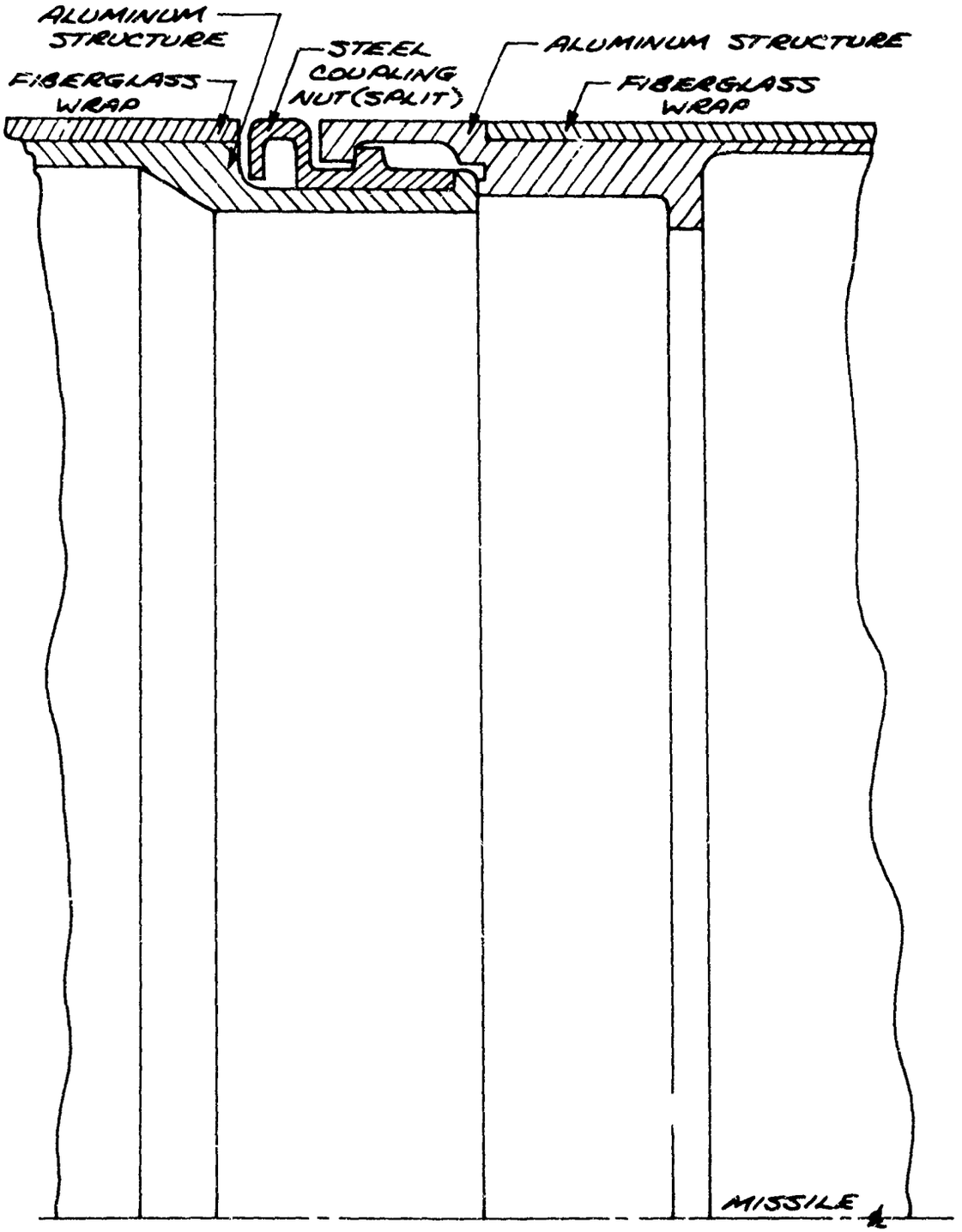


JOINT DIAMETER : 13.5 INCHES

SCALE : FULL

FIGURE 5-2

CONTINUOUS LAND RING JOINT



JOINT DIAMETER : 13.5 INCHES

SCALE : FULL

FIGURE 5-3

MISSILE JOINT INDUCED VIBRATION
TEST SET-UP

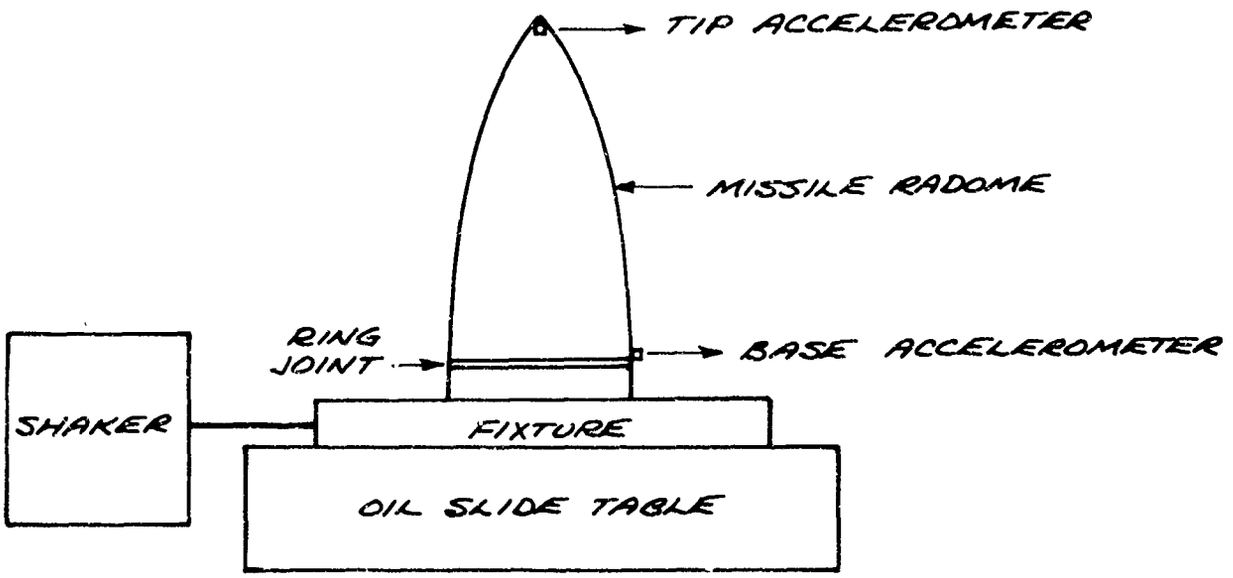


FIGURE 5-4

FLIGHT TEST MISSILE JOINT LOCATIONS

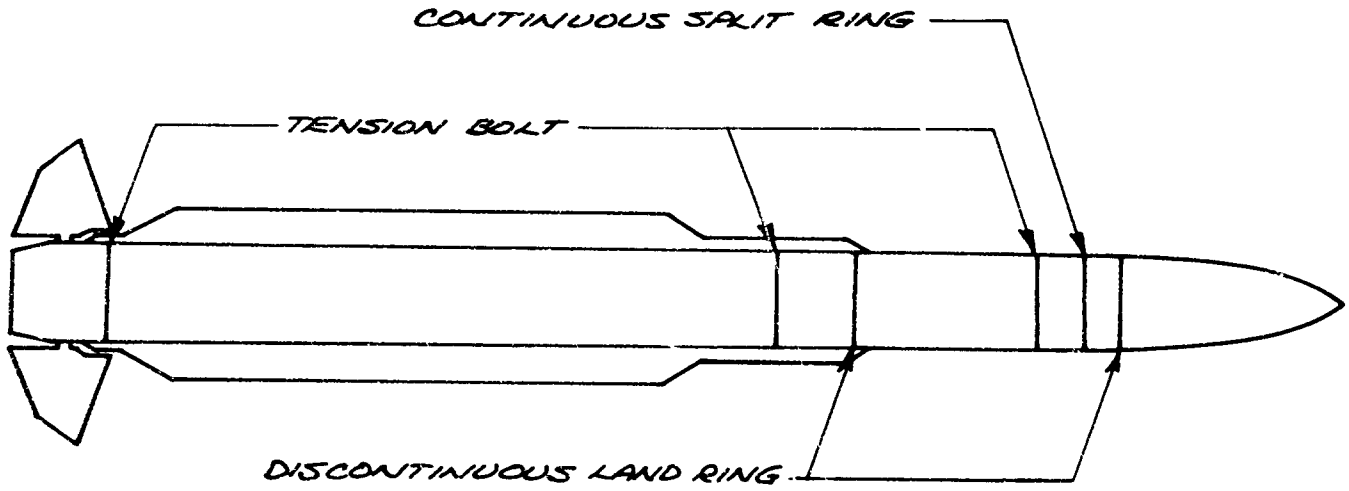


FIGURE 5-5

TEFLON COUPLING RING
JOINT IMPACT NOISE SUPPRESSION
VERSUS BASIC JOINT NOISE FACTOR

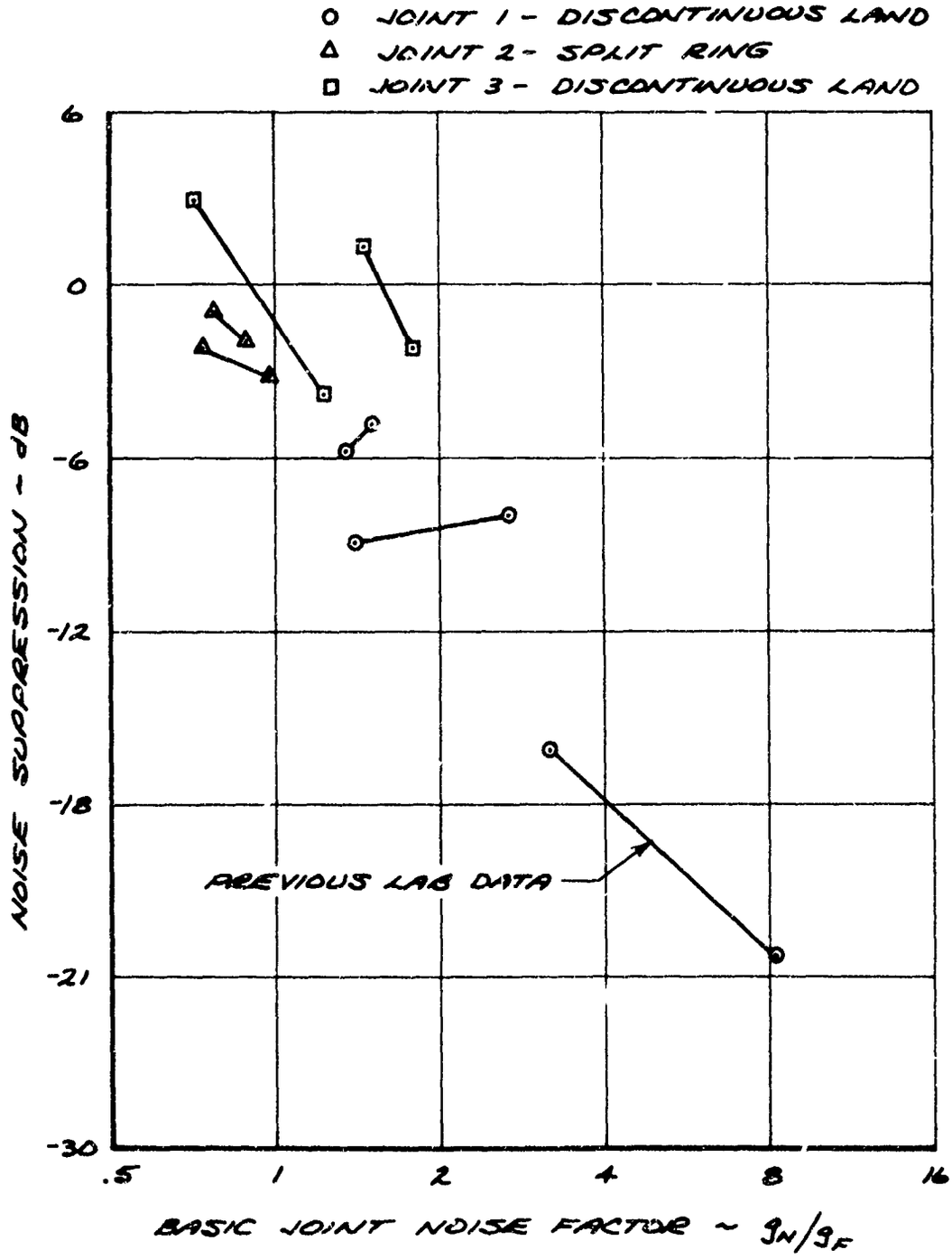
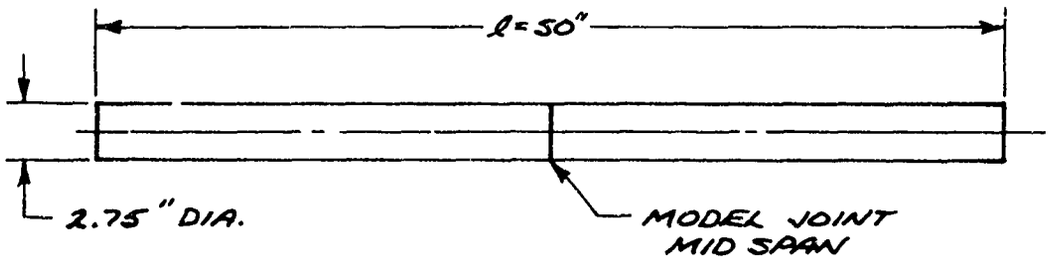
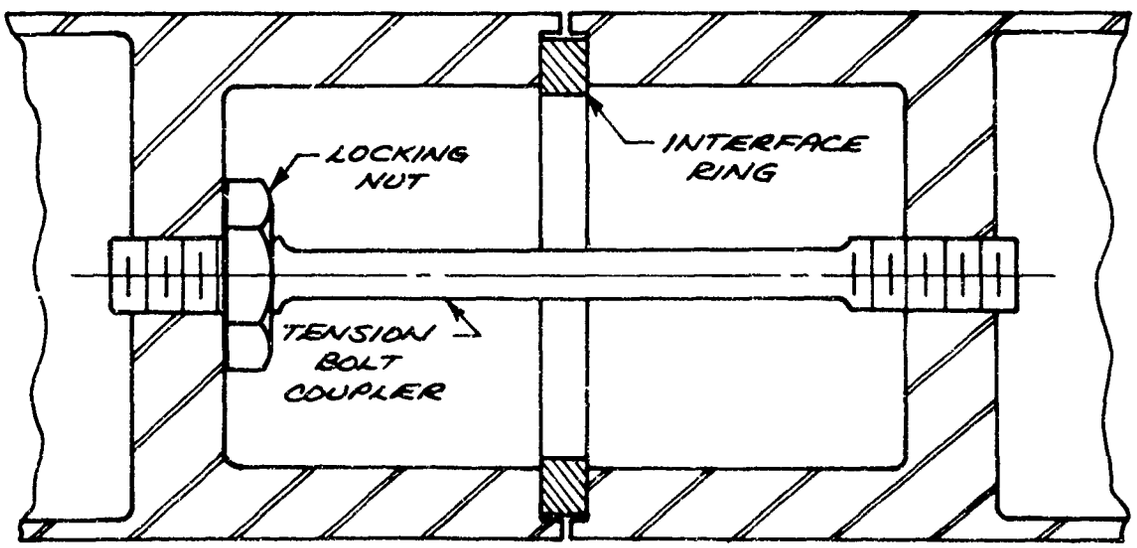


FIGURE 5-6

IDEALIZED RING JOINT MODEL





JOINT CROSS SECTION DETAIL

FIGURE 5-7

SCALE MODEL RING JOINT
PRELOAD VERSUS TORQUE

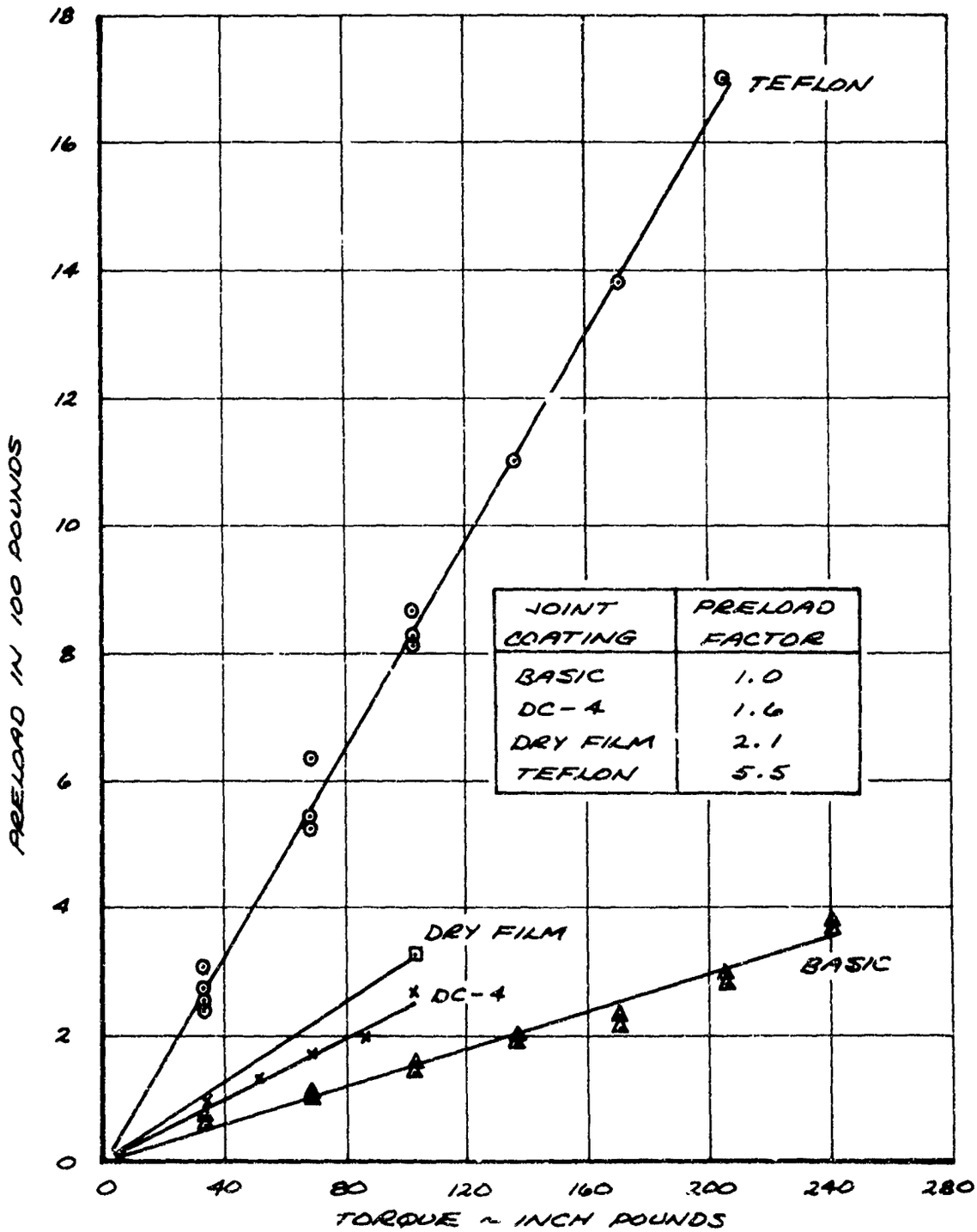


FIGURE 5-8

RING JOINT MODEL TEST SET-UP
(FREE-FREE SUSPENSION)

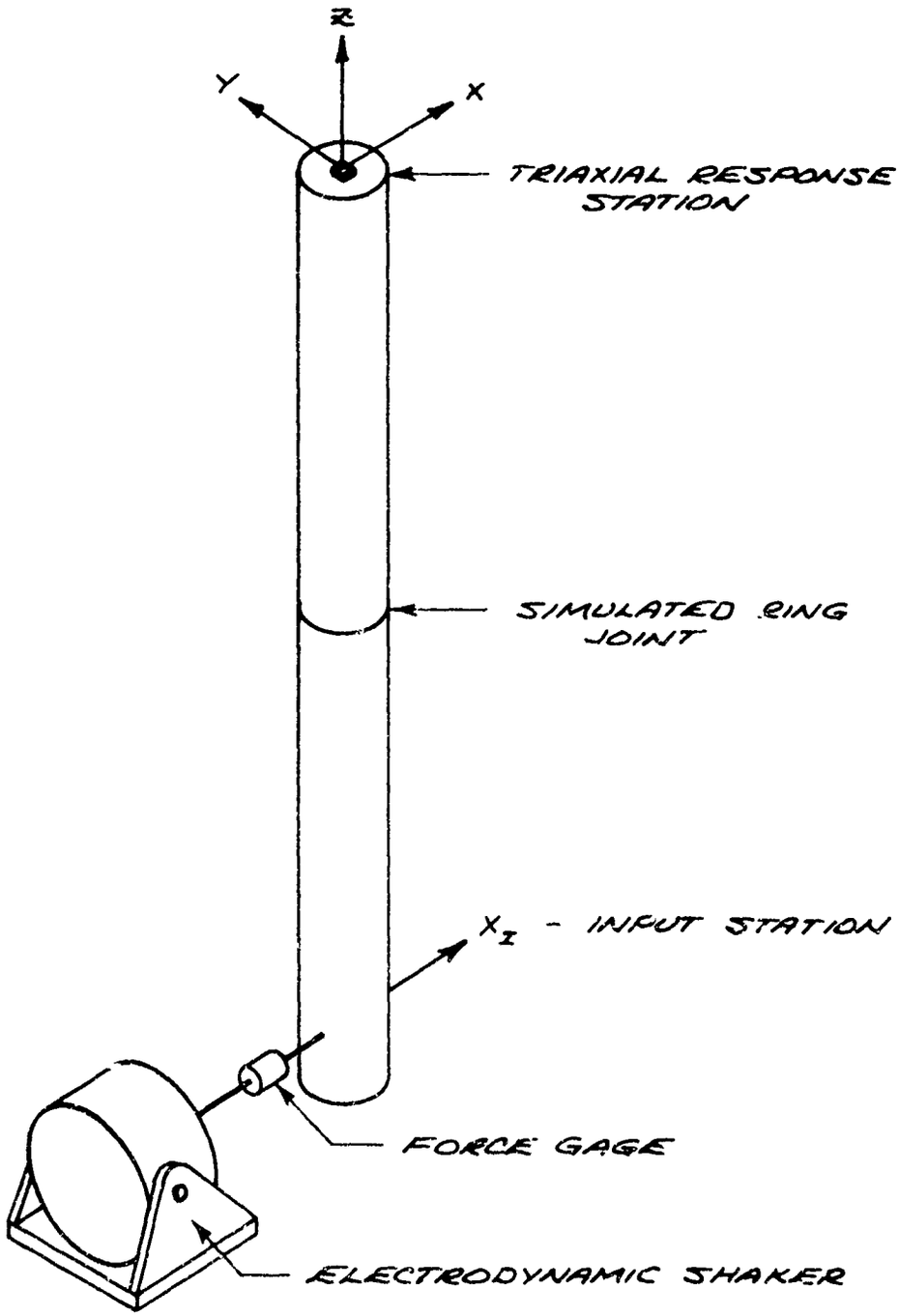
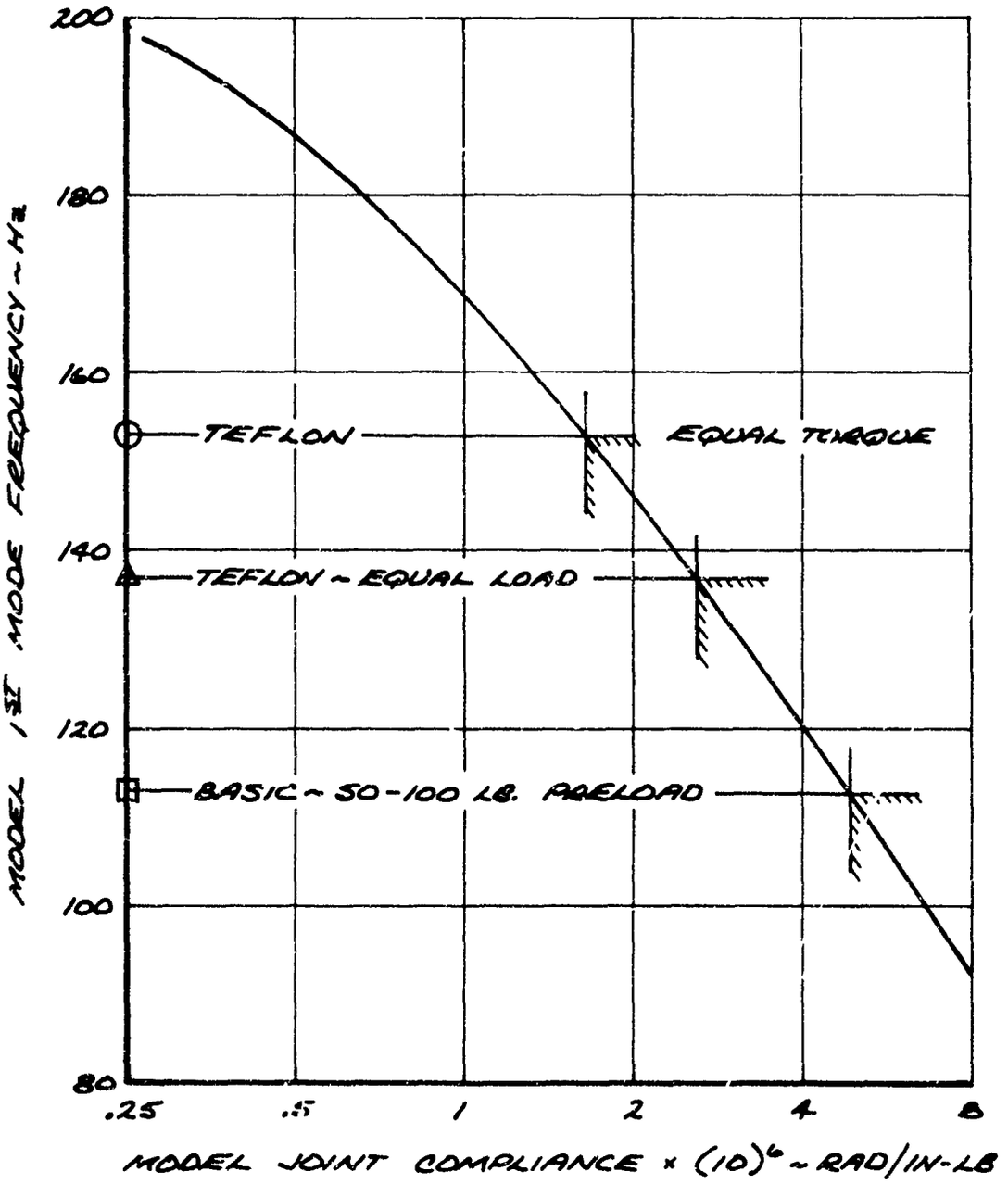


FIGURE 5-9

MODEL 1ST MODE FREQUENCY
VERSUS EFFECTIVE JOINT COMPLIANCE



Section 6.0

INTEGRATION INTO OVERALL SYSTEM REQUIREMENTS

The study thus far has been concerned with structural dynamic characteristics of joints such as stiffness, tightness and damping. There are a number of other characteristics that influence the design of tactical missile airframe joints. These include strength, weight, volumetric efficiency, degree of enclosure, producibility and maintainability. A brief discussion of each of these topics is now presented to provide an overview of airframe joint characteristics.

A rating scheme is then developed which is intended to facilitate the integration of these various characteristics into the overall system requirements. The rating scheme will then be applied to three different joints as an illustration. The three joints, which are used in the Medium Range Standard Missile (RIM-66), are shown in Figures 6-1 thru 6-3.

6.1 SYSTEM CONSIDERATIONS

The airframe joints of a tactical missile possess attributes which must satisfy a number of requirements. The dominant requirements which will be considered here are strength, weight, volumetric efficiency, degree of enclosure, producibility and missile maintainability.

6.1.1 Strength

The static load carrying capability of the airframe of a typical tactical missile is often determined by the airframe joints rather than the shell structure between joints. The fatigue capability of the airframe is also frequently determined by the joints. The reason that airframe joints are relatively inefficient load carrying members when compared to the adjacent shell structure is associated with the distortion of the load path created by the presence of the joint.

The critical static strength requirements for airframe joints are frequently the bending moments that arise from lateral loading conditions such as handling of the assembled missile or free flight steering maneuvers. There are of course shear, torque and longitudinal load requirements imposed on airframe joints. However, the strength requirement that drives the design of tactical missile airframe joints is usually the bending moment.

The strength of a joint can be quite sensitive to design details that are sometimes quite subtle. Since stress concentrations play an important role in the strength of joints, considerations such as ductility of the material and avoidance of sharp or rapid transitions are

important. The static strength of the three airframe joints that are studied in this section of the report provide an indication of the variation in strength. The strengths are listed below.

Joint Type	Illustration (Figure No.)	Strength (Inch-Pounds)
Continuous Land	6-1	104,000 to 209,000
Four Bolt Tension	6-2	231,000 to 347,000
Eight Bolt Tension	6-3	345,000 to 425,000

The variation in the strength for the first and third joints represent the effect of minor design changes that were implemented to improve the strength of the joint. The variation in the strength of the second joint is due to a combination of material property and dimensional differences.

A measure of the strength efficiency of a joint can be developed by ratioing the strength of the joint to the flexural strength of the adjacent shell structure.

Joint Type	Strength Efficiency - (%)
Continuous Land	28 to 57
Four Bolt Tension	41 to 62
Eight Bolt Tension	62 to 76

6.1.2 Weight

The weight of a joint is defined as the weight of the airframe in the vicinity of the joint less the weight of the thin shell sections if they were extended to the joint interface. Thus it is seen that the build-up in the shell adjacent to a joint is included as part of the weight of the joint. The weight of the fasteners, covers and fairings associated with the joint are also included in the weight figure. The weight of each of the three joints was calculated using the approach outlined above. The weight of the three joints is listed below.

Joint Type	Weight (Pounds)
Continuous Land	3.83
Four Bolt Tension	8.81
Eight Bolt Tension	8.80

A measure of the weight efficiency of a joint can be developed by ratioing the weight of the thin shell sections over half a body diameter if no joint were present to the weight of the same region of the structure with the joint present. This efficiency is of course referenced to the thin shell section which may not have been designed for minimum weight.

Joint Type	Weight Efficiency - (%)
Continuous Land	37
Four Bolt Tension	26
Eight Bolt Tension	48

6.1.3 Volumetric Efficiency

The presence of joints in an airframe influence the volume available to package the electronics, propulsion and ordnance. A measure of volumetric efficiency that reflects the influence that joints have on packaging volume is the open cross sectional area of the joint. The volumetric efficiency of the three joints are tabulated below.

Joint Type	Volumetric Efficiency
Continuous Land	86%
Four Bolt Tension	91%
Eight Bolt Tension	54%

The first and second joints are quite efficient with respect to volume required while the third joint is inefficient in that it occupies almost one half of the cross sectional area.

The significance of volumetric efficiency is dependent upon the design application. If the design is such that the packaged volume must pass thru the inside diameter of the joint, the volume penalty is experienced over the entire length of the packaged item. Thus a substantial volume penalty would be incurred for such an application. However, if the packaged volume need not pass thru the inside diameter of the joint, the volume penalty is experienced only over the relatively short length of the joint. Applications in which the packaged volume need not pass thru the inside diameter of the joint are usually those in which the entire packaged volume is loaded from the opposite end of the airframe section. The volume constraint of the joint on the opposite end is then of course the governing factor.

6.1.4 Degree of Enclosure

The sealing or degree of enclosure characteristics of joints are a consideration in most tactical missile applications. It

is generally preferable to provide sealing at the airframe joints for the entire interior of the missile rather than for selected sensitive components. The purpose of the seal is to preclude the entrance of moisture, sand and dust.

Sealing of airframe joints is generally accomplished by using elastomeric O-rings in the joint interface. Typically an annular groove is machined in one of the mating surfaces and the O-ring is sized such that it is stretched when installed in the groove. The tension in the installed O-ring provides for the retention of it during assembly of the joint.

The O-ring provides sealing of the primary potential leakage path to the interior of the airframe. There are however, a number of secondary leakage paths that must be sealed with certain joint designs. The eight bolt tension joint shown in Figure 6-3 is an example of a design that has potential secondary leakage paths. The eight fasteners pass from the exterior to the sealed interior of the airframe. This provides eight potential leakage paths. Sealing of the fastener assembly is accomplished by providing a spotfaced surface on the casting under the washer. The machined surfaces and the contact stresses generated on assembly of the joint provide sealing of the fastener areas. Other joint designs such as the discontinuous land shown in Figure 6-1 and the four bolt tension shown in Figure 6-2 preclude the existence of secondary leakage paths by keeping the fastener totally external to sealed interior.

6.1.5 Producibility

The producibility attribute of a joint design is concerned with the cost of manufacturing the joint hardware. Since costs are highly dependent upon production quantities, no attempt will be made here to generate quantitative cost figures. Rather the producibility of the joint will be based upon the complexity of the machining involved in fabrication of the hardware.

The continuous land joint shown in Figure 6-1 has three machined elements. Two of the machined elements are complex in that a large acme thread surface and tight tolerances are involved. The two elements are the split coupling nut and the mating female surface. Thus the producibility of this joint design is rated low.

The four bolt tension joint shown in Figure 6-2 has six machined elements, four of which are simply bolts. The two major elements require only straight forward machining to moderate tolerances. Thus the producibility of this joint design is rated high.

The eight bolt tension joint shown in Figure 6-3 has two major machined elements plus eight fastener assemblies. The tolerances involved are moderate, but the geometry of the assembly is such that an elaborate

casting is required for one member and considerable machining is required on the other member to minimize weight. Thus the producibility of this joint design is rated low.

6.1.6 Maintainability

The ease of assembly and disassembly of a joint design effects both the producibility and maintainability of tactical missiles. Extensive functional testing of the missile electronics is performed during both manufacturing and deployment. All repair work and certain types of functional testing require disassembly of the airframe joints. Logistic policies also commonly require periodic disassembly of the joints. The time and equipment required to assemble and disassemble as well as the opportunity for human error or damage to the hardware become important considerations when large quantities of hardware or frequent testing are involved.

The maintainability of the joint hardware itself is limited to inspection of the hardware such as the machined surfaces at disassembly and replacement of the O-rings and possibly certain of the fasteners at reassembly.

The ease of assembly and reassembly of the continuous land joint is somewhat greater than that of the four and eight bolt tension joints. Although the continuous land joint has a single fastener that requires roughly only one full turn to engage or disengage, it is difficult to position to start the thread engagement. The tension bolt joints are easier to position but the need to individually torque each fastener on assembly is time consuming.

6.2 INTEGRATION METHOD

The various attributes of airframe joints that were discussed in section 6.1 plus the structural dynamic attributes must be considered in an integrated fashion to produce an overall rating of different joint designs. This is accomplished by assigning a figure of merit to the individual joint attributes, a relative weighting among the attributes, and finally summing the ratings over the attributes.

The three joints shown in Figures 6-1 thru 6-3 will be rated as an illustration. Equal weightings among the attributes are used, although unequal weightings can of course be used to emphasize or deemphasize certain attributes relative to the others. The four ratings of excellent, good, fair and poor are used for the attributes based on the quantitative and qualitative factors proposed in Table 6-1. In addition to the joint attributes discussed in Section 6.1, the structural dynamic attributes of stiffness and tightness are included in Table 6-1. The stiffness rating is the NASA rating discussed in Reference 3. The tightness attribute

refers to self induced noise characteristics that are discussed in Section 5 of the present report.

The illustrative rating comparison for the three joints (Figures 6-1 thru 6-3) is presented in Table 6-2. Using equal weightings for each of the eight joint attributes results in the best overall rating for the four bolt tension joint. The overall rating using equal weighting factors, does not reveal large differences between the three joints. However, the use of unequal weighting factors in which certain attributes are assigned very high or very low emphasis would produce more dramatic differences in the overall ratings.

Table 6-1
Proposed Joint Attribute Rating Basis

Attribute	Measure or Units	Rating			
		Excellent	Good	Fair	Poor
Stiffness[1]	Inch-Pounds/Radian	$(10)^{10}/C$	$(10)^{9}/C$	$(10)^{8}/C$	$(10)^{7}/C$
Tightness	Noise generation	Low			High
Strength Efficiency	Per cent	>75	75 to 50	50 to 25	<25
Weight Efficiency	Per cent	>60	60 to 40	40 to 20	<20
Volumetric Efficiency	Per cent	>90	90 to 70	70 to 50	<50
Degree of Enclosure	No. of locations requiring sealing	1	2 to 5	>5	Unsealable
Producibility	Manufacturing cost	Low			High
Maintainability	Ease of assembly and disassembly	Simple			Difficult

(1) NASA stiffness rating as defined on page 16 of Reference 1, $C = (20/D)^3$, D = body diameter in inches.

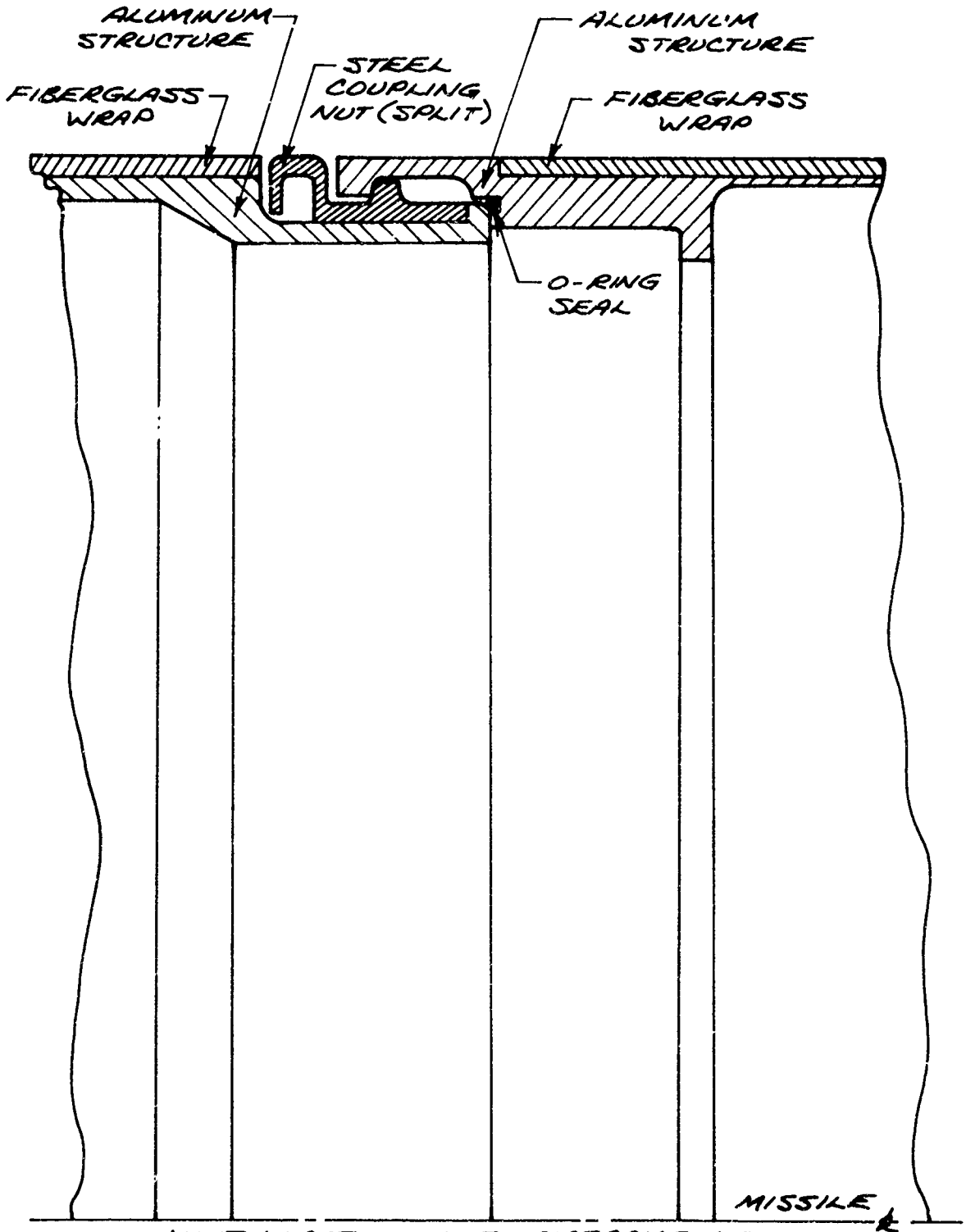
Table 6-2
Illustrative Rating Comparison for Three Joints

Attribute	Ratings[1]		
	Continuous Land	Four Bolt Tension	Eight Bolt Tension
Stiffness	F	G	F
Tightness	P	G	G
Strength	G	G	E
Weight	G	F	G
Volume	G	E	F
Degree of Enclosure	E	E	F
Producibility	F	E	F
Maintainability	E	G	F
Overall	G(-)	G	F(+)

(1) E = Excellent, G = Good, F = Fair, P = Poor

FIGURE 6-1

CONTINUOUS LAND RING JOINT



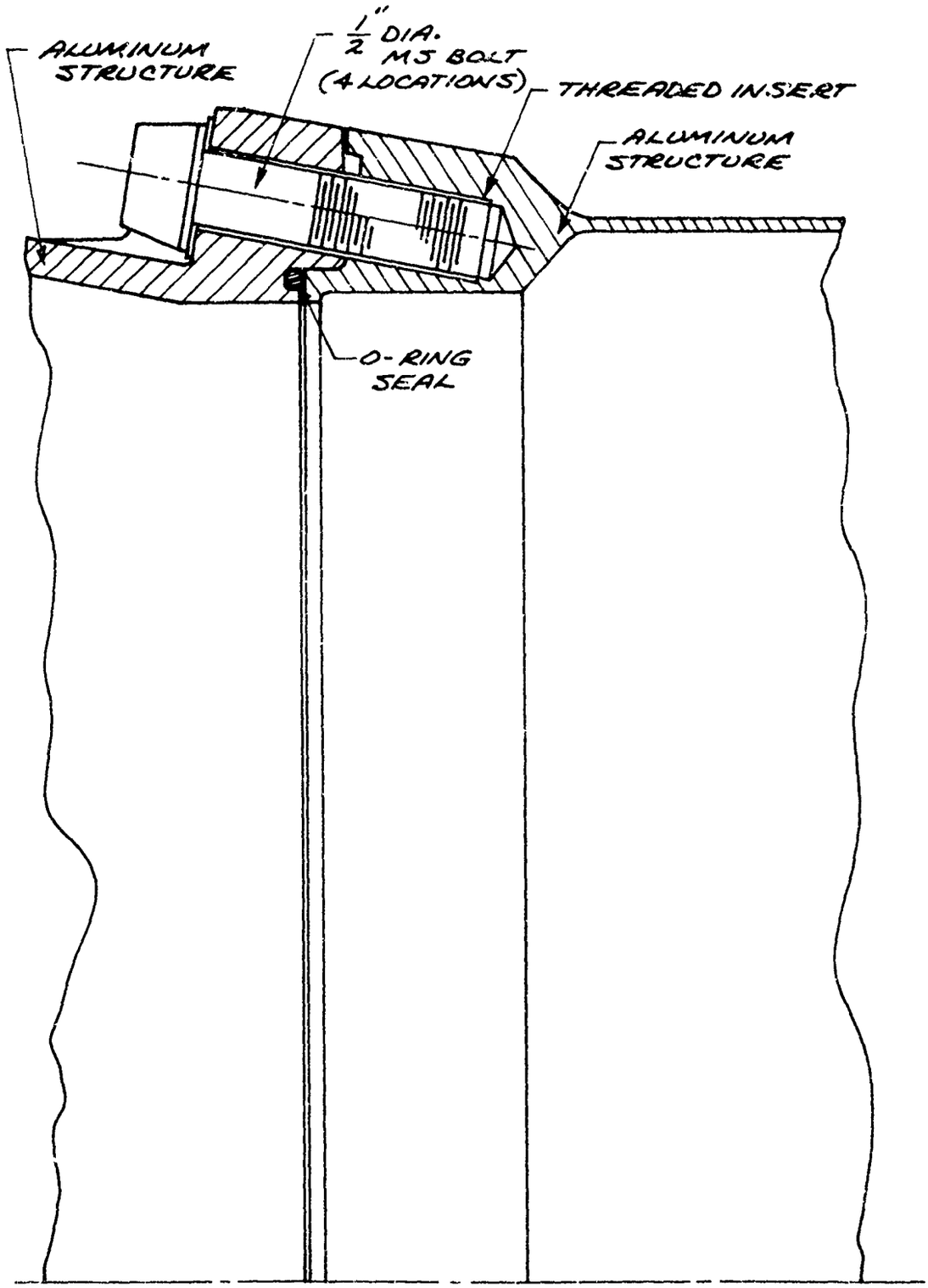
JOINT LOCATION: 22% AIRFRAME LENGTH

JOINT DIAMETER: 13.5 INCHES

SCALE: FULL

FIGURE 6-2

FOUR BOLT TENSION JOINT



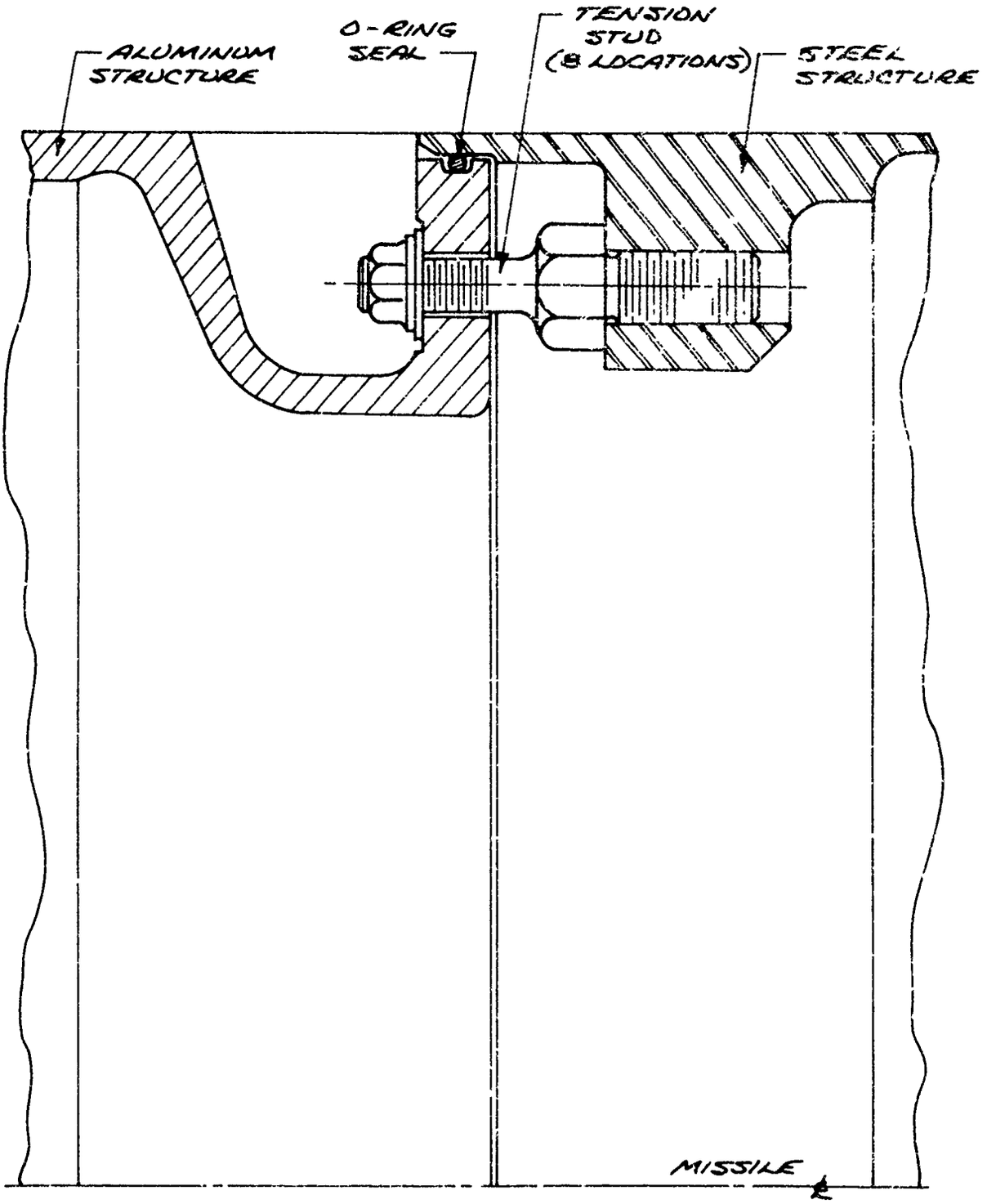
JOINT LOCATION : 35 % AIRFRAME LENGTH

JOINT DIAMETER : 13.5 INCHES

SCALE : FULL

FIGURE 6-3

EIGHT BOLT TENSION JOINT



JOINT LOCATION : 41 % AIRFRAME LENGTH
JOINT DIAMETER : 13.5 INCHES
SCALE : FULL

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1. Maloney, J. G., Shelton, M. T., and Underhill, D. A., "Structural Dynamic Properties of Tactical Missile Joints - Phase I", General Dynamics, Pomona Division Report No. CR-6-348-945-001, June 1970.

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APPENDIX

JOINT COMPLIANCE EXTRACTION CODE

USER'S MANUAL

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INTRODUCTION

The computational system used for implementing the method of analysis described in Section 4 is composed of the following two digital computer programs:

1) Program FILLIN

2) Program JOINTS

Computer program FILLIN is a small prelude program that accepts measured modal data obtained at a set of test missile stations and interpolates these data to provide "measured" modal data at a set of missile stations consistent with theoretical modal data calculated within computer program JOINTS. This preliminary step is needed so that a comparison of experimental and theoretical modal data at identical missile stations can be made within computer program JOINTS.

Within the Appendix input data instructions, data output and program limitations are discussed for both computer programs FILLIN and JOINTS. Computer program FORTRAN listings and a sample application data deck listing are also presented.

PROGRAM FILLIN

Because comparisons between experimental and theoretical modal data are made at all modal analysis stations, within computer program JOINTS, computer program FILLIN was written to provide interpolated measured modal data for the modal analysis stations. The resulting interpolated measured mode shape deflections and slopes are punched on cards for the complete set of modal analysis missile stations in a format acceptable for subsequent input to computer program JOINTS.

Usually, only mode shape deflections are measured in the laboratory while both mode shape deflections and slopes are computed. Therefore, an added feature of computer program FILLIN is the computation of mode shape slopes from the measured mode shape deflection data.

Computer program FILLIN has the following restrictions:

1) There must be at least two experimental points on each appendage (to establish slope).

2) There must be at least two experimental points on either side of a joint (to establish shear discontinuity).

Computer program FILLIN and JOINTS were written to be run on the CDC 6400 digital computer with 32K words of memory storage, under control of the CDC 6000 Series Scope Monitor System (Version 3.3), at General

Dynamics, Pomona Division. All programs and subroutines are written in the CDC 6400 FORTRAN Extended Language (Version 3.0) and should be easily implemented on any machine having a FORTRAN IV compiler. Input/output devices required are the card reader (logical unit 60), the line printer (logical unit 6) and the card punch.

Computer program FILLIN is composed of the following routines:

1) Program FILLIN

2) Subroutine SQUARE

3) Subroutine PARAB

4) Subroutine LINFIT

In addition, FORTRAN library routines EOF (end of file) and EXIT are called. FORTRAN listings of these four routines comprising computer program FILLIN are presented in Tables A-4 through A-7.

The input data instructions showing card formats for computer program FILLIN are presented in Table A-1. A listing of a sample data deck is presented in Table A-15. Data output consists of a listing of the input data and the interpolated experimental data (mode shape deflections and slopes) computed at all modal analysis stations. It is suggested that the results obtained from computer program FILLIN be checked before using the punched output as input to program JOINTS.

PROGRAM JOINTS

A simplified flow diagram of computer program JOINTS is presented in Table A-2. The procedure for joint compliance extraction is described as follows:

1) A starting value of joint compliance is assumed for each joint at which the compliance is unknown (initially from the input data).

2) Modes and the resulting cost function and first order gradients are computed for this initial configuration.

3) Each unknown joint compliance is varied independently from the trial configuration.

4) Modes and the resulting cost function and first order gradients are computed for each of these configurations obtained in Step 3.

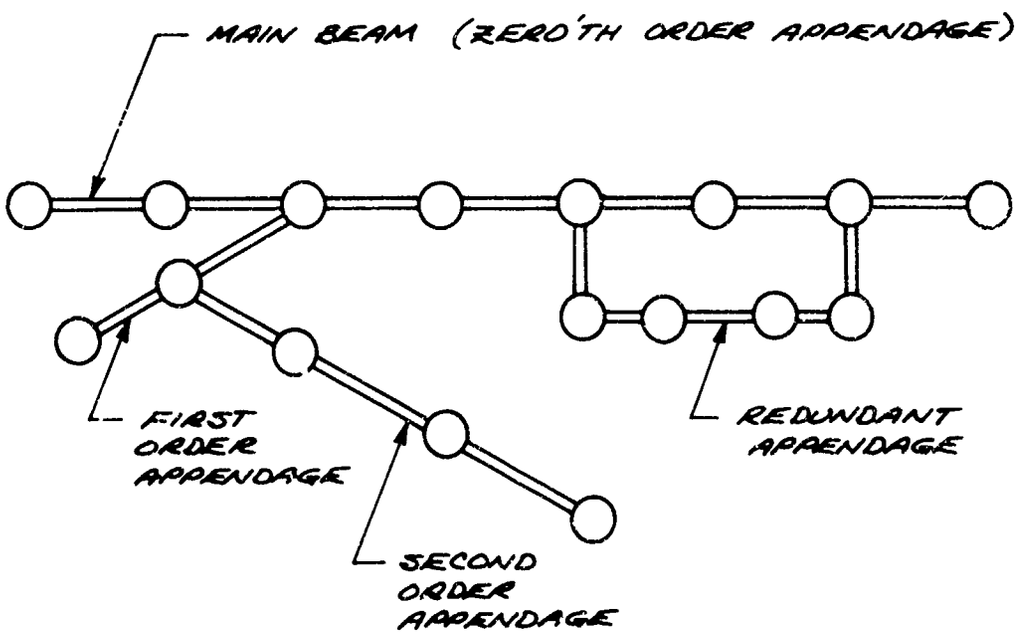
5) Second order gradients are computed from the finite differences of the results obtained in Step 4.

6) A new trial set of joint compliances is calculated using the first and second order gradients terms.

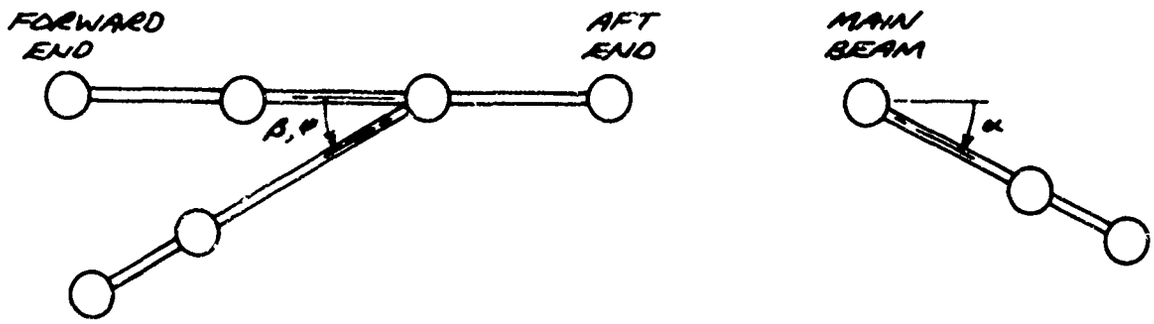
7) If the trial set of compliances has converged within a specified tolerance, the analysis stops. Otherwise Step 2 is reentered and the analysis continues.

These seven steps comprise a cycle of iterations (a configuration for each of the unknown springs plus the nominal configuration). A detailed description of the computational procedure for first and second order gradients and the new trial spring rates is presented in Section 4.

A brief description of the mathematical model of a missile is presented here to aid in understanding the input data to program JOINTS. A missile is modeled using a lumped parameter representation. A typical model is shown below.



Appendage attachment angles are defined by the following diagram.



If this is the top view, the marked angle is φ. If this is the side view, the marked angle is β.

End view of main beam looking aft.

The following five types of stations are available for modeling a missile system:

1) mass

2) spring

3) appendage attachment

4) forward redundant appendage attachment

5) aft redundant appendage attachment

When modeling a system for input to the computer, each station input can perform only one function, that is, a mass station cannot have a spring associated with it or be an appendage attachment station.

The main beam or zero order appendage must be input first. The first station on the main beam must be labeled one. After that, any other positive integer may be used as a station identification number. As a general practice, station identification numbers should be unique since appendage attachment designations are made using these identification numbers. Simple appendages are entered next starting from their free end. Redundant appendages are entered last starting from their forward attachment end. Within the main beam or any appendages, station location values must be entered in increasing order (consecutive stations may have equal station locations). Redundant appendages must lie along the main beam and have the same type of motion (bending, torsion or longitudinal) as the main beam. Redundant appendages may not overlap but simple appendages may be attached to redundant appendages.

Complications arise due to the manner in which the Myklestad subroutine in Computer Program JOINTS functions. The number of stations in the actual mathematical model of a missile (input stations) is added to by the Myklestad subroutine for the following reasons:

1) A joint is represented by a single input station. However, for computations, a second station (at the same location) is needed to define the displacement and slope discontinuities at the joint.

2) At appendage attachment stations, an additional station is added (at the same location) to show the shear and moment discontinuities at the attachment station.

3) For each appendage and for the main beam, an additional station is added at the end of each beam system (at the same location as the last station) to allow for imposition of the boundary conditions.

Computer Program JOINTS is composed of the following routines.

1) Program JOINTS

2) Subroutine STEER

3) Subroutine ALTER

4) Subroutine RENORM

5) Subroutine MYKL

6) Subroutine MEMSET

7) Subroutine MATNF5

In addition, FORTRAN library routines EOF (end of file), EXIT, SQRT, ABS, LABS, LOCF (storage address of variable in machine), SIN and COS are called. FORTRAN listings of these seven routines comprising computer program JOINTS are presented in Tables A-8 through A-14.

Computer program JOINTS and FILLIN have the following size limitations:

1) A maximum of 100 theoretical missile stations

2) A maximum of 10 experimental and theoretical modes

3) A maximum of 10 redundant appendages

The input data instructions showing card formats for computer program JOINTS are presented in Table A-3. A FORTRAN listing of the program and its subroutines is presented in Table A-8 thru A-14. A listing of a sample data deck is presented in Table A-16.

Data output from the program consists of a listing of the input data, the input configuration for each iteration, a comparison of experimental and theoretical modes (deflections and slopes) and frequencies and cost function data for each iteration.

SAMPLE APPLICATION

A sample application is included to assist the user in checkout of the codes. Assume three experimental modes for a missile have been measured in the laboratory. A 59 station mathematical model has been developed, which includes two simple appendages and one redundant appendage. Three theoretical modes are to be computed and four joint compliances are to be extracted from the measured data using computer program JOINTS.

First, computer program FILLIN is run to determine the experimental mode shape deflections and slopes at the modal analysis stations. The data deck listing for computer program FILLIN is presented in Table A-15.

With the experimental mode shape deflections and slopes defined at the desired stations, computer program JOINTS is then run. The data deck listing for computer program JOINTS is presented in Table A-16. The entire output listing from the computer program is not presented because of the large quantity of output. Key output data are given in Table A-17. Certain of the results are plotted in Figure A-1. Other application examples are presented in Section 4 of this report.

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TABLE A-1

INPUT DATA INSTRUCTIONS FOR COMPUTER PROGRAM FILLIN

~~FORTRAN CODING AND DATA FORM~~

PROBLEM: PROGRAM FILLIN

PROGRAMMER: D.O. RIFE

ONE GENERAL TITLE CARD

MYKLESTAD FORMAT BEAM DESCRIPTIONS OF STATIONS AT WHICH MODE SHAPE DEFLECTIONS AND SLOPES ARE DESIRED (CARD FORMAT - 2I4, 3I2, 2X, 7E8.0)

ID(1)	IA(1)	IT(1)	XSTA(1)	COMP1(1)	COMP2(1)
ID(2)	IA(2)	IT(2)	XSTA(2)	COMP1(2)	COMP2(2)
⋮	⋮	⋮	⋮	⋮	⋮
ID(K)	IA(K)	IT(K)	XSTA(K)	COMP1(K)	COMP2(K)
⋮	⋮	⋮	⋮	⋮	⋮

ID(I) - STATION IDENTIFICATION COUNTER FOR STATION I. ID(I) > 0

NOTE: THE FIRST STATION OF THE MAIN BEAM MUST BE LABELED 1, I.E. ID(1) = 1
AS A GENERAL PRACTICE, STATION IDENTIFICATION COUNTERS SHOULD BE UNIQUE SINCE APPENDAGE ATTACHMENT STATION NUMBERS REFER TO THESE IDENTIFICATION COUNTERS.

IA(I) - APPENDAGE ATTACHMENT STATION IDENTIFICATION NUMBER FOR STATION I. IA(I) ≥ 0

NOTE: EXCEPT FOR MAIN BEAM IN WHICH IA(I) = 0, THE APPENDAGE ATTACHMENT STATION IDENTIFICATION NUMBER MUST REFER TO A STATION ID. COUNTER, I.E., IA(I) = ID(J) FOR A STATION J IN WHICH IT(J) = 2
(WITHIN AN APPENDAGE, ALL APPENDAGE ATTACHMENT NUMBERS ARE EQUAL)

IT(I) - DESIGNATION OF STATION TYPE FOR STATION I

0 - MASS STATION
1 - SPRING STATION
2 - APPENDAGE ATTACHMENT STATION
3 - FORWARD REDUNDANT APPENDAGE ATTACHMENT STATION
4 - AFT REDUNDANT APPENDAGE ATTACHMENT STATION

NOTE: ENTER ALL REDUNDANT APPENDAGES LAST STARTING FROM THE FORWARD END.

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TABLE A-1 (CONT'D)

~~FORTRAN CODING AND DATA FORM~~

PROBLEM

PROGRAMMER

```
XSTA(I)   - STATION LOCATION OF STATION I - INCHES
            NOTE: WITHIN THE MAIN BEAM OR ANY APPENDAGE, XSTA(I+1) ≥ XSTA(I)
                  (A STATION LOCATION IS NEEDED FOR EACH CARD INPUT, CAN BE ZERO)

COMP1(I)  - SHEAR COMPLIANCE FOR STATION I - IN/LB                    COMP1(I) > 0.0
            NOTE: ENTER A VALUE HERE ONLY IF IT(I)=1

COMP2(I)  - FLEXURAL COMPLIANCE FOR STATION I - RAD/IN*LB             COMP2(I) > 0.0
            NOTE: ENTER A VALUE HERE ONLY IF IT(I)=1

NOTE: ENTER ALL MAIN BEAM CARDS FIRST, THEN APPENDAGE CARDS - MAIN BEAM AND
      APPENDAGE CARDS MUST BE IN ORDER AS PROGRAM DOES NO SORTING.
      ENTER SIMPLE APPENDAGES STARTING AT FREE END, ENDING AT ATTACHED END.
      ID(I)=0 ENDS THE READING OF THE BEAM DESCRIPTION CARDS - READ A MAXIMUM
      OF 100 OF THESE CARDS (COUNTING THE ID(I)=0 CARD)

OPTION CARD (CARD FORMAT - 3I5)

 NSTA|NESTA| NEXP|

NSTA  - NUMBER OF INTERNAL THEORETICAL STATIONS AT WHICH INTERPOLATED
        EXPERIMENTAL MODE SHAPE DEFLECTIONS AND SLOPES WILL BE PUNCHED.
        (100 IS MAXIMUM BECAUSE OF PROGRAM JOINTS)                    3≤NSTA≤100

NESTA - NUMBER OF STATIONS AT WHICH EXPERIMENTAL MODES WERE MEASURED.
        NOTE: NSTA>NESTA                                              2≤NESTA≤99

NEXP  - NUMBER OF EXPERIMENTAL MODES                                  1≤NEXP≤10
```

TABLE A-1 (CONT'D)

~~FORTRAN CODING AND DATA FORM~~

PROBLEM | ~~AWO~~ | ~~CWO~~ | ~~WAP~~

PROGRAMMER | ~~PHONE EXT~~ | ~~DATE~~

APPENDAGE INDICATORS AND STATIONS AT WHICH EXPERIMENTAL MODES WERE MEASURED

(CARD FORMAT - 4(I10, E10.0))

JA(1)	XESTA(1)	JA(2)	XESTA(2)	..	..	JA(NESTA)	XESTA(NESTA)

JA(I) - APPENDAGE ATTACHMENT STATION IDENTIFICATION NUMBER FOR MEASUREMENT STATION I

NOTE: JA(I) = IA(J) WHERE IA(J) APPEARS IN THE BEAM DESCRIPTION ABOVE (ENTER APPENDAGES IN THE SAME ORDER AS IN THE BEAM DESCRIPTION)

XESTA(I) - STATION LOCATION OF MEASUREMENT STATION I - INCHES

NOTE: WITHIN THE MAIN BEAM OR ANY APPENDAGE, XESTA(I+1) > XESTA(I)

EXPERIMENTAL MODE SHAPE DEFLECTIONS (CARD FORMAT - 6X, 2I3, 5E12.5)

1	1	PHI(1,1)	PHI(1,2)	PHI(1,3)	PHI(1,4)	PHI(1,5)
2	1	PHI(2,1)	PHI(2,2)	PHI(2,3)	PHI(2,4)	PHI(2,5)
:	:	:	:	:	:	:
NESTA	1	PHI(NESTA,1)	PHI(NESTA,2)	PHI(NESTA,3)	PHI(NESTA,4)	PHI(NESTA,5)
1	6	PHI(1,6)	PHI(1,7)	:	PHI(1,NEXP)	
2	6	PHI(2,6)	PHI(2,7)	:	PHI(2,NEXP)	
:	:	:	:	:	:	
NESTA	6	PHI(NESTA,6)	PHI(NESTA,7)	:	PHI(NESTA,NEXP)	

PHI(I, J) - EXPERIMENTAL MODE SHAPE DEFLECTION (IN/IN) AT MEASUREMENT STATION I FOR EXPERIMENTAL MODE J

NOTE: THERE MUST BE AT LEAST TWO MEASUREMENT POINTS ON AN APPENDAGE AND AT LEAST TWO MEASUREMENT POINTS ON EITHER SIDE OF EACH JOINT.
ADDITIONAL DATA DECKS MAY BE SUBMITTED, STARTING WITH A NEW TITLE CARD, ETC.

TABLE A-2.

FLOW DIAGRAM OF COMPUTER PROGRAM JOINTS

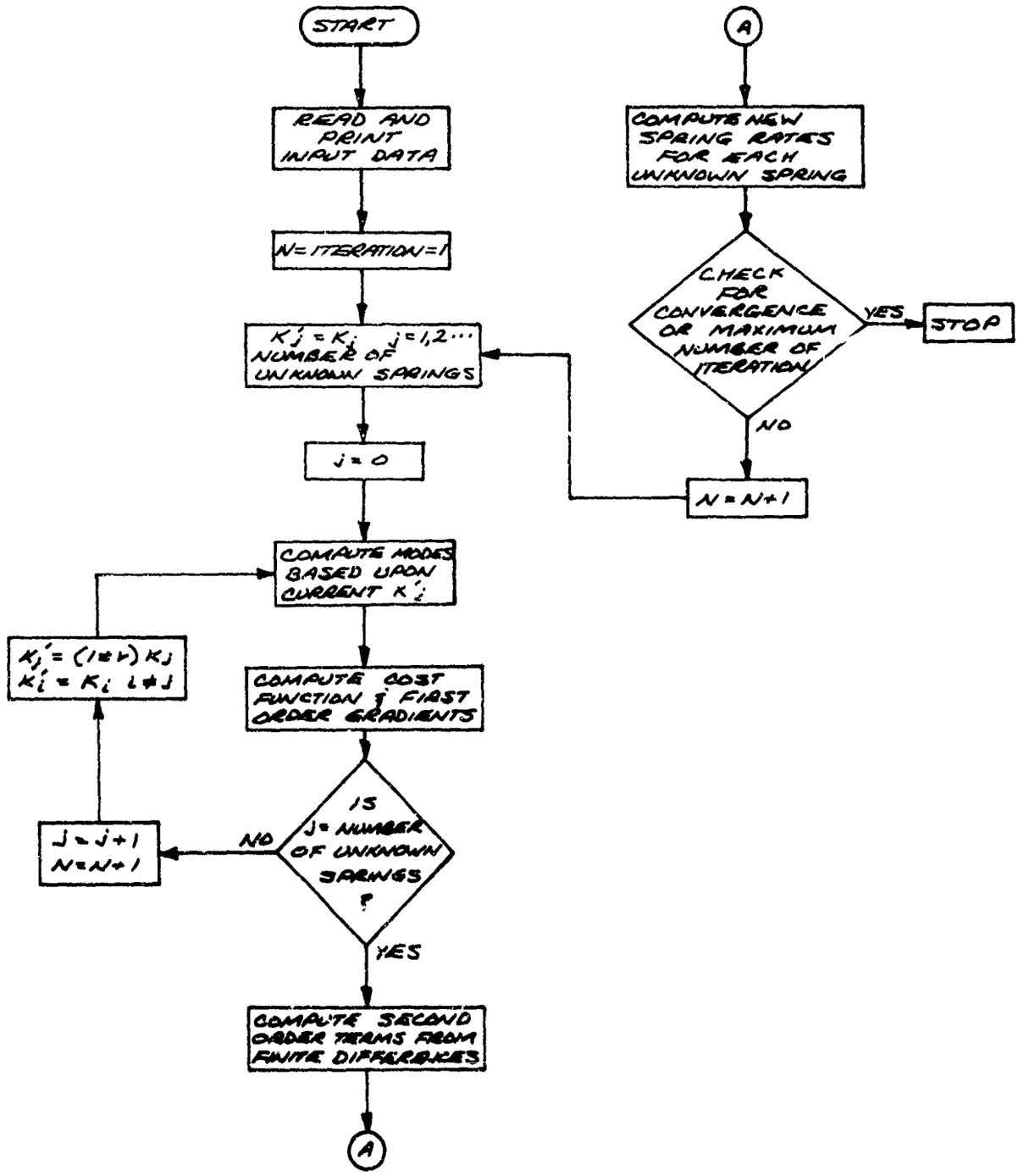

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TABLE A-3

INPUT DATA INSTRUCTIONS FOR COMPUTER PROGRAM JOINTS

~~FORTRAN CODING AND DATA FORM~~

PROBLEM: PROGRAM JOINTS

PROGRAMMER: M.T. SHELTON, D.O. RIFE

```
                                   ONE GENERAL TITLE CARD

OPTION CARDS (CARD FORMAT - 8I5,4E10.0)

KNORM    NT   NEXP   NWTITMAXNVSPR NSTANESTA    STEP      TOL       CLOSE     XRATIO
KCHECK   XMASS

KNORM   -  CARD NUMBER (NOT A STATION IDENTIFICATION COUNTER) AT WHICH
           THEORETICAL MODES WILL BE NORMALIZED.                    0≤KNORM≤NSTA
           NOTE: THIS IS AN INTERNAL STATION CARD NUMBER, NOT AN INPUT CARD NUMBER
                 IF KNORM IS BLANK OR ZERO, PROGRAM SETS KNORM=1

NT      -  NUMBER OF THEORETICAL MODES TO BE COMPUTED                  1≤NT≤10

NEXP    -  NUMBER OF EXPERIMENTAL MODES BEING INPUT                    1≤NEXP≤10
           NOTE: SAME VALUE AS IN PROGRAM FILLIN

NWT     -  MODE SHAPE AND MODE FREQUENCY WEIGHTING FACTOR OPTION
           IF BLANK OR ZERO, PROGRAM COMPUTES WEIGHTING FACTORS.
           OTHERWISE, WEIGHTING FACTORS ARE INPUT.

ITMAX   -  MAXIMUM NUMBER OF ITERATIONS FOR ANALYSIS                   ITMAX≥1
           NOTE: THE PROGRAM COMPUTES ITERATIONS IN THE FOLLOWING MANNER:
                 THE NOMINAL CONFIGURATION OF A CYCLE OF ITERATIONS IS DESIGNATED
                 AS ITERATION NUMBER 1. EACH SPRING WHICH CAN VARY IS COUNTED AS
                 ANOTHER ITERATION. THEREFORE, TO COMPLETE ONE FULL CYCLE OF
                 ITERATIONS REQUIRES NVSPR+1 ITERATIONS. AFTER EACH CYCLE OF
                 ITERATIONS, THE PROGRAM COMPUTES A NEW NOMINAL CONFIGURATION
                 AND THE PROCESS OF ITERATION COUNTING CONTINUES AS BEFORE. THE
                 PROGRAM ALWAYS COMPLETES A CYCLE OF ITERATIONS BEFORE STOPPING.
```

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TABLE A-3 (CONT'D.)

~~FORTRAN CODING AND DATA FORM~~

PROBLEM | ~~ANG~~ | ~~EWO~~ | ~~MAP~~

PROGRAMMER | ~~PHONE EXT~~ | ~~DATE~~

```
NVSPR    - NUMBER OF SPRINGS WHOSE COMPLIANCES CAN BE VARIED.                    1≤NVSPR≤10

NSTA     - NUMBER OF INTERNAL THEORETICAL STATIONS.                              3≤NSTA≤100
           NOTE: SAME VALUE AS IN PROGRAM FILLIN.

NESTA    - NUMBER OF STATIONS AT WHICH EXPERIMENTAL MODES WERE MEASURED
                                                                                 2≤NESTA≤99
           NOTE: THIS PARAMETER HAS BEEN INCLUDED FOR USE WHEN PROGRAMS FILLIN
                 AND JOINTS ARE COMBINED. SINCE THIS HAS NOT OCCURRED, SET NESTA=NSTA

STEP     - PARAMETER USED IN DETERMINING CHANGE IN SPRING RATES FOR VARYING
           SPRINGS. A VALUE OF STEP ≈ 0.15 IS RECOMMENDED.                       0.0<STEP<1.0
           NOTE: K_NEW=(1±STEP)*K_OLD

TOL      - PARAMETER USED IN DETERMINING SOLUTION TOLERANCE FOR SPRING RATES.
           A VALUE OF TOL ≈ 0.01 IS RECOMMENDED.                                 0.0<TOL<1.0
           NOTE: IF ABS(K_CURRENT/K_PREVIOUS CYCLE -1.0)<TOL FOR ALL VARYING SPRINGS,
                 ANALYSIS IS STOPPED.

CLOSE    - PARAMETER USED IN DETERMINING STARTING FREQUENCY FOR MYKLESTAD MODE
           SEARCH. A VALUE OF CLOSE ≈ 0.90 IS RECOMMENDED.                       0.0≤CLOSE≤1.0
           NOTE: IF BLANK OR ZERO, PROGRAM MAKES A CONTINUOUS SEARCH STARTING
                 FROM PREVIOUS MODE FREQUENCY. FOR STARTING FREQUENCY FOR MODE 1,
                 SEE LAST CARD INPUT IN DATA DECK.
                 IF CLOSE≠0.0, f_START(I)=CLOSE*EFREQ(I) WHERE I IS THE MODE COUNTER.
                 OTHERWISE, f_START(I)=f_MODE(I-1).

XRATIO   - PARAMETER USED IN DETERMINING NEXT CYCLE INITIAL SPRING RATE VALUES
           WHEN COST FUNCTION HAS INCREASED.                                     0.0≤XRATIO≤1.0
           NOTE: IF XRATIO IS BLANK OR ZERO, PROGRAM SETS XRATIO=0.5
```

TABLE A-3 (CONT'D.)

~~FORTRAN CODING AND DATA FORM~~

PROBLEM | ~~AWO~~ | ~~EWO~~ | ~~MAP~~

PROGRAMMER | ~~PHONE EXT~~ | ~~DATE~~

```
KCHECK  -  OPTION FOR ASKING PROGRAM TO SEE IF A MODE MAY HAVE BEEN MISSED
           DURING THE MYKLESTAD MODE SEARCH PHASE OF THE ANALYSIS.
           NOTE: IF KCHECK≠2, PROGRAM WILL CHECK TO SEE IF MODE HAS BEEN MISSED.
                 OTHERWISE, NO CHECK WILL BE MADE.
                 THIS OPTION SHOULD NOT BE EXERCISED IF MYKLESTAD MODEL CONTAINS
                 REDUNDANT APPENDAGES.

XMASS   -  TOTAL SYSTEM MASS (REQUIRED)                                LB-SEC²/IN

WEIGHTING FACTORS - DO NOT READ IF NWT=0 (CARD FORMAT - 8E10.0)

 PWMAT(1) | PWMAT(2) |   ..   | PWMAT(K) |   ..   |   ..   | PWMAT(NEXP)
 FWMAT(1) | FWMAT(2) |   ..   | FWMAT(K) |   ..   |   ..   | FWMAT(NEXP)

PWMAT(I) - RELATIVE MODE SHAPE DEFLECTION AND SLOPE WEIGHTING FACTOR FOR MODE I.
                                                          0.0<PWMAT(I)

FWMAT(I) - RELATIVE MODE FREQUENCY WEIGHTING FACTOR FOR MODE I.     0.0<FWMAT(I)

EXPERIMENTAL FREQUENCIES (CARD FORMAT - 8E10.0)

 EFREQ(1) | EFREQ(2) |   ..   | EFREQ(K) |   ..   |   ..   | EFREQ(NT) |

EFREQ(I) - EXPERIMENTAL MODE FREQUENCY FOR MODE I - HZ.  0.0<EFREQ(I)<EFREQ(I+1)
           NOTE: WHERE MODES HAVE BEEN MEASURED, ENTER MEASURED MODE FREQUENCIES
                 OTHERWISE, ESTIMATE WHERE MODES MAY BE FOUND.
```

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TABLE A-3 (CONT'D.)

~~FORTRAN CODING AND DATA FORM~~

PROBLEM | ~~ANO~~ | ~~ENG~~ | ~~MAP~~

PROGRAMMER | ~~PHONE EXT.~~ | ~~DATE~~

```
VARIABLE SPRINGS (CARD FORMAT - 2I4,2E8.0,I4)

KSTA(1)  KVAR(1)  SPRINGL(1)  SPRINGU(1)  KTYPE(1)
KSTA(2)  KVAR(2)  SPRINGL(2)  SPRINGU(2)  KTYPE(2)
   :        :        :           :          :
KSTA(K)  KVAR(K)  SPRINGL(K)  SPRINGU(K)  KTYPE(K)
   :        :        :           :          :
KSTA     KVAR     SPRINGL     SPRINGU     KTYPE
(NVSPR)  (NVSPR)  (NVSPR)     (NVSPR)     (NVSPR)

KSTA(I)        - CARD NUMBER (NOT A STATION IDENTIFICATION COUNTER) FROM INPUT
                 MYKLESTAD BEAM DESCRIPTION OF VARYING SPRING NUMBER I
                                                          1≤KSTA(I)≤NESTA

KVAR(I)        - CARD NUMBER (NOT A STATION IDENTIFICATION COUNTER) FROM INTERVAL
                 MYKLESTAD BEAM DESCRIPTION OF VARYING SPRING NUMBER I
                 NOTE: KVAR(I)≥KSTA(I)                    1≤KVAR(I)≤NSTA

SPRINGL(I)     - LOWER LIMIT TO WHICH SPRING RATE MAY BE CHANGED FOR VARYING
                 SPRING NUMBER I - LB/IN OR IN-LB/RAD     0.0<SPRINGL(I)

SPRINGU(I)     - UPPER LIMIT TO WHICH SPRING RATE MAY BE CHANGED FOR VARYING
                 SPRING NUMBER I - LB/IN OR IN-LB/RAD     0.0<SPRINGU(I)
                 NOTE: SPRINGU(I)>SPRINGL(I)

KTYPE(I)       - TYPE OF SPRING OPTION COUNTER FOR VARYING SPRING NUMBER I
                                                          1≤KTYPE(I)≤2
                 IF KTYPE(I)=1, A SHEAR SPRING HAS BEEN INDICATED AND SPRINGL(I)
                                AND SPRINGU(I) ARE INPUT IN UNITS OF LB/IN.
                 IF KTYPE(I)=2, A FLEXURAL SPRING HAS BEEN INDICATED AND SPRINGL(I)
                                AND SPRINGU(I) ARE INPUT IN UNITS OF IN-LB/RAD.
```

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TABLE A-3 (CONT'D.)

~~FORTRAN CODING AND DATA FORM~~

PROBLEM

PROGRAMMER

```
EXPERIMENTAL MODE SHAPE DEFLECTIONS AND SLOPES (CARD FORMAT - 6X,2I3,5E12.5)

      1    1   EPHI(1,1)    EPHI(1,2)    EPHI(1,3)    EPHI(1,4)    EPHI(1,5)
      2    1   EPHI(2,1)    EPHI(2,2)    EPHI(2,3)    EPHI(2,4)    EPHI(2,5)
      :    :       :            :            :            :            :
  NESTA    1 EPHI(NESTA,1) EPHI(NESTA,2) EPHI(NESTA,3) EPHI(NESTA,4) EPHI(NESTA,5)
      1    6   EPHI(1,6)    EPHI(1,7)        :        EPHI(1,NEXP)
      2    6   EPHI(2,6)    EPHI(2,7)        :        EPHI(2,NEXP)
      :    :       :            :            :            :
  NESTA    6 EPHI(NESTA,6) EPHI(NESTA,7)     :        EPHI(NESTA,NEXP)

      1    1   EPHIP(1,1)   EPHIP(1,2)   EPHIP(1,3)   EPHIP(1,4)   EPHIP(1,5)
      2    1   EPHIP(2,1)   EPHIP(2,2)   EPHIP(2,3)   EPHIP(2,4)   EPHIP(2,5)
      :    :       :            :            :            :            :
  NESTA    1 EPHIP(NESTA,1) EPHIP(NESTA,2) EPHIP(NESTA,3) EPHIP(NESTA,4) EPHIP(NESTA,5)
      1    6   EPHIP(1,6)   EPHIP(1,7)       :        EPHIP(1,NEXP)
      2    6   EPHIP(2,6)   EPHIP(2,7)       :        EPHIP(2,NEXP)
      :    :       :            :            :            :
  NESTA    6 EPHIP(NESTA,6) EPHIP(NESTA,7)    :        EPHIP(NESTA,NEXP)

EPHI(I,J)  - EXPERIMENTAL MODE SHAPE DEFLECTION AT INTERNAL MYKLESTAD BEAM
             STATION I FOR EXPERIMENTAL MODE NUMBER J - IN/IN

EPHIP(I,J) - EXPERIMENTAL MODE SHAPE SLOPES AT INTERNAL MYKLESTAD BEAM
             STATION I FOR EXPERIMENTAL MODE NUMBER J - RAD/IN

NOTE: THESE CARDS ARE PUNCHED BY PROGRAM FILLIN.
```

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TABLE 19-3 (CONT'D.)

~~FORTRAN CODING AND DATA FORM~~

PROBLEM

PROGRAMMER

```
MYKLESTAD FORMAT BEAM DESCRIPTIONS OF STATIONS (CARD FORMAT - 2I4, 3I2, 2X, 7E8.0)

ITEM1(1) ITEM2(1) (1) (1) (1)   DATA1(1) DATA2(1) DATA3(1) DATA4(1) DATA5(1) DATA6(1) DATA7(1)
ITEM1(2) ITEM2(2) (2) (2) (2)   DATA1(2) DATA2(2) DATA3(2) DATA4(2) DATA5(2) DATA6(2) DATA7(2)
   :        :      :   :   :       :       :       :       :       :       :       :       :
ITEM1(K) ITEM2(K) (K) (K) (K)   DATA1(K) DATA2(K) DATA3(K) DATA4(K) DATA5(K) DATA6(K) DATA7(K)
   :        :      :   :   :       :       :       :       :       :       :       :       :

ITEM1(I) - STATION IDENTIFICATION COUNTER FOR STATION I                    ITEM1(I) > 0
           NOTE: THE FIRST STATION OF THE MAIN BEAM MUST BE LABELED 1,
                 I.E., ITEM1(1) = 1. AS A GENERAL PRACTICE, STATION IDENTIFICATION
                 COUNTERS SHOULD BE UNIQUE SINCE APPENDAGE ATTACHMENT STATION
                 NUMBERS REFER TO THESE IDENTIFICATION COUNTERS.

ITEM2(I) - APPENDAGE ATTACHMENT STATION IDENTIFICATION NUMBER FOR STATION I
                                                                           ITEM2(I) ≥ 0
           NOTE: EXCEPT FOR THE MAIN BEAM IN WHICH ITEM2(I) = 0, THE APPENDAGE
                 ATTACHMENT STATION IDENTIFICATION NUMBER MUST REFER TO A
                 STATION ID. COUNTER, I.E. ITEM2(I) = ITEM1(J) FOR A STATION J
                 IN WHICH ITEM4(J) = 2
                 (WITHIN AN APPENDAGE, ALL ATTACHMENT NUMBERS ARE EQUAL)

ITEM3(I) - DESIGNATION OF APPENDAGE ORDER FOR STATION I                    ITEM3(I) ≥ -1
           NOTE: IF MAIN BEAM, ITEM3(I) = 0
                 IF APPENDAGE ATTACHES TO MAIN BEAM, ITEM3(I) = 1
                 IF APPENDAGE ATTACHES TO A FIRST ORDER APPENDAGE, ITEM3(I) = 2
                 ETC.
                 FOR A REDUNDANT APPENDAGE, ITEM3(I) = -1
```

TABLE A-3 (CONT'D.)

~~FORTRAN CODING AND DATA FORM~~

PROBLEM | ~~ENG~~ | ~~MAP~~

PROGRAMMER | ~~PHONE EXT.~~ | ~~DATE~~

```
ITEM4(I)  -  DESIGNATION OF STATION TYPE FOR STATION I                    0≤ITEM4(I)≤4
                 0  -  MASS STATION
                 1  -  SPRING STATION
                 2  -  APPENDAGE ATTACHMENT STATION
                 3  -  FORWARD REDUNDANT APPENDAGE ATTACHMENT STATION
                 4  -  AFT REDUNDANT APPENDAGE ATTACHMENT STATION
            NOTE: ENTER ALL REDUNDANT APPENDAGES LAST STARTING FROM FORWARD END

ITEMS(I)  -  DESIGNATION OF TYPE OF MOTION FOR STATION I                  0≤ITEMS(I)≤2
                 0  -  BENDING
                 1  -  TORSION
                 2  -  COMPRESSIVE

            BENDING(ITEMS(I)=0)          TORSION(ITEMS(I)=1)          COMPRESSIVE(ITEMS(I)=2)

DATA1(I)    EI  -  LB*IN²                GJ  -  LB*IN²                EA  -  LB
DATA2(I)    WEIGHT  -  LB
DATA3(I)    X  -  IN                     X  -  IN                     X  -  IN
DATA4(I)    Jm  -  LB*IN²                Ix  -  LB*IN²                WEIGHT  -  LB
DATA5(I)    Km  -  IN/LB  OR  α  -  DEG  α  -  DEG                    α  -  DEG
DATA6(I)    Kα  -  RAD/IN*LB  OR  β-DEG  β-DEG  OR  Kβ-RAD/IN*LB      β-DEG  OR  Kβ-IN*LB
DATA7(I)                  φ  -  DEG    φ  -  DEG                    φ  -  DEG

NOTE: ENTER ALL MAIN BEAM CARDS FIRST, THEN APPENDAGE CARDS - MAIN BEAM AND
      APPENDAGE CARDS MUST BE IN ORDER AS PROGRAM DOES NO SORTING.
      ENTER APPENDAGES STARTING AT FREE END, ENDING AT ATTACHED END.
      EVERY STATION EXCEPT LAST SHOULD HAVE A VALUE IN DATA1(I). THIS IS THE
      STIFFNESS FROM X(I) TO X(I+1).
      WEIGHT AND INERTIA VALUES ARE ASSUMED TO BE LUMPED AT X(I)
      WEIGHTS AND INERTIA SHOULD ONLY BE ENTERED IF ITEM4(I)=0
```

GENERAL DYNAMICS
Electro Dynamic Division
POMONA OPERATION

TABLE A-3 (CONT'D.)

~~FORTRAN CODING AND DATA FORM~~

PROBLEM

PROGRAMMER

```
WITHIN THE MAIN BEAM OR ANY APPENDAGE, X(I+1) ≥ X(I)
(A STATION LOCATION IS NEEDED FOR EACH CARD INPUT, CAN BE ZERO)
PARAMETERS SHOULD ONLY BE ENTERED IN DATA5(I), DATA6(I) AND DATA7(I)
IF ITEM4(I)=1 OR 2
ITEM1(I)=0 ENDS THE READING OF THE BEAM DESCRIPTION CARDS - READ A
MAXIMUM OF 100 OF THESE CARDS (COUNTING THE ITEM1(I)=0 CARD)

ALSO CONTAINED ON THE ITEM1(I)=0 CARD ARE THE FOLLOWING PARAMETERS:

ITEM2(I) - DESIGNATION OF BOUNDARY CONDITIONS FOR MAIN BEAM          1≤ITEM2(I)≤6
           1 - FREE FORWARD END, FREE AFT END
           2 - FREE FORWARD END, CLAMPED AFT END
           3 - CLAMPED FORWARD END, CLAMPED AFT END
           4 - FREE FORWARD END, PINNED AFT END
           5 - PINNED FORWARD END, CLAMPED AFT END
           6 - PINNED FORWARD END, PINNED AFT END

DATA1(I) -- STARTING FREQUENCY FOR MYKLESTAD MODE SEARCH FOR MODE 1 - HZ
                                                                DATA1(I)≥0.0
           NOTE: IF DATA1(I) IS BLANK OR ZERO, PROGRAM SETS DATA1(I)=2.5 HZ

DATA2(I) - TOLERANCE ON FREQUENCY FOR MODE DETERMINATION          DATA2(I)≥0.0
           NOTE: IF DATA2(I) IS BLANK OR ZERO, PROGRAM SETS DATA2(I)=1.0x10^-5

DATA3(I) -- FREQUENCY CHANGE BITE SIZE PARAMETER                  DATA3(I)≥0.0
           (FREQnew=FREQold *DATA3(I))
           NOTE: IF DATA3(I) IS BLANK OR ZERO, PROGRAM SETS DATA3(I)=1.10

DATA4(I) - UPPER MODE SEARCH FREQUENCY - HZ                       DATA4(I)≥0.0
           NOTE: IF DATA4(I) IS BLANK OR ZERO, PROGRAM SETS DATA4(I)=250.0
```

NOTE: ADDITIONAL DATA DECKS MAY BE SUBMITTED, STARTING WITH A NEW TITLE CARD, ETC.

Table A-4
FORTRAN Listing of Program FILLIN

```
      PROGRAM FILLIN(INPUT=65,OUTPUT=65,TAPE 60=INPUT,PUNCH=65)
      DIMENSION XSTA(200),XESTA(200),EPHI(200,10),EPHIP(200,10),PHI(200,
     110),NAEND(11),NAAS(200),ITME(5,201),DAAT(7,201),TITLE(8),NAONE(11)
     2,LABEL(200),ITYPE(200),PSAVE(10),NAS(200),
     3SHEL(5),LAONE(11),LAEND(11)
      COMMON Y(4),PH(4) A(3),X,P,PP,D,YSQ(4)
   10 READ20,TITLE
   20 FORMAT(8A10)
      IF(EOF(60))30,40
   30 CALL EXIT
   40 PRINT 50,TITLE
   50 FORMAT(1H1,15X,8A10)
C
C     READ BEAM DESCRIPTION
C
      NX=0
   60 NX=NX+1
      READ70,(ITME(LL,NX),LL=1,5),(DAAT(KK,NX),KK=1,7)
   70 FORMAT(2I4,3I2,2X,7E8.0)
      IF(ITME(1,NX).NE.0)GO TO 60
C     READ CONTROL CARD
C
      READ80,NSTA,NESTA,NEXP
   80 FORMAT(3I5)
      PRINT 90,NSTA,NESTA
   90 FORMAT(///20X,*NUMBER OF MYKLESTAD STATIONS=*,I5,10X,*NUMBER OF EX
     1PERIMENTAL POINTS=*,I5)
      NCARD=NX
C
C     PRINT BEAM DESCRIPTION
C
      PRINT 100
  100 FORMAT(///,20X,*MYKLESTAD INPUT*,///)
      DO 110 I=1,NCARD
  110 PRINT 120,I,(ITME(J,I),J=1,5),(DAAT(JJ,I),JJ=1,7)
  120 FORMAT (6I4,4X,7E13.5)
C
C     READ IN AND PRINT MEASUREMENT STATIONS AND APPENDAGE INDICATORS
C
      READ130,(NAAS(I),XESTA(I),I=1,NESTA)
  130 FORMAT((4(I10,E10.0)))
      PRINT 140,(I,NAAS(I),XESTA(I),I=1,NESTA)
  140 FORMAT(1H1,10X,*MODAL MEASUREMENT STATIONS AND APPENDAGE ATTACHMEN
     1T STATION NUMBERS*,/(20X,2I10,10X,E13.5))
      L=1
      LAONE(1)=1
      DO 150 I=2,NESTA
      IF(NAAS(I).EQ.NAAS(I-1))GO TO 150
      LAEND(L)=I-1
      L=L+1
```

Table A-4
(Cont'd.)

```
      LAONE(L)=I                                                        FIL 510
  150 CONTINUE                                                          FIL 520
      LAEND(L)=NESTA                                                    FIL 530
C                                                                       FIL 540
C     READ AND PRINT EXPERIMENTAL MODE SHAPES OR SLOPES                 FIL 550
C                                                                       FIL 560
      PRINT 160                                                         FIL 570
  160 FORMAT(1H1,20X,*EXPERIMENTAL MODE SHAPES*,//)                     FIL 580
      MSTA=NESTA                                                        FIL 590
      IF(NEXP.GT.5)MSTA=2*NESTA                                         FIL 600
      DO 180 IT=1,MSTA                                                  FIL 610
      READ190,J,K,(SHEL(L),L=1,5)                                       FIL 620
      PRINT 200,J,NAAS(IT),K,(SHEL(L),L=1,5)                            FIL 630
      DO 170 L=1,5                                                      FIL 640
  170 PHI(J,(K+L-1))=SHEL(L)                                            FIL 650
  180 CONTINUE                                                          FIL 660
  190 FORMAT(6X,2I3,5E12.5)                                             FIL 670
  200 FORMAT(6X,3I6,5X,5E12.5)                                          FIL 680
C                                                                       FIL 690
C     DEFINE MYKLESTAD OUTPUT STATIONS                                  FIL 700
C     DEFINE APPENDAGE END POINTS                                       FIL 710
C     INITIALIZE NAT=NUMBER OF APPENDAGES, NA=APPENDAGE NUMBER,         FIL 720
C     NAONE(NA),NAEND(NA)=NUMBERS OF FIRST AND LAST STATIONS,           FIL 730
C     DEFINE STATION TYPE,ITYPE(J)=0(NO JOINT),1(LEFT SIDE ROTATIONAL   FIL 740
C     SPRING), 2 (LEFT SIDE SHEAR SPRING), 3 (LEFT SIDE ROTATIONAL AND  FIL 750
C     SHEAR SPRINGS), 4 (RIGHT SIDE ROTATIONAL SPRING), 5 (RIGHT SIDE   FIL 760
C     SHEAR SPRING), 6 (RIGHT SIDE ROTATIONAL AND SHEAR SPRINGS)        FIL 770
C                                                                       FIL 780
      NAT=NA=NAONE(1)=1                                                 FIL 790
      NN=1                                                              FIL 800
      K=0                                                               FIL 810
      DO 270 J=1,NSTA                                                   FIL 820
      XSTA(J)=DAAT(3,NN)                                                FIL 830
      LABEL(J)=ITME(1,NN)                                               FIL 840
      NAS(J)=ITME(2,NN)                                                 FIL 850
      ITYPE(J)=0                                                        FIL 860
      IF(K.NE.0)GO TO 210                                               FIL 870
      IF(ITME(4,NN).EQ.0)GO TO 230                                      FIL 880
      IF(ITME(4,NN).NE.1)GO TO 260                                      FIL 890
      IF(DAAT(6,NN).NE.0)ITYPE(J)=1                                     FIL 900
      IF(DAAT(5,NN).NE.0)ITYPE(J)=2                                     FIL 910
      IF(DAAT(5,NN).NE.0.AND.DAAT(6,NN).NE.0)ITYPE(J)=3                 FIL 920
      GO TO 260                                                         FIL 930
  210 K=0                                                               FIL 940
      IF(ITME(4,NN).NE.1)GO TO 220                                      FIL 950
      IF(DAAT(6,NN).NE.0)ITYPE(J)=4                                     FIL 960
      IF(DAAT(5,NN).NE.0)ITYPE(J)=5                                     FIL 970
      IF(DAAT(5,NN).NE.0.AND.DAAT(6,NN).NE.0)ITYPE(J)=6                 FIL 980
      GO TO 230                                                         FIL 990
  220 NN=1+NN                                                           FIL1000
```

Table A-4
(Cont'd.)

```
      GO TO 270                                                         FIL1010
  230 IF(ITME(1,NN+1).EQ.0)GO TO 240                                    FIL1020
      IF(ITME(2,NN).NE.ITME(2,NN+1))GO TO 240                           FIL1030
      NN=1+NN                                                           FIL1040
      K=0                                                               FIL1050
      GO TO 270                                                         FIL1060
  240 NAEND(NA)=1+J                                                     FIL1070
      IF(ITME(1,NN+1).EQ.0)GO TO 250                                    FIL1080
      NA=1+NA                                                           FIL1090
      NAONE(NA)=2+J                                                     FIL1100
      GO TO 260                                                         FIL1110
  250 NAT=NA                                                            FIL1120
  260 K=1                                                               FIL1130
  270 CONTINUE                                                          FIL1140
      NAEND(NAT)=NSTA                                                   FIL1150
C                                                                       FIL1160
      PRINT 280,NAT                                                     FIL1170
  280 FORMAT(//10X,*NUMBER OF APPENDAGES INCLUDING MAIN BEAM=*,I3)      FIL1180
      PRINT 290                                                         FIL1190
  290 FORMAT(//10X*APPENDAGE NUMBER*,5X*FIRST STATION*,5X*END STATION*) FIL1200
      PRINT 300,(J,NAONE(J),NAEND(J),J=1,NAT)                           FIL1210
  300 FORMAT(20X,I3,12X,I3,12X,I3)                                      FIL1220
      PRINT 310                                                         FIL1230
  310 FORMAT(1H1,T10*STATION NUMBER*T30*STATION*T50*LABEL*T70*TYPE*T90*A FIL1240
     1PPENDAGE LABEL*/)                                                 FIL1250
      PRINT 320,(J,XSTA(J),LABEL(J),ITYPE(J),NAS(J),J=1,NSTA)           FIL1260
  320 FORMAT(I20,15X,F13.5,I7,I18,I20)                                  FIL1270
C                                                                       FIL1280
      DO 840 L=1,NAT                                                    FIL1290
      II=NAONE(L)                                                       FIL1300
      IFN=NAEND(L)                                                      FIL1310
      JI=LAONE(L)                                                       FIL1320
      JFN=LAEND(L)                                                      FIL1330
      JN=JFN-JI+1                                                       FIL1340
      DO 830 I=II,IFN                                                   FIL1350
      X=XSTA(I)                                                         FIL1360
      IT=ITYPE(I)+1                                                     FIL1370
      GO TO (330,450,540,630,690,760,790)IT                             FIL1380
C     PLAIN STATION                                                     FIL1390
  330 IF(X.LE.XESTA(JI+1))GO TO 390                                     FIL1400
      IF(X.GE.XESTA(JFN-1))GO TO 400                                    FIL1410
      IF(JN.GT.4)GO TO 360                                              FIL1420
      IF(JN.EQ.4)GO TO 410                                              FIL1430
      JO=JI                                                             FIL1440
      JE=JI+1                                                           FIL1450
      Y(1)=XESTA(JO)                                                    FIL1460
      Y(2)=XESTA(JE)                                                    FIL1470
  340 D=1.0/(Y(2)-Y(1))                                                 FIL1480
      DO 350 M=1,NEXP                                                   FIL1490
      PH(1)=PHI(JO,M)                                                   FIL1500
```

Table A-4
(Cont'd.)

```
      PH(2)=PHI(JE,M)                                                   FIL1510
      CALL LINFIT                                                       FIL1520
      EPHI(I,M)=P                                                       FIL1530
  350 EPHIP(I,M)=PP                                                     FIL1540
      GO TO (830,460,550,680,700,770,820)IT                             FIL1550
  360 JJ=JI+1                                                           FIL1560
      JM=JFN-2                                                          FIL1570
      DO 370 J=JJ,JM                                                    FIL1580
      IF(X.GT.XESTA(J).AND.X.LE.XESTA(J+1))GO TO 380                    FIL1590
  370 CONTINUE                                                          FIL1600
  380 JONE=J-1                                                          FIL1610
      GO TO 420                                                         FIL1620
  390 Y(1)=XESTA(JI)                                                    FIL1630
      Y(2)=XESTA(JI+1)                                                  FIL1640
      JO=JI                                                             FIL1650
      JE=JI+1                                                           FIL1660
      GO TO 340                                                         FIL1670
  400 Y(1)=XESTA(JFN-1)                                                 FIL1680
      Y(2)=XESTA(JFN)                                                   FIL1690
      JO=JFN-1                                                          FIL1700
      JE=JFN                                                            FIL1710
      GO TO 340                                                         FIL1720
  410 JONE=JI                                                           FIL1730
  420 CONTINUE                                                          FIL1740
      DO 440 M=1,NEXP                                                   FIL1750
      DO 430 K=1,4                                                      FIL1760
      Y(K)=XESTA(K+JONE-1)                                              FIL1770
  430 PH(K)=PHI(K+JONE-1,M)                                             FIL1780
      CALL SQUARE                                                       FIL1790
      CALL PARAB                                                        FIL1800
      EPHI(I,M)=P                                                       FIL1810
  440 EPHIP(I,M)=PP                                                     FIL1820
      GO TO (830,460,550,680,700,770,820)IT                             FIL1830
  450 KSAVE=1                                                           FIL1840
      GO TO 330                                                         FIL1850
  460 KSAVE=KSAVE+1                                                     FIL1860
      IF(KSAVE.EQ.3)GO TO 520                                           FIL1870
      DO 470 M=1,NEXP                                                   FIL1880
  470 PSAVE(M)=EPHI(I,M)                                                FIL1890
      DO 480 J=JI,JFN                                                   FIL1900
      JJ=J                                                              FIL1910
      IF(X.EQ.XESTA(J))GO TO 500                                        FIL1920
      IF(X.LT.XESTA(J))GO TO 490                                        FIL1930
  480 CONTINUE                                                          FIL1940
      GO TO 510                                                         FIL1950
  490 JFN=JJ-1                                                          FIL1960
      GO TO 510                                                         FIL1970
  500 JFN=JJ                                                            FIL1980
  510 JL=JJ-JI                                                          FIL1990
      IF(JL.GT.3)JI=JJ-3                                                FIL2000
```

Table A-4
(Cont'd.)

```
      JN=JFN-JI+1                                                       FIL2010
      GO TO 330                                                         FIL2020
  520 DO 530 M=1,NEXP                                                   FIL2030
  530 EPHI(I,M)=PSAVE(M)                                                FIL2040
      JI=LAONE(L)                                                       FIL2050
      JFN=LAEND(L)                                                      FIL2060
      JN=JFN-JI+1                                                       FIL2070
      GO TO 830                                                         FIL2080
  540 KSAVE=1                                                           FIL2090
      GO TO 630                                                         FIL2100
  550 KSAVE=1+KSAVE                                                     FIL2110
      IF(KSAVE.EQ.3)GO TO 610                                           FIL2120
      DO 560 M=1,NEXP                                                   FIL2130
  560 PSAVE(M)=EPHIP(I,M)                                               FIL2140
      DO 570 J=JI,JFN                                                   FIL2150
      JJ=J                                                              FIL2160
      IF(X.EQ.XESTA(J))GO TO 590                                        FIL2170
      IF(X.LT.XESTA(J))GO TO 580                                        FIL2180
  570 CONTINUE                                                          FIL2190
      GO TO 600                                                         FIL2200
  580 JFN=JJ-1                                                          FIL2210
      GO TO 600                                                         FIL2220
  590 JFN=JJ                                                            FIL2230
  600 JL=JJ-JI                                                          FIL2240
      IF(JL.GT.3)JI=JJ-3                                                FIL2250
      JN=JFN-JI+1                                                       FIL2260
      GO TO 330                                                         FIL2270
  610 DO 620 M=1,NEXP                                                   FIL2280
  620 EPHIP(I,M)=PSAVE(M)                                               FIL2290
      JI=LAONE(L)                                                       FIL2300
      JFN=LAEND(L)                                                      FIL2310
      JN=JFN+1-JI                                                       FIL2320
      GO TO 830                                                         FIL2330
C                                                                       FIL2340
C     STATION TO LEFT OF A ROTATIONAL AND A SHEAR SPRING                FIL2350
C                                                                       FIL2360
  630 DO 640 J=JI,JFN                                                   FIL2370
      JJ=J                                                              FIL2380
      IF(X.EQ.XESTA(J))GO TO 660                                        FIL2390
      IF(X.LT.XESTA(J))GO TO 650                                        FIL2400
  640 CONTINUE                                                          FIL2410
      GO TO 670                                                         FIL2420
  650 JFN=JJ-1                                                          FIL2430
      GO TO 670                                                         FIL2440
  660 JFN=JJ                                                            FIL2450
  670 JL=JJ-JI                                                          FIL2460
      IF(JL.GT.3)JI=JJ-3                                                FIL2470
      JN=JFN-JI+1                                                       FIL2480
      GO TO 330                                                         FIL2490
  680 JFN=LAEND(L)                                                      FIL2500
```

Table A-4
(Cont'd.)

```
      JI=LAONE(L)                                                       FIL2510
      JN=JFN+1-JI                                                       FIL2520
      GO TO 830                                                         FIL2530
C                                                                       FIL2540
C     STATION TO RIGHT OF A ROTATIONAL SPRING                           FIL2550
C                                                                       FIL2560
  690 KSAVE=1                                                           FIL2570
      GO TO 330                                                         FIL2580
  700 KSAVE=1+KSAVE                                                     FIL2590
      IF(KSAVE.EQ.3)GO TO 740                                           FIL2600
      DO 710 M=1,NEXP                                                   FIL2610
  710 PSAVE(M)=EPHI(I,M)                                                FIL2620
      DO 720 J=JI,JFN                                                   FIL2630
      JJ=J                                                              FIL2640
      IF(X.LE.XESTA(J))GO TO 730                                        FIL2650
  720 CONTINUE                                                          FIL2660
      GO TO 830                                                         FIL2670
  730 JI=JJ                                                             FIL2680
      IF(JI+3.LE.JFN)JFN=JI+3                                           FIL2690
      JN=JFN-JI+1                                                       FIL2700
      GO TO 330                                                         FIL2710
  740 DO 750 M=1,NEXP                                                   FIL2720
  750 EPHI(I,M)=PSAVE(M)                                                FIL2730
      JI=LAONE(L)                                                       FIL2740
      JFN=LAEND(L)                                                      FIL2750
      JN=JFN-JI+1                                                       FIL2760
      GO TO 830                                                         FIL2770
C                                                                       FIL2780
C     STATION TO RIGHT OF A SHEAR SPRING                                FIL2790
C                                                                       FIL2800
  760 KSAVE=1                                                           FIL2810
      GO TO 790                                                         FIL2820
  770 DO 780 M=1,NEXP                                                   FIL2830
      EPHIP(I,M)=0.5*(EPHIP(I-1,M)+EPHIP(I,M))                          FIL2840
  780 EPHIP(I-1,M)=EPHIP(I,M)                                           FIL2850
      GO TO 830                                                         FIL2860
C                                                                       FIL2870
C     STATION TO THE RIGHT OF A ROTATIONAL SPRING AND A SHEAR SPRING    FIL2880
C                                                                       FIL2890
  790 DO 800 J=JI,JFN                                                   FIL2900
      JJ=J                                                              FIL2910
      IF(X.LE.XESTA(J))GO TO 810                                        FIL2920
  800 CONTINUE                                                          FIL2930
      GO TO 830                                                         FIL2940
  810 JI=JJ                                                             FIL2950
      IF(JI+3.LE.JFN)JFN=JI+3                                           FIL2960
      JN=JFN-JI+1                                                       FIL2970
      GO TO 330                                                         FIL2980
  820 JFN=LAEND(L)                                                      FIL2990
      JI=LAONE(L)                                                       FIL3000
```

Table A-4
(Cont'd.)

```
      JN=JFN+1-JI                                                       FIL3010
      IF(IT.EQ.6)GO TO 770                                              FIL3020
  830 CONTINUE                                                          FIL3030
  840 CONTINUE                                                          FIL3040
      DO 880 I=1,NEXP                                                   FIL3050
      PRINT 850,I                                                       FIL3060
  850 FORMAT(1H1,20X*COMPLETE EXPERIMENTAL MODE*,I4,//,T15,*STATION NUMB FIL3070
     1ER*,T30,*STATION LABEL*,T45,*APPENDAGE LABEL*,T70,*STATION TYPE*,T FIL3080
     295,*STATION*,T98,*DISPLACEMENT*,T118,*SLOPE*,//)                  FIL3090
      DO 860 J=1,NSTA                                                   FIL3100
  860 PRINT 870,J,LABEL(J),NAS(J),ITYPE(J),XSTA(J),EPHI(J,I),EPHIP(J,I) FIL3110
  870 FORMAT(20X,I5,I10,2I20,5X,3E15.5)                                 FIL3120
  880 CONTINUE                                                          FIL3130
      NP=1                                                              FIL3140
  890 IT=1                                                              FIL3150
      NE=NEXP                                                           FIL3160
      IF(NEXP.GT.5)NE=5                                                 FIL3170
  900 DO 920 J=1,NSTA                                                   FIL3180
      PUNCH 910,J,IT,(EPHI(J,L),L=IT,NE)                                FIL3190
  910 FORMAT(6X,2I3,5E12.5)                                             FIL3200
  920 CONTINUE                                                          FIL3210
      IF(NEXP.GT.NE)GO TO 930                                           FIL3220
      GO TO 940                                                         FIL3230
  930 IT=6                                                              FIL3240
      NE=NEXP                                                           FIL3250
      GO TO 900                                                         FIL3260
  940 NP=NP+1                                                           FIL3270
      IF(NP.EQ.3)GO TO 960                                              FIL3280
      DO 950 L=1,NEXP                                                   FIL3290
      DO 950 J=1,NSTA                                                   FIL3300
  950 EPHI(J,L)=EPHIP(J,L)                                              FIL3310
      GO TO 890                                                         FIL3320
  960 CONTINUE                                                          FIL3330
      GO TO 10                                                          FIL3340
      END                                                               FIL3350
```

Table A-5
FORTRAN Listing of Subroutine SQUARE

```
      SUBROUTINE SQUARE                                                 SQU  10
      COMMON Y(4),PH(4),A(3),X,P,PP,D,YSQ(4)                            SQU  20
      DIMENSION Z(4),F(4)                                               SQU  30
      DO 10 I=1,4                                                       SQU  40
      Z(I)=Y(I)                                                         SQU  50
      F(I)=PH(I)                                                        SQU  60
      Y(I)=0.0                                                          SQU  70
      YSQ(I)=0.0                                                        SQU  80
   10 PH(I)=0.0                                                         SQU  90
      DO 20 I=1,4                                                       SQU 100
      PH(1)=PH(1)+F(I)                                                  SQU 110
      Y(1)=Y(1)+Z(I)                                                    SQU 120
      YSQ(1)=YSQ(1)+Z(I)*Z(I)                                           SQU 130
      PH(2)=PH(2)+F(I)*Z(I)                                             SQU 140
      YSQ(2)=YSQ(2)+Z(I)*Z(I)*Z(I)                                      SQU 150
      PH(3)=PH(3)+F(I)*Z(I)*Z(I)                                        SQU 160
   20 YSQ(3)=YSQ(3)+Z(I)**4                                             SQU 170
      PH(1)=0.25*PH(1)                                                  SQU 180
      Y(1)=0.25*Y(1)                                                    SQU 190
      YSQ(1)=0.25*YSQ(1)                                                SQU 200
      Y(2)=YSQ(1)/Y(1)                                                  SQU 210
      PH(2)=0.25*PH(2)/Y(1)                                             SQU 220
      YSQ(2)=0.25*YSQ(2)/Y(1)                                           SQU 230
      PH(3)=0.25*PH(3)/YSQ(1)                                           SQU 240
      Y(3)=0.25*Y(3)/YSQ(1)                                             SQU 250
      YSQ(3)=0.25*YSQ(3)/YSQ(1)                                         SQU 260
      D=1.0/(Y(2)*YSQ(3)+Y(1)*YSQ(2)+Y(3)*YSQ(1)-Y(2)*YSQ(1)-Y(1)*YSQ(3) SQU 270
     1-Y(3)*YSQ(2))                                                     SQU 280
      END                                                               SQU 290
```

Table A-6
FORTRAN Listing of Subroutine PARAB

```
      SUBROUTINE PARAB                                                  PAR  10
      COMMON Y(4),PH(4),A(3),X,P,PP,D,YSQ(4)                            PAR  20
      A(1)=D*(PH(1)*(Y(2)*YSQ(3)-Y(3)*YSQ(2))+PH(2)*                    PAR  30
     1(Y(3)*YSQ(1)-Y(1)*YSQ(3))-PH(3)*(Y(2)*YSQ(1)-Y(1)*YSQ(2)))        PAR  40
      A(2)=D*(PH(1)*(YSQ(2)-YSQ(3))+PH(2)*(YSQ(3)-YSQ(1))+PH(3)*(YSQ(1)- PAR  50
     1YSQ(2)))                                                          PAR  60
      A(3)=D*(PH(1)*(Y(3)-Y(2))+PH(2)*(Y(1)-Y(3))+PH(3)*(Y(2)-Y(1)))    PAR  70
      P=A(1)+A(2)*X+A(3)*X*X                                            PAR  80
      PP=A(2)+2*A(3)*X                                                  PAR  90
      END                                                               PAR 100
```

Table A-7
FORTRAN Listing of Subroutine LINFIT

```
SUBROUTINE LINFIT                                                    LIN  10
COMMON Y(4),PH(4),A(3),X,P,PP,D,YSQ(4)                               LIN  20
A(1)=D*(Y(2)*PH(1)-Y(1)*PH(2))                                       LIN  30
A(2)=D*(PH(2)-PH(1))                                                 LIN  40
P=A(1)+A(2)*X                                                        LIN  50
PP=A(2)                                                              LIN  60
END                                                                  LIN  70
```

Table A-8
FORTRAN Listing of Program JOINTS

```
      PROGRAM JOINTS (INPUT,OUTPUT,TAPE60=INPUT,TAPE6=OUTPUT)
C
C     PROGRAM JOINTS - PROBLEM 2049   02/26/71   VARIABLE DELTAK
C                      WITH SHEAR SPRINGS
C
      DIMENSION MAXSIGN(10),NSMAXPH(10),NAONE(10),NAEND(10)
      DIMENSION TITLE(8),          GM(10),SHFL(5),BB(10,10),CC(10,10)
      DIMENSION STFREQ(10),XFSTA(100)
C
C     STORAGE COMMON TO SUBROUTINE MYKL
C
      COMMON    FINK(300)
      COMMON    A(4,4,101),SAP(4,4),AP(4,4),VINV(4,4),ALV(4,4),T(4,4),AL
     1VT(4,4),TAP(4,4,100),VEC(4,101),ITEM(6,101),CATA(8,101),I1(300),IR
     2(300),OM(300),FUNC(300),R(3),KKK(100),MODE(100),JCINT(101),AL(4,4)
     3,I6(101),PRNT(4),HOL(12)
      COMMON    ICON(10),ICB(10),FPM(10,4,4),FOM(10,4,4),VSAVE(4),ARSTAR
     1(10,6,4),          ARPB(4,4),ARPA(4,4),APR(4,4),DANV(2,2),DENV(2,2
     2),THMAN(6,6),BMAN(6,6),BINV(6,6),RMUL(6,4)
      COMMON    I4(101)
      COMMON    ITMF(5,101),DAAT(7,101),IETM(5),DTAA(7)
C
C     STORAGE COMMON TO SUBROUTINE STEEP
C
      COMMON/1/ MWH, ISTOP,NSTA,NT,NEXP,STEP,ITMAX,TOL,ITER
      COMMON/2/     KKKK,ALPHA,F,PFK(20),INTEG(20)
      COMMON/3/PWMAT(10),FWMAT(10),EOMEGS(10),KVAR(20),SPRINGL(20),SPRIN
     1GU(20),EPHI(100,10),EPHIP(100,10),EFREQ(10),TFREQ(10)
      COMMON/4/TOMEGS(10),TPHI(100,10),TPHIP(100,10)
      COMMON/5/JA,JB,JD,FF,    SPFK(10),AA(10,10),ASPRING(20)
      COMMON/6/NVSPR,SPRING(10),SSPRING(10),KSTA(10),KTYPE(10),COMP(10)
      COMMON/7/XRATIO,OLDSPR(10)
      COMMON/8/KNORM,XSTA(100)
      CALL MEMSET (PINK(1),DTAA(7))
C
C     READ AND PRINT TITLE
C
   10 READ20,TITLE
   20 FORMAT(8A10)
      IF(EOF(60))30,40
   30 CALL EXIT
   40 PRINT 50,TITLE
   50 FORMAT(1H1,20X*EXTRACTION OF JOINT COMPLIANCES FROM ELASTIC MODE T
     1EST DATA*//20X,8A10///)
C
C     INITIALIZATION PASS
C
      ISTOP=0
      ITER=1
C
```

Table A-8
(Cont'd.)

```
C     READING OPTIONS, WEIGHTING MATRICES, AND LIMITS                   JTS 510
C                                                                       JTS 520
      READ60,KNORM,NT,NEXP,NWT,ITMAX,NVSPR,NSTA,NESTA,STEP,TOL,CLOSE,  X JTS 530
     1RATIO                                                             JTS 540
   60 FORMAT(4I5,4I5,4E10.0)                                            JTS 550
      IF(KNORM.EQ.0) KNORM=1                                            JTS 560
      NOTM=NT                                                           JTS 570
      PRINT 70,    NT,NEXP,ITMAX,NVSPR,NSTA,STEP,CLOSE,NWT,NESTA        JTS 580
   70 FORMAT(//40X,* NT      = *,I13,/40X,* NEXP    = *,I13,/40X,* ITMAX  JTS 590
     1= *,I13,/40X,* NVSPR  = *,I13,/40X,* NSTA    = *,I13,/40X,* STEP   JTS 600
     2=*,E13.5,/40X,* CLOSE =*,E13.5,/40X,* NWT    =*,I13,20X,*NESTA =*,I JTS 610
     313)                                                               JTS 620
      KCLOSE=0                                                          JTS 630
      IF(CLOSE.EQ.0.0) KCLOSE=1                                         JTS 640
      PRINT 80,TOL                                                      JTS 650
   80 FORMAT( 40X,* TOL     = *,E13.5)                                  JTS 660
      READ90,KCHECK,XMASS                                               JTS 670
   90 FORMAT(I5,E10.0)                                                  JTS 680
      IF(KCHECK.NE.2)GO TO 110                                          JTS 690
      PRINT 100,XMASS                                                   JTS 700
  100 FORMAT(//20X*MODES WILL NOT BE CHECKED*,//20X,*XMASS = *,E13.5)   JTS 710
      GO TO 130                                                         JTS 720
  110 PRINT 120,XMASS                                                   JTS 730
  120 FORMAT(//20X*MODES WILL BE CHECKED*,//20X,*XMASS = *,E13.5)       JTS 740
  130 IF(NWT.EQ.0)GO TO 145                                             JTS 750
      READ140,(PWMAT(I),I=1,NEXP)                                       JTS 760
  140 FORMAT (8E10.0)                                                   JTS 770
      READ140,(FWMAT(I),I=1,NEXP)                                       JTS 772
      GO TO 149                                                         JTS 773
  145 DO 146 I=1,NEXP                                                   JTS 775
  146 PWMAT(I)=FWMAT(I)=1.0                                             JTS 778
  149 PRINT 150                                                         JTS 780
  150 FORMAT(//10X,* RELATIVE MODE SHAPE WEIGHTING FACTORS * )          JTS 790
      PRINT 160,(PWMAT(I),I=1,NEXP)                                     JTS 800
  160 FORMAT(/ 1X,10E13.5)                                              JTS 810
      PRINT 170                                                         JTS 830
  170 FORMAT(//10X,* RELATIVE MODE FREQUENCY WEIGHTING FACTORS * )      JTS 840
      PRINT 160,(FWMAT(I),I=1,NEXP)                                     JTS 850
  180 READ140,(EFREQ(I),I=1,NT)                                         JTS 860
      PRINT 190                                                         JTS 870
  190 FORMAT(//10X,* EXPERIMENTAL FREQUENCIES *)                        JTS 880
      PRINT 160,(EFREQ(I),I=1,NT)                                       JTS 890
      DO 200 I=1,NT                                                     JTS 900
  200 EOMEGS(I)=(6.283185*EFREQ(I))**2                                  JTS 910
      RNST=XMASS/(2.0*NESTA)                                            JTS 950
      WF=EOMEGS(NEXP)**2                                                JTS 970
      DO 220 I=1,NEXP                                                   JTS 980
      PWMAT(I)=RNST*WF*PWMAT(I)                                         JTS1000
  220 FWMAT(I)=FWMAT(I)*WF/(EOMEGS(I)**2)                               JTS1010
      PRINT 223                                                         JTS1020
```

Table A-8
(Cont'd.)

```
  223 FORMAT(//10X,* MODE SHAPE WEIGHTING FACTORS * )                    JTS1025
      PRINT 160,(PWMAT(I),I=1,NEXP)                                      JTS1030
      PRINT 226                                                          JTS1040
  226 FORMAT(//10X,* MODE FREQUENCY WEIGHTING FACTORS * )                JTS1045
      PRINT 160,(FWMAT(I),I=1,NEXP)                                      JTS1050
  230 READ240,(KSTA(I),KVAR(I),SPRINGL(I),SPRINGU(I),KTYPE(I),I=1,NVSPR) JTS1060
  240 FORMAT(2I4,2E8.0,I4)                                               JTS1070
      PRINT 250                                                          JTS1080
  250 FORMAT(//22X,* K*,* KVAR(I)*,2X,* SPRINGL(I)*,2X,* SPRINGU(I)*,2X, JTS1090
     1* KTYPE*)                                                          JTS1100
      PRINT 260,(KSTA(I),KVAR(I),SPRINGL(I),SPRINGU(I),KTYPE(I),I=1,NVSP JTS1110
     1R)                                                                 JTS1120
  260 FORMAT(/ (20X,I4,I8,2E13.5,I6))                                    JTS1130
      DO 270 I=1,10                                                      JTS1140
      DO 270 J=1,NSTA                                                    JTS1150
      EPHI(J,I)=0.0                                                      JTS1160
  270 EPHIP(J,I)=0.0                                                     JTS1170
C                                                                        JTS1180
C     READING EXPERIMENTAL MODAL DATA                                    JTS1190
C                                                                        JTS1200
      IF(NESTA.EQ.NSTA)GO TO 290                                         JTS1210
      READ140,(XESTA(I),I=1, NESTA)                                      JTS1220
      PRINT 280                                                          JTS1230
  280 FORMAT(//30X,*MODE MEASUREMENT STATIONS, XESTA(I)*)                JTS1240
      PRINT 160,(XESTA(I),I=1,NESTA)                                     JTS1250
  290 PRINT 300                                                          JTS1260
  300 FORMAT(1H1,20X,25H EXPERIMENTAL MODE SHAPES,//)                    JTS1270
      MSTA=NESTA                                                         JTS1280
      IF(NEXP.GT.5)MSTA=2*NESTA                                          JTS1290
      DO 320 IT=1,MSTA                                                   JTS1300
      READ330,J,K,(SHEL(L),L=1,5)                                        JTS1310
      PRINT 330,J,K,(SHEL(L),L=1,5)                                      JTS1320
      DO 310 L=1,5                                                       JTS1330
  310 EPHI(J,(K+L-1))=SHEL(L)                                            JTS1340
  320 CONTINUE                                                           JTS1350
  330 FORMAT(6X,2I3,5E12.5)                                              JTS1360
      PRINT 340                                                          JTS1370
  340 FORMAT(1H1,20X,25H EXPERIMENTAL MODE SLOPES,//)                    JTS1380
      DO 360 IT=1,MSTA                                                   JTS1390
      READ330,J,K,(SHEL(L),L=1,5)                                        JTS1400
      PRINT 330,J,K,(SHEL(L),L=1,5)                                      JTS1410
      DO 350 L=1,5                                                       JTS1420
  350 EPHIP(J,(K+L-1))=SHEL(L)                                           JTS1430
  360 CONTINUE                                                           JTS1440
C                                                                        JTS1450
C     READ BEAM DESCRIPTION                                              JTS1460
C                                                                        JTS1470
      NX=0                                                               JTS1480
  370 NX=NX+1                                                            JTS1490
      READ380,(ITME(LL,NX),LL=1,5),(DAAT(KK,NX),KK=1,7)                  JTS1500
```

Table A-8
(Cont'd.)

```
  380 FORMAT (2I4,3I2,2X,7E8.0)                                          JTS1510
      IF(ITME(1,NX).NE.0)GO TO 370                                       JTS1520
C                                                                        JTS1530
C     LAST DATA CARD HAS BEEN READ                                       JTS1540
C                                                                        JTS1550
      NCARD=NX                                                           JTS1560
C                                                                        JTS1570
C     PRINT BEAM DESCRIPTION                                             JTS1580
C                                                                        JTS1590
      PRINT 390                                                          JTS1600
  390 FORMAT(1H1,* BEAM DESCRIPTION READ BY PROGRAM JOINTS*///)          JTS1610
      DO 410 I=1,NCARD                                                   JTS1620
      PRINT 400,(ITME(J,I),J=1,5),(DAAT(JJ,I),JJ=1,7)                    JTS1630
  400 FORMAT ((5I4,4X,7E13.5))                                           JTS1640
  410 CONTINUE                                                           JTS1650
C                                                                        JTS1660
C     SETTING STATIONS TO INTERNAL COUNTERS                              JTS1670
C     DEFINE APPENDAGE NUMBERS = NA, TOTAL NUMBER = NAT, FIRST AND LAST  JTS1680
C     STATION NUMBERS = NAONE(NA) AND NAEND(NA),                         JTS1690
C                                                                        JTS1700
      NAT=NA=NAONE(1)=1                                                  JTS1710
      NN=1                                                               JTS1720
      K=0                                                                JTS1730
      DO 460 J=1,NSTA                                                    JTS1740
      XSTA(J)=DAAT(3,NN)                                                 JTS1750
      IF(K.NE.0)GO TO 420                                                JTS1760
      IF(ITME(4,NN).NE.0)GO TO 450                                       JTS1770
      IF(ITME(1,NN+1).EQ.0)GO TO 430                                     JTS1780
      IF(ITME(2,NN).NE.ITME(2,NN+1))GO TO 430                            JTS1790
  420 NN=NN+1                                                            JTS1800
      K=0                                                                JTS1810
      GO TO 460                                                          JTS1820
  430 NAEND(NA)=J+1                                                      JTS1830
      IF(ITME(1,NN+1).EQ.0)GO TO 440                                     JTS1840
      NA=NA+1                                                            JTS1850
      NAONE(NA)=J+2                                                      JTS1860
      GO TO 450                                                          JTS1870
  440 NAT=NA                                                             JTS1880
  450 K=1                                                                JTS1890
  460 CONTINUE                                                           JTS1900
      PRINT 470,NAT                                                      JTS1910
  470 FORMAT(/10X,*NAT = *,I3)                                           JTS1920
      PRINT 480                                                          JTS1930
  480 FORMAT(/10X,*  J*,5X,*NAONE(J)*,5X,*NAEND(J)*)                     JTS1940
      PRINT 490,(J,NAONE(J),NAEND(J),J=1,NAT)                            JTS1950
  490 FORMAT(10X,I3,5X,I8,5X,I8)                                         JTS1960
C                                                                        JTS1970
C     COMPUTING GENERALIZED MASS FOR THE INPUT MODES                     JTS1980
C                                                                        JTS1990
      DO 520 I=1,NEXP                                                    JTS2000
```

Table A-8
(Cont'd.)

```
      NN=0                                                              JTS2010
      JJ=0                                                              JTS2020
      GM(I)=0.0                                                         JTS2030
  500 NN=NN+1                                                           JTS2040
      JJ=JJ+1                                                           JTS2050
      IF(ITME(4,NN).NE.0)GO TO 510                                      JTS2060
      GM(I)=GM(I)+DAAT(2,NN)*EPHI(JJ,I)*EPHI(JJ,I)+DAAT(4,NN)*EPHIP(JJ,I JTS2070
     1)*EPHIP(JJ,I)                                                     JTS2080
      IF(ITME(2,NN).NE.ITME(2,NN+1)) JJ=JJ+1                            JTS2090
      IF(JJ.LT.NSTA)GO TO 500                                           JTS2100
      GO TO 520                                                         JTS2110
  510 JJ=JJ+1                                                           JTS2120
      GO TO 500                                                         JTS2130
  520 GM(I)=GM(I)/386.4                                                 JTS2140
      PRINT 530                                                         JTS2150
  530 FORMAT(/5X,* THE GENERALIZED MASS ASSOCIATED WITH THE INPUT MODES* JTS2160
     1/)                                                                JTS2170
      PRINT 540,(GM(I),I=1,NEXP)                                        JTS2180
  540 FORMAT(1X,5E20.8)                                                 JTS2190
C     DEFINE STATION NUMBER OF LARGEST DISPLACEMENT FOR EACH            JTS2200
C     EXPERIMENTAL MODE NSMAXPH(I)                                      JTS2210
      DO 550 I=1,NEXP                                                   JTS2220
      NSMAXPH(I)=1                                                      JTS2230
      MAXSIGN(I)=1                                                      JTS2240
      IF(EPHI(1,I).LT.0.0) MAXSIGN(I)=-1                                JTS2250
      PHMAX=ABS(EPHI(1,I))                                              JTS2260
      NAE=NAEND(1)                                                      JTS2270
      DO 550 J=2,NAE                                                    JTS2280
      IF(ABS(EPHI(J,I)).LE.PHMAX)GO TO 550                              JTS2290
      PHMAX=ABS(EPHI(J,I))                                              JTS2300
      MAXSIGN(I)=1                                                      JTS2310
      IF(EPHI(J,I).LT.0.0) MAXSIGN(I)=-1                                JTS2320
      NSMAXPH(I)=J                                                      JTS2330
  550 CONTINUE                                                          JTS2340
C                                                                       JTS2350
C     NORMALIZING THE INPUT MODES TO A GENERALIZED MASS OF 1.0          JTS2360
C                                                                       JTS2370
      DO 560 I=1,NEXP                                                   JTS2380
      FACT=SQRT(1.0/GM(I))                                              JTS2390
      DO 560 J=1,NSTA                                                   JTS2400
      EPHI(J,I)=FACT*EPHI(J,I)                                          JTS2410
  560 EPHIP(J,I)=FACT*EPHIP(J,I)                                        JTS2420
      KKKK=0                                                            JTS2430
      DO 600 J=1,NVSPR                                                  JTS2440
      NN=KSTA(J)                                                        JTS2450
      IF(KTYPF(J).EQ.2)GO TO 570                                        JTS2460
      IF(DAAT(5,NN).EQ.0.)GO TO 580                                     JTS2470
      SPRING(J)=1.0/DAAT(5,NN)                                          JTS2480
      GO TO 600                                                         JTS2490
  570 IF(DAAT(6,NN).EQ.0.)GO TO 580                                     JTS2500
```

Table A-8
(Cont'd.)

```
      SPRING(J)=1.0/DAAT(6,NN)                                          JTS2510
      GO TO 600                                                         JTS2520
  580 PRINT 590,J                                                       JTS2530
  590 FORMAT(//6H  ****,18H COMPLIANCE NUMBER,I3,15H IS ZERO.  ****)    JTS2540
      ISTOP=1                                                           JTS2550
  600 CONTINUE                                                          JTS2560
      ITME(3,NCARD)=1                                                   JTS2570
      IF(DAAT(4,NCARD).EQ.0.0) DAAT(4,NCARD)=250.                       JTS2580
      IF(DAAT(3,NCARD).EQ.0.0) DAAT(3,NCARD)=1.10                       JTS2590
      IF(DAAT(1,NCARD).EQ.0.0) DAAT(1,NCARD)=2.5                        JTS2600
      SFREQ=DAAT(1,NCARD)                                               JTS2610
      STOPFR=DAAT(4,NCARD)                                              JTS2620
      DO 610 J=1,NVSPR                                                  JTS2630
  610 SSPRING(J)=SPRING(J)                                              JTS2640
      JA=0                                                              JTS2650
      JB=0                                                              JTS2660
      JD=0                                                              JTS2670
      MIKE=0                                                            JTS2680
      DELF=DAAT(3,NCARD)                                                JTS2690
      DO 620 I=1,NT                                                     JTS2700
  620 STFREQ(I)=EFREQ(I)                                                JTS2710
      IF(ISTOP.EQ.1)GO TO 10                                            JTS2720
      MWH=0                                                             JTS2730
      IF(XMASS.GT.0.0) GO TO 630                                        JTS2732
      PRINT 625                                                         JTS2734
  625 FORMAT(//10X,62H* MISSILE MASS HAS BEEN READ AS ZERO.  THIS CASE T JTS2736
     1ERMINATED. *)                                                     JTS2737
      GO TO 10                                                          JTS2738
C                                                                       JTS2740
C     END OF INITIALIZATION PASS                                        JTS2750
C     GENERAL PASS                                                      JTS2760
C                                                                       JTS2770
  630 CONTINUE                                                          JTS2780
      DO 650 J=1,NVSPR                                                  JTS2790
      NN=KSTA(J)                                                        JTS2800
      IF(KTYPE(J).EQ.2)GO TO 640                                        JTS2810
      DAAT(5,NN)=1.0/SPRING(J)                                          JTS2820
      GO TO 650                                                         JTS2830
  640 DAAT(6,NN)=1.0/SPRING(J)                                          JTS2840
  650 CONTINUE                                                          JTS2850
      IF(ITER.EQ.1)GO TO 670                                            JTS2860
      DO 660 I=1,NT                                                     JTS2870
  660 STFREQ(I)=TFREQ(I)                                                JTS2880
  670 CONTINUE                                                          JTS2890
      NT=NCTM                                                           JTS2900
      MTS=0                                                             JTS2910
      DO 680 I=1,NT                                                     JTS2920
      TFREQ(I)=0.0                                                      JTS2930
      DO 680 K=1,NSTA                                                   JTS2940
      TPHI(K,I)=0.0                                                     JTS2950
```

Table A-8
(Cont'd.)

```
  680 TPHIP(K,I)=0.0                                                    JTS2960
      DAAT(1,NCARD)=SFREQ                                               JTS2970
C                                                                       JTS2980
C     SOLVE FOR NEW FREQUENCIES AND MODE SHAPES                         JTS2990
C                                                                       JTS3000
      PRINT 690,ITER                                                    JTS3010
  690 FORMAT(1H1,40X,21H INPUT FOR ITERATION ,I3/)                      JTS3020
      LIME=0                                                            JTS3030
      DO 830 I=1,NCTM                                                   JTS3040
      DAAT(3,NCARD)=DELF                                                JTS3050
      DAAT(4,NCARD)=STOPER                                              JTS3060
      IF(MTS.EQ.1)GO TO 830                                             JTS3070
      IF(I.EQ.1)GO TO 760                                               JTS3080
      IF(KCLOSE.EQ.1)GO TO 730                                          JTS3090
      IF(STFREQ(I).NE.0.0)GO TO 710                                     JTS3100
      PRINT 700,I                                                       JTS3110
  700 FORMAT(13H  *** STFREQ(,I2,35H) EQUALS 0.0, THIS CASE TERMINATED.) JTS3120
      MIKE=1                                                            JTS3130
      GO TO 810                                                         JTS3140
  710 XFREQ=CLOSE* EFREQ(I)                                             JTS3150
      YFREQ=DELF*EFREQ(I-1)                                             JTS3160
      IF(XFREQ.GT.YFREQ)GO TO 720                                       JTS3170
      XFREQ= EFREQ(I-1)+( EFREQ(I)- EFREQ(I-1))/2.0                     JTS3180
      DAAT(3,NCARD)=1.0+((EFREQ(I)-EFREQ(I-1))/(6.0*EFREQ(I)))          JTS3190
  720 DAAT(1,NCARD)=XFREQ                                               JTS3200
      GO TO 740                                                         JTS3210
  730 DAAT(1,NCARD)=DAAT(3,NCARD)*TFREQ(I-1)                            JTS3220
  740 IF(DAAT(1,NCARD).GT.DAAT(4,NCARD))GO TO 810                       JTS3230
      PRINT 750,(ITME(J,NCARD),J=1,5),(DAAT(JJ,NCARD),JJ=1,7)           JTS3240
  750 FORMAT(/(5I4,4X,7E13.5))                                          JTS3250
  760 CALL MYKL(FREQ,GAM,LIME)                                          JTS3260
      LIME=1                                                            JTS3270
      IF(FREQ.NE.0.)GO TO 780                                           JTS3280
      PRINT 770                                                         JTS3290
  770 FORMAT(/* ERROR IN COMPUTED MODE FREQUENCIES.  FREQ=0.0, THIS CASE JTS3300
     1 ABORTED *)                                                       JTS3310
      MIKE=1                                                            JTS3320
  780 CONTINUE                                                          JTS3330
      IF(I.EQ.1)GO TO 790                                               JTS3340
      IF(FREQ.EQ.TFREQ(I-1))GO TO 820                                   JTS3350
  790 CONTINUE                                                          JTS3360
      DO 800 K=1,NSTA                                                   JTS3370
      TPHI(K,I)=VEC(4,K)                                                JTS3380
  800 TPHIP(K,I)=VEC(3,K)                                               JTS3390
      TFREQ(I)=FREQ                                                     JTS3400
      GM(I)=GAM                                                         JTS3410
      GO TO 830                                                         JTS3420
  810 IF(MTS.EQ.1)GO TO 830                                             JTS3430
      NT=I                                                              JTS3440
      MTS=1                                                             JTS3450
```

Table A-8
(Cont'd.)

```
      GO TO 830                                                         JTS3460
  820 NT=I-1                                                            JTS3470
      MTS=1                                                             JTS3480
  830 CONTINUE                                                          JTS3490
      IF(MIKE.EQ.1)GO TO 10                                             JTS3500
C                                                                       JTS3510
C     MATCHING CORRESPONDING MODES                                      JTS3520
C                                                                       JTS3530
C     FIND MISSING MODES                                                JTS3540
C                                                                       JTS3550
      NT=NCTM                                                           JTS3560
      DO 1070 I=1,NT                                                    JTS3570
      IF(KCHECK.EQ.2)GO TO 1040                                         JTS3580
      LBITE=0                                                           JTS3590
  840 NSGNCH=0                                                          JTS3600
      DO 860 NA=1,NAT                                                   JTS3610
      NSGN=1                                                            JTS3620
      IF(TPHIP(NAONE(NA),I).LT.0.0)NSGN=-1                              JTS3630
      N1=NAONE(NA)+1                                                    JTS3640
      N2=NAEND(NA)                                                      JTS3650
      DO 850 J=N1,N2                                                    JTS3660
      NSG=1                                                             JTS3670
      IF( TPHIP(J,I).LT.0.0)NSG=-1                                      JTS3680
      IF(NSG.EQ.NSGN)GO TO 850                                          JTS3690
      NSGN=NSG                                                          JTS3700
      NSGNCH=NSGNCH+1                                                   JTS3710
  850 CONTINUE                                                          JTS3720
  860 CONTINUE                                                          JTS3730
      IF(NSGNCH.EQ.I)GO TO 1040                                         JTS3740
      LBITE=LBITE+1                                                     JTS3750
      GO TO (940,960,870)LBITE                                          JTS3760
  870 PRINT 880                                                         JTS3770
  880 FORMAT(1H1,20X*MODES HAVE BEEN MISSED THREE TIMES.....CURRENT MODE JTS3780
     1S AND SLOPES*//)                                                  JTS3790
      NL=1                                                              JTS3800
  890 NN=NL+3                                                           JTS3810
      IF(NN.GT.NT)NN=NT                                                 JTS3820
      DO 900 KS=1,NSTA                                                  JTS3830
  900 PRINT 910,KS,(TPHI(KS,KM),TPHIP(KS,KM),KM=NL,NN)                  JTS3840
  910 FORMAT((2X,I4,4(3X,2F13.5)))                                      JTS3850
      NL=NL+4                                                           JTS3860
      IF(NL.LE.NT)GO TO 890                                             JTS3870
      PRINT 920                                                         JTS3880
  920 FORMAT(//20X*FREQUENCIES AND GENERALIZED MASSES* ,//)             JTS3890
      PRINT 930,(KM,TFREQ(KM),GM(KM),KM=1,NT)                           JTS3900
  930 FORMAT((10X,I5,2(10XF17.7)))                                      JTS3910
      GO TO 10                                                          JTS3920
  940 PRINT 950,I                                                       JTS3930
  950 FORMAT(//20X*MODE*,I5,3X*HAS BEEN MISSED ONCE*)                   JTS3940
      GO TO 980                                                         JTS3950
```

Table A-8
(Cont'd.)

```
  960 PRINT 970,I                                                       JTS3960
  970 FORMAT(//20X*MODE*,I5,3X*HAS BEEN MISSED TWICE*)                  JTS3970
  980 CONTINUE                                                          JTS3980
      IF(NSGNCH.GT.NT)GO TO 1000                                        JTS3990
      MN=NSGNCH                                                         JTS4000
      MM=MN+NT                                                          JTS4010
      MI=I+NT                                                           JTS4020
      DO 990 M=MN,NT                                                    JTS4030
      TFREQ(-M+MM)=TFREQ(-M+MI)                                         JTS4040
      GM(-M+MM)=GM(-M+MI)                                               JTS4050
      DO 990 L=1,NSTA                                                   JTS4060
      TPHI(L,-M+MM)=TPHI(L,-M+MI)                                       JTS4070
  990 TPHIP(L,-M+MM)=TPHIP(L,-M+MI)                                     JTS4080
      INF=MN-1                                                          JTS4090
      DAAT(4,NCARD)=0.99*TFREQ(INF+1)                                   JTS4100
      GO TO 1010                                                        JTS4110
 1000 INF=NT                                                            JTS4120
      DAAT(4,NCARD)=0.99*TFREQ(NT)                                      JTS4130
 1010 DAAT(3,NCARD)=1.0+0.2*(DAAT(3,NCARD)-1.0)                         JTS4140
      DO 1030 IN=I,INF                                                  JTS4150
      DAAT(1,NCARD)=SFREQ*(0.9**LBITE)                                  JTS4160
      IF(IN.NE.1)DAAT(1,NCARD)=1.01*TFREQ(I-1)                          JTS4170
      PRINT 750,(ITME(J,NCARD),J=1,5),(DAAT(JJ,NCARD),JJ=1,7)           JTS4180
      CALL MYKL(FREQ,GAM,LIME)                                          JTS4190
      DO 1020 K=1,NSTA                                                  JTS4200
      TPHI(K ,IN)=VEC(4,K)                                              JTS4210
 1020 TPHIP(K,IN)=VEC(3,K)                                              JTS4220
      TFREQ(IN)=FREQ                                                    JTS4230
 1030 GM(IN)=GAM                                                        JTS4240
      GO TO 840                                                         JTS4250
C     COMPARE POLARITY TO THAT OF EXPERIMENTAL MODE                     JTS4260
C                                                                       JTS4270
 1040 CONTINUE                                                          JTS4280
      IF(I.GT.NEXP)GO TO 1070                                           JTS4290
      NSIGN=1                                                           JTS4300
      IF(TPHI(NSMAXPH(I),I).LT.0.0)NSIGN=-1                             JTS4310
      IF(NSIGN.NE.MAXSIGN(I))GO TO 1050                                 JTS4320
      GO TO 1070                                                        JTS4330
 1050 DO 1060 J=1,NSTA                                                  JTS4340
      TPHI(J,I)=-TPHI(J,I)                                              JTS4350
 1060 TPHIP(J,I)=-TPHIP(J,I)                                            JTS4360
 1070 CONTINUE                                                          JTS4370
      PRINT 1080                                                        JTS4380
 1080 FORMAT(/*  COMPUTED GENERALIZED MASS FOR THE MYKL MODES ARE */)   JTS4390
      PRINT 1090,(GM(I),I=1,NT)                                         JTS4400
 1090 FORMAT(2X,10E13.5)                                                JTS4410
C                                                                       JTS4420
C     NORMALIZING MYKL MODES TO A GENERALIZED MASS OF 1.0               JTS4430
C                                                                       JTS4440
      DO 1100 I=1,NT                                                    JTS4450
```

Table A-8
(Cont'd.)

```
      TOMEGS(I)=(6.283185*TFREQ(I))**2                                  JTS4460
      FACT=SQRT(1.0/GM(I))                                              JTS4470
      DO 1100 J=1,NSTA                                                  JTS4480
      TPHI(J,I)=FACT*TPHI(J,I)                                          JTS4490
 1100 TPHIP(J,I)=FACT*TPHIP(J,I)                                        JTS4500
      PRINT 1110                                                        JTS4510
 1110 FORMAT(/*  THE THEORETICAL MODES HAVE BEEN NORMALIZED *)          JTS4520
C                                                                       JTS4530
C     CHECK MODE SHAPE AND FREQUENCY                                    JTS4540
C     LOGIC FOR CONTROLING PROGRAM MYKL WILL BE LOCATED HERE            JTS4550
C                                                                       JTS4560
C     OBTAIN NEW ESTIMATES OF THE JOINT COMPLIANCES                     JTS4570
C                                                                       JTS4580
      CALL STEEP                                                        JTS4590
      IF(ITMAX.GT.1) GO TO 1115                                         JTS4593
      ITER=1                                                            JTS4594
      CALL RENORM                                                       JTS4595
      GO TO 10                                                          JTS4597
 1115 IF((MWH.LT.1).OR.(MWH.GT.2))GO TO 1120                            JTS4600
      CALL ALTER                                                        JTS4610
      GO TO 630                                                         JTS4620
 1120 IF(ISTOP.EQ.0)GO TO 1130                                          JTS4630
      CALL RENORM                                                       JTS4640
      GO TO 10                                                          JTS4650
 1130 IF(JA.EQ.2)GO TO 1140                                             JTS4660
      GO TO 630                                                         JTS4670
C                                                                       JTS4680
C     CONVERGENCE CHECK ON SOLUTION                                     JTS4690
C                                                                       JTS4700
 1140 KZERO=0                                                           JTS4710
      DO 1150 K=1,NVSPR                                                 JTS4720
      DELTAK=ASPRING(K)-SSPRING(K)                                      JTS4730
      IF(DELTAK.EQ.0.0) KZERO=1                                         JTS4740
      IF(KZERO.EQ.1)GO TO 1160                                          JTS4750
      DO 1150 J=1,NVSPR                                                 JTS4760
 1150 BB(K,J)=(AA(J,K)-SPFK(J))/DELTAK                                  JTS4770
 1160 CONTINUE                                                          JTS4780
      IF(KZERO.EQ.0)GO TO 1180                                          JTS4790
      PRINT 1170                                                        JTS4800
 1170 FORMAT(10X,37H DELTAK = 0.0, THIS CASE TERMINATED. )              JTS4810
      GO TO 10                                                          JTS4820
 1180 CONTINUE                                                          JTS4830
C                                                                       JTS4840
C     BB(J,K)=THE MATRIX OF SECOND ORDER DERIVATIVES                    JTS4850
C                                                                       JTS4860
      PRINT 1190                                                        JTS4870
 1190 FORMAT(//10X,* THE SECOND ORDER DERIVATIVES ARE */)                JTS4880
      DO 1200 J=1,NVSPR                                                 JTS4890
 1200 PRINT 1210,(BB(J,K),K=1,NVSPR)                                    JTS4900
 1210 FORMAT(1X,10E13.5)                                                JTS4910
```

Table A-8
(Cont'd.)

```
C                                                                       JTS4920
C     AVERAGING THE SECOND ORDER DERIVATIVES                            JTS4930
C                                                                       JTS4940
      DO 1220 K=1,NVSPR                                                 JTS4950
      DO 1220 J=1,NVSPR                                                 JTS4960
 1220 AA(K,J)=(BB(K,J)+BB(J,K))/2.0                                     JTS4970
      DO 1230 J=1,NVSPR                                                 JTS4980
      DO 1230 K=1,NVSPR                                                 JTS4990
 1230 BB(J,K)=AA(J,K)                                                   JTS5000
      PRINT 1240                                                        JTS5010
 1240 FORMAT(//10X,* THE AVERAGED SECOND ORDER DERIVATIVES ARE */)      JTS5020
      DO 1250 J=1,NVSPR                                                 JTS5030
 1250 PRINT 1210,(BB(J,K),K=1,NVSPR)                                    JTS5040
C                                                                       JTS5050
C     CALL INVERSION ROUTINE                                            JTS5060
C                                                                       JTS5070
      CALL MATNF 5 (BB,NVSPR,10,   1.0,DET,IERROR)                      JTS5080
      PRINT 1260,DET                                                    JTS5090
 1260 FORMAT(/* DET = *,E16.7)                                          JTS5100
      PRINT 1270                                                        JTS5110
 1270 FORMAT(//10X,* THE INVERSE OF THE SECOND ORDER DERIVATIVES ARE */) JTS5120
      DO 1280 J=1,NVSPR                                                 JTS5130
 1280 PRINT 1210,(BB(J,K),K=1,NVSPR)                                    JTS5140
C                                                                       JTS5150
C     CHECKING THE INVERSE OF THE SECOND ORDER TERMS                    JTS5160
C                                                                       JTS5170
      DO 1290 I=1,NVSPR                                                 JTS5180
      DO 1290 J=1,NVSPR                                                 JTS5190
      CC(I,J)=0.0                                                       JTS5200
      DO 1290 K=1,NVSPR                                                 JTS5210
 1290 CC(I,J)=CC(I,J)+AA(I,K)*BB(K,J)                                   JTS5220
      PRINT 1300                                                        JTS5230
 1300 FORMAT(//*  THE INVERSE OF THE SECOND ORDER DERIVATIVES TIMES THE JTS5240
     1SECOND ORDER DERIVATIVES EQUAL */)                                JTS5250
      DO 1310 J=1,NVSPR                                                 JTS5260
 1310 PRINT 1210,(CC(J,K),K=1,NVSPR)                                    JTS5270
C                                                                       JTS5280
C     COMPUTING NEW SPRINGS RATES UTILIZING SECOND ORDER TERMS          JTS5290
C                                                                       JTS5300
      DO 1340 J=1,NVSPR                                                 JTS5310
      TEMP=0.0                                                          JTS5320
      DO 1320 K=1,NVSPR                                                 JTS5330
 1320 TEMP=TEMP+BB(J,K)*SPFK(K)                                         JTS5340
      SPRING(J)=SSPRING(J)-TEMP                                         JTS5350
      RATIO=ABS(SPRING(J)/SSPRING(J)-1.0)                               JTS5360
      IF(RATIO.LT.0.025)GO TO 1330                                      JTS5370
      XNUM=ASPRING(J)-SSPRING(J)                                        JTS5380
      XDEN=SPRING(J)-SSPRING(J)                                         JTS5390
      IF(XDEN.EQ.0.0)GO TO 1330                                         JTS5400
      RATIO=XNUM/XDEN                                                   JTS5410
```

Table A-8
(Cont'd.)

```
      IF(RATIO.LT.0.0) SPRING(J)=ASPRING(J)                                JTS5420
 1330 CONTINUE                                                             JTS5430
      IF(SPRING(J).LT.SPRINGL(J))SPRING(J)=SPRINGL(J)                      JTS5440
      IF(SPRING(J).GT.SPRINGU(J))SPRING(J)=SPRINGU(J)                      JTS5450
      COMP(J)=1.0/SPRING(J)                                                JTS5460
 1340 CONTINUE                                                             JTS5470
      PRINT 1350                                                           JTS5480
 1350 FORMAT(//20X,2H J,8X,5H K(J),9X,8H COMP(J),12X,8H SPFK(J),/)         JTS5490
      PRINT 1360,(J,SPRING(J),COMP(J),SPFK(J),J=1,NVSPR)                   JTS5500
 1360 FORMAT(18X,I4,2E16.6,E20.6)                                          JTS5510
      IF(ITER.LT.ITMAX)GO TO 1380                                          JTS5520
      PRINT 1370                                                           JTS5530
 1370 FORMAT(//* THE MAXIMUM NUMBER OF ITERATIONS HAS BEEN EXCEEDED *)     JTS5540
      ISTOP=1                                                              JTS5550
 1380 CONTINUE                                                             JTS5560
      MM=0                                                                 JTS5570
      DO 1400 J=1,NVSPR                                                    JTS5580
      RATIO=ABS(SPRING(J)/SSPRING(J)-1.0)                                  JTS5590
      IF(RATIO-TOL)1390,1400,1400                                          JTS5600
 1390 MM=MM+1                                                              JTS5610
 1400 CONTINUE                                                             JTS5620
      IF(MM.LT.NVSPR)GO TO 1420                                            JTS5630
      PRINT 1410                                                           JTS5640
 1410 FORMAT(//*  THE MINIMUM COST FUNCTION HAS BEEN FOUND *)              JTS5650
      ISTOP=1                                                              JTS5660
 1420 CONTINUE                                                             JTS5670
      DO 1430 J=1,NVSPR                                                    JTS5680
      OLDSPR(J)=SSPRING(J)                                                 JTS5690
      SSPRING(J)=SPRING(J)                                                 JTS5700
 1430 CONTINUE                                                             JTS5710
      IF(ISTOP.EQ.1)GO TO 630                                              JTS5720
      JD=0                                                                 JTS5730
      JA=1                                                                 JTS5740
      JB=0                                                                 JTS5750
      MWH=0                                                                JTS5760
      GO TO 630                                                            JTS5770
      END                                                                  JTS5780
```

Table A-9

FORTRAN Listing of Subroutine STEEP

```
      SUBROUTINE STEEP                                                  STP  10
C                                                                       STP  20
C     ESTIMATE SPRING VALUES TO IMPROVE MATCH OF BEAM MODEL             STP  30
C                                                                       STP  40
      COMMON/1/ MWH, ISTOP,NSTA,NT,NEXP,STEP,ITMAX,TOL,ITER             STP  50
      COMMON/2/      KKKK,ALPHA,F,PFK(20),INTEG(20)                     STP  60
      COMMON/3/PWMAT(10),FWMAT(10),EOMEGS(10),KVAR(20),SPRINGL(20),SPRIN STP  70
     1SU(20),EPHI(100,10),EPHIP(100,10),EFREQ(10),TFREQ(10)             STP  80
      COMMON/4/TOMEGS(10),TPHI(100,10),TPHIP(100,10)                    STP  90
      COMMON/5/JA,JB,JC,FF,     SPFK(10),AA(10,10),ASPRING(20)          STP 100
      COMMON/6/NVSPR,SPRING(10),SSPRING(10),KSTA(10),KTYPE(10),COMP(10) STP 110
      DIMENSION FACT(10),PXK(200),        FWI(10),FXI(10)               STP 120
C                                                                       STP 130
C     PRINTING OUT A COMPARISON OF EXPERIMENTAL AND THEORETICAL MODES   STP 140
C                                                                       STP 150
      PRINT 10, ITER                                                    STP 160
   10 FORMAT(1H1,* COMPARISON OF EXPERIMENTAL MODES TO THEORETICAL MODES STP 170
     1 FOR ITERATION NUMBER*,I3/)                                       STP 180
      NL=1                                                              STP 190
   20 NN=NL+3                                                           STP 200
      IF(NN.GT.NT)    NN=NT                                             STP 210
      DO 30 J=1,NSTA                                                    STP 220
   30 PRINT 40,  J,(EPHI(J,I),TPHI(J,I),I=NL,NN)                        STP 230
   40 FORMAT(2X,I4, 3X,2E13.5,3X,2E13.5,3X,2E13.5,3X,2E13.5)            STP 240
      NL=NL+4                                                           STP 250
      IF(NL.LE.NT)GO TO 20                                              STP 260
      PRINT 50                                                          STP 270
   50 FORMAT(1H1,* COMPARISON OF SLOPES -- EXPERIMENTAL TO THEORETICAL*/ STP 280
     1)                                                                 STP 290
      NL=1                                                              STP 300
   60 NN=NL+3                                                           STP 310
      IF(NN.GT.NT)    NN=NT                                             STP 320
      DO 70 J=1,NSTA                                                    STP 330
   70 PRINT 40,  J,(EPHIP(J,I),TPHIP(J,I),I=NL,NN)                      STP 340
      NL=NL+4                                                           STP 350
      IF(NL.LE.NEXP)GO TO 60                                            STP 360
      PRINT 80, ITER                                                    STP 370
   80 FORMAT(1H1,47X,* ITERATION*,I4//)                                 STP 380
      PRINT 90                                                          STP 390
   90 FORMAT(10X,* MODE*,10X,* EXPERIMENTAL FREQ*,10X,* THEORETICAL FREQ STP 400
     1*/)                                                               STP 410
      PRINT 100,(I,EFREQ(I),TFREQ(I),I=1,NT)                            STP 420
  100 FORMAT(10X,I5,10X,E18.7,10X,E17.7)                                STP 430
C                                                                       STP 440
C                                                                       STP 450
C     COMPUTATION OF THE QUADRATIC COST FUNCTION                        STP 460
C                                                                       STP 470
      FW=0.0                                                            STP 480
      FX=0.0                                                            STP 490
      NSP1=NSTA+1                                                       STP 500
```

Table A-9
(Cont'd.)

```
      NSX2=NSTA*2                                                       STP 510
      DO 130 I=1,NEXP                                                   STP 520
      FWI(I)=0.5*FWMAT(I)*(EOMEGS(I)-TOMEGS(I))*(EOMEGS(I)-TOMEGS(I))   STP 530
      FW=FW+FWI(I)                                                      STP 540
      FAC =0.0                                                          STP 550
      DO 110 J=1,NSTA                                                   STP 560
  110 FAC =FAC +(EPHI(J,I)-TPHI(J,I))*(EPHI(J,I)-TPHI(J,I))             STP 570
      DO 120 J=  NSP1,NSX2                                              STP 580
      JJ=J-NSTA                                                         STP 590
  120 FAC =FAC +(EPHIP(JJ,I)-TPHIP(JJ,I))*(EPHIP(JJ,I)-TPHIP(JJ,I))     STP 600
      FXI(I)=0.5*FAC*PWMAT(I)                                           STP 610
  130 FX=FX+FXI(I)                                                      STP 620
      F=FW+FX                                                           STP 630
      PRINT 140,F,FW,FX                                                 STP 640
  140 FORMAT(//22H  THE COST FUNCTION = ,E13.5,10X,6H FW = ,E13.5,10X,6H STP 650
     1 FX = ,E13.5/)                                                    STP 660
      PRINT 150,(I,FWI(I),FXI(I),I=1,NEXP)                              STP 670
  150 FORMAT(38X,I3,10X,E13.5,16X,E13.5)                                STP 680
      IF(ITER.EQ.1) FF=F                                                STP 690
      IF(JB.EQ.1) MWH=0                                                 STP 700
      IF(JB.NE.0)GO TO 160                                              STP 710
      IF(ITER.EQ.1)GO TO 160                                            STP 720
      IF(FF.GT.F) FF=F                                                  STP 730
      MWH=MWH+1                                                         STP 740
      IF(FF.GE.F) MWH=0                                                 STP 750
      IF((MWH.EQ.0).OR.(MWH.GT.2))GO TO 160                             STP 760
      GO TO 390                                                         STP 770
  160 IF(ISTOP.EQ.1)GO TO 390                                           STP 780
C                                                                       STP 790
C     COMPUTATION OF THE GRADIENTS FOR EACH UNKNOWN SPRING              STP 800
C     POMEGK(PARTIAL DERIVATIVE OF OMEGA SQUARED WITH RESPECT TO SPRING STP 810
C    1RATES K)                                                          STP 820
C                                                                       STP 830
      DO 280 J=1,NVSPR                                                  STP 840
      NN=KVAR(J)+1                                                      STP 850
      PFK(J)=0.0                                                        STP 860
      IF(JB.NE.0) AA(J,JB)=0.0                                          STP 870
      DO 280 I=1,NEXP                                                   STP 880
      IF(KTYPE(J).EQ.1)GO TO 170                                        STP 890
      POMEGK=(TPHIP(NN-1,I)-TPHIP(NN,I))**2                             STP 900
      GO TO 180                                                         STP 910
  170 POMEGK=(TPHI(NN-1,I)-TPHI(NN,I))**2                               STP 920
  180 CONTINUE                                                          STP 930
C                                                                       STP 940
C     PXK(PARTIAL DERIVATIVE OF PHI WITH RESPECT TO SPRING RATES K)     STP 950
C                                                                       STP 960
      DO 190 NX=1,NSX2                                                  STP 970
  190 PXK(NX)=0.0                                                       STP 980
      DO 240 L=1,NT                                                     STP 990
      IF(L.EQ.I)GO TO 240                                               STP1000
```

Table A-9
(Cont'd.)

```
      IF(KTYPE(J).EQ.1)GO TO 200                                        STP1010
      FACT(L)=(TPHIP(NN-1,L)*TPHIP(NN-1,I)-TPHIP(NN-1,L)*TPHIP(NN,I)-TPH STP1020
     1IP(NN,L)*TPHIP(NN-1,I)+TPHIP(NN,L)*TPHIP(NN,I))/(TOMEGS(I)-TOMEGS( STP1030
     2L))                                                               STP1040
      GO TO 210                                                         STP1050
  200 FACT(L)=(TPHI(NN-1,L)*TPHI(NN-1,I)-TPHI(NN-1,L)*TPHI(NN,I)-TPHI(NN STP1060
     1,L)*TPHI(NN-1,I)+TPHI(NN,L)*TPHI(NN,I))/(TOMEGS(I)-TOMEGS(L))     STP1070
  210 CONTINUE                                                          STP1080
      DO 220 NX=1,NSTA                                                  STP1090
  220 PXK(NX)=PXK(NX)+FACT(L)*TPHI(NX,L)                                STP1100
      DO 230 NX=NSP1,NSX2                                               STP1110
      NY=NX-NSTA                                                        STP1120
  230 PXK(NX)=PXK(NX)+FACT(L)*TPHIP(NY,L)                               STP1130
  240 CONTINUE                                                          STP1140
C                                                                       STP1150
C     COMPUTATION OF PFK(J)--PARTIAL DERIVATIVE OF F WRT K              STP1160
C                                                                       STP1170
      PFKX=0.0                                                          STP1180
      PFKW=0.0                                                          STP1190
      DO 250 N=1,NSTA                                                   STP1200
  250 PFKX=PFKX+PWMAT(I)*(TPHI(N,I)-EPHI(N,I))*PXK(N)                   STP1210
      DO 260 N=NSP1,NSX2                                                STP1220
      NY=N-NSTA                                                         STP1230
  260 PFKX=PFKX+PWMAT(I)*(TPHIP(NY,I) -EPHIP(NY,I))*PXK(N)              STP1240
      PFKW=FWMAT(I)*(TOMEGS(I)-EOMEGS(I))*POMEGK                        STP1250
      PFK(J)=PFK(J)+PFKX+PFKW                                           STP1260
      IF(JB.EQ.0)GO TO 270                                              STP1270
      AA(J,JB)=AA(J,JB)+PFKX+PFKW                                       STP1280
  270 CONTINUE                                                          STP1290
  280 CONTINUE                                                          STP1300
      IF(JB.EQ.NVSPR)GO TO 380                                          STP1310
      IF(JD.EQ.1)GO TO 300                                              STP1320
      JA=1                                                              STP1330
      JB=0                                                              STP1340
      JD=1                                                              STP1350
      DO 290 J=1,NVSPR                                                  STP1360
  290 SPFK(J)=PFK(J)                                                    STP1370
  300 CONTINUE                                                          STP1380
C                                                                       STP1390
C     COMPUTING WHERE THE COST FUNCTION GOES TO ZERO                    STP1400
C                                                                       STP1410
      JC=JB+1                                                           STP1420
      IF(SPFK(JC).GT.0.0)GO TO 310                                      STP1430
      ALPHA=-STEP*SSPRING(JC)                                           STP1440
      GO TO 320                                                         STP1450
  310 ALPHA=STEP*SSPRING(JC)                                            STP1460
  320 CONTINUE                                                          STP1470
C                                                                       STP1480
C     COMPUTING NEW GUESSES FOR THE VARIABLE SPRINGS                    STP1490
C                                                                       STP1500
```

Table A-9
(Cont'd.)

```
      IF(JB.EQ.0)GO TO 330                                              STP1510
      SPRING(JB)=SSPRING(JB)                                            STP1520
  330 CONTINUE                                                          STP1530
      JB=JB+1                                                           STP1540
      SPRING(JB)=SSPRING(JB)-ALPHA                                      STP1550
      IF(SPRING(JB).LT.SPRINGL(JB))SPRING(JB)=SPRINGL(JB)               STP1560
      IF(SPRING(JB).GT.SPRINGU(JB))SPRING(JB)=SPRINGU(JB)               STP1570
      ASPRING(JB)=SPRING(JB)                                            STP1580
      DO 340 J=1,NVSPR                                                  STP1590
  340 COMP(J)=1.0/SPRING(J)                                             STP1600
      PRINT 350                                                         STP1610
  350 FORMAT(/20X,2H J,8X,5H K(J),          11X,7H PFK(J),12X,8H COMP STP1620
     1(J)/)                                                             STP1630
      PRINT 360,(J,SPRING(J),      PFK(J),COMP(J),J=1,NVSPR)            STP1640
  360 FORMAT(18X,I4,E16.5,      2E18.5)                                 STP1650
      PRINT 370,ALPHA                                                   STP1660
  370 FORMAT(/10X,*  ALPHA = *,E16.5)                                   STP1670
      ITER=ITER+1                                                       STP1680
C                                                                       STP1690
      GO TO 390                                                         STP1700
C                                                                       STP1710
C                                                                       STP1720
  380 JA=2                                                              STP1730
      ITER=ITER+1                                                       STP1740
C                                                                       STP1750
C     RETURN TO PROGRAM JOINTS                                          STP1760
C                                                                       STP1770
  390 CONTINUE                                                          STP1780
      END                                                               STP1790
```

Table A-10
FORTRAN Listing of Subroutine ALTER

```
      SUBROUTINE ALTER                                                  ALT  10
C                                                                       ALT  20
C     ESTIMATE NEW SPRING RATES WHEN THE COST FUNCTION HAS INCREASED    ALT  30
C                                                                       ALT  40
      COMMON/6/NVSPR,SPRING(10),SSPRING(10),KSTA(10),KTYPE(10),COMP(10) ALT  50
      COMMON/7/XRATIO,OLDSPR(10)                                        ALT  60
      DIMENSION RATIO(10)                                               ALT  70
      DO 10 J=1,NVSPR                                                   ALT  80
      RATIO(J)=0.0                                                      ALT  90
      IF(OLDSPR(J).EQ.0.)GO TO 10                                       ALT 100
      RATIO(J)=SSPRING(J)/OLDSPR(J)                                     ALT 110
   10 CONTINUE                                                          ALT 120
      IF(XRATIO.EQ.0.) XRATIO=0.5                                       ALT 130
      XRATIO=1.0+XRATIO                                                 ALT 140
      YRATIO=1.0/XRATIO                                                 ALT 150
      KOUNT=0                                                           ALT 160
      DO 30 J=1,NVSPR                                                   ALT 170
      IF(RATIO(J).LE.XRATIO)GO TO 20                                    ALT 180
      SSPRING(J)=XRATIO*OLDSPR(J)                                       ALT 190
      KOUNT=KOUNT+1                                                     ALT 200
      GO TO 30                                                          ALT 210
   20 IF(RATIO(J).GE.YRATIO)GO TO 30                                    ALT 220
      SSPRING(J)=YRATIO*OLDSPR(J)                                       ALT 230
      KOUNT=KOUNT+1                                                     ALT 240
   30 CONTINUE                                                          ALT 250
      IF(KOUNT.NE.0)GO TO 50                                            ALT 260
      DO 40 J=1,NVSPR                                                   ALT 270
   40 SSPRING(J)=(SSPRING(J)-OLDSPR(J))/2.0+OLDSPR(J)                   ALT 280
   50 DO 60 J=1,NVSPR                                                   ALT 290
      SPRING(J)=SSPRING(J)                                              ALT 300
      COMP(J)=1.0/SSPRING(J)                                            ALT 310
   60 CONTINUE                                                          ALT 320
      PRINT 70                                                          ALT 330
   70 FORMAT(1H1,//20X,76H SINCE THE COST FUNCTION HAS INCREASED, NEW SP ALT 340
     1RING RATES HAVE BEEN COMPUTED.///)                                ALT 350
      PRINT 80                                                          ALT 360
   80 FORMAT(/20X,2H J,8X,5H K(J),9X,8H COMP(J),/)                      ALT 370
      PRINT 90,(J,SPRING(J),COMP(J),J=1,NVSPR)                          ALT 380
   90 FORMAT(18X,I4,2E16.6)                                             ALT 390
      END                                                               ALT 400
```

Table A-11

FORTRAN Listing of Subroutine RENORM

```
      SUBROUTINE RENORM                                                 REN  10
C                                                                       REN  20
C     RENORMALIZATION OF THE EXPERIMENTAL AND THEORETICAL MODES         REN  30
C                                                                       REN  40
      COMMON/1/ MWH, ISTOP,NSTA,NT,NEXP,STEP,ITMAX,TOL,ITER             REN  50
      COMMON/3/PWMAT(10),FWMAT(10),EOMEGS(10),KVAR(20),SPRINGL(20),SPRIN REN  60
     1GU(20),EPHI(100,10),EPHIP(100,10),EFREQ(10),TFREQ(10)             REN  70
      COMMON/4/TOMEGS(10),TPHI(100,10),TPHIP(100,10)                    REN  80
      COMMON/8/KNORM,XSTA(100)                                          REN  90
      DATA (MODE=10H MODE      ),(NAME1=10H EPHI      ),(NAME2=10H TPHI  REN 100
     1  ),(NAME3=10H EPHIP     ),(NAME4=10H TPHIP     )                 REN 110
      DO 20 I=1,NEXP                                                    REN 120
      IF(EPHI(KNORM,I).EQ.0.)GO TO 20                                   REN 130
      FACT=1.0/EPHI(KNORM,I)                                            REN 140
      DO 10 J=1,NSTA                                                    REN 150
      EPHI(J,I)=FACT*EPHI(J,I)                                          REN 160
      EPHIP(J,I)=FACT*EPHIP(J,I)                                        REN 170
   10 CONTINUE                                                          REN 180
   20 CONTINUE                                                          REN 190
      DO 40 I=1,NT                                                      REN 200
      IF(TPHI(KNORM,I).EQ.0.)GO TO 40                                   REN 210
      FACT=1.0/TPHI(KNORM,I)                                            REN 220
      DO 30 J=1,NSTA                                                    REN 230
      TPHI(J,I)=FACT*TPHI(J,I)                                          REN 240
      TPHIP(J,I)=FACT*TPHIP(J,I)                                        REN 250
   30 CONTINUE                                                          REN 260
   40 CONTINUE                                                          REN 270
   50 PRINT 60, ITER                                                    REN 280
   60 FORMAT(1H1,* COMPARISON OF EXPERIMENTAL MODES TO THEORETICAL MODES REN 290
     1 FOR ITERATION NUMBER*,I3/)                                       REN 300
      NL=1                                                              REN 310
      NN=NL+3                                                           REN 320
      IF(NN.GT.NEXP) NN=NEXP                                            REN 330
      PRINT 70,(MODE,I,I=NL,NN)                                         REN 340
   70 FORMAT(10X,4(18X,A6,I2))                                          REN 350
      PRINT 80,(NAME1,NAME2,I=NL,NN)                                    REN 360
   80 FORMAT(3X,2H K,6X,6H XSTA ,4(8X,A6,6X,A6))                        REN 370
      DO 90 J=1,NSTA                                                    REN 380
   90 PRINT 100,J,XSTA(J), (EPHI(J,I),TPHI(J,I),I=NL,NN)                REN 390
  100 FORMAT(1X,I4,2X,E12.5,4(2X,2E12.5))                               REN 400
      NL=NL+4                                                           REN 410
      IF(NL.LE.NEXP)GO TO 50                                            REN 420
  110 PRINT 120                                                         REN 430
  120 FORMAT(1H1,* COMPARISON OF SLOPES -- EXPERIMENTAL TO THEORETICAL*/ REN 440
     1)                                                                 REN 450
      NL=1                                                              REN 460
      NN=NL+3                                                           REN 470
      IF(NN.GT.NEXP) NN=NEXP                                            REN 480
      PRINT 70,(MODE,I,I=NL,NN)                                         REN 490
      PRINT 80,(NAME3,NAME4,I=NL,NN)                                    REN 500
```

Table A-11
(Cont'd.)

```
      DO 130 J=1,NSTA                                                   REN 510
  130 PRINT 100,J,XSTA(J),(EPHIP(J,I),TPHIP(J,I),I=NL,NN)               REN 520
      NL=NL+4                                                           REN 530
      IF(NL.LE.NEXP)GO TO 110                                           REN 540
      END                                                               REN 550
```

Table A-12
FORTRAN Listing of Subroutine MYKL

```
      SUBROUTINE MYKL (FREQ,GAM,LIME)                                   MYK  10
C     MYKL MODIFIED TO LIMIT NUMBER OF INTERNAL STATIONS TO 100         MYK  20
      COMMON     FINK(300)                                              MYK  30
      COMMON     A(4,4,101),SAP(4,4),AP(4,4),VINV(4,4),ALV(4,4),T(4,4),AL MYK  40
C     COMMON     A(4,4,300),SAP(4,4),AP(4,4),VINV(4,4),ALV(4,4),T(4,4),AL MYK  50
     1 BT(4,4),TAP(4,4,100),VEC(4,101),ITEM(6,101),DATA(8,101),I1(300),IR MYK  60
C    1VT(4,4),TAP(4,4,100),VEC(4,300),ITEM(6,300),DATA(8,300),I1(300),IR MYK  70
     2(300),OM(300),FUNC(300),R(3),KKK(100),MODE(100),JOINT(101),AL(4,4) MYK  80
C    2(300),OM(300),FUNC(300),R(3),KKK(100),MODE(100),JOINT(300),AL(4,4) MYK  90
     3,I6(101),PRNT(4),HOL(12)                                          MYK 100
C    3,I6(300),PRNT(4),HOL(12)                                          MYK 110
      COMMON     ICON(10),ICB(10),FPM(10,4,4),FQM(10,4,4),VSAVE(4),ARSTAR MYK 120
     1(10,6,4),          ARPB(4,4),ARPA(4,4),APR(4,4),DANV(2,2),DENV(2,2 MYK 130
     2),THMAN(6,6),BMAN(6,6),BINV(6,6),RMUL(6,4)                        MYK 140
      COMMON     I4(101)                                                MYK 150
C     COMMON     I4(300)                                                MYK 160
      COMMON     ITME(5,101),DAAT(7,101),IETM(5),DTAA(7)                MYK 170
C     COMMON     ITME(5,250),DAAT(7,250),IETM(5),DTAA(7)                MYK 180
   10 ITMIN=1                                                           MYK 190
      ILAF=1                                                            MYK 200
      N=0                                                               MYK 210
      NX=0                                                              MYK 220
   20 N=N+1                                                             MYK 230
      NX=NX+1                                                           MYK 240
      DO 30 I=1,5                                                       MYK 250
   30 ITEM(I,N)=ITME(I,NX)                                              MYK 260
      DO 40 I=1,7                                                       MYK 270
   40 DATA(I,N)=DAAT(I,NX)                                              MYK 280
      IF(LIME.EQ.1)GO TO 60                                             MYK 290
      WRITE(6,50) (ITEM(1,N),I=1,5),(DATA(J,N),J=1,7)                   MYK 300
   50 FORMAT(5I4,4X,7(   E13.5))                                        MYK 310
   60 CONTINUE                                                          MYK 320
      IF(ITEM(1,N))70,100,70                                            MYK 330
   70 ITEM(6,N)=ITEM(1,N)                                               MYK 340
      ITEM(1,N)=N                                                       MYK 350
      IF(N.EQ.1)GO TO 20                                                MYK 360
      IF(ITEM(2,N).EQ.ITEM(2,N-1))GO TO 20                              MYK 370
      DO 80 I=1,6                                                       MYK 380
      ITEM(I,N+1)=ITEM(I,N)                                             MYK 390
   80 ITEM(I,N)=ITEM(I,N-1)                                             MYK 400
      ITEM(1,N)=N                                                       MYK 410
      ITEM(1,N+1)=N+1                                                   MYK 420
      ITEM(4,N)=0                                                       MYK 430
      DO 90 J=1,7                                                       MYK 440
      DATA(J,N+1)=DATA(J,N)                                             MYK 450
   90 DATA(J,N)=0.0                                                     MYK 460
      DATA(3,N)=DATA(3,N-1)                                             MYK 470
      N=N+1                                                             MYK 480
      GO TO 20                                                          MYK 490
  100 DO 110 I=1,6                                                      MYK 500
```

Table A-12
(Cont'd.)

```
      ITEM(I,N+1)=ITEM(I,N)                                          MYK 510
  110 ITEM(I,N)=ITEM(I,N-1)                                          MYK 520
      ITEM(1,N)=N                                                    MYK 530
      ITEM(4,N)=0                                                    MYK 540
      DO 120 J=1,7                                                   MYK 550
      DATA(J,N+1)=DATA(J,N)                                          MYK 560
  120 DATA(J,N)=0.0                                                  MYK 570
      DATA(3,N)=DATA(3,N-1)                                          MYK 580
      N=N+1                                                          MYK 590
      NN=N-1                                                         MYK 600
      M=N                                                            MYK 610
      DO 150 I=2,NN                                                  MYK 620
      N=I-1                                                          MYK 630
      DATA(8,N)=DATA(3,I)-DATA(3,N)                                  MYK 640
      IF(ITEM(2,N)-ITEM(2,I))130,140,130                             MYK 650
  130 DATA(8,N)=0.0                                                  MYK 660
  140 DATA(8,I)=0.0                                                  MYK 670
  150 CONTINUE                                                       MYK 680
      DO 160 K=1,100                                                 MYK 690
      DO 160 I=1,4                                                   MYK 700
      DO 160 J=1,4                                                   MYK 710
  160 A(I,J,K)=0.0                                                   MYK 720
      KZ=0                                                           MYK 730
      KOWT=1                                                         MYK 740
      ITER=1                                                         MYK 750
      W2=DATA(1,M)                                                   MYK 760
      IF(W2)180,170,180                                              MYK 770
  170 W2=2.5                                                         MYK 780
  180 W2=(W2*3.141593*2.0)**2                                        MYK 790
      EPS=DATA(2,M)                                                  MYK 800
      IF(EPS)200,190,200                                             MYK 810
  190 EPS=.1E-4                                                      MYK 820
  200 GAMA=DATA(3,M)                                                 MYK 830
      IF(GAMA)220,210,220                                            MYK 840
  210 GAMA=1.10                                                      MYK 850
  220 GUMMA=1.+(GAMA-1.)*.05                                         MYK 860
      UPBND=DATA(4,M)                                                MYK 870
      IF(UPBND)240,230,240                                           MYK 880
  230 UPBND=250.0                                                    MYK 890
  240 UPBND=UPBND*6.283185                                           MYK 900
      K=1                                                            MYK 910
      SAMA=GAMA                                                      MYK 920
      DO 330 I=1,NN                                                  MYK 930
      IF(ITEM(4,I)-1)250,280,300                                     MYK 940
  250 A(1,1,K)=1.0                                                   MYK 950
      A(2,2,K)=1.0                                                   MYK 960
      A(3,1,K)=-DATA(8,I)/DATA(1,I)                                  MYK 970
      IF(DATA(1,I).EQ.0.0)A(3,1,K)=0.0                               MYK 980
      DATA(5,I)=DATA(5,I)/57.29578                                   MYK 990
      DATA(6,I)=DATA(6,I)/57.29578                                   MYK1000
```

Table A-12
(Cont'd.)

```
      IF(ITEM(5,I))260,260,270                                          MYK1010
  260 A(1,2,K)=-DATA(8,I)                                               MYK1020
      A(3,2,K)=.5*DATA(8,I)**2/DATA(1,I)                                MYK1030
      IF(DATA(1,I).EQ.0.0)A(3,2,K)=0.0                                  MYK1040
      A(4,1,K)=-A(3,2,K)                                                MYK1050
      A(4,2,K)=DATA(8,I)**3/(6.0*DATA(1,I))                             MYK1060
      IF(DATA(1,I).EQ.0.0)A(4,2,K)=0.0                                  MYK1070
  270 K=K+1                                                             MYK1080
      GO TO 330                                                         MYK1090
  280 A(3,1,K)=-DATA(6,I)                                               MYK1100
      IF(ITEM(5,I))290,290,300                                          MYK1110
  290 A(4,2,K)=-DATA(5,I)                                               MYK1120
  300 KK=K+1                                                            MYK1130
      DATA(5,I)=DATA(5,I)/57.29578                                      MYK1140
      DATA(6,I)=DATA(6,I)/57.29578                                      MYK1150
      A(1,1,K)=1.0                                                      MYK1160
      A(1,1,KK)=1.0                                                     MYK1170
      A(2,2,K)=1.0                                                      MYK1180
      A(2,2,KK)=1.0                                                     MYK1190
      A(3,1,KK)=-DATA(8,I)/DATA(1,I)                                    MYK1200
      IF(DATA(1,I).EQ.0.0)A(3,1,KK)=0.0                                 MYK1210
      A(3,3,K)=1.0                                                      MYK1220
      A(3,3,KK)=1.0                                                     MYK1230
      A(4,4,K)=1.0                                                      MYK1240
      A(4,4,KK)=1.0                                                     MYK1250
      IF(ITEM(5,I))310,310,320                                          MYK1260
  310 A(1,2,KK)=-DATA(8,I)                                              MYK1270
      A(3,2,KK)=DATA(8,I)**2*.5/DATA(1,I)                               MYK1280
      IF(DATA(1,I).EQ.0.0)A(3,2,KK)=0.0                                 MYK1290
      A(4,1,KK)=-A(3,2,KK)                                              MYK1300
      A(4,2,KK)=DATA(8,I)**3/(6.0*DATA(1,I))                            MYK1310
      IF(DATA(1,I).EQ.0.0)A(4,2,KK)=0.0                                 MYK1320
      A(4,3,KK)=DATA(8,I)                                               MYK1330
  320 K=K+2                                                             MYK1340
  330 CONTINUE                                                          MYK1350
      NSTA=K-1                                                          MYK1360
      DO 340 I=1,NN                                                     MYK1370
      DATA(7,I)=DATA(7,I)/57.29578                                      MYK1380
      DATA(2,I)=DATA(2,I)/386.4                                         MYK1390
  340 DATA(4,I)=DATA(4,I)/386.4                                         MYK1400
      KORP=0                                                            MYK1410
      DO 360 I=1,NN                                                     MYK1420
      IF(ITEM(3,I)-KORP )360,360,350                                    MYK1430
  350 KORP =ITEM(3,I)                                                   MYK1440
  360 CONTINUE                                                          MYK1450
      K=1                                                               MYK1460
      DO 390 I=1,NN                                                     MYK1470
      IF(ITEM(4,I)-1)370,380,380                                        MYK1480
  370 I1(K)=ITEM(1,I)                                                   MYK1490
      I6(K)=ITEM(6,I)                                                   MYK1500
```

Table A-12
(Cont'd.)

```
      I4(K)=ITEM(4,I)                                                   MYK1510
      IR(K)=KORP-ITEM(3,I)                                              MYK1520
      IF(ITEM(3,I).LT.0) IR(K)=-1                                       MYK1530
      K=K+1                                                             MYK1540
      GO TO 390                                                         MYK1550
  380 KK=K+1                                                            MYK1560
      I1(K)=ITEM(1,I)                                                   MYK1570
      I6(K)=ITEM(6,I)                                                   MYK1580
      I1(KK)=I1(K)                                                      MYK1590
      I6(KK)=I6(K)                                                      MYK1600
      I4(K)=ITEM(4,I)                                                   MYK1610
      I4(KK)=I4(K)                                                      MYK1620
      IR(K)=KORP-ITEM(3,I)                                              MYK1630
      IF(ITEM(3,I).LT.0) IR(K)=-1                                       MYK1640
      IR(KK)=IR(K)                                                      MYK1650
      K=K+2                                                             MYK1660
  390 CONTINUE                                                          MYK1670
      NSUP=NSTA                                                         MYK1680
      DO 400 K=1,NSTA                                                   MYK1690
      I=I1(K)                                                           MYK1700
      IF(ITEM(3,I))410,400,400                                          MYK1710
  400 CONTINUE                                                          MYK1720
      GO TO 420                                                         MYK1730
  410 NSTA=K-1                                                          MYK1740
  420 DIV=1.0                                                           MYK1750
  430 DO 450 I=1,4                                                      MYK1760
      DO 440 J=1,4                                                      MYK1770
  440 SAP(I,J)=0.0                                                      MYK1780
  450 SAP(I,I)=1.0                                                      MYK1790
  460 JNT=1                                                             MYK1800
      NOR=0                                                             MYK1810
      KIAP=KORP                                                         MYK1820
  470 K=1                                                               MYK1830
  480 CONTINUE                                                          MYK1840
      KS=K                                                              MYK1850
      IF(IR(K).LT.0)GO TO 490                                           MYK1860
      IF(IR(K)+KIAP-KORP)1110,490,1110                                  MYK1870
  490 I=I1(K)                                                           MYK1880
      MF=I                                                              MYK1890
      J1=I+1                                                            MYK1900
      IF(IR(K).GE.0)GO TO 510                                           MYK1910
      IF(J1-M)500,980,500                                               MYK1920
  500 IF(ITEM(2,I)-ITEM(2,J1))980,510,980                               MYK1930
  510 IF(ITEM(4,I)-1)520,540,540                                        MYK1940
  520 A(1,3,K)=W2*DATA(4,I)                                             MYK1950
      A(1,4,K)=-W2*DATA(2,I)*DATA(8,I)                                  MYK1960
      A(2,4,K)=W2*DATA(2,I)                                             MYK1970
      A(3,3,K)=1.0+W2*DATA(4,I)*A(3,1,K)                                MYK1980
      A(3,4,K)=W2*DATA(2,I)*A(3,2,K)                                    MYK1990
      A(4,3,K)=DATA(8,I)+W2*DATA(4,I)*A(4,1,K)                          MYK2000
```

Table A-12
(Cont'd.)

```
      A(4,4,K)=1.0+DATA(2,I)*W2*A(4,2,K)                                MYK2010
      IF(ITEM(5,I))540,540,530                                          MYK2020
  530 A(4,3,K)=0.0                                                      MYK2030
  540 IF(I4(K)-3)670,590,600                                            MYK2040
  550 NDR=NDR+1                                                         MYK2050
      DO 560 J=1,4                                                      MYK2060
      DO 560 L=1,4                                                      MYK2070
  560 APR(    L,J)=AP(L,J)                                              MYK2080
      KQR=I6(K)                                                         MYK2090
      ICB(NDR)=K                                                        MYK2100
      DO 580 J=1,4                                                      MYK2110
      DO 570 L=1,4                                                      MYK2120
  570 SAP(L,J)=0.0                                                      MYK2130
  580 SAP(J,J)=1.0                                                      MYK2140
      GO TO 670                                                         MYK2150
  590 IF(I4(K-1)-3)550,670,550                                          MYK2160
  600 IF(I4(K-1)-4)610,670,610                                          MYK2170
  610 KKEEP=K                                                           MYK2180
      DO 620 J=1,4                                                      MYK2190
      DO 620 L=1,4                                                      MYK2200
  620 ARPB(L,J)=AP(L,J)                                                 MYK2210
      KS1=NSTA+1                                                        MYK2220
      DO 640 J=1,4                                                      MYK2230
      DO 630 L=1,4                                                      MYK2240
  630 SAP(L,J)=0.0                                                      MYK2250
  640 SAP(J,J)=1.0                                                      MYK2260
      DO 650 LX=KS1,NSUP                                                MYK2270
      IT=I1(LX)                                                         MYK2280
      IF(ITEM(2,IT)-KQR)650,660,650                                     MYK2290
  650 CONTINUE                                                          MYK2300
      WRITE(6,790)KQR                                                   MYK2310
      GO TO 2190                                                        MYK2320
  660 M=LX                                                              MYK2330
      ICON(NDR)=K                                                       MYK2340
      GO TO 480                                                         MYK2350
  670 DO 690 L=1,4                                                      MYK2360
      DO 690 J=1,4                                                      MYK2370
      AP(L,J)=0.                                                        MYK2380
      DO 690 IC=1,4                                                     MYK2390
      AP(L,J)=AP(L,J)+A(L,IC,K)*SAP(IC,J)/DIV                           MYK2400
      IF(AP(L,J)-1.0E+19)690,680,680                                    MYK2410
  680 DIV=DIV*1.0E+5                                                    MYK2420
      GO TO 430                                                         MYK2430
  690 CONTINUE                                                          MYK2440
      DO 700 L=1,4                                                      MYK2450
      DO 700 J=1,4                                                      MYK2460
  700 SAP(L,J)=AP(L,J)                                                  MYK2470
      IF(J1-M)710,720,710                                               MYK2480
  710 IF(ITEM(2,I)-ITEM(2,J1))720,1110,720                              MYK2490
  720 AL(1,1)=SAP(1,3)                                                  MYK2500
```

Table A-12
(Cont'd)

```
      AL(1,2)=SAP(1,4)                                                  MYK2510
      AL(2,1)=SAP(2,3)                                                  MYK2520
      AL(2,2)=SAP(2,4)                                                  MYK2530
      IF(KIAP)730,1130,730                                              MYK2540
  730 DETV=SAP(3,3)*SAP(4,4)-SAP(3,4)*SAP(4,3)                          MYK2550
      IF(DETV)740,2220,740                                              MYK2560
  740 VINV(1,1)=SAP(4,4)/DETV                                           MYK2570
      VINV(2,1)=SAP(4,3)/DETV*(-1.0)                                    MYK2580
      VINV(1,2)=SAP(3,4)/DETV*(-1.0)                                    MYK2590
      VINV(2,2)=SAP(3,3)/DETV                                           MYK2600
      ALV(1,1)=AL(1,1)*VINV(1,1)+AL(1,2)*VINV(2,1)                      MYK2610
      ALV(1,2)=AL(1,1)*VINV(1,2)+AL(1,2)*VINV(2,2)                      MYK2620
      ALV(2,1)=AL(2,1)*VINV(1,1)+AL(2,2)*VINV(2,1)                      MYK2630
      ALV(2,2)=AL(2,1)*VINV(1,2)+AL(2,2)*VINV(2,2)                      MYK2640
      DO 750 K2=2,NSUP                                                  MYK2650
      KQ=K2                                                             MYK2660
      IF(ITEM(2,I)-I6(K2))750,770,750                                   MYK2670
  750 CONTINUE                                                          MYK2680
      WRITE(6,760)I6(KQ)                                                MYK2690
  760 FORMAT(25H NO APPENDAGE STATION FORI3)                            MYK2700
      GO TO 2190                                                        MYK2710
  770 IQ=I1(KQ)                                                         MYK2720
      IF(ITEM(4,IQ)-2)780,800,780                                       MYK2730
  780 WRITE(6,790)I6(KQ)                                                MYK2740
  790 FORMAT(8H STATIONI3,28H IS NOT AN APPENDAGE STATION)              MYK2750
      GO TO 2190                                                        MYK2760
  800 IT=1+3*ITEM(5,IQ)+ITEM(5,I)                                       MYK2770
      T(1,1)=0.0                                                        MYK2780
      T(1,2)=0.0                                                        MYK2790
      T(2,1)=0.0                                                        MYK2800
      T(2,2)=0.0                                                        MYK2810
      RAD=SQRT((COS(DATA(7,IQ)))**2+(SIN(DATA(7,IQ))*COS(DATA(6,IQ)))**2 MYK2820
     1)                                                                 MYK2830
      IF(RAD)820,820,810                                                MYK2840
  810 CL=(COS(DATA(7,IQ))*COS(DATA(6,IQ)))/RAD                          MYK2850
      CU=SIN(DATA(7,IQ))*COS(DATA(6,IQ))/RAD                            MYK2860
      CV=COS(DATA(7,IQ))*SIN(DATA(6,IQ))/RAD                            MYK2870
      GO TO 830                                                         MYK2880
  820 CL=0.0                                                            MYK2890
      CU=SIN(DATA(5,IQ))                                                MYK2900
      CV=COS(DATA(5,IQ))                                                MYK2910
  830 GO TO (840,850,860,870,880,890,900,910,920),IT                    MYK2920
  840 T(1,1)=CL/SQRT(CL**2+CU**2)                                       MYK2930
      T(2,2)=CL/SQRT(CL**2+CV**2)                                       MYK2940
      T(2,2)=ABS(T(2,2))                                                MYK2950
      GO TO 930                                                         MYK2960
  850 T(1,1)=CU                                                         MYK2970
      GO TO 930                                                         MYK2980
  860 T(2,1)=-CV                                                        MYK2990
      GO TO 930                                                         MYK3000
```

Table A-12
(Cont'd.)

```
  870 T(1,1)=-SQRT(1.0-CL**2)                                          MYK3010
      GO TO 930                                                        MYK3020
  880 T(1,1)=CL                                                        MYK3030
      GO TO 930                                                        MYK3040
  890 GO TO 2200                                                       MYK3050
  900 T(1,2)=SQRT(1.0-CL**2)                                           MYK3060
      GO TO 930                                                        MYK3070
  910 GO TO 2200                                                       MYK3080
  920 T(1,1)=CL                                                        MYK3090
  930 ALVT(1,1)=ALV(1,1)*T(1,1)+ALV(1,2)*T(1,2)                        MYK3100
      ALVT(1,2)=ALV(1,1)*T(2,1)+ALV(1,2)*T(2,2)                        MYK3110
      ALVT(2,1)=ALV(2,1)*T(1,1)+ALV(2,2)*T(1,2)                        MYK3120
      ALVT(2,2)=ALV(2,1)*T(2,1)+ALV(2,2)*T(2,2)                        MYK3130
      A(1,3,KQ)=T(1,1)*ALVT(1,1)+T(1,2)*ALVT(2,1)                      MYK3140
      A(1,4,KQ)=T(1,1)*ALVT(1,2)+T(1,2)*ALVT(2,2)                      MYK3150
      A(2,3,KQ)=T(2,1)*ALVT(1,1)+T(2,2)*ALVT(2,1)                      MYK3160
      A(2,4,KQ)=T(2,1)*ALVT(1,2)+T(2,2)*ALVT(2,2)                      MYK3170
  940 TAP(1,1,JNT)=VINV(1,1)*T(1,1)+VINV(1,2)*T(1,2)                   MYK3180
      TAP(1,2,JNT)=VINV(1,1)*T(2,1)+VINV(1,2)*T(2,2)                   MYK3190
      TAP(2,1,JNT)=VINV(2,1)*T(1,1)+VINV(2,2)*T(1,2)                   MYK3200
      TAP(2,2,JNT)=VINV(2,1)*T(2,1)+VINV(2,2)*T(2,2)                   MYK3210
      JOINT(K)=JNT                                                     MYK3220
      KKK(JNT)=KQ                                                      MYK3230
      JNT=JNT+1                                                        MYK3240
  950 DO 970 ISP=1,4                                                   MYK3250
      DO 960 JSP=1,4                                                   MYK3260
  960 SAP(ISP,JSP)=0.0                                                 MYK3270
  970 SAP(ISP,ISP)=1.0                                                 MYK3280
      GO TO 1110                                                       MYK3290
  980 DO 990 J=1,4                                                     MYK3300
      DO 990 L=1,4                                                     MYK3310
  990 ARPA(L,J)=AP(L,J)                                                MYK3320
      DO 1000 I=1,2                                                    MYK3330
      II=I+2                                                           MYK3340
      DO 1000 J=1,2                                                    MYK3350
 1000 DANV(I,J)=ARPB(II,J)+ARPA(II,J)                                  MYK3360
      IF(ITEM(5,MF).NE.0) DANV(2,2)=1.0/DIV                            MYK3370
      DEDET=1.0/(DANV(1,1)*DANV(2,2)-DANV(1,2)*DANV(2,1))              MYK3380
      DENV(1,1)=DANV(2,2)*DEDET                                        MYK3390
      DENV(2,2)=DANV(1,1)*DEDET                                        MYK3400
      DENV(1,2)=-DANV(1,2)*DEDET                                       MYK3410
      DENV(2,1)=-DANV(2,1)*DEDET                                       MYK3420
      DO 1010 J=1,6                                                    MYK3430
      DO 1010 I=1,6                                                    MYK3440
 1010 THMAN(I,J)=0.0                                                   MYK3450
      DO 1020 LL=1,5,2                                                 MYK3460
      DO 1020 J=1,2                                                    MYK3470
      JJ=J+LL-1                                                        MYK3480
      DO 1020 I=1,2                                                    MYK3490
      II=I+LL-1                                                        MYK3500
```

Table A-12
(Cont'd.)

```
1020 THMAN(II,JJ)=DENV(I,J)                                          MYK3510
     BMAN(1,1)=-ARPA(3,1)-ARPB(3,1)                                  MYK3520
     BMAN(1,2)=-ARPA(3,2)-ARPB(3,2)                                  MYK3530
     BMAN(2,1)=-ARPA(4,1)-ARPB(4,1)                                  MYK3540
     BMAN(2,2)=-ARPA(4,2)-ARPB(4,2)                                  MYK3550
     BMAN(1,3)=ARPB(1,1)-ARPA(1,1)                                   MYK3560
     BMAN(1,4)=ARPB(1,2)-ARPA(1,2)                                   MYK3570
     BMAN(2,3)=ARPB(2,1)-ARPA(2,1)                                   MYK3580
     BMAN(2,4)=ARPB(2,2)-ARPA(2,2)                                   MYK3590
     BMAN(1,5)=-BMAN(1,3)                                            MYK3600
     BMAN(1,6)=-BMAN(1,4)                                            MYK3610
     BMAN(2,5)=-BMAN(2,3)                                            MYK3620
     BMAN(2,6)=-BMAN(2,4)                                            MYK3630
     BMAN(3,3)=-ARPA(3,1)                                            MYK3640
     BMAN(3,4)=-ARPA(3,2)                                            MYK3650
     BMAN(4,3)=-ARPA(4,1)                                            MYK3660
     BMAN(4,4)=-ARPA(4,2)                                            MYK3670
     BMAN(3,5)=-ARPB(3,1)                                            MYK3680
     BMAN(3,6)=-ARPB(3,2)                                            MYK3690
     BMAN(4,5)=-ARPB(4,1)                                            MYK3700
     BMAN(4,6)=-ARPB(4,2)                                            MYK3710
     BMAN(5,3)=-1.0                                                  MYK3720
     BMAN(5,5)= 1.0                                                  MYK3730
     BMAN(6,4)=-1.0                                                  MYK3740
     BMAN(6,6)= 1.0                                                  MYK3750
     DO 1030 I=1,6                                                   MYK3760
     DO 1030 J=1,6                                                   MYK3770
     BINV(I,J)=0.0                                                   MYK3780
     DO 1030 MM=1,6                                                  MYK3790
1030 BINV(I,J)=BINV(I,J)+BMAN(I,MM)*THMAN(MM,J)                      MYK3800
     DO 1040 J=1,4                                                   MYK3810
     DO 1040 I=1,6                                                   MYK3820
1040 RMUL(I,J)=0.0                                                   MYK3830
     DO 1050 J=1,2                                                   MYK3840
     DO 1050 I=1,4                                                   MYK3850
1050 RMUL(I,J)=-ARPB(I,J)                                            MYK3860
     DO 1060 J=3,4                                                   MYK3870
     DO 1060 I=1,2                                                   MYK3880
1060 RMUL(I,J)=-ARPB(I,J)-ARPA(I,J)                                  MYK3890
     DO 1070 J=3,4                                                   MYK3900
     DO 1070 I=3,4                                                   MYK3910
1070 RMUL(I,J)=-ARPB(I,J)                                            MYK3920
     DO 1080 I=3,4                                                   MYK3930
     II=I+2                                                          MYK3940
     DO 1080 J=3,4                                                   MYK3950
1080 RMUL(II,J)=-ARPA(I,J)                                           MYK3960
     DO 1090 J=1,4                                                   MYK3970
     DO 1090 I=1,6                                                   MYK3980
     ARSTAR(NDR,I,J)=0.0                                             MYK3990
     DO 1090 MM=1,6                                                  MYK4000
```

Table A-12
(Cont'd.)

```
1090 ARSTAR(NDR,I,J)=ARSTAR(NDR,I,J)+BINV(I,MM)*RMUL(MM,J)          MYK4010
     DO 1100 J=1,4                                                  MYK4020
     DO 1100 I=1,4                                                  MYK4030
     SAP(I,J)=0.0                                                   MYK4040
     DO 1100 MM=1,4                                                 MYK4050
1100 SAP(I,J)=SAP(I,J)+ARSTAR(NDR,I,MM)*APR(MM,J)                   MYK4060
     K=KKEEP                                                        MYK4070
     K=K+1                                                          MYK4080
     GO TO 480                                                      MYK4090
1110 K=K+1                                                          MYK4100
     IF(K.LE.NSTA)GO TO 480                                         MYK4110
     IF(KIAP)480,480,1120                                           MYK4120
1120 KIAP=KIAP-1                                                    MYK4130
     GO TO 470                                                      MYK4140
1130 I2N=ITEM(2,M)                                                  MYK4150
     KKK(JNT)=1                                                     MYK4160
     JOINT(K)=JNT                                                   MYK4170
     MODE(JNT)=ITEM(5,1)+1                                          MYK4180
     IF(I2N-7)1140,2240,2240                                        MYK4190
1140 IF(I2N)2190,2190,1150                                          MYK4200
1150 GO TO (1160,1190,1200,1230,1240,1250),I2N                      MYK4210
1160 IF(ITEM(5,1))1180,1180,1170                                    MYK4220
1170 AP(2,4)=1.0/DIV                                                MYK4230
1180 FUNC(ITER)=AP(1,3)*AP(2,4)-AP(1,4)*AP(2,3)                     MYK4240
     GO TO 1260                                                     MYK4250
1190 FUNC(ITER)=AP(3,3)*AP(4,4)-AP(3,4)*AP(4,3)                     MYK4260
     GO TO 1260                                                     MYK4270
1200 IF(ITEM(5,1))1220,1220,1210                                    MYK4280
1210 AP(4,2)=1.0/DIV                                                MYK4290
1220 FUNC(ITER)=AP(3,1)*AP(4,2)-AP(3,2)*AP(4,1)                     MYK4300
     GO TO 1260                                                     MYK4310
1230 FUNC(ITER)=AP(1,3)*AP(4,4)-AP(1,4)*AP(4,3)                     MYK4320
     GO TO 1260                                                     MYK4330
1240 FUNC(ITER)=AP(3,2)*AP(4,3)-AP(4,2)*AP(3,3)                     MYK4340
     GO TO 1260                                                     MYK4350
1250 FUNC(ITER)=AP(1,2)*AP(4,3)-AP(1,3)*AP(4,2)                     MYK4360
1260 OM(ITER)=SQRT(W2)                                              MYK4370
     PRNT(1)=ITER                                                   MYK4380
     PRNT(2)=OM(ITER)/6.283185                                      MYK4390
     PRNT(3)=FUNC(ITER)                                             MYK4400
     GO TO (1270,1380),ILAF                                         MYK4410
1270 IF(KOWT.GT.1)GO TO 1330                                        MYK4420
1280 IF(ITHIN.LT.3) GO TO 1300                                      MYK4430
     OM(ITER+1)=OM(ITER)*GAMA                                       MYK4440
     IF(OM(ITER+1).GE.THIS)GO TO 1290                               MYK4450
     GO TO 1310                                                     MYK4460
1290 KOWT=1                                                         MYK4470
     ITHIN=1                                                        MYK4480
1300 OM(ITER+1)=OM(ITER)*GAMA                                       MYK4490
1310 ITER=ITER+1                                                    MYK4500
```

Table A-12
(Cont'd.)

```
      IF(ITER-298)1320,2190,2190                                        MYK4510
 1320 IF(OM(ITER).GT.OPBND)GO TO 2190                                   MYK4520
      KOWT=KOWT+1                                                       MYK4530
      W2=OM(ITER)**2                                                    MYK4540
      IF(W2.EQ.0.0)GO TO 2190                                           MYK4550
      GO TO 420                                                         MYK4560
 1330 IF((FUNC(ITER)/FUNC(ITER-1)).GT.0.0)GO TO 1350                    MYK4570
      ITHIN=1                                                           MYK4580
 1340 ILAF=2                                                            MYK4590
      SINLO=FUNC(ITER-1)                                                MYK4600
      SMX=ABS(SINLO)                                                    MYK4610
      SINHI=FUNC(ITER)                                                  MYK4620
      BIX=ABS(SINHI)                                                    MYK4630
      GOLO=OM(ITER-1)                                                   MYK4640
      GOHI=OM(ITER)                                                     MYK4650
      GO TO 1410                                                        MYK4660
 1350 IF(ITHIN.EQ.3)GO TO 1280                                          MYK4670
      FINK(ITER)=FUNC(ITER)-FUNC(ITER-1)                                MYK4680
      IF(KOWT.LT.3)GO TO 1280                                           MYK4690
      IF((FINK(ITER)/FINK(ITER-1)).LE.0.0)ITHIN=ITHIN+1                 MYK4700
      GO TO (1280,1360,1370),ITHIN                                      MYK4710
 1360 THAT=OM(ITER-1)                                                   MYK4720
      THEM=FUNC(ITER-1)                                                 MYK4730
      GO TO 1280                                                        MYK4740
 1370 THIS=OM(ITER)                                                     MYK4750
      OM(ITER)=THAT                                                     MYK4760
      FUNC(ITER)=THEM                                                   MYK4770
      GO TO 1280                                                        MYK4780
 1380 IF(FUNC(ITER)/SINLO)1390,1390,1400                                MYK4790
 1390 SINHI=FUNC(ITER)                                                  MYK4800
      GOHI=OM(ITER)                                                     MYK4810
      GO TO 1410                                                        MYK4820
 1400 SINLO=FUNC(ITER)                                                  MYK4830
      GOLO=OM(ITER)                                                     MYK4840
 1410 IF(KZ.LE.3)GO TO 1420                                             MYK4850
      OM(ITER+1)=(SINHI*GOLO-SINLO*GOHI)/(SINHI-SINLO)                  MYK4860
      OM(ITER+1)=ABS(OM(ITER+1))                                        MYK4870
      GO TO 1430                                                        MYK4880
 1420 OM(ITER+1)=(GOHI+GOLO)*.5                                         MYK4890
      IF(KZ.EQ.0)GO TO 1440                                             MYK4900
 1430 CONTINUE                                                          MYK4910
      IF(ABS(1.0-(OM(ITER+1)/OM(ITER))).LE.EPS)GO TO 1460               MYK4920
 1440 KZ=KZ+1                                                           MYK4930
      IF(KZ-16)1310,1310,1450                                           MYK4940
 1450 KOWT=1                                                            MYK4950
      KZ=0                                                              MYK4960
      ITHIN=1                                                           MYK4970
      ILAF=1                                                            MYK4980
      OM(ITER)=GOHI                                                     MYK4990
      FUNC(ITER)=SINHI                                                  MYK5000
```

Table A-12
(Cont'd.)

```
      GO TO 1280                                                        MYK5010
 1460 SAMBO=ABS(FUNC(ITER))                                             MYK5020
      IF(SAMBO-BIX)1470,1470,1450                                       MYK5030
 1470 IF(SAMBO-SMX)1480,1480,1450                                       MYK5040
 1480 OMEG=OM(ITER)                                                     MYK5050
      IF(NDR.EQ.0)GO TO 1530                                            MYK5060
      DO 1520 LAP=1,NDR                                                 MYK5070
      DO 1500 J=1,4                                                     MYK5080
      DO 1490 I=1,4                                                     MYK5090
      FPM(LAP,I,J)=0.0                                                  MYK5100
 1490 FQM(LAP,I,J)=0.0                                                  MYK5110
      FPM(LAP,J,J)=1.0                                                  MYK5120
 1500 FQM(LAP,J,J)=1.0                                                  MYK5130
      DO 1510 I=1,2                                                     MYK5140
      II=I+4                                                            MYK5150
      DO 1510 J=1,4                                                     MYK5160
      FQM(LAP,I,J)=ARSTAR(LAP,II,J)                                     MYK5170
 1510 FPM(LAP,I,J)=FPM(LAP,I,J)-ARSTAR(LAP,II,J)                        MYK5180
 1520 CONTINUE                                                          MYK5190
 1530 CONTINUE                                                          MYK5200
      KZ=0                                                              MYK5210
      GO TO (1540,1580,1620,1660,1680,1700),I2N                         MYK5220
 1540 IF(ITEM(5,1))1550,1550,1560                                       MYK5230
 1550 VEC(3,1)=-AP(1,4)/AP(1,3)                                         MYK5240
      VEC(4,1)=1.0                                                      MYK5250
      GO TO 1570                                                        MYK5260
 1560 VEC(3,1)=1.0                                                      MYK5270
      VEC(4,1)=0.0                                                      MYK5280
 1570 VEC(1,1)=0.0                                                      MYK5290
      VEC(2,1)=0.0                                                      MYK5300
      GO TO 1720                                                        MYK5310
 1580 IF(ITEM(5,1))1590,1590,1600                                       MYK5320
 1590 VEC(3,1)=-AP(3,4)/AP(3,3)                                         MYK5330
      VEC(4,1)=1.0                                                      MYK5340
      GO TO 1610                                                        MYK5350
 1600 VEC(3,1)=1.0                                                      MYK5360
      VEC(4,1)=0                                                        MYK5370
 1610 VEC(1,1)=0                                                        MYK5380
      VEC(2,1)=0.0                                                      MYK5390
      GO TO 1720                                                        MYK5400
 1620 IF(ITEM(5,1))1630,1630,1640                                       MYK5410
 1630 VEC(1,1)=-AP(3,2)/AP(3,1)                                         MYK5420
      VEC(2,1)=1.0                                                      MYK5430
      GO TO 1650                                                        MYK5440
 1640 VEC(1,1)=1.0                                                      MYK5450
      VEC(2,1)=0.0                                                      MYK5460
 1650 VEC(3,1)=0.0                                                      MYK5470
      VEC(4,1)=0.0                                                      MYK5480
      GO TO 1720                                                        MYK5490
 1660 IF(ITEM(5,1))1670,1670,2240                                       MYK5500
```

Table A-12
(Cont'd.)

```
1670 VEC(1,1)=0.0                                                       MYK5510
     VEC(2,1)=0.0                                                       MYK5520
     VEC(3,1)=-AP(1,4)/AP(1,3)                                          MYK5530
     VEC(4,1)=1.0                                                       MYK5540
     GO TO 1720                                                         MYK5550
1680 IF(ITEM(5,1))1690,1690,2240                                        MYK5560
1690 VEC(1,1)=0.0                                                       MYK5570
     VEC(2,1)=-AP(3,3)/AP(3,2)                                          MYK5580
     VEC(3,1)=1.0                                                       MYK5590
     VEC(4,1)=0.0                                                       MYK5600
     GO TO 1720                                                         MYK5610
1700 IF(ITEM(5,1))1710,1710,2240                                        MYK5620
1710 VEC(1,1)=0.0                                                       MYK5630
     VEC(2,1)=-AP(4,3)/AP(4,2)                                          MYK5640
     VEC(3,1)=1.0                                                       MYK5650
     VEC(4,1)=0.0                                                       MYK5660
1720 NSH=0                                                              MYK5670
     DO 1870 K=2,KS                                                     MYK5680
     I=I1(K)                                                            MYK5690
     IF(I4(K)-3)1850,1730,1820                                          MYK5700
1730 IF(I4(K-1)-3)1850,1740,1850                                        MYK5710
1740 NSH=NSH+1                                                          MYK5720
     DO 1750 J=1,4                                                      MYK5730
1750 VSAVE(J)=VEC(J,K-1)                                                MYK5740
     DO 1760 J=1,4                                                      MYK5750
     VEC(J,K)=0.0                                                       MYK5760
     DO 1760 MM=1,4                                                     MYK5770
1760 VEC(J,K)=VEC(J,K)+FPM(NSH,J,MM)*VSAVE(MM)                          MYK5780
     KL=ICON(NSH)                                                       MYK5790
     DO 1770 J=1,4                                                      MYK5800
     VEC(J,KL)=0.0                                                      MYK5810
     DO 1770 MM=1,4                                                     MYK5820
1770 VEC(J,KL)=VEC(J,KL)+FQM(NSH,J,MM)*VSAVE(MM)                        MYK5830
1780 KL=KL+1                                                            MYK5840
     IF(KL.GT.NSJP)GO TO 1810                                           MYK5850
     I=I1(KL)                                                           MYK5860
     IF(I.EQ.I1(KL-1))GO TO 1790                                        MYK5870
     IF(ITEM(2,I)-ITEM(2,I-1))1810,1790,1810                            MYK5880
1790 DO 1800 J=1,4                                                      MYK5890
     VEC(J,KL)=0.0                                                      MYK5900
     DO 1800 MM=1,4                                                     MYK5910
1800 VEC(J,KL)=VEC(J,KL)+A(J,MM,KL-1)*VEC(MM,KL-1)                      MYK5920
     GO TO 1780                                                         MYK5930
1810 CONTINUE                                                           MYK5940
     GO TO 1870                                                         MYK5950
1820 IF(I4(K-1)-4)1850,1830,1850                                        MYK5960
1830 DO 1840 J=1,4                                                      MYK5970
     VEC(J,K)=0.0                                                       MYK5980
     DO 1840 MM=1,4                                                     MYK5990
1840 VEC(J,K)=VEC(J,K)+ARSTAR(NSH,J,MM)*VSAVE(MM)                       MYK6000
```

Table A-12
(Cont'd.)

```
      GO TO 1870                                                        MYK601
 1850 DO 1860 J=1,4                                                     MYK602
      VEC(J,K)=0.0                                                      MYK603
      DO 1860 MM=1,4                                                    MYK604
 1860 VEC(J,K)=VEC(J,K)+A(J,MM,K-1)*VEC(MM,K-1)                         MYK605
 1870 CONTINUE                                                          MYK606
      IF(KORP)2010,2010,1880                                            MYK607
 1880 KIAP=1                                                            MYK608
 1890 DO 1990 K=KS,NSTA                                                 MYK609
      I=I1(K)                                                           MYK610
      IF(ITEM(2,I)-ITEM(2,I-1))1910,1900,1910                           MYK611
 1900 IF(IR(K)+KIAP-KORP)1990,1970,1990                                 MYK612
 1910 IF(IR(K)+KIAP-KORP)1990,1920,1990                                 MYK613
 1920 DO 1930 K2=1,NSUP                                                 MYK614
      KQ=K2                                                             MYK615
      IF(ITEM(2,I)-I6(KQ))1930,1940,1930                                MYK616
 1930 CONTINUE                                                          MYK617
      GO TO 2190                                                        MYK618
 1940 VEC(1,K)=0.0                                                      MYK619
      VEC(2,K)=0.0                                                      MYK620
      DO 1950 J1=1,JNT                                                  MYK621
      J=J1                                                              MYK622
      IF(KKK(J1)-KQ)1950,1960,1950                                      MYK623
 1950 CONTINUE                                                          MYK624
 1960 VEC(3,K)=TAP(1,1,J)*VEC(3,KQ)+TAP(1,2,J)*VEC(4,KQ)                MYK625
      MODE(J)=ITEM(5,I)+1                                               MYK626
      VEC(4,K)=TAP(2,1,J)*VEC(3,KQ)+TAP(2,2,J)*VEC(4,KQ)                MYK627
      GO TO 1990                                                        MYK628
 1970 DO 1980 I=1,4                                                     MYK629
      VEC(I,K)=0.0                                                      MYK630
      DO 1980 J=1,4                                                     MYK631
 1980 VEC(I,K)=VEC(I,K)+A(I,J,K-1)*VEC(J,K-1)                           MYK632
 1990 CONTINUE                                                          MYK633
      IF(KIAP-KORP)2000,2010,2000                                       MYK634
 2000 KIAP=KIAP+1                                                       MYK635
      GO TO 1890                                                        MYK636
 2010 GAM=0.0                                                           MYK637
      DO 2020 K=1,NSUP                                                  MYK638
      KN=K                                                              MYK639
      IF(ITEM(4,M)-I6(K))2020,2030,2020                                 MYK640
 2020 CONTINUE                                                          MYK641
      GO TO 2080                                                        MYK642
 2030 IF(ITEM(5,KN)-1)2040,2050,2050                                    MYK643
 2040 B=VEC(4,KN)                                                       MYK644
      GO TO 2060                                                        MYK645
 2050 B=VEC(3,KN)                                                       MYK646
 2060 DO 2070 K=1,NSUP                                                  MYK647
      DO 2070 J=1,4                                                     MYK648
 2070 VEC(J,K)=VEC(J,K)/B                                               MYK649
 2080 DO 2090 K=1,NSUP                                                  MYK650
```

Table A-12
(Cont'd.)

```
      I=I1(K)                                                           MYK6510
2090  GAM=GAM+DATA(4,I)*VEC(3,K)**2+DATA(2,I)*VEC(4,K)**2               MYK6520
      GK=GAM*OMEG**2                                                    MYK6530
      IF(NDR)2100,2120,2100                                             MYK6540
2100  JUG=JNT+NDR                                                       MYK6550
      KKK(JUG)=KKK(JNT)                                                 MYK6560
      MODE(JUG)=MODE(JNT)                                               MYK6570
      JU1=JUG-1                                                         MYK6580
      J1=0                                                              MYK6590
      DO 2110 J=JNT,JU1                                                 MYK6600
      J1=J1+1                                                           MYK6610
      KKK(J)=ICB(J1)                                                    MYK6620
2110  MODE(J)=MODE(JUG)                                                 MYK6630
      JNT=JUG                                                           MYK6640
2120  CONTINUE                                                          MYK6650
      DO 2170 JJ=1,JNT                                                  MYK6660
      KQ=KKK(JJ)                                                        MYK6670
      IQ=I6(KQ)                                                         MYK6680
      II=MODE(JJ)                                                       MYK6690
      IF(II)2190,2190,2130                                              MYK6700
2130  GO TO (2140,2150,2160),II                                         MYK6710
2140  GO TO 2170                                                        MYK6720
2150  GO TO 2170                                                        MYK6730
2160  GO TO 2170                                                        MYK6740
2170  CONTINUE                                                          MYK6750
      FREQ=OMEG/6.283185                                                MYK6760
      FREP=OM(ITER+1)/6.283185                                          MYK6770
      ITEM(3,M)=ITEM(3,M)-1                                             MYK6780
      IF(ITEM(3,M))2190,2190,2180                                       MYK6790
2180  KOHT=2                                                            MYK6800
      OM(1)=GOHI                                                        MYK6810
      FUNC(1)=SINHI                                                     MYK6820
      IF(FUNC(1).EQ.0.0)FUNC(1)=-SINLO                                  MYK6830
      GAMA = SAMA                                                       MYK6840
      ILAF=1                                                            MYK6850
      OM(2)=GOHI*GAMA                                                   MYK6860
      ITER=2                                                            MYK6870
      MFAP=1                                                            MYK6880
      W2=OM(2)**2                                                       MYK6890
      ITMIN=1                                                           MYK6900
      GO TO 420                                                         MYK6910
2190  RETURN                                                            MYK6920
2200  WRITE(6,2210)IT                                                   MYK6930
2210  FORMAT(29H NO T GIVEN FOR JOINT TYPE = I3)                        MYK6940
      GO TO 2190                                                        MYK6950
2220  WRITE(6,2230)I6(KQ),KIAP                                          MYK6960
2230  FORMAT(24H DETERMINANT V OF JOINT I3,17H APPENDAGE ORDER I3,5H = 0 MYK6970
     1.)                                                                MYK6980
      GO TO 2190                                                        MYK6990
2240  WRITE(6,2250)I2N                                                  MYK7000
```

Table A-12

(Cont'd.)

```
2250 FORMAT(25H BOUNDARY NOT IN TABLE = I3)                    MYK7010
     GO TO 2190                                                MYK7020
     END                                                       MYK7030
```

Table A-13
FORTRAN Listing of Subroutine MEMSET

```
      SUBROUTINE MEMSET (IA,IB)                                         MST  10
      DIMENSION IA(1)                                                   MST  20
      K=IABS(LOCF(IB)-LOCF(IA))+1                                       MST  30
      DO 10 J=1,K                                                       MST  40
   10 IA(J)=0                                                           MST  50
      END                                                               MST  60
```

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Table A-14
FORTRAN Listing of Subroutine MATNF5

```
      SUBROUTINE MATNF5(A,N,NDIM,DETSCL,DET,IROAR)                      MTN  10
      DIMENSION A(1)                                                    MTN  20
      DIMENSION PIVOT(170),INDEX(170,2),IPIVOT(170)                     MTN  30
   10 EQUIVALENCE(IROW,JROW),(ICOL,JCOL),(AMAX,T,SWAP)                  MTN  40
C                                                                       MTN  50
C     BLOCK 100  INITIALIZE                                             MTN  60
C                                                                       MTN  70
   20 IROAR=0                                                           MTN  80
      DET=DETSCL                                                        MTN  90
   30 DO 40 J=1,N                                                       MTN 100
   40 IPIVOT(J)=0                                                       MTN 110
      DO 210 I=1,N                                                      MTN 120
C                                                                       MTN 130
C     BLOCK 200  SEARCH FOR PIVOT ELEMENT                               MTN 140
C                                                                       MTN 150
   50 AMAX=0.0                                                          MTN 160
      DO 100 J=1,N                                                      MTN 170
      IF(IPIVOT(J)-1)60,100,60                                          MTN 180
   60 DO 90 K=1,N                                                       MTN 190
      IF(IPIVOT(K)-1)70,90,290                                          MTN 200
   70 JK=J+NDIM*(K-1)                                                   MTN 210
      IF(ABS(AMAX)-ABS(A(JK)))80,90,90                                  MTN 220
   80 IROW=J                                                            MTN 230
      ICOL=K                                                            MTN 240
      AMAX=A(JK)                                                        MTN 250
   90 CONTINUE                                                          MTN 260
  100 CONTINUE                                                          MTN 270
  110 IF(AMAX)120,300,120                                               MTN 280
C                                                                       MTN 290
C     BLOCK 300  INTERCHANGE ROWS TO PUT PIVOTAL ELEMENT ON DIAGONAL    MTN 300
C                                                                       MTN 310
  120 IPIVOT(ICOL)=IPIVOT(ICOL)+1                                       MTN 320
      IF(IROW-ICOL)130,150,130                                          MTN 330
  130 DET=-DET                                                          MTN 340
      DO 140 L=1,N                                                      MTN 350
      LD=NDIM*(L-1)                                                     MTN 360
      IROL=IROW+LD                                                      MTN 370
      ICOL=ICOL+LD                                                      MTN 380
      SWAP=A(IROL)                                                      MTN 390
      A(IROL)=A(ICOL)                                                   MTN 400
  140 A(ICOL)=SWAP                                                      MTN 410
  150 INDEX(I,1)=IROW                                                   MTN 420
      INDEX(I,2)=ICOL                                                   MTN 430
      ILOC=ICOL+NDIM*(ICOL-1)                                           MTN 440
      PIVOT(I)=A(ILOC)                                                  MTN 450
      DET=DET*PIVOT(I)                                                  MTN 460
C                                                                       MTN 470
C     BLOCK 400  DIVIDE PIVOT ROW BY PIVOT ELEMENT                      MTN 480
C                                                                       MTN 490
  160 A(ILOC)=1.0                                                       MTN 500
```

Table A-14
(Cont'd.)

```
      DO 170 L=1,N                                                      MTN 510
      ICLL=ICOL+NDIM*(L-1)                                              MTN 520
      A(ICLL)=A(ICLL)/PIVOT(I)                                          MTN 530
  170 CONTINUE                                                          MTN 540
C                                                                       MTN 550
C     BLOCK 500  REDUCE NON-PIVOT ROWS                                  MTN 560
C                                                                       MTN 570
  190 DO 210 L1=1,N                                                     MTN 580
      IF(L1-ICOL)190,210,190                                            MTN 590
  190 ICOL=NDIM*(ICOL-1)                                                MTN 600
      L1C=L1+ICOL                                                       MTN 610
      T=A(L1C)                                                          MTN 620
      A(L1C)=0.0                                                        MTN 630
      DO 200 L=1,N                                                      MTN 640
      LD=NDIM*(L-1)                                                     MTN 650
      L1D=L1+LD                                                         MTN 660
      ICD=ICOL+LD                                                       MTN 670
  200 A(L1D)=A(L1D)-A(ICD)*T                                            MTN 680
  210 CONTINUE                                                          MTN 690
C                                                                       MTN 700
C     BLOCK 600  INTERCHANGE COLUMNS                                    MTN 710
C                                                                       MTN 720
  220 DO 250 I=1,N                                                      MTN 730
      L=N+1-I                                                           MTN 740
      IF(INDEX(L,1)-INDEX(L,2))230,250,230                              MTN 750
  230 JROW=INDEX(L,1)                                                   MTN 760
      JCOL=INDEX(L,2)                                                   MTN 770
      JROW=NDIM*(JROW-1)                                                MTN 780
      JCOL=NDIM*(JCOL-1)                                                MTN 790
      DO 240 K=1,N                                                      MTN 800
      KR=K+JROW                                                         MTN 810
      KC=K+JCOL                                                         MTN 820
      SWAP=A(KR)                                                        MTN 830
      A(KR)=A(KC)                                                       MTN 840
      A(KC)=SWAP                                                        MTN 850
  240 CONTINUE                                                          MTN 860
  250 CONTINUE                                                          MTN 870
      RETURN                                                            MTN 880
C                                                                       MTN 890
C     BLOCK 9000   ERROR INDICATIONS                                    MTN 900
C                                                                       MTN 910
  260 WRITE(6,270)IROAR                                                 MTN 920
  270 FORMAT(31H0 SUBROUTINE MATNF4 ERROR TYPE I5)                      MTN 930
  280 CALL EXIT                                                         MTN 940
  290 IROAR=1                                                           MTN 950
      GO TO 260                                                         MTN 960
  300 IROAR=-5                                                          MTN 970
      RETURN                                                            MTN 980
      END                                                               MTN 990
```

TABLE B-15
SAMPLE DATA DECK LISTING FOR PROGRAM FILLIN

```
-----------------------------  CARD COLUMNS  -----------------------------
00000000011111111112222222222333333333344444444445555555555666666666677777777778
12345678901234567890123456789012345678901234567890123456789012345678901234567890
--------------------------------------------------------------------------------

   FILLIN TEST CASE  TYPICAL MISSILE AIRFRAME
  1              0.16 +7    .040    7.8
 15              1.16 +8    .412   15.     2.447
 20              2.75 +8    .629   20.     7.002
 25              4.72 +8    .728   25.    11.50
 30              6.92 +8   1.003   30.15  20.13
 35              3.90 +8    .783   35.5   10.93
 37        2     3.83 +8           37.3
 39              2.51 +8   4.138   39.8   22.15
 45              3.59 +8   1.016   45.4   24.36
 46        1     5.81 +8           46.8                     .93 -7
 47              5.81 +8    .614   47.2   13.83
 48        3     1.57 +8           48.
 49              1.57 +8    .323   49.4    7.92
 55              1.57 +8    .560   55.    13.75
 60              1.57 +8   1.161   59.5   28.46
 61              4.53 +8           61.8
 62        1     4.53 +8           62.59                    .62 -8
 63        4     3.23 +8           63.
 66              2.59 +8   3.106   66.    41.24
 67              3.56 +8    .809   67.97  11.32
 70        1     7.07 +8           70.                      .12 -6
 71              1.29 +8    .687   71.38  19.42
 76              4.88 +8    .925    7.4   26.13
 77        1     4.98 +8           77.6                     .62 -8
 78        2     4.54 +8           78.25
 79              4.54 +8    .846   79.    19.89
 80        1     8.02 +8           80.5                     .93 -7
 82              7.10 +8   7.075   82.    92.66
 90              5.26 +8   2.791   90.    81.50
100              5.26 +8   3.000  100.    92.34
110              5.26 +8   2.883  110.    88.78
120              5.26 +8   2.883  120.    88.78
130              5.26 +8   2.883  130.    88.78
140              5.26 +8   2.883  140.    88.78
150              5.26 +8   2.883  150.    88.78
157              1.20 +9          157.5
160              9.41 +8   4.468  160.   138.91
168              1.23 +9   7.011  170.4   94.76
170        1     2.47 +8          170.5                     .43 -7
171              2.47 +8   1.387  171.7   26.71
174              3.88 +8          174.
178              5.98 +7   8.351  177.38 109.66
182              5.98 +7   2.508  182.2   24.63
191  37 1:       2.43 +5   1.132   30.3
192  37 1: 1     2.43 +5          30.31          .19 -3
```

Table A-15
(cont'd.)

```
-------------------------------     CARD COLUMNS     -------------------------------
00000000011111111112222222222333333333344444444445555555555666666666677777777778
12345678901234567890123456789012345678901234567890123456789012345678901234567890
--------------------------------------------------------------------------------

 193  37 1:        2.43 +5    .081    32.3
 194  37 1.        1.62 +6   2.251    35.3    18.60
 195  37 1: 1      8.09 +6            36.9                     .80 -5
 196  37 1.        8.09 +6    .453    37.02
 198  37 1:        8.09 +6            37.3
 315  78 1:        9.70 +7   5.849    72.9
 325  78 1.        1.21 +8   1.614    77.3
 328  78 1: 1      1.21 +8            78.              .26 -4   .32 -6
 330  78 1:        1.13 +7            78.25
 265  48-1: 1      5.66 +8            48.              .28 -4
 267  48-1:        5.66 +8   8.430    50.5     7.49
 268  48-1.        5.66 +8   4.431    55.      7.49
 269  48-1:        5.66 +8   9.717    59.5     8.20
 271  48-1. 1      5.66 +8            63.              .62 -4 1.
       1 3          40.              1.01    200.
   78   58     3
            7.5                 16.                 26.                 35.5
            40.5                45.                 48.5                52.
            57.                 62.                 66.                 69.5
            71.                 76.                 79.                 80.
            81.                 85.                 90.                 95.
            100.                105.                110.                115.
            120.                125.                130.                135.
            140.                145.                155.                160.
            165.                170.                171.                176.
            183.            37  30.            37  30.3            37  30.32
        37  32.             37  35.            37  36.89           37  37.
        37  37.3            78  70.5           78  75.            78   77.5
        78    78.01         78    78.25        48    45.          48   47.99
        48    49.5          48    55.          48    59.5         48    62.
        48    63.01         48    66.
        1  1    1.0         1.0          1.0
        2  1     .803        .905         .757
        3  1     .583        .813         .514
        4  1     .403        .706         .308
        5  1     .3          .655         .186
        6  1     .2          .639         .091
        7  1     .111        .579         .006
        8  1     .038        .521        -.043
        9  1    -.068        .353        -.103
       10  1    -.149        .212        -.131
       11  1    -.195        .094        -.117
       12  1    -.220       -.025        -.083
       13  1    -.234       -.081        -.048
       14  1    -.280       -.257         .015
       15  1    -.311       -.397         .049
```

Table A-15
(Cont'd.)

```
------------------------------     CARD COLUMNS     ------------------------------
00000000011111111112222222222333333333344444444445555555555666666666677777777778
12345678901234567890123456789012345678901234567890123456789012345678901234567890
-------------------------------------------------------------------------------
```

16	1	-.315	-.435	.069
17	1	-.311	-.436	.079
18	1	-.304	-.501	.126
19	1	-.306	-.616	.202
20	1	-.296	-.663	.250
21	1	-.280	-.701	.281
22	1	-.260	-.710	.308
23	1	-.242	-.709	.324
24	1	-.223	-.732	.342
25	1	-.198	-.755	.344
26	1	-.170	-.674	.336
27	1	-.143	-.641	.321
28	1	-.113	-.571	.298
29	1	-.079	-.504	.268
30	1	-.043	-.420	.229
31	1	.030	-.217	.141
32	1	.068	-.112	.09
33	1	.111	.072	.02
34	1	.148	.176	-.05
35	1	.161	.215	-.068
36	1	.237	.392	-.173
37	1	.268	.567	-.278
38	1	.797	-10.28	-.64
39	1	.78	-9.35	-.6
40	1	.65	-5.6	-.28
41	1	.53	-3.0	-.03
42	1	.42	-0.5	.17
43	1	.362	.691	.278
44	1	.36	.69	.275
45	1	.354	.687	.268
46	1	-.345	-.429	-.036
47	1	-.325	-.436	.013
48	1	-.321	-.439	.041
49	1	-.319	-.44	.046
50	1	-.311	-.441	.049
51	1	.2	.635	.09
52	1	.135	.59	.01
53	1	.103	.635	-.155
54	1	-.01	.68	-.265
55	1	-.10	.54	-.36
56	1	-.161	.487	-.422
57	1	-.15	.19	-.13
58	1	-.19	.1	-.115

TABLE A-16
SAMPLE DATA DECK LISTING FOR PROGRAM JOINTS

```
------------------------------     CARD COLUMNS     ------------------------------
00000000011111111112222222222333333333344444444445555555555666666666677777777778
12345678901234567890123456789012345678901234567890123456789012345678901234567890
--------------------------------------------------------------------------------

    PROGRAM JOINTS TEST CASE
    1    3    3    1   10    4   78   78  0.15      0.001          .9
    2   0.264
  1.0        1.0        1.0
  1.0        1.0        1.0
 59.3      116.       153.
  10  11  .1  +8  1.  +8   2
  21  26  .5  +7  5.  +7   2
  27  35  .1  +8  1.  +8   2
  48  58  .1  +6  1.  +6   2
        1  1  .99305E+00  .99665E+00  .99142E+00
        2  1  .82618E+00  .91618E+00  .78559E+00
        3  1  .77703E+00  .89471E+00  .73663E+00
        4  1  .66545E+00  .84066E+00  .60805E+00
        5  1  .53995E+00  .77872E+00  .46133E+00
        6  1  .41282E+00  .71442E+00  .31713E+00
        7  1  .37409E+00  .70447E+00  .27764E+00
        8  1  .37409E+00  .70447E+00  .27764E+00
        9  1  .31913E+00  .67842E+00  .21627E+00
       10  1  .19196E+00  .61390E+00  .86290E-01
       11  1  .15979E+00  .59723E+00  .57824E-01
       12  1  .15979E+00  .59723E+00  .57824E-01
       13  1  .15042E+00  .59237E+00  .49532E-01
       14  1  .13144E+00  .58253E+00  .32737E-01
       15  1  .13144E+00  .58253E+00  .32737E-01
       16  1  .10106E+00  .55586E+00  .96847E-02
       17  1 -.14839E-01  .41939E+00 -.66610E-01
       18  1 -.93783E-01  .29449E+00 -.98593E-01
       19  1 -.13327E+00  .22284E+00 -.11155E+00
       20  1 -.14322E+00  .19475E+00 -.11030E+00
       21  1 -.14322E+00  .19475E+00 -.11030E+00
       22  1 -.14822E+00  .18249E+00 -.10969E+00
       23  1 -.14822E+00  .18249E+00 -.10969E+00
       24  1 -.18578E+00  .90383E-01 -.10511E+00
       25  1 -.20661E+00  .25042E-01 -.88056E-01
       26  1 -.22617E+00 -.42329E-01 -.67804E-01
       27  1 -.22617E+00 -.42329E-01 -.67804E-01
       28  1 -.23708E+00 -.92267E-01 -.50985E-01
       29  1 -.29274E+00 -.32567E+00  .31853E-01
       30  1 -.29464E+00 -.33381E+00  .34456E-01
       31  1 -.29464E+00 -.33381E+00  .34456E-01
       32  1 -.30085E+00 -.36042E+00  .42963E-01
       33  1 -.30085E+00 -.36042E+00  .42963E-01
       34  1 -.30908E+00 -.39140E+00  .52867E-01
       35  1 -.31141E+00 -.42991E+00  .71247E-01
       36  1 -.31141E+00 -.42991E+00  .71247E-01
```

Table A-16
(ont'd.)

```
--------------------------------------- CARD COLUMNS ---------------------------------------
00000000011111111112222222222333333333344444444445555555555666666666677777777778
12345678901234567890123456789012345678901234567890123456789012345678901234567890
----------------------------------------+---------+---------+---------+---------+---------+
```

37	1	-.31075E+00	-.45913E+00	.91805E-01
38	1	-.30233E+00	-.58973E+00	.19073E+00
39	1	-.27819E+00	-.68768E+00	.27681E+00
40	1	-.24224E+00	-.71739E+00	.32324E+00
41	1	-.19671E+00	-.71357E+00	.33832E+00
42	1	-.14245E+00	-.63215E+00	.31740E+00
43	1	-.78407E-01	-.49883E+00	.26426E+00
44	1	-.75292E-02	-.31736E+00	.18385E+00
45	1	.49843E-01	-.14328E+00	.10883E+00
46	1	.69465E-01	-.82199E-01	.82546E-01
47	1	.15548E+00	.20953E+00	-.65211E-01
48	1	.15636E+00	.21245E+00	-.66965E-01
49	1	.15636E+00	.21245E+00	-.66965E-01
50	1	.16575E+00	.23778E+00	-.83601E-01
51	1	.18630E+00	.30551E+00	-.12344E+00
52	1	.21903E+00	.42650E+00	-.19370E+00
53	1	.26103E+00	.54700E+00	-.26600E+00
54	1	.26103E+00	.54700E+00	-.26600E+00
55	1	.78000E+00	-.93500E+01	-.60000E+00
56	1	.77943E+00	-.93190E+01	-.59867E+00
57	1	.65071E+00	-.56155E+01	-.28149E+00
58	1	.54672E+00	-.33377E+01	-.73377E-01
59	1	.41079E+00	-.31095E+00	.18714E+00
60	1	.36169E+00	.69730E+00	.27837E+00
61	1	.36377E+00	.58673E+00	.26450E+00
62	1	.35960E+00	.60980E+00	.27453E+00
63	1	.35400E+00	.68700E+00	.26800E+00
64	1	.35400E+00	.68700E+00	.26800E+00
65	1	-.33433E+00	-.43273E+00	-.28667E-02
66	1	-.32051E+00	-.43896E+00	.38411E-01
67	1	-.32020E+00	-.43960E+00	.46600E-01
68	1	-.31933E+00	-.43996E+00	.45875E-01
69	1	-.31100E+00	-.44100E+00	.49000E-01
70	1	-.31100E+00	-.44100E+00	.49000E-01
71	1	.13478E+00	.58985E+00	.97324E-02
72	1	.13382E+00	.87727E+00	-.12500E+00
73	1	.82455E-01	.80682E+00	-.17500E+00
74	1	-.10000E-01	.68000E+00	-.26500E+00
75	1	-.10000E+00	.54000E+00	-.36000E+00
76	1	-.18540E+00	.46580E+00	-.44680E+00
77	1	-.14987E+00	.19030E+00	-.13005E+00
78	1	-.14987E+00	.19030E+00	-.13005E+00
1	1	-.23176E-01	-.11176E-01	-.28588E-01
2	1	-.23176E-01	-.11176E-01	-.28588E-01
3	1	-.19867E-01	-.96208E-02	-.22893E-01
4	1	-.24768E-01	-.12001E-01	-.20537E-01

able A-16
(cont'd.)

```
--------------------------------- CARD COLUMNS ---------------------------------
00000000011111111112222222222333333333344444444445555555555666666666777777777778
12345678901234567890123456789012345678901234567890123456789012345678901234567890
--------------------------------------------------------------------------------

  5  1 -.21830E-01 -.11039E-01 -.24761E-01
  6  1 -.25699E-01 -.12996E-01 -.29145E-01
  7  1 -.21270E-01 -.10082E-01 -.23752E-01
  8  1 -.21270E-01 -.10082E-01 -.23752E-01
  9  1 -.22695E-01 -.10757E-01 -.25343E-01
 10  1 -.22627E-01 -.11727E-01 -.20024E-01
 11  1 -.22222E-01 -.35556E-02 -.21111E-01
 12  1 -.20857E-01 -.16571E-01 -.14000E-01
 13  1 -.23524E-01 -.12192E-01 -.20818E-01
 14  1 -.23923E-01 -.12399E-01 -.21171E-01
 15  1 -.23923E-01 -.12399E-01 -.21171E-01
 16  1 -.21405E-01 -.22829E-01 -.15240E-01
 17  1 -.19312E-01 -.27955E-01 -.10185E-01
 18  1 -.16843E-01 -.30562E-01 -.55264E-02
 19  1 -.17494E-01 - 31743E-01 -.57399E-02
 20  1 -.16200E-01 -.28200E-01 -.56000E-02
 21  1 -.71429E-02 -.34000E-01  .97143E-02
 22  1 -.12229E-01 -.29990E-01  .14927E-02
 23  1 -.12229E-01 -.29990E-01  .14927E-02
 24  1 -.12812E-01 -.31418E-01  .15639E-02
 25  1 -.94716E-02 -.33228E-01  .89118E-02
 26  1 -.71429E-02 -.34000E-01  .97143E-02
 27  1 -.92000E-02 -.35200E-01  .12600E-01
 28  1 -.91541E-02 -.37013E-01  .12965E-01
 29  1 -.94904E-02 -.40664E-01  .13000E-01
 30  1 -.92000E-02 -.35200E-01  .12600E-01
 31  1 -.40000E-02 -.38000E-01  .20000E-01
 32  1 -.95946E-02 -.41111E-01  .13142E-01
 33  1 -.95946E-02 -.41111E-01  .13142E-01
 34  1 -.96866E-02 -.41505E-01  .13268E-01
 35  1 -.40000E-02 -.38000E-01  .20000E-01
 36  1  .17500E-02 -.16250E-01  .11750E-01
 37  1  .82451E-03 -.17875E-01  .12834E-01
 38  1  .92996E-03 -.17279E-01  .12805E-01
 39  1  .31590E-02 -.65641E-02  .71590E-02
 40  1  .38679E-02 -.18828E-02  .40726E-02
 41  1  .49226E-02  .16749E-02  .77617E-03
 42  1  .57506E-02  .11929E-01 -.31200E-02
 43  1  .68015E-02  .14865E-01 -.62313E-02
 44  1  .73400E-02  .19740E-01 -.88800E-02
 45  1  .77870E-02  .24240E-01 -.10429E-01
 46  1  .79106E-02  .24624E-01 -.10595E-01
 47  1  .87572E-02  .29155E-01 -.17539E-01
 48  1  .74000E-02  .20800E-01 -.14000E-01
 49  1  .92000E-02  .35400E-01 -.21000E-01
 50  1  .88731E-02  .29253E-01 -.17205E-01
```

Table A-16
(Cont'd.)

```
----------------------------------     CARD COLUMNS     ----------------------------------
00000000011111111112222222222333333333344444444445555555555666666666677777777778
12345678901234567890123456789012345678901234567890123456789012345678901234567890
----------------------------------------------------------------------------------

      51   1  .89920E-02  .29645E-01 -.17435E-01
      52   1  .87143E-02  .25000E-01 -.15000E-01
      53   1  .87143E-02  .25000E-01 -.15000E-01
      54   1  .87143E-02  .25000E-01 -.15000E-01
      55   1 -.56667E-01  .31000E+01  .13333E+00
      56   1 -.56667E-01  .31000E+01  .13333E+00
      57   1 -.56667E-01  .31000E+01  .13333E+00
      58   1 -.40809E-01  .89668E+00  .78299E-01
      59   1 -.30688E-01  .63016E+00  .57143E-01
      60   1 -.30688E-01  .63016E+00  .57143E-01
      61   1 -.20000E-01 -.10000E-01 -.23333E-01
      62   1 -.20000E-01 -.10000E-01 -.23333E-01
      63   1 -.20000E-01 -.10000E-01 -.23333E-01
      64   1 -.20000E-01 -.10000E-01 -.23333E-01
      65   1  .44444E-02 -.15556E-02  .10889E-01
      66   1  .35587E-02 -.15063E-02  .11415E-01
      67   1  .16000E-02 -.12000E-02  .11200E-01
      68   1  .33333E-01 -.41667E-02  .12500E-01
      69   1  .33333E-01 -.41667E-02  .12500E-01
      70   1  .33333E-01 -.41667E-02  .12500E-01
      71   1 -.0207      -.0283      -.0202
      72   1 -.0207      -.0283      -.0202
      73   1 -.20545E-01 -.28182E-01 -.20000E-01
      74   1 -.20545E-01 -.28182E-01 -.20000E-01
      75   1 -.24400E-01 -.21200E-01 -.24000E-01
      76   1 -.24400E-01 -.21200E-01 -.24000E-01
      77   1 -.13378E-01 -.30100E-01  .0015056
      78   1 -.13378E-01 -.30100E-01  .0015056
  1              0.16 +7    .040    7.8
 15              1.16 +8    .412   15.      2.447
 20              2.75 +8    .629   20.      7.002
 25              4.72 +8    .728   25.     11.50
 30              6.92 +8   1.003   30.15   20.13
 35              3.90 +8    .783   35.5    10.93
 37        2     3.83 +8           37.3
 39              2.51 +8   4.138   39.8    22.15
 45              3.59 +8   1.016   45.4    24.36
 46        1     5.81 +8           46.8                      .93 -7
 47              5.81 +8    .614   47.2    13.83
 48        3     1.57 +8           48.
 49              1.57 +8    .323   49.4     7.92
 55              1.57 +8    .560   55.     13.75
 60              1.57 +8   1.161   59.5    28.46
 61              4.53 +8           61.8
 62        1     4.53 +8           62.59                     .62 -8
 63        4     3.23 +8           63.
```

Table A-16
(Cont'd.)

```
----------------------     CARD COLUMNS     ----------------------
00000000011111111112222222222333333333344444444445555555555666666
12345678901234567890123456789012345678901234567890123456789012345
-------------------------------------------------------------------

 66                2.59 +8   3.106   66.     41.24
 67                3.56 +8    .809   67.97   11.32
 70          1     7.07 +8          70.                          .12 -6
 71                1.29 +8    .687   71.38   19.42
 76                4.89 +8    .925   77.4    26.13
 77          1     4.88 +8          77.6                         .62 -8
 78          2     4.54 +8          78.25
 79                4.54 +8    .846   79.     19.89
 80          1     8.02 +8          80.5                         .93 -7
 82                7.10 +8   7.075   82.     92.66
 90                5.26 +8   2.791   90.     81.30
100                5.26 +8   3.000  100.     92.34
110                5.26 +8   2.883  110.     88.78
120                5.26 +8   2.883  120.     88.78
130                5.26 +8   2.883  130.     88.78
140                5.26 +8   2.883  140.     88.78
150                5.26 +8   2.883  150.     88.78
157                1.20 +9          157.5
160                9.41 +8   4.468  160.    138.91
168                1.23 +9   7.011  170.4    94.76
170          1     2.47 +8          170.5                        .43 -7
171                2.47 +8   1.387  171.7    26.71
174                3.88 +8          174.
178                5.98 +7   8.351  177.38  109.66
182                5.98 +7   2.508  182.2    24.63
191   37 1         2.43 +5   1.132   30.3
192   37 1 1       2.43 +5          30.31            .19 -3
193   37 1         2.43 +5    .081  32.3
194   37 1         1.62 +6   2.251   35.3    18.60
195   37 1 1       8.09 +6          36.9                         .80 -5
196   37 1         8.09 +6    .453  37.02
198   37 1         8.09 +6          37.3
315   78 1         9.70 +7   5.049  72.0
325   78 1         1.21 +8   1.614  77.3
328   78 1 1       1.21 +8          78.              .26 -4   .32 -6
330   78 1         1.13 +7          78.25
265   48-1 1       5.66 +8          48.              .28 -4
267   48-1         5.66 +8   8.430  50.5     7.49
268   48-1         5.66 +8   4.431  55.      7.49
269   48-1         5.66 +8   9.717  59.5     8.20
271   48-1 1       5.66 +8          63.              .62 -4 1.
        1 3         40.             1.02   200.
```

Table A-17

Key Output Data from Sample Data Deck

Parameter	Iteration		
	0	1	2
Cost Functions			
Overall	.68164 E + 12	.65905 E + 11	.36836 E + 11
Frequency	.17047 E + 12	.39695 E + 11	.96240 E + 10
Mode Shape	.51117 E + 12	.26210 E + 11	.27212 E + 11
Compliances			
C_1	.93000 E - 7	.83152 E - 7	.53820 E - 7
C_2	.12000 E - 6	.12038 E - 6	.80930 E - 7
C_3	.93000 E - 7	.60380 E - 7	.40304 E - 7
C_4	.30000 E - 5	.69565 E - 5	.59244 E - 5
Frequencies			
f_1	.4888485 E + 2	.4894103 E + 2	.5546776 E + 2
f_2	.1435402 E + 3	.1078903 E + 3	.1124721 E + 3
f_3	.1435414 E + 3	.1441162 E + 3	.1485364 E + 3
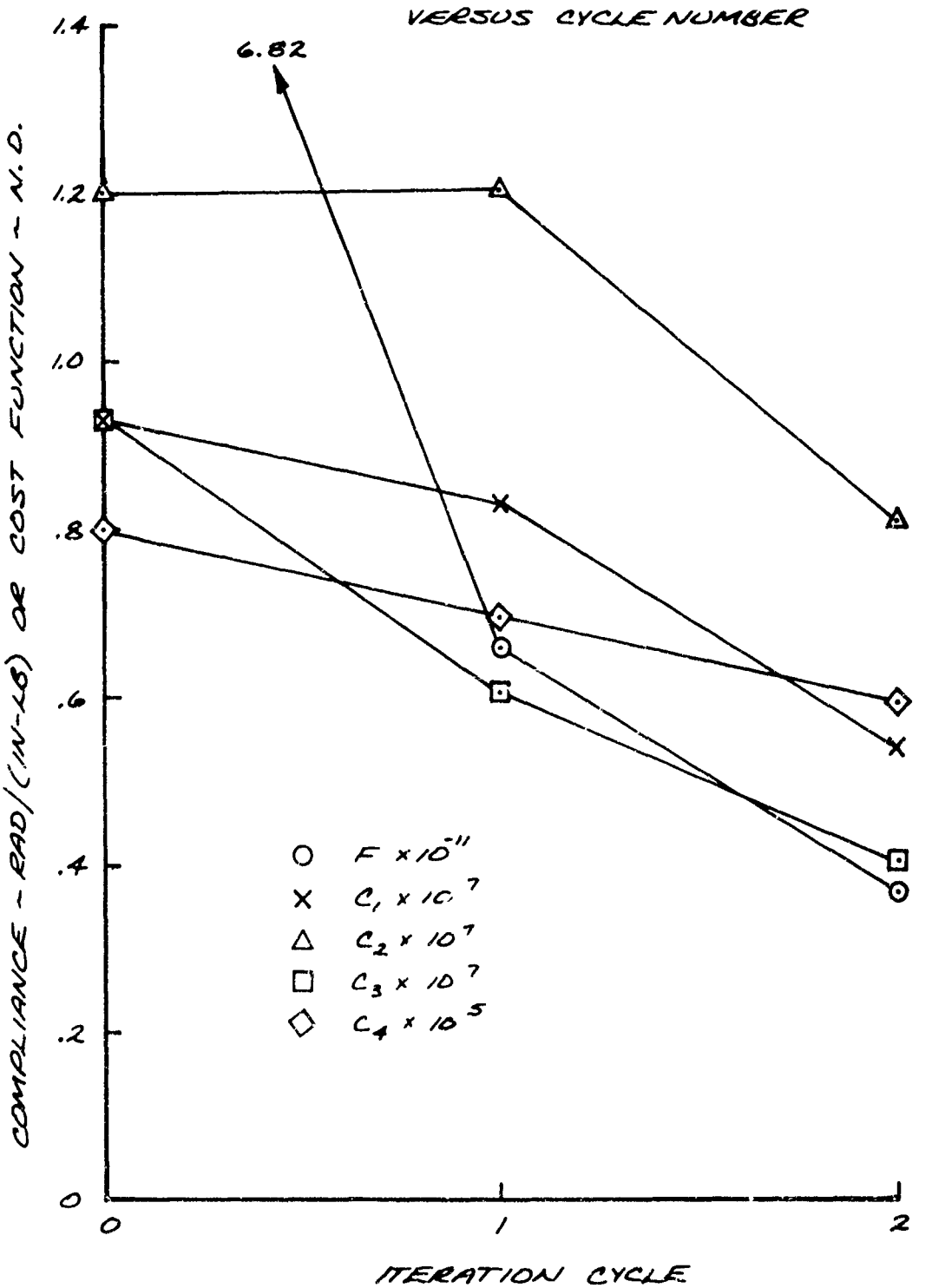
FIGURE A-1
SAMPLE APPLICATION
VALUES OF UNKNOWN JOINT
COMPLIANCES AND COST FUNCTION
VERSUS CYCLE NUMBER