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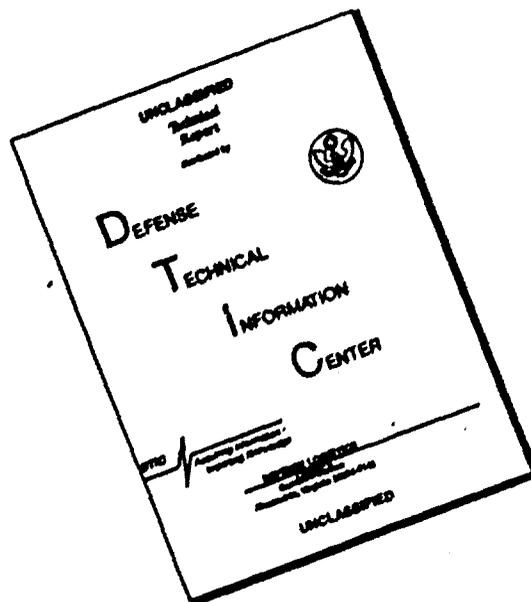
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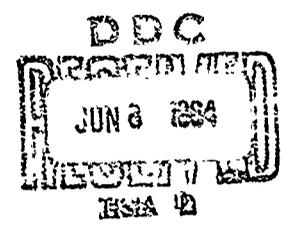
CONFAC II
A GENERAL COMPUTER PROGRAM FOR THE
DETERMINATION OF RADIANT-INTERCHANGE
CONFIGURATION AND FORM FACTORS

TECHNICAL DOCUMENTARY REPORT No. FDL-TDR-64-43

APRIL 1964

AIR FORCE FLIGHT DYNAMICS LABORATORY
RESEARCH AND TECHNOLOGY DIVISION
AIR FORCE SYSTEMS COMMAND
WRIGHT-PATTERSON AIR FORCE BASE, OHIO

Project No. 6146, Task No. 614618



(Prepared under Contract No. AF 33(657)-8953 by the
Space and Information Systems Division of
North American Aviation, Inc., Downey, California;
Kempton A. Toups, author)

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300 - May 1964 - 162-39-786

FOREWORD

This computer program is one of a series of digital computer programs developed as in-house effort in support of the Space Vehicle Thermal and Atmospheric Control Study. The study is sponsored by the Flight Dynamics Laboratory of the Research and Technology Division under Contract AF33(657)-3253 and is under the direction of W. Uhl of the Environmental Control Branch. R. E. Sexton of S&ID served as Project Manager of the study program. H. L. Nordwall reviewed and edited the contractor's report for publication as an FDL TDR.

The program described in this report represents the second stage in the development of a general configuration factor computer program. This report partly incorporates SID 62-393 (ASD TN 61-101), which describes CONFAC I, the first program developed under the Space Vehicle Thermal and Atmospheric Control Study.

This report may also be identified by Contractor's Report No. SID 63-1397.

ABSTRACT

A simple numerical method is derived for the determination of the geometric radiant-interchange factors used in radiant heat transfer and illumination. A FORTRAN II digital computer program utilizing this method is developed which provides a rapid and accurate means of computation of configuration and form factors. The source of flux may be any general plane polygon and the receiver may be any general plane or nonplanar polygon, the surface of an arbitrary polyhedron, or an arbitrary combination of such surfaces.

It is therefore possible to accurately determine configuration and form factors from a plane surface to another surface occluded by complex intervening surfaces. Form factors are computed rapidly -- averaging less than two seconds on the IBM 7094 for simple, unobstructed plane surfaces, and less than 30 seconds for simple polyhedra. Also, means are provided to internally generate a variety of regular polygons or polyhedra and to transform surface spatial coordinates for convenience of data entry and/or motion simulation. Simplicity of data entry, flexibility of application, and economy of operation are principal features of this program. Sample problems illustrating these important aspects are provided.

This report has been reviewed and is approved.



W. J. BAKER
Asst. for R&T
Vehicle Equipment Division
AF Flight Dynamics Laboratory

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NOMENCLATURE

| | |
|-------------------------|--|
| A | Area |
| e | Exchange coefficient |
| c | Configuration factor (italicized) |
| f | Form factor (italicized) |
| h,k,l | Translation components |
| i,j,k | Unit vectors along the X-,Y-,Z-axis, respectively |
| O | Center of unit sphere, origin of coordinate system |
| R | Radius of sphere |
| S | Distance between two areas |
| X,Y,Z or x,y,z | Spatial coordinates of a point relative to X, Y, Z axis |
| α, β, γ | Direction angles of a line relative to X, Y, Z axis respectively |
| γ | Angle between Z axis and vector normal to plane |
| θ | Angle between two vectors |
| π | Numerical constant = 3.14159 + |
| ω | Solid angle |

Subscripts

| | |
|------------|-------------------------------------|
| A,B,C | Points on an area |
| s | Sector |
| ΔA | Finite incremental area |
| dA | Differential area |
| dA-A | From a differential area to an area |

NOMENCLATURE (cont'd)

Subscripts (cont'd)

| | |
|------------|------------------|
| 1,2, | Areas 1,2, |
| 12 | Area 1 to area 2 |
| ϵ | Elliptical |

SECTION I

INTRODUCTION

The geometric form factor, f_{12} , is defined as the fraction of radiant energy emanating from finite surface A_1 which is intercepted by another surface A_2 .

$$f_{12} = \frac{\text{Flux received by finite surface } A_2}{\text{Flux emitted by finite surface } A_1} \quad (1)$$

The geometric configuration factor, c_{12} , is defined in a similar manner, except that the emitting surface is infinitesimal, (sometimes referred to as the point configuration factor),

$$c_{12} = \frac{\text{Flux received by finite surface } A_2}{\text{Flux emitted by infinitesimal surface } dA_1} \quad (2)$$

The subscripts denote the direction of flow of net flux; c_{12} and f_{12} pertain respectively to the configuration and form factor from surface A_1 to surface A_2 . It is assumed that each surface is isothermal and radiates diffusely, i.e., follows Lambert's cosine distribution law.

The "closed-form" determination of the configuration or form factor by classical integration techniques is impossible or impractical in most situations. Experimental techniques and devices have been reported in the literature (Reference 1), and probably the most useful is Pleije's Globoscope (Reference 4). Experimental techniques produce only the configuration factor, however. Nonetheless, they are useful for many applications where only one or just a few configuration factors are required and nominal accuracy is sufficient.

However, if a large number of form factors are required in a short period of time, experimental techniques are not practical. This report presents a numerical method and a computer program which enables rapid and accurate computation of configuration and form factors between plane surfaces, and plane or solid surfaces. The source (surface 1) may be any general plane polygon; the receiver (surface 2) may be any arbitrarily oriented general plane or nonplanar polygon, the surface of an arbitrary solid, or an arbitrary combination of planes, nonplanes, or solids. Form factors (which nominally are derived from 625 configuration factors) are computed rapidly, averaging less than 2 seconds by IBM 7094 time for simple plane surfaces, and less than 30 seconds from simple plane surfaces to simple solids. Table 1 compares solutions obtained by CONFAC II to those given in Reference 1.

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Table 1, Comparison of Configuration and Form Factors Computed by CONFACII to Those Given in Reference 1

| Configuration | Reference 1 | Computer (Trapezoidal Rule) | |
|----------------------------|-------------|-----------------------------|--------------|
| | | 24 x 24 grid | 60 x 60 grid |
| P-1, X = 1, Y = 1 | 0.13853 | 0.138532 | 0.138532 |
| X = 0.1, Y = 0.1 | 0.00314 | 0.003141 | 0.003141 |
| X = 1, Y = 4 | 0.17527 | 0.175270 | 0.175270 |
| X = 0.1, Y = 0.4 | 0.01147 | 0.011471 | 0.011471 |
| X = 1, Y = ∞ * | 0.17678 | 0.176777 | 0.176777 |
| X = 0.1, Y = ∞ * | 0.02488 | 0.024876 | 0.024876 |
| P-2, ϕ = 30°, L = 0, N = 1 | 0.4665 | 0.466506 | 0.466506 |
| ϕ = 30°, L = 1, N = 1 | 0.1759 | 0.175923 | 0.175923 |
| ϕ = 30°, L = 0, N = 4 | 0.4665 | 0.466506 | 0.466506 |
| ϕ = 30°, L = 4, N = 4 | 0.0964 | 0.096447 | 0.096447 |
| ϕ = 120°, L = 0, N = 1 | 0.125 | 0.125000 | 0.125000 |
| ϕ = 120°, L = 1, N = 1 | 0.0236 | 0.023554 | 0.023554 |
| ϕ = 120°, L = 0, N = 4 | 0.125 | 0.125000 | 0.125000 |
| ϕ = 120°, L = 4, N = 4 | 0.0077 | 0.007683 | 0.007683 |
| **P-6, E = 1, D = 1 | 0.276 | 0.275 | --- |
| E = 1, D = 2 | 0.438 | 0.436 | --- |
| E = 1, D = ∞ | 0.500 | 0.498 | --- |
| E = 2, D = 1 | 0.724 | 0.722 | --- |
| E = 2, D = ∞ | 0.800 | 0.799 | --- |
| **P-8, D = 4, L = 2 | 0.08074 | 0.08055 | --- |
| D = 2, L = 4 | 0.24774 | 0.2472 | --- |
| A-1, X = 1, Y = 1 | 0.19982 | 0.19972 | 0.19981 |
| X = 0.1, Y = 0.1 | 0.00316 | 0.00316 | 0.00316 |
| X = 1, Y = 4 | 0.34596 | 0.34559 | 0.34590 |
| X = 0.1, Y = 0.4 | 0.01207 | 0.01207 | 0.01207 |
| X = 1, Y = ∞ * | 0.41421 | 0.40549 | 0.41075 |
| X = 0.1, Y = ∞ * | 0.04988 | 0.04884 | 0.04946 |
| A-2, ϕ = 30°, L = 1, N = 1 | 0.6207+ | 0.61769 | 0.61878 |
| ϕ = 30°, L = 4, N = 4 | 0.3961+ | 0.39431 | 0.39450 |
| ϕ = 120°, L = 1, N = 1 | 0.0870+ | 0.08665 | 0.08662 |
| ϕ = 120°, L = 4, N = 4 | 0.0433+ | 0.04272 | 0.04235 |

* 10^8 was assumed to approximate ∞ for computer run

** 32 sided regular polygon used to simulate circular cross-section

+ These values were obtained by numerical integration across surface A_1 , according to Reference 1

The FORTRAN II Computer Program described herein, CONFAC II, is a follow-on development of an earlier version, CONFAC I (Reference 5). The original program has been extensively modified and significant improvements in the flexibility of application have been achieved. CONFAC I was developed principally to compute geometric form factors between plane surfaces; no application to nonplanar surfaces or bodies was originally intended. However, because of the particular analytical approach utilized and the data handling techniques developed, it was possible to use the basic plane-to-plane program to compute factors to nonplanar surfaces, provided proper restrictions were observed.

The principal similarities and differences between CONFAC I and CONFAC II are as follows:

1. Both CONFAC I and CONFAC II require that Surface 1 be a plane polygon; it may be arbitrarily oriented in the coordinate system in which it is described (entered) in data.
2. Both CONFAC I and CONFAC II specify that if Surface 2 is a plane polygon, it may be arbitrarily oriented with respect to Surface 1 and within its own coordinate system.
3. Both CONFAC I and CONFAC II require that, if Surface 2 is a nonplanar surface, then the surface boundaries must present a valid silhouette from any point on the active side of Surface 1.
4. CONFAC I specifies that no part of nonplanar Surface 2 may lie below the "horizon" of Surface 1 when viewed from the active side of Surface 1. CONFAC II does not require that all of a nonplanar Surface 2 appear above the horizon of Surface 1. CONFAC II will automatically bisect a nonplanar Surface 2 and compute the factor to only the part which Surface 1 "sees."
5. CONFAC I cannot, in general, be used to compute the factor to a solid surface. CONFAC II will compute the factor to arbitrary solid surfaces or regular solids such as parallelepipeds, cylinders, cones, etc., with the restriction that all of the surface must appear above the horizon of Surface 1. CONFAC I cannot, in general, be used to compute factors to surfaces which are occluded or "shadowed" in a varying manner by intervening surfaces; on the other hand, the factor in such instances can be determined by CONFAC II with few restrictions.
6. CONFAC I has only two principal classes of data -- surface data and surface transformation data. No distinction of data entry is made between plane and nonplane surfaces. Surface data is distinguished from transformation data by the position of the data name on the data name card. CONFAC II, however, utilizes nine data classifications, as follows:

- Class 1 - Plane polygon, silhouette developed directly from data
- Class 2 - Nonplane polygon, silhouette developed directly from data
- Class 3 - Internally generated disk, silhouette developed directly from generated data
- Class 4 - Plane polygon, silhouette internally developed
- Class 5 - Nonplane surface or solid, silhouette internally developed
- Class 6 - Internally generated regular disk or solid, silhouette internally developed
- Class 7 - Sphere
- Class 8 - Multisurface, silhouette internally developed from all surfaces taken together
- Class 9 - Transformation data

7. CONFAC II incorporates a silhouette generator subroutine which is utilized when the factor to solids or, in certain cases, to non-solids is requested. The silhouette generator computes the perspective of Surface(s) 2 from preselected positions on Surface 1 from which configuration factors are computed.
8. CONFAC II incorporates an internal automatic surface generator which computes the surface boundary coordinates of regular plane and solid surfaces from input data specifications. This feature enables the analyst to create surfaces such as circular or elliptical disks, parallelepipeds, pyramids, cones, truncated cones, cylinders, etc. An endless variety of regular surfaces can be created by CONFAC II.
9. CONFAC II incorporates extremely fast computation of factors to a sphere which is arbitrarily oriented with respect to Surface 1.

SECTION II
ANALYTICAL PROCEDURES

CONFIGURATION AND FORM FACTOR

The general equation that must be solved in the determination of the radiant-interchange form factor is (see Figure 1)

$$f_{12} = \frac{1}{A_1} \iint_{A_1} \iint_{A_2} \frac{\cos \theta_1 \cos \theta_2 dA_2 dA_1}{\pi S^2} \quad (1)$$

The following part of the integrand is the factor from the elemental surface dA_1 to the total surface A_2 , referred to as the configuration factor or plane point factor, c_{12} .

$$c_{12} = \iint_{A_2} \frac{\cos \theta_1 \cos \theta_2}{\pi S^2} dA_2 \quad (2)$$

Therefore,

$$f_{12} = \frac{1}{A_1} \iint_{A_1} c_{12} dA_1 \quad (3)$$

A very simple geometric interpretation of Equation 2 is given by Nusselt. The principal value of the Nusselt concept is that the computational procedure is simplified and made more accurate by the fact that no mathematical or numerical integration is required to compute the configuration factor. However, the Nusselt method yields only the configuration factor from the elemental area dA_1 ; one must still integrate all such factors over surface A_1 to yield the form factor f_{12} as given in Equation 3.

The Nusselt concept utilizes a hemisphere of radius R constructed over the incremental plane area dA_1 , as shown in Figure 1. Every point defining the boundary of surface A_2 is projected radially to the hemisphere surface and then vertically downward to the plane of dA_1 , the equatorial plane of the hemisphere. The locus of all points thus projected encloses an area, A''_2 , on the hemisphere base. This area A''_2 , divided by the area of the base, is the configuration factor from dA_1 to A_2 .

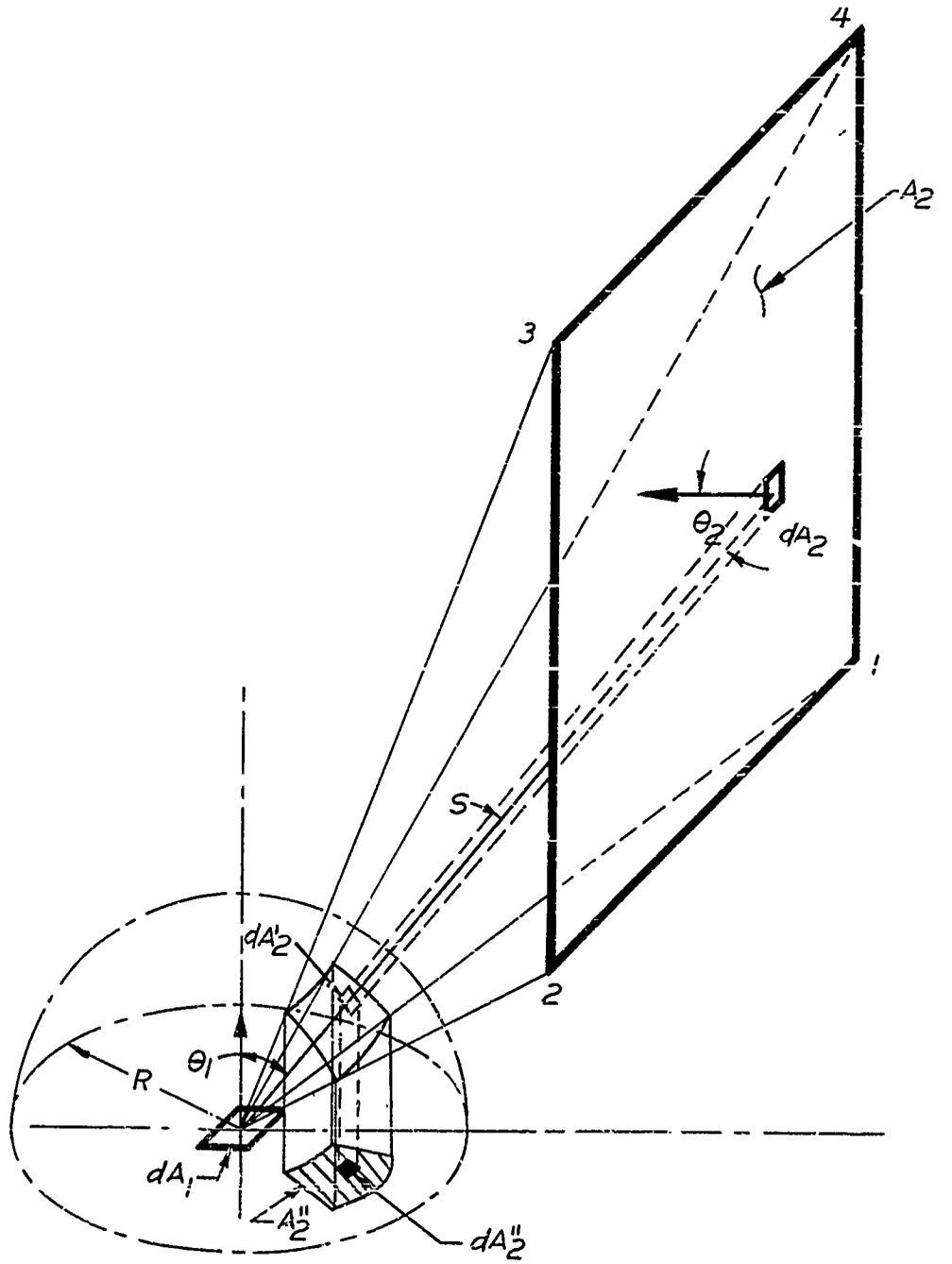


FIGURE 1. NUSSULT GEOMETRICAL RELATIONSHIPS

The validity of this conclusion can be demonstrated as follows. Note that the elemental area dA_2 is described in surface A_2 by the elemental solid angle $d\omega_1$, or

$$d\omega_1 = \frac{\cos \theta_2 dA_2}{S^2} \quad (4)$$

Similarly, on the sphere having radius R ,

$$d\omega_1 = \frac{dA_2'}{R^2} \quad (5)$$

Because dA_2'' is the projection of dA_2' on the hemisphere base,

$$dA_2' = \frac{dA_2''}{\cos \theta_1} \quad (6)$$

Inserting Equation 6 in Equation 5,

$$d\omega_1 = \frac{dA_2''}{R^2 \cos \theta_1} \quad (7)$$

The right side of Equation 4 appears explicitly in Equation 1 and, because Equation 7 is identical to Equation 4, Equation 2 becomes

$$c_{12} = \iint_{A_2} \frac{\cos \theta_1}{\pi} \left(\frac{dA_2''}{R^2 \cos \theta_1} \right) = \frac{\iint_{A_2} dA_2''}{\pi R^2} = \frac{A_2''}{\pi R^2}$$

For a sphere of unit radius (unit sphere),

$$c_{12} = \frac{A_2''}{\pi} \quad (8)$$

which completes the proof of Nusselt's method. By inserting Equation 8 in Equation 3, the original equation becomes greatly simplified; only one area integration is now required.

$$f_{12} = \frac{1}{A_1} \iint_{A_1} \frac{A_2''}{\pi} dA_1 \quad (9)$$

The computer program described herein solves Equation 9 numerically by successive algebraic evaluation of A_2'' at preselected points on Surface A_1 , with subsequent numerical integration to yield f_{12} , or

$$f_{12} = \frac{1}{A_1} \sum_{A_1} \frac{A_2''}{\pi} \Delta A_1 \quad (10)$$

It should be emphasized that area A_2'' is, in fact, formed by the doubly projected silhouette of surface A_2 as it appears from dA_1 .

The element dA_1 is assumed to be oriented in the XY plane and at the origin of the coordinate system of Surface A_2 . The area A_2'' can be found from the line integral where $y_1 = F(x_1)$ is the locus of the boundary of A_2 ,

$$A_2'' = \frac{1}{2} \int_C (x_1 dy_1 - y_1 dx_1) \quad (11)$$

Let $z = F(x,y)$ be the locus of the silhouette of A_2 , and S the distance from dA_1 to the point (x,y,z) on the silhouette of A_2 .

$$S = \sqrt{x^2 + y^2 + z^2}$$

From similar triangles,

$$x_1 = \frac{x}{S}, \quad dx_1 = \frac{1}{S} dx + x d\left(\frac{1}{S}\right)$$

$$y_1 = \frac{y}{S}, \quad dy_1 = \frac{1}{S} dy + y d\left(\frac{1}{S}\right)$$

Inserting in Equation 11

$$A_2'' = \frac{1}{2} \int_C \frac{xdy - ydx}{S^2} \quad (12)$$

Equation 12 can be transposed to finite difference form by replacing the differentials with increments for numerical evaluation. Because of the problems of increment size control, it appears desirable to solve Equation 12 for a finite line segment in space and to allow the analyst to control accuracy of configuration factor computation by suitable selection of line segments describing Surface 2. If the surface is actually a polygon or polyhedra, the simulation is perfect; if the surface boundary is curved, like a disk, for example, the validity of the result is a function of the number of line segments used.

However, a much simpler and more easily understood geometric derivation, using the unit sphere, yields the result in superior computational form. Referring to Figure 2, note that the radial projection of line segment AB on the hemisphere surface forms the circular arc A'B'. Projection of A'B' to the base plane produces the elliptical arc A''B'', forming the elliptical section A''OB'' with the origin.

If all line segments describing Surface 2 are similarly projected, the area A_2'' will be formed by a closed series of elliptical arcs. Surface A_2 does not have to be a plane. Actually, the area A_2 results from the geometry of a silhouette; any surface or object projecting an identical silhouette in the same spatial position on the hemisphere surface will produce the same area A_2 and the same point factor.

Inspection reveals that the magnitude of area A_2'' can be determined by computing the area of each elliptical sector, properly signed, followed by an algebraic summation.

In Figure 2, the area of elliptical sector A_E is the projected area of circular sector A_S . If the angle between the plane of the circular sector A'OB' and the XY plane is γ , then

$$\cos \gamma = \frac{A_E}{A_S} \quad (13)$$

The area A_S is computed from the usual polar equation, with θ in radians,

$$A_S = \frac{1}{2} R^2 \theta$$

For the unit radius sphere,

$$A_S = \frac{\theta}{2} \quad (14)$$

Substituting Equation 14 in Equation 13, and solving for A_E ,

$$A_E = \frac{\theta}{2} \cos \gamma \quad (15)$$

For a polygon of N sides, the net area A_2'' is found by algebraic summation of all computed A_E .

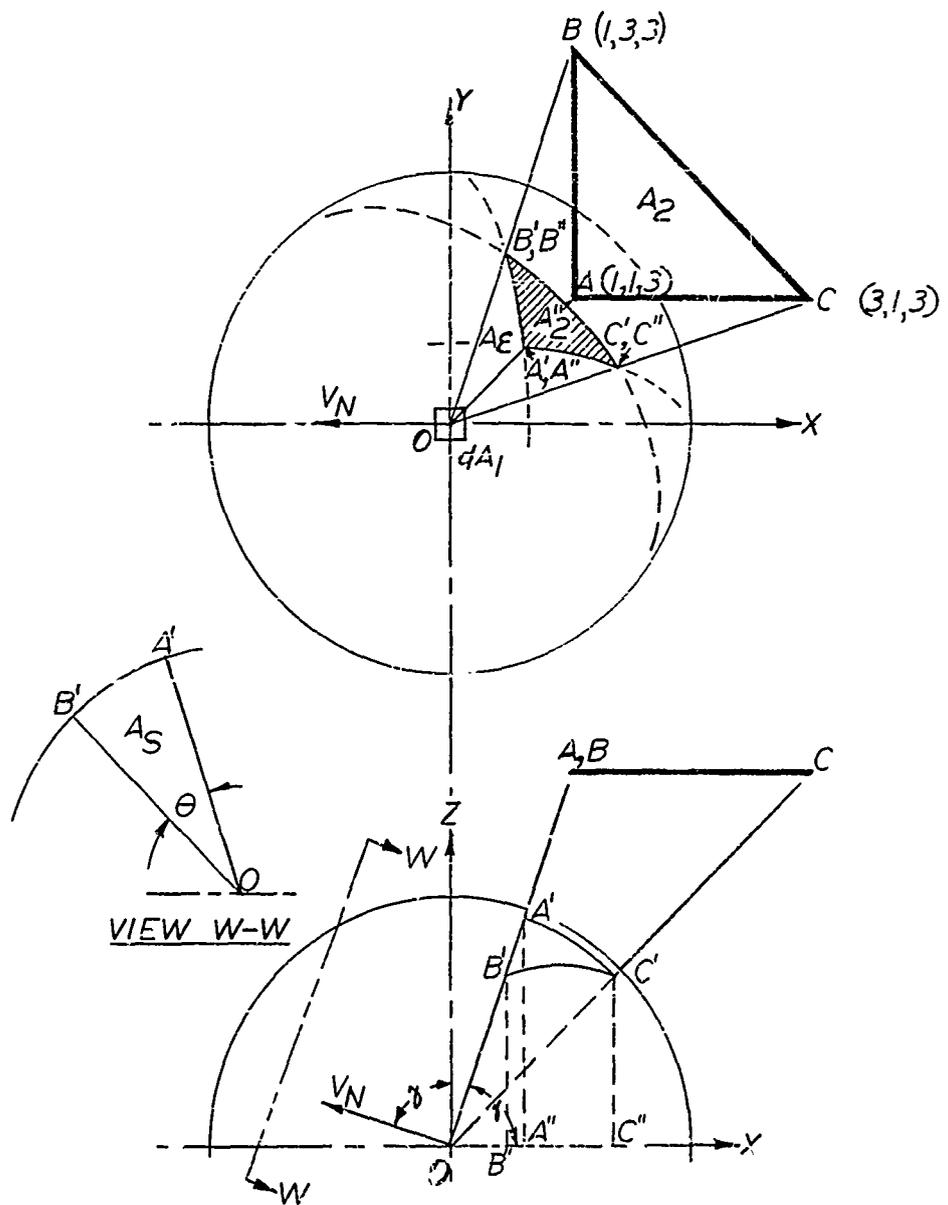


FIGURE 2. GEOMETRY OF NEW METHOD OF CONFIGURATION FACTOR COMPUTATION

$$\Lambda_2'' = \frac{1}{2} \left| \sum_{n=1}^N \theta_n \cos \gamma_n \right| \quad (16)$$

Substituting in Equation 8, we have

$$\epsilon_{12}'' = \frac{i}{2\pi} \left| \sum_{n=1}^N \theta_n \cos \gamma_n \right| \quad (17)$$

A general analytical derivation of this equation is given in Reference 3, and is reported to be originally developed by Omoto in 1924.

The absolute value notation will be explained later. The use of vector algebra greatly facilitates the computation of θ and $\cos \gamma$. Taking, for example, directed line segments of \vec{OA} and \vec{OB} , the vector dot product is

$$\vec{OA} \cdot \vec{OB} = x_A x_B + y_A y_B + z_A z_B \quad (18)$$

The cross product $\vec{OA} \times \vec{OB}$ in determinant form is

$$\vec{OA} \times \vec{OB} = \begin{vmatrix} i & j & k \\ x_A & y_A & z_A \\ x_B & y_B & z_B \end{vmatrix}$$

which, upon expansion, becomes the normal vector \vec{V}_N ,

$$\vec{V}_N = \vec{OA} \times \vec{OB} = (y_A z_B - z_A y_B) i + (x_B z_A - z_B x_A) j + (x_A y_B - x_B y_A) k \quad (19)$$

where i , j , and k are mutually orthogonal unit base vectors directed along the principal axes.

\vec{V}_N is equal in magnitude to twice the area of the triangle AOB and is oriented normal to the plane of AOB so that the three vectors form a right-handed system. The magnitude is computed by the Pythagorean theorem,

$$|\vec{V}_N| = \sqrt{(y_A z_B - z_A y_B)^2 + (x_B z_A - x_A z_B)^2 + (x_A y_B - x_B y_A)^2} \quad (20)$$

The angle θ may be evaluated from either the dot or the cross product by use of inverse functions, specifically

$$\theta = \cos^{-1} \left[\frac{\vec{O}\vec{A} \cdot \vec{O}\vec{B}}{|\vec{O}\vec{A}| |\vec{O}\vec{B}|} \right] \text{ or } \sin^{-1} \left[\frac{|\vec{V}_N|}{|\vec{O}\vec{A}| |\vec{O}\vec{B}|} \right]$$

However, an overall economy of computation results from the use of the arctan function,

$$\theta = \tan^{-1} \left[\frac{|\vec{V}_N|}{\vec{O}\vec{A} \cdot \vec{O}\vec{B}} \right] \quad (21)$$

As noted earlier, the angle γ is defined as the angle between the plane of AOB and the XY plane. It is also the angle between the vector \vec{V}_N and the Z axis; $\cos \gamma$ is therefore the direction cosine of \vec{V}_N with respect to the Z axis. Using the Z component in Equation 19,

$$\cos \gamma = \frac{x_A y_B - x_B y_A}{|\vec{V}_N|} \quad (22)$$

If the numerator and denominator are both divided by 2,

$$\cos \gamma = \frac{\frac{x_A y_B - x_B y_A}{2}}{\frac{|\vec{V}_N|}{2}}$$

This shows that $\cos \gamma$ is also equal to the ratio of the signed projected area of triangle AOB on the XY plane and the plane area of triangle AOB.

In the right-handed system shown, $\cos \gamma$ is positive when the order of computation of the vectors in the cross product causes the normal vector \vec{V}_N to point in the direction of the +Z axis ($0 < \gamma < 90$). The order in which one proceeds from point to point on the boundary of Surface 2 will sign each elliptical sector accordingly; however, because the sectors are summed algebraically, the same absolute magnitude will result regardless of order. Because the point factor is always a positive number, the order is computationally unimportant. Nevertheless, the program requires that data be entered in counterclockwise order for other reasons. This will be discussed in more detail later.

The relative ease with which the point factor can be computed is best illustrated by an example. Using the triangle shown in Figure 2, and starting with line segment \overline{AB} , from Equation 18

$$\vec{OA} \cdot \vec{OB} = 1 + 3 + 9 = 13$$

from Equation 20

$$|\vec{V}_{AB}| = |\vec{OA} \times \vec{OB}| = \sqrt{(-6)^2 + 0 + (2)^2} = \sqrt{40}$$

From Equation 21

$$\theta_{AB} = \tan^{-1} \left[\frac{\sqrt{40}}{13} \right] \cong 0.453$$

From Equation 22

$$\cos \gamma_{AB} = \frac{2}{\sqrt{40}} = 0.316$$

Moving to BC,

$$\vec{OB} \cdot \vec{OC} = 3 + 3 + 9 = 15$$

$$|\vec{V}_{BC}| = \sqrt{6^2 + 6^2 + (-8)^2} = \sqrt{136}$$

$$\theta_{BC} = \tan^{-1} \left[\frac{\sqrt{136}}{15} \right] \cong 0.661$$

$$\cos \gamma_{BC} = \frac{-8}{\sqrt{136}} = -0.686$$

Finally, line segment \vec{CA} ,

$$\vec{OC} \cdot \vec{OA} = 3 + 1 + 9 = 13$$

$$|\vec{VA}| = \sqrt{0 + 6^2 + (-2)^2} = \sqrt{40}$$

$$\theta_{CA} = \tan^{-1} \left(\frac{\sqrt{40}}{13} \right) \cong 0.453$$

$$\cos \gamma_{CA} = \frac{2}{\sqrt{40}} = 0.316$$

The configuration factor is, therefore, from Equation 17,

$$\begin{aligned} \epsilon_{12} &= \frac{1}{2\pi} \left| 2(0.453)(0.316) + (0.661)(-0.686) \right| \\ &= \frac{1}{2\pi} \left| -0.167 \right| \end{aligned}$$

$$\epsilon_{12} = 0.0266$$

Note the repetitive nature of the computation. Thus, all surfaces represented by straight line segments in space can be analyzed in the simple, direct manner shown.

COORDINATE TRANSFORMATION

The task of computing factors, even when simple "closed-form" solutions are available, is oftentimes laborious because the surfaces under consideration appear in difficult, skewed relative positions. A significant part of this effort has been eliminated by the program through the capability of general coordinate transformation (translation and/or rotation). Surface data may be entered for each surface using an individually convenient local origin. The surfaces may then be linked together by transforming one or both surfaces to a convenient third origin which is common to both surfaces. The fact that internally generated surfaces may also be transformed (excluding multisurfaces) makes this feature a very powerful tool.

Actually, two different types of coordinate transformation are used by the program. The transformation discussed in the prior paragraph is termed a "primary" transformation, and is under control of the user through transformation data entry. The second type of transformation is termed an "auxiliary" transformation, and is under internal program control only. An auxiliary transformation transforms the surface coordinates of both surfaces into a new coordinate system formed so that the XY plane of the coordinate system lies in the reference plane of one of the surfaces. The reference plane of a surface is the plane formed by the first, second and last point describing that surface. The origin of an auxiliary coordinate system is located at point i in the particular surface controlling the transformation. The X-axis is directed along the line segment formed by points 1 and 2. The surface unit orientation vector becomes the Z axis; the Y axis is computed orthogonal to the X and Z axes, thus locating the XY plane in the control surface reference plane.

The auxiliary transformation actually serves two purposes. First, it is utilized by Subroutine DOICU to facilitate reconstruction of the "seen" part of surfaces which are not entirely seen by the other surface. Secondly, the program requires that prior to computation of the configuration factors, Surface 1 must appear in the XY plane of the final coordinate system along with Surface 2 in its proper relative position. This is necessary to enable Subroutine MAP to select points on Surface 1 from which factors to Surface 2 may be directly computed, or from which silhouettes of Surface 2 may be generated and factors computed.

For example, suppose Figure 3 represents the surfaces of various items of equipment appearing in a compartment. The unprimed coordinate system shown may be conveniently chosen at a corner or axis of symmetry, perhaps as shown on a mechanical drawing. This system may not be convenient for data entry of the disk, however. The primed coordinate system with the origin at the center of the disk is the more logical choice in this case. The previously described surface generator will generate the disk about this origin. The disk data can then be transformed from the primed to the unprimed system by a primary transformation. The choice of generating the cube and transforming, or directly entering data from the unprimed system, is left to the user as it requires about equal effort both ways. The plate coordinates can be easily entered from the unprimed system. Now, suppose we desire the form factor from the disk to the plate. If the data are entered as discussed above (including the transformation data), the program will generate the disk and then primary transform disk coordinates to the unprimed system. Since the disk is bisected by the plate, an auxiliary transformation of all coordinates, both disk and plate, will be made from the unprimed to the quad-primed system. Now, that portion of the disk appearing above the active side of the plate will be determined, and an auxiliary transformation of the plate and the truncated disk will be made to the double primed coordinate system, i.e., the reference plane of the disk. The disk is now in a position for mapping, and the plate coordinates are proper for obtaining the configuration factors. A similar manipulation of surface data would be made to obtain the form factor to the cube with one exception -no truncation of the disk would occur and the auxiliary

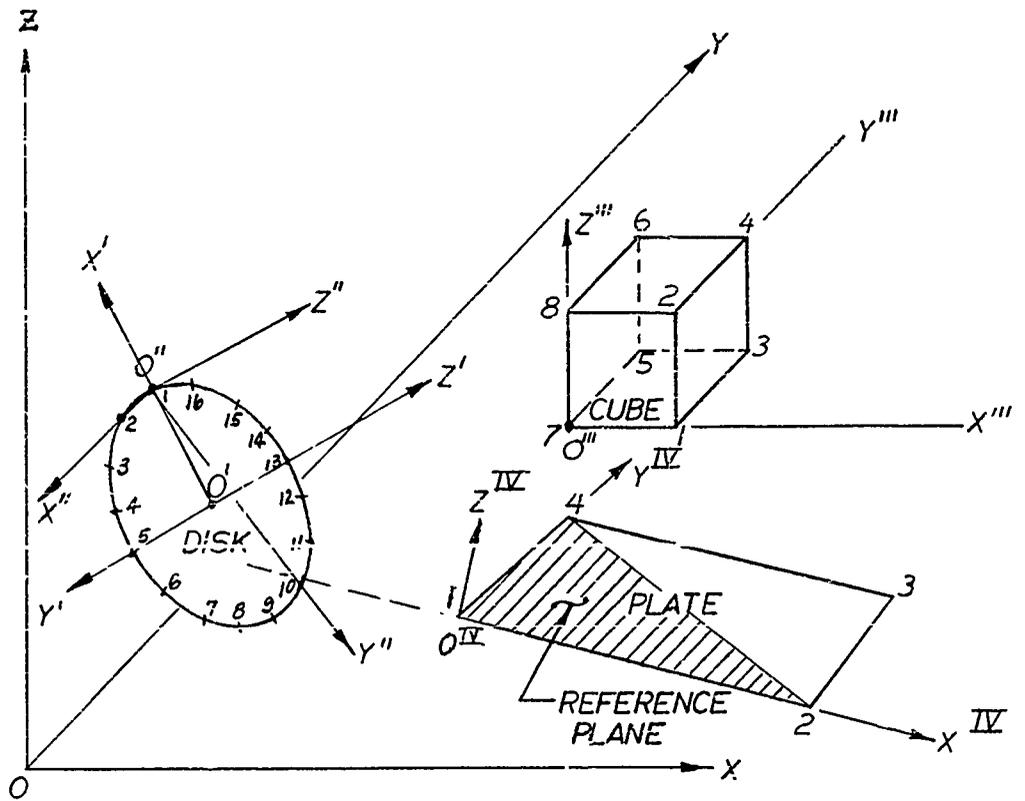


FIGURE 3. SURFACE COORDINATE TRANSFORMATION

transformation to the double-primed system would occur immediately after primary transformation.

The transformation technique utilized for a primary transformation differs from the customary method whereby "old" coordinates plus translation data and direction cosines or Euler angles are supplied, from which a "new" set of coordinates are derived. The program requires the coordinates of any three points (not in a line) measured from the new origin. These data are then used to derive direction cosines and translation terms, by which the old coordinates are then transformed to the new origin.

The reader may find it easier to visualize transformation in terms of the movement of the surfaces instead of the origins. In the case of the disk, again referring to Figure 3, we may say we generated the disk with its center at the origin of the unprimed system and in its XY plane, and then moved the surface to the position indicated by the primed system. This viewpoint appears more realistic when motion is simulated by transforming a surface along a particular path.

The mathematical treatment of primary and auxiliary transformation is presented in Appendix C.

SILHOUETTE GENERATOR

As noted in the introduction, CONFAC I cannot, in general, be used to compute the form factor to solid surfaces. Subroutine FACTOR requires a single array be made available containing the surface boundary points, and only those points, which, when taken in numerical sequence, form a valid silhouette of Surface 2 from a particular point in Surface 1. It is impossible to generally satisfy this requirement with a single input array if Surface 1 is finite and Surface 2 is arbitrarily nonplanar or solid. It is the function of the silhouette generator to determine which points in a given set of Surface 2 data form the silhouette from preselected viewpoints on Surface 1.

The silhouette generator computes the silhouette from the perspective of Surface 2 developed on the Z-unity ($Z = +1$) plane. The perspective on the Z-unity plane is the locus formed in the plane by the boundary of the solid angle subtended by Surface 2.

For example, the view of a cube from two positions on the XY plane is shown in Figure 4. The coordinates of each point in the Z-unity plane are derived in the following manner from the coordinates of its corresponding point on the cube. Note the triangle formed by the origin, point 2 in the cube, and point Q, the vertical projection of point 2 on the XY plane. A similar triangle is constructed from point 2' to point N. From similar triangles,

$$\frac{ON}{OQ} = \frac{Z_2'}{Z_2} \quad (22)$$

In like manner, using triangles RON and SOQ in the top view,

$$\frac{ON}{OO} = \frac{OR}{OS} = \frac{NR}{QS}$$

but $OR = X_2'$, $OS = X_2$, $NR = Y_2'$, $QS = Y_2$ and $Z_2' = 1$.

Therefore,

$$\frac{X_2'}{X_2} = \frac{Z_2'}{Z_2} = \frac{1}{Z_2}$$

$$X_2' = \frac{X_2}{Z_2} \tag{23}$$

and similarly,

$$Y_2' = \frac{Y_2}{Z_2} \tag{24}$$

This reduction to two dimensions results in considerable simplification. Given the coordinates (X, Y) and point connections data, it is possible to determine the line segments forming the silhouette by application of a simple criterion. At each point on the silhouette, those line segments forming the largest included angle define the silhouette. For example, at point 2' in the lower silhouette in Figure 4, vectors 2' - 3', 2' - 1' and 2' - 4' emerge from the point. Vectors 2' - 3' and 2' - 4' obviously form the silhouette, and can be numerically selected by applying the criterion.

Figure 5 shows the development of the Z-unity plane silhouette of a multisurface. In contrast to point D, Surfaces S2 and S3 appear separated in the silhouette when viewed from C.

Note the line connecting 4 to 7. This artifice - a "bridge" line - is utilized to cause the silhouette generator to include both surfaces in the silhouette, otherwise surface S3 would be ignored. Because the line has no width, it has no effect on the factor computation, but the silhouette generator follows the line as if it were a boundary of the multisurface S2 plus S3.

The distinguishing difference between the silhouettes shown in Figure 4 and Figure 5 is the fact that "crossover" occurs in Figure 5. The silhouette at a crossover is formed by intersecting line segments at a point between line segment extremities. The detection of such intersections, and the computation of the coordinates of the intersection, requires considerable analysis with resultant increased computer time. Because of this, silhouette analysis is termed "simple" if no investigation is made by the silhouette generator to detect crossovers, and "complex" when such is made. Only multisurface data (class 8) are run in the complex mode. All other surface data requiring the silhouette generator (classes 4, 5 and 6) are run in the simple mode.

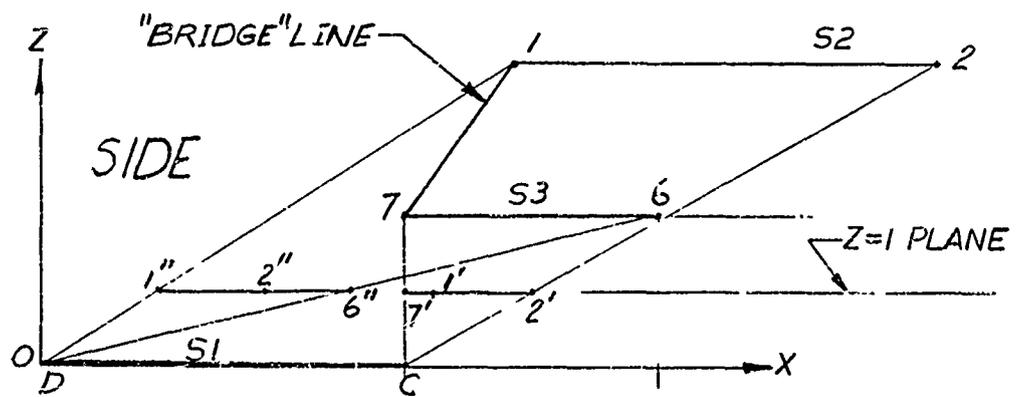
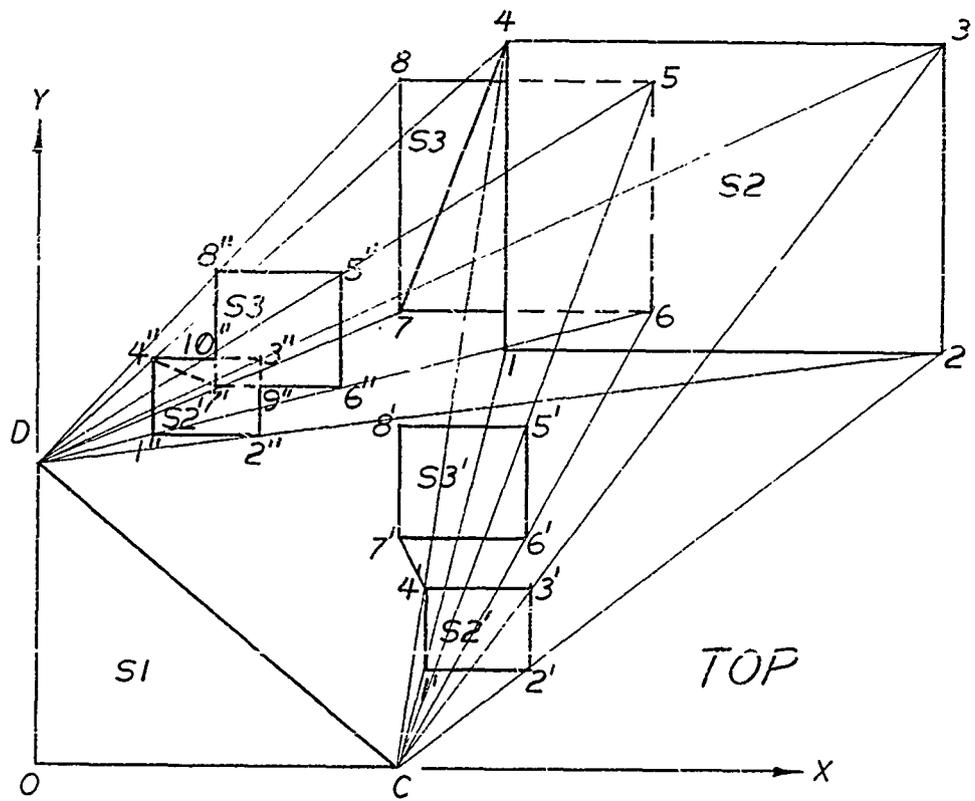


FIGURE 5. COMPLEX (MULTISURFACE) SILHOUETTE GEOMETRY

SURFACE GENERATOR

The program cannot directly compute factors to curved surfaces or boundaries such as disks, cylinders, etc. A series of line segments must be substituted for a curved line. In general, the more line segments used, the more accurate the simulation. Because every surface point requires 3 coordinates (and connecting points data, when the silhouette must be computed), preparation and entry of data for even a modest simulation of a cylinder can involve a considerable amount of effort. The internal surface generator eliminates practically all of this effort.

The surface generator is used to create surfaces entered under data classes 3 or 6. Regular plane polygons are created under Class 3, but no connections data are generated. A regular plane polygon or solid surface, including connections data, is created under a class 6 entry.

The surface generator "creates" a surface in accordance with cross section specifications. The following information is required to create a class 3 surface:

1. Number of cross section division (sides) ≥ 3
2. Coordinates (X, Y, Z) of center of polygon
3. X-axis Radius
4. Y-axis Radius

Because a class 6 surface may have one or more cross sections, the following data are required:

1. Number of cross section division (sides) ≥ 3
2. Number of cross sections
3. Coordinates (X, Y, Z) of first cross section
4. X-axis Radius of first cross section
5. Y-axis Radius of first cross section

If more than one cross section is specified, the following data are required for each additional cross section: X-axis radius, Y-axis radius and Z-coordinate. All cross sections are created parallel to the XY plane of the generator coordinate system, and must be specified above the XY plane. Note that X, Y coordinates are required to locate the first cross section only. If more than one is specified, all are oriented along the same vertical centerline to the position specified by the respective Z coordinate.

The basic generating element is the ellipse. Because only complete polygons are generated, the total angle of 2π radians about the vertical centerline is divided by the number of sides specified to yield the unit parametric angle ϕ in the equations of the ellipse:

$$\phi = \frac{2\pi}{N}$$

$$X = (XR) \cos \phi$$

$$Y = (YR) \sin \phi$$

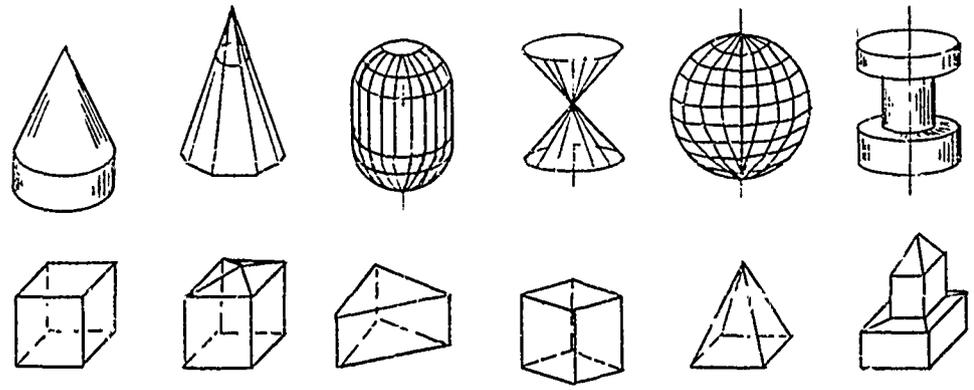
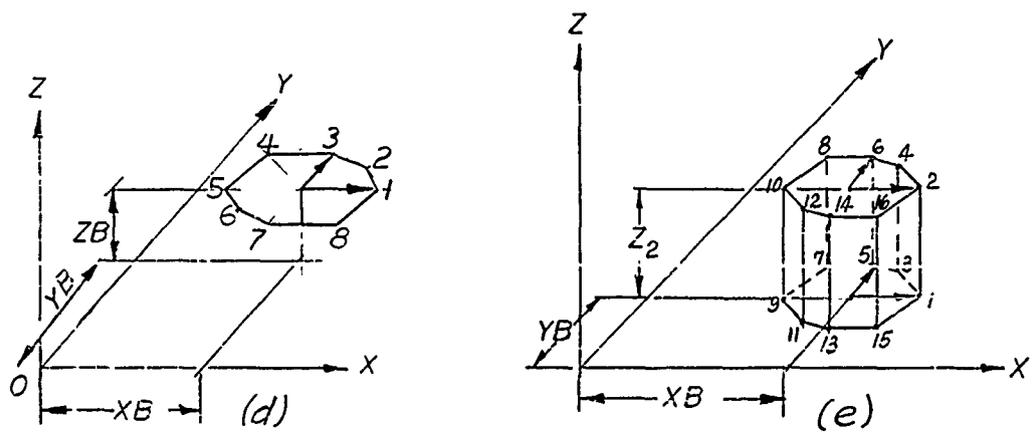
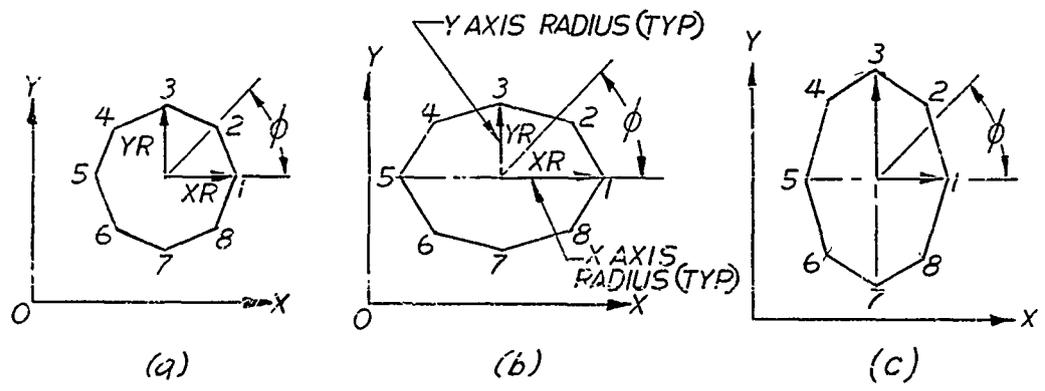
Instead of the conventional semi-major and semi-minor expressions, the terms "X-Radius" and "Y-Radius" are utilized - the larger of the two becomes the semi-major axis as shown in Figures 6 (a), (b), and (c). When $XR = YR$, the generating figure is circular and a regular polygon of N sides results. Notice that the generating figure always circumscribes the generated polygon. The radius vector always starts in the same relative position parallel to X-axis and moves counterclockwise about the vertical centerline of the generated cross section. Considerable computing time is saved by using $\sin(\phi + \beta)$, $\cos(\phi + \beta)$ trigonometric formulae for computation of X , Y after unit values are obtained by use of computer library functions.

Figure 6 (d) shows an eight-sided polygon elevated above the XY plane. Figure 6 (e) indicates the order in which point numbers are assigned to a solid surface. The first point is always assigned to the first coordinates in the first cross section. Numbers are assigned in numerical sequence vertically until the last cross section is numbered, for a particular value of ϕ ; the sequence is continued in similar manner with the first cross section and the next value of ϕ , until all points are defined.

Point connections data are also computed for each point for Class 6 surfaces. For example, in Figure 6 (e), points 2, 3 and 15 are computed for point 1; points 1, 4 and 16 are computed for point 2, etc. This information is used by the silhouette generator.

An example of the variety of objects which may be created by a few cards of specifications are shown in Figure 6 (f). The cone vertex is generated merely by specifying zero X-radius and Y-radius.

The internal surface generator also computes the surface area of the generated solid, if the cross sections are similar. Because the silhouette generator analyzes the solid figure, the total surface area is computed. For instance, the area of the prismatic cylinder shown in Figure 6 (e) would include the top and bottom polygons. The surface area computation analytical development is given in Appendix D.



(f)

FIGURE 6. CONFAC II SURFACE GENERATOR

SECTION III

COMPUTER PROGRAM CONTENTS

PROGRAM DESCRIPTION

The program is written in IBM 7090 FORTRAN II source language. The source deck consists of the Main Program and Subroutines UNIVFC, TXFRM, COICU, MAP, SILFAC and FACTOR. An input-output tape compatibility Subroutine written in IBM 7090 (FAP) machine language is included. Algebraic routines required from library tape are SQRT (Square Root), ARCTAN (Inverse tangent trigonometric function), COS (Cosine trigonometric function), and SIN (Sine trigonometric function). The source programs are presently dimensioned so that a 32 K core size is required. NAA Library Subroutines COUNTV and TIMEV are also used by Subroutine SILFAC when operating in the NAA 7094 system.

Main Program

The functions performed by the Main Program are as follows:

1. Reads in surface, transformation and run data.
2. Processes input surface data and prints immediately upon completion. Run instruction data are read in and processed one card at a time and processed at once. No printout of the complete run instructions is given, as was in CONFAC I.
3. Selects the proper data for processing according to the run instructions.
4. Examines each run instruction and calls in proper subroutines for processing.
5. Prints diagnostic error indications when possible.
6. Prints standard or detailed output as indicated by run instructions.

Subroutine UNIVFC

This subroutine computes the components of a unit orientation vector normal to the reference plane formed by the first, second and last point in surface data classes 1, 3, 4 and plane 6. The cross product of vectors 1-2 and 1-last is computed and normalized. The vector is formed normal to point 1, and is located on the active side of the surface, thus orienting the surface.

It also computes a new fourth point normal to the new three points submitted in transformation data and an old fourth point normal to the old three points in the surface data to be transformed.

Subroutine TXFRM

The first section performs the auxiliary transformation. This transformation is used to reconstruct a surface which is bisected by the second surface. It also tests Surface 1 to determine if the reference plane is substantially in the XY plane of its coordinate system. If it is not, an auxiliary transformation is effected to move the surfaces to fulfill this requirement prior to computation of silhouettes or factors.

This subroutine also performs a primary transformation as indicated by P.U. instructions and transformation data. This transformation, if indicated for a surface, is accomplished prior to entry to subroutine DOICU so that tests of the surface "view" of each other occur in their transformed position(s).

Subroutine DOICU

The function of this subroutine is conveyed literally by its name DO-I-C-U. Given surfaces A1 and A2 with the "active" side of each surface identified by the surface orientation unit vector, the question is asked; Is all, part, or none of surface A1 "seen" by A2? Conversely, does A2 see all, none, or part of A1? This is accomplished by computing the vector dot product formed by the unit vector in one surface with the vector formed by point 1 in the first surface and each point in the other surface (See Figure 7). The sign of the dot product indicates whether the angle between the vectors is less than or greater than 90° , which reveals the position of the point relative to the plane of the viewing surface. In Figure 7 (a) the dot products from surface A1 to A2 are all positive, and conversely, all from A2 to A1 are likewise positive: A1 sees all of A2; A2 sees all of A1. However, in Figure 7 (b) all dot products from A2 to A1 are positive, but all from A1 to A2 are negative. Hence, in general, if all dot products from one surface to another are all negative, then the surfaces do not see each other, even though the converse products may be positive. There is also the trivial case where all products are zero, in which case the surfaces are in the same plane, and obviously again cannot see each other.

Figure 7 (c) shows a surface A2 bisecting surface A1. In this case, some of the dot products from A2 and A1 are positive and some negative. In Figure 7 (d) both A1 and A2 are bisected. Nonplanar surface A3 was added to show how it would be bisected by A1. Surface A3 has no orientation vector and thus no test is made of the view from this surface. The vertical dashed line in A2 represents how the plane 1-2-5-6 in A3 might bisect A2. DOICU will not detect this condition. If the configuration factor, C_{23} , were required, DOICU would properly bisect A3. However, if the factor to the concave side only is desired, an error would result because part of A2 sees the convex side of A3. This represents one of the limitations of CONFAC I which is carried over to CONFAC II.

If a surface is bisected, DOICU reconstructs the surface data to exclude the area not seen by the other surface. If point 1 in the original surface is

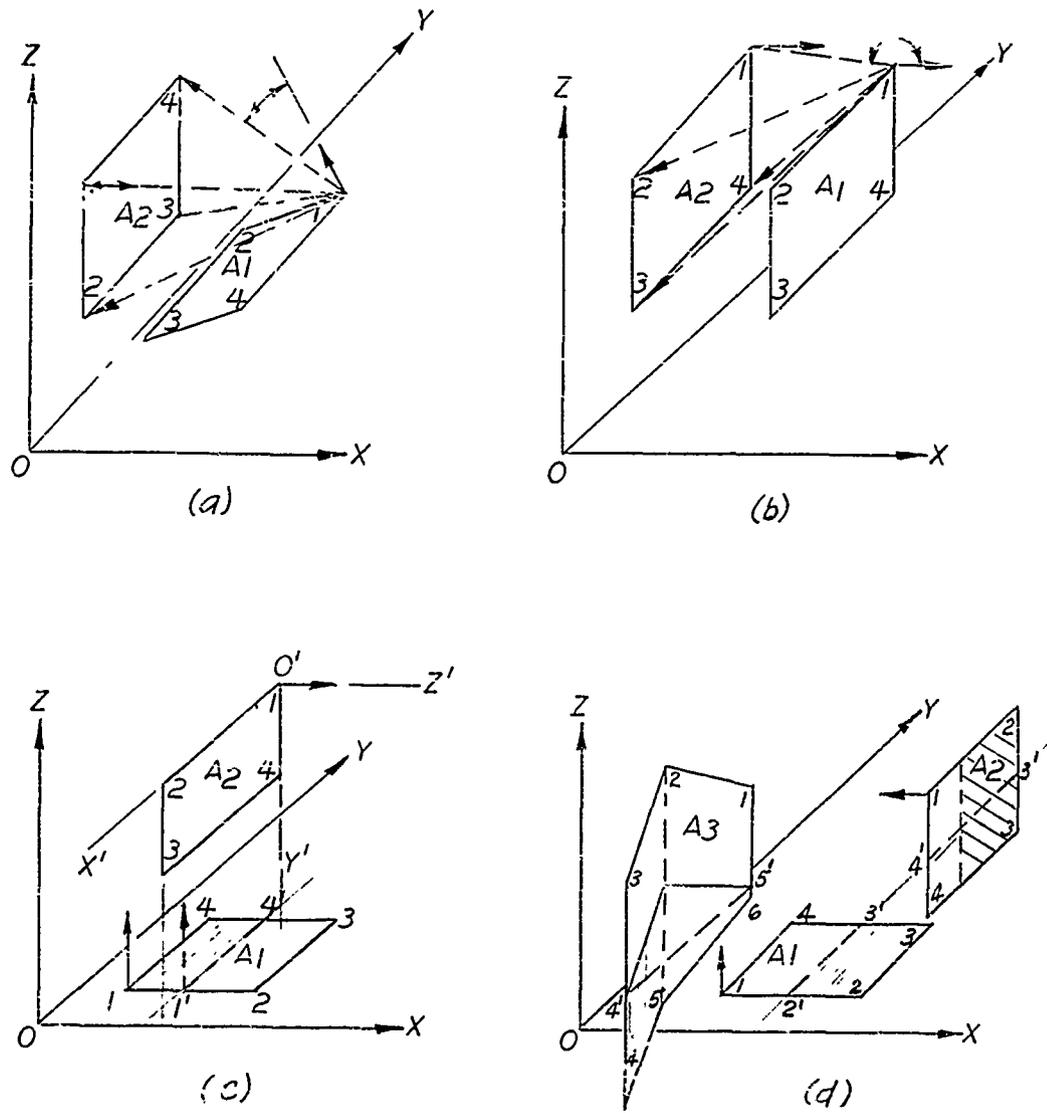


FIGURE 7. DOICU SURFACE ANALYSIS

removed as a result, a new orientation vector is created over the new point 1 as shown in Figure 7 (c). Notice that in reconstructing A3 [Figure 7 (d)], DOICU created the new array 1, 2, 3, 4', 5'. This "surface" is identical to the actual surface seen by A1 insofar as factor computation from A1 is concerned.

The bisection of a surface is done in a simple manner, with the aid of the auxiliary transformation capability. For example, in Figure 7 (c), the coordinates of both surfaces are transformed so that A2 lies in the XY plane of the auxiliary (primed) coordinate system. Each point in A1 is tested, in numerical order, until a change in the sign of the Z-coordinate occurs. The coordinates of the new points where the transition line segment crosses the X' Y' plane ($Z' = 0$) are obtained by computing X and Y intercepts of traces projected on X' Z', Y' Z' principal planes.

Subroutine MAP

The double integral in Equation (9) and its numerical counterpart in Equation (10) mathematically represent the volume under a surface defined by the configuration factor $c_{12} = f(X,Y)$. Subroutine MAP decides the location (X,Y) from which each factor to Surface 2 will be computed.

It is assumed that Surface 1, being classed as a plane, is a plane surface throughout. The program insures only that the reference plane of Surface 1 is in the XY plane of the final coordinate system. MAP will use the X,Y coordinates of all points, and assumes a value of 0 for all Z coordinates. This procedure cannot properly map a nonplanar surface.

Subroutine MAP determines the maximum Y coordinate and the minimum Y coordinate from among the points defining Surface 1 (Figure 8). The total vertical distance between Y_{max} and Y_{min} is divided into equal vertical increments, as specified by the run instructions. Then, horizontal lines are scribed across (parallel to X-axis) the surface at each vertical increment position, including Y_{max} and Y_{min} . The point at which a horizontal line intersects the left (toward the negative X direction) boundary of Surface 1 is termed "X-left" and the intersection on the right, "X-right". Each horizontal line segment thus created is termed a "mapping line". Each mapping line segment is also divided into an equal number of increments as specified by the run instructions. All mapping lines are divided into the same number of increments, not necessarily the same size of increment. Obviously, if Surface 1 converges to a point instead of a line at Y_{max} or Y_{min} , the horizontal increment is 0. A configuration factor is computed at each increment point along a mapping line, including X-left and X-right, which means the number of factors per line is one greater than the number of increments.

The number of increments is automatically set to 24 horizontal and 24 vertical, but can be separately specified by input data to 3, 6, 18, 24, 30, 36, 42, 48, 54, or 60. The details are discussed in Section IV.

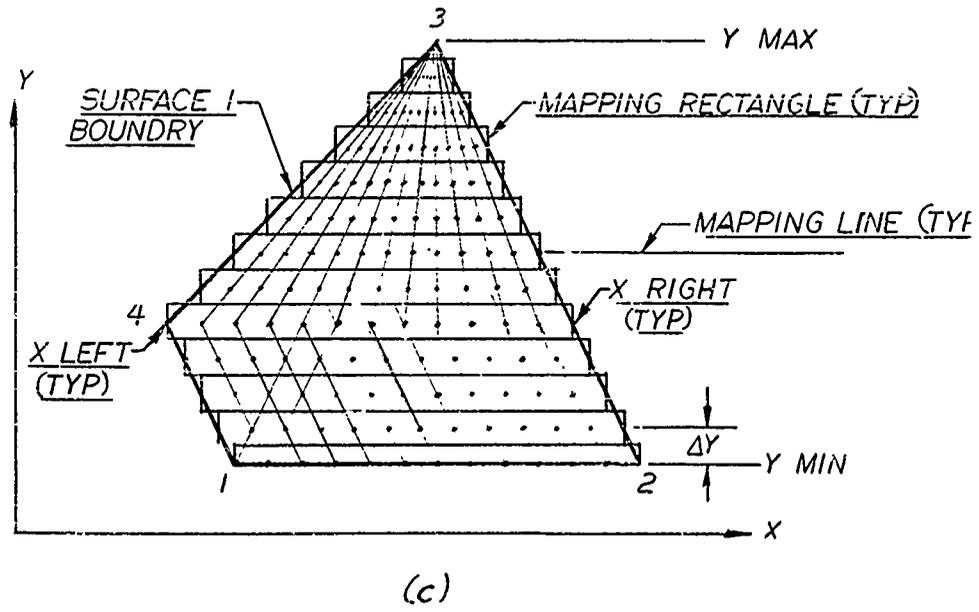
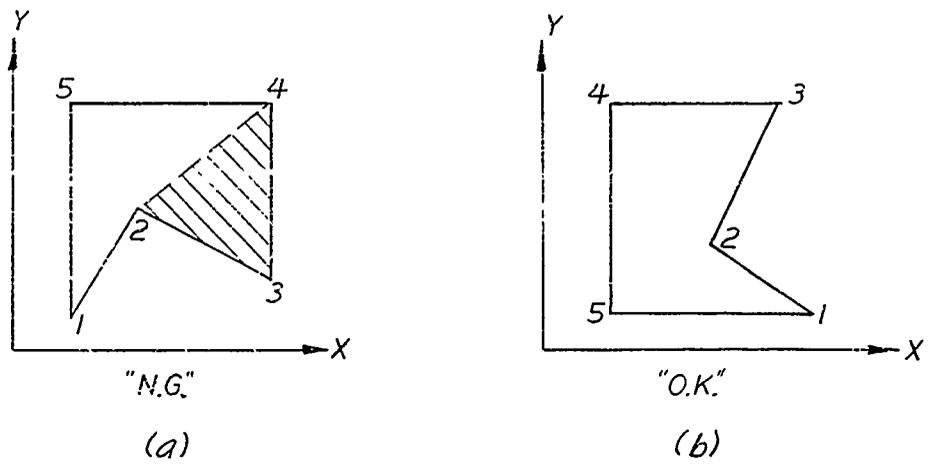


FIGURE 8. MAPPING PROCEDURE

A typical example of Surface 1 manning using a standard (24 x 24) increment is shown in Figure 8 (c). The manning area is also computed by Subroutine MAP, it is the sum of the rectangular areas formed by each manning line. A measure of form factor accuracy is the degree with which the manning area approximates the actual surface area.

Figure 8 (a) illustrates a Surface 1 orientation which cannot be satisfactorily manned because the crosshatched area is ignored. The program does not detect more than one left and one right intersection between a manning line and the surface boundary; therefore, point 3 is ignored. The same surface rotated sufficiently may be acceptable, however, clearing this restriction, as shown in Figure 8 (b).

Subroutine SILFAC

This subroutine computes the silhouette of Surface 2 which appears from the points selected on Surface 1 by Subroutine MAP, and then computes the configuration factor from this silhouette. After all configuration factors have been determined, the form factor is computed by numerical integration.

Surface data entered as Class 4, 5, 6, 7 or 8 is processed by SILFAC. Class 7 data, a sphere, is processed in this routine, but the silhouette generator is not utilized; a closed form solution is used instead (see Appendix E).

Classes 4, 5 and 6 are processed by the silhouette generator in the 'simple' mode; only those points given in connections data are analyzed to select the next point on the silhouette. Surfaces such as planes, cylinders, parallelpiped, etc. may be processed in the simple mode.

Class 8, a multisurface, is the only class processed in the complex mode. One or more (limitations on data are given at the end of this section and in Section IV) surfaces may be processed as a multisurface. Processing in the complex mode is complicated because the computer must test all line segments in all surfaces (including the surface in which the segment appears) in order to select the next point forming the silhouette, or to compute the next point on the silhouette. This analysis is further complicated by ambiguities resulting from normal imprecision in input data and internal arithmetic roundoff, necessitating the use of numerous time consuming tolerance tests. Consequently, a factor computation in the complex mode takes considerably longer than the simple mode.

If a surface is processed as simple when it should be complex a wrong silhouette will be computed whenever a crossover (an intersection of two line segments) occurs. The configuration factor computed from that silhouette will be wrong.

It is possible to detect certain kinds of trouble in the silhouette generator from the detailed silhouette output which lists the points forming the

silhouette. Normally, the silhouette will start at the lowest leftmost point in the Z-units plane perspective developed for the noted point in Surface 1, and move progressively from point to point in a counterclockwise manner, keeping the perspective area to the left. When a crossover occurs, the point is computed and assigned the next highest number in the silhouette array. For example, from point "9" in Figure 5, the silhouette derived in the complex mode would appear in the detailed silhouette output as "Line No., Point No., 1" 2" 9" 6" 5" 8" 10" 4" 1." However, if this problem were run in simple (both surfaces entered together as Class 4) instead, Surface 53 would be ignored because the crossover at point 9 would not be computed. The silhouette would appear normal, but actually be wrong, as follows:

Line No., Point No., 1" 2" 3" 4" 1"

A bad silhouette can sometimes be detected by the presence of internal "looming". Normally, a silhouette is completed by a return to the starting point. But, if, for some reason, a wrong path is chosen, it may loop a polygon within the perspective. Looming is characterized by the repeated appearance of the same sequence of numbers. No internal pattern recognition is attempted, the only detection is visual examination of the detailed output.

The coordinates of the silhouette on the Z = 1 plane are used directly for factor computation instead of the actual points on the surface in space. Because the Z - coordinate of each point is 1, the configuration factor equations for this special case can be simplified, and computing time reduced. SIMFAC, therefore, contains its own equations for configuration factor computation and numerical integration across Surface 1. The integration process is similar to the procedure given in Subroutine FACTOR. Subroutine FACTOR has been retained from COMFAC I for factor computations not utilizing the silhouette generator.

Subroutine FACTOR

This subroutine computes configuration factors from each point on Surface 1 selected by MAP to Surface 2. The exchange coefficient is computed by numerical integration of configuration factors across Surface 1, from which the form factor is finally derived as the area-weighted mean of all configuration factors.

Factors are computed for each point along each mapping line, moving from X-left to X-right, by translating the origin of the Surface 2 coordinate system in X. The analysis and equations are organized for minimum computational time; constants at each loop level are computed once prior to loop entry. Because the usual output desired is only the form factor, configuration factors never are not computed unless a detailed output is requested. A numerical integration of computed point function with respect to X is performed before proceeding to the next line. After all horizontal integrations are completed, these products are integrated with respect to Y, and divided by the mapping area computed in subroutine MAP.

A standard 24 X 24 grid results in 625 configuration factors to be computed. The question naturally arises as to whether this many configuration factors are actually required. If the configuration factor changes very little across Surface 1, then it is probably too many; but if there are sharp changes in the factor, and third place accuracy is desired, then it is probably sufficient. Contrary to off-hand expectations, a more sophisticated integration rule such as Simson's or Weddle's is not as accurate as the trapezoidal rule for standard increments if the factor function alone changes rapidly. Weddle's rule was initially used which explains why the program increment control is in groups of six (except the initial 3 which is not in ONFAC I). If the factor varies smoothly, a 6 x 6 weddle's rule integration (49 factors) is probably as accurate as the standard 625 factors presently used by the trapezoidal rule. The time saved is appreciable when running many factors. If desired, Weddle's rule may be inserted in the source deck and compiled with no other changes required.

The form factor computed by the above is from that part of Surface 1 which "sees" Surface 2. If Surface 1 is bisected, then the computed factor must be reduced in proportion to the area reduction. This is required because the total active side of Surface 1 entered in data is considered the radiant surface.

GENERAL RULES AND RESTRICTIONS

The following general rules and restrictions must be observed for normal program operation:

1. All data must be derived from right-handed rectangular coordinate systems.
2. Points 1, 2 and the last point in plane surface input data (Class 1 and 4) must not form a straight line in space.
3. The active side of a plane or nonplanar surface is established by entering the boundary points in counterclockwise order, as they appear when facing the active side.
4. If the factor to a Class 2 (nonplanar) surface is required, only the active surfaces should be seen from any point on Surface 1, and they must also be seen from every point on Surface 1.
5. All surfaces used as Surface 2 which utilizes the silhouette generator (Classes 5, 6, 8, or 4 if included in Class 8) must appear above the plane of Surface 1, i.e., all Z - coordinates must be nonzero and positive, prior to factor computation.
6. A primary transformation of Class 8 data is not permitted. Also, no auxiliary transformation is permitted; Surface 1 must be in the XY plane of the Multisurface coordinate system as entered in data.
7. Detailed restrictions and limitations upon input data are given in Section IV.

SECTION IV

INPUT DATA

DATA SPECIFICATIONS AND SPECIFIC RESTRICTIONS

Input data consists of externally computed surface data, specifications for internally created surfaces, transformation data and run instructions (vector requests). Also title and comments cards may be entered as required.

Data type is classified by the use of an integer from 1 to 9 placed in column 1 of the data name card, followed by a 1 to 5 FORTRAN character name to provide data identity within each class. The classes of data are described below.

Class 1 - Plane Polygon

The X, Y, and Z coordinates of each point defining the surface boundary are required. Only one side of a simple plane surface can be made active i.e., may interchange radiant flux with another surface. The active side is established in the following manner: Face or look at the desired active side, and select any point on the surface boundary as point number one. Proceeding in a counterclockwise direction about the boundary of the surface, select the remaining points in sequence. If this rule is followed, the surface will always be on the left when moving along the boundary.

The X, Y, and Z coordinates of each point are entered on the data cards in the above sequence, and each point is numbered internally according to its position in the data.

It is assumed that a Class 1 surface is a plane surface. No internal check is made to verify this (in contrast to CONFAC I). If a substantially nonplanar surface is classed as a plane surface, serious errors in naming could result if used as Surface 1, or wrong factors computed if used as Surface 2.

No point connections data are entered under Class 1; the silhouette generator is not used.

Class 2 - Nonplanar Surface

Two or more plane surfaces, not in the same plane, adjoining or connected, and entered as one package is termed a nonplanar surface.

A Class 2 surface can be used as Surface 2 if the side of each facet selected as the active side, and only those sides, are seen from everywhere on the active side of Surface 1. The counterclockwise order of data

entry establishing the active side is also required as in Class 1, but no orientation vector is generated.

No connection data is required because the silhouette generator is not used.

Class 3 - Internally Generated Plane Polygon, No Connections Data

The internal surface generator will compute the coordinates of each point defining a plane polygon, parallel to the XY plane, with an orientation vector erected over point 1 and directed toward the +Z axis. A detailed description of the internal surface generator is given in Section II.

The data required for a Class 3 surface is:

No. of sides, $3 \leq N \leq 100$

X - Axis Radius

Y - Axis Radius

X, Y, and Z coordinates to center of polygon

A Class 3 surface is used in the same manner as a Class 1 surface. The same rules and restrictions apply.

Class 4 - Plane Polygon with Connections Data and Class 5 - Nonplanar Polygon or Solid Surface with Connections Data

A Class 4 surface is actually a Class 1 surface with connections data added making it possible for it to be processed with the silhouette generator. But, in general, no useful purpose is gained by the use of the silhouette generator to process a plane surface, unless combined with other surfaces. Therefore, a Class 4 surface is processed as a Class 1 surface, unless it is listed under a Class 8 entry.

A Class 5 surface is always processed in the simple mode by SILFAC unless listed under a Class 8 entry.

A maximum of 100 boundary points may be entered describing a Class 4 or 5 surface. Up to 4 connecting points for each boundary point may be entered. If more than four connecting points are required, one may enter more boundary data points having the same coordinates and connecting to each other, using the surplus (3) connections to satisfy the additional connections requirement. However, if more than two such identical boundary points are used, the surface cannot be processed in the simple mode. This restriction in most practical situations can be circumvented by separating the points slightly with little effect on the final form factor computed. If this cannot be done, the surface must be listed under a Class 8 name and processed in the complex mode.

Class 6 - Internally Generated Polygon or Polyhedron, Including Connections Data

A detailed description of the internal surface generator is given in Section II. A class 6 surface is always processed by SILFAC - in the simple mode if used directly, and complex if listed under Class 8. The data required to create a Class 6 surface are:

1. No. of cross sections
2. No. of cross sections divisions (sides)
3. Coordinates and generating radii of first cross section.
4. Z-coordinate and generating radii of additional cross sections, if any.

Attention is directed to general restrictions 4 and 5 in Section III.

Class 7 - Sphere

The radius and the X, Y, and Z coordinates of the sphere are required. A primary transformation of a sphere is pointless and therefore not permitted. Arbitrary orientation of both Surface 1 and sphere is allowed. One peculiarity exists which differs from the usual treatment of bisected surfaces. If the plane of Surface 1 bisects the sphere, the area of the spherical surface above the horizon of Surface 1 will be computed. Now the sphere cannot bisect Surface 1 in the usual sense, but it is possible a bisected sphere may be partly or totally inside the boundaries of Surface 1 - embedded in the surface. In this case, the program will merely assign a zero for the configuration factor when the viewpoint from Surface 1 is inside the sphere. This zero will be interpreted as usual with the other factors computed along each scanning line. No computation of the Surface 1 area seeing the sphere is made, however, even though part of Surface 1 is not seen by the sphere.

Class 8 - Multisurface

A Multisurface consists of from one to eleven Class 4, 5, or 6 surfaces. A Class 8 surface, and only a Class 8 surface, is processed in the complex mode. The only data entry necessary to indicate the surfaces which comprise a Multisurface are the names assigned each surface.

Class 9 - Transformation Data

Transformation Data consists of the coordinates of three points in a surface, not in a straight line, derived from the "new" position of a surface which has been moved in its coordinate system. One may, with equal validity, interpret the transformation to mean that the origin of the coordinate system is being moved to a different position, and the data are the coordinates of

each point taken from the new origin. The three points selected need not be chosen or entered in any particular order, nor must the same points be used if more than one different primary transformation of the same surface is desired.

Run Instructions

Run instructions specify, for each factor desired, the following:

1. The name of Surface 1 (emitter)
2. The name of Surface 2 (receiver)
3. Transformation data name(s) for Surface 1 and/or 2, if required.
4. Whether a standard or detailed output is desired, by inserting code letter "D" for detailed output.
5. The horizontal and/or vertical divisions to be used in mapping surface 1. The major divisions which may be used are 6, 12, 18, 24, 30, 36, 42, 48, 54 and 60, but in run instructions these divisions are specified, respectively, by the integers 1, 2, 3, 4, 5, 6, 7, 8, 9 and 10. A special division of 7 may be specified by the integer 11.

DATA DIMENSION RESTRICTIONS

1. A maximum of 100 boundary points (300 coordinates) for each surface entered as Class 1, 2, 4, and 5.
2. A maximum of 100 points, equivalent to 100 sides, generated by Class 3 data.
3. For Class 6 data, the number of sides plus one, times the number of cross sections, must not exceed 101 if plane, and 102 if non-planar.
4. The grand total of surfaces entered or generated by Class 4, 5 and 6 must not exceed 11.
5. The grand total of surfaces entered or generated by Classes 1, 2, 3, 4, 5 and 6 must not exceed 26. If a detailed silhouette output is requested, the grand total must not exceed 16.
6. The total number of Class 7 data must not exceed 9.
7. The total number of Class 8 data must not exceed 12.
8. The total number of Class 9 data must not exceed 10.

PROGRAM CONTROL

The program deck setup is shown in Figure 36. Note the presence of a "T" card immediately following the * DATA Card and the variable format. A "T" card has a "T" in column 1, and serves two purposes. Columns 2 - 72 may contain job title, name of programmer, etc. and will be printed in the output of input data and each factor result. The "T" card also initializes data storage locations, so that new input data can be read in. This means, however, that the old data is effectively wiped out, and is no longer available for fact or computations, unless re-entered as input data. It is obviously unnecessary to use the "T" card unless all available locations are used up.

Actually, a "T" card does not necessarily have to follow the variable format unless one desires the title to be printed, because the data location counters are automatically initialized at the start of the program. But subsequent re-initialization can be accomplished only by a card with a "T" in column 1.

It appears desirable to have separate identification of the various factors computed, and a comments card has been provided for that purpose. The comments card has a "C" in column 1, and a comment may appear in columns 2 - 72. A comments card may be inserted between run instruction cards, and the line of comment given on the card will be printed below the title on all output thereafter, unless superseded by another comments card.

Comments output may be entirely suppressed by using another comments card containing blanks in columns 2 - 72.

FORMAT

All data may be entered on NAA FORTRAN Fixed 10 Decimal Data sheets. Each line represents 12 card columns with six lines per card, making a total of 72 card columns available for data entry. Columns 73 - 80 are used for card identification and/or numerical sequencing for sorting purposes.

Title Card

A title card is characterized by an alphabetical "T" placed in column 1. Columns 2 - 72 available for job identification, as shown on Figure 9.

Comments Card

A comments card is characterized by an alphabetical "C" placed in column 1. Columns 2 - 72 are available for run comments, as shown on Figure 9.

Surface and Transformation Data

All surface and transformation data is preceded by a name card uniquely identifying the data. A name consists of six FORTRAN characters (a computer "word") and always occupies the first six columns of the name card. The data

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DECOR NO. UNIT | | PROGRAMS 1 & 2 OF 2 | DATE 8/1/51 | PAGE 1 | JOB NO. |
|----------------|----------------|---------------------|------------------|--------|---------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | | |
| 1 | | | | | |
| 2 | | | | | |
| 3 | | | | | |
| 4 | | | | | |
| 5 | | | | | |
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FIGURE 9. "T" and "C" Control Card Format

class, an integer from 1 to 9, must always be placed in column 1. The remainder of the name occupies columns 2 - 6, and it is important to note that a blank space is considered a character and a part of the name. For example, the name 1S1 is not the same as 1_S1 or 1__S1.

The next word on the name card, columns 7 - 12 must be left blank. The remainder of the name card, (columns 13 - 72) may be left blank or contents written to further identify the data, and will be printed out along with the name of the surface as part of the "Input Data" print out.

The data identified by the name card must follow the name card. There are seven different formats which must be adhered to in entering data.

Class 1 and 2

The number of points to be entered describing the surface appears on the first line, Figure 10, followed by the X, Y, and Z coordinates of each point in sequence. The order in which the points are selected in the surface is explained in detail in Section IV.

Class 3

The number of sides are entered on the first line, followed by the X, Y, and Z coordinates of the center of the internally generated polygon, the X-axis radius and the Y-axis radius as shown in Figure 11.

Class 4

The total number of points describing the surface are entered on the first line as shown in Figure 12. The X, Y, and Z coordinates of the first point follow on the next three lines. The fourth line, representing 12 columns, is divided into four equal parts of 3 columns each. Each point in the surface connecting to point 1 is entered, up to a maximum of four. The pattern is repeated for the remaining points describing the surfaces.

Class 6

The numbers of surface cross section boundary divisions (sides) is given on the first line as shown in Figure 13. The number of cross sections desired is specified on the second line, followed by the X, Y, and Z coordinates of the base (1st) cross section. The X-axis radius of the base cross section is given on the last line of the first card. The Y-axis radius is entered on the first line of the second card, followed by, if more than one cross section is specified, the following, repeated for each cross section. The height (Z-coordinate) of the cross section above the XY plane, the X-axis radius and the Y-axis.

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | FORM | PROGRAMMER | I A SURF | DATE | SCALE | NAME | JOB NO. |
|----------|----------------|--|----------|------|-------|------|---------|
| NUMBER | IDENTIFICATION | DESCRIPTION DO NOT KEY PUNCH | | | | | |
| 1 | 1 1 1 1 1 | NAME OF CLASS 1 OR 2 SURFACE, CLASS 1-2 | | | | | |
| 2 | | CLASS 1 - PLAN NUMBER, SIZE "1" IN COL. 1 | | | | | |
| 3 | | CLASS 2 - MONOLAYER NUMBER, SIZE "2" IN COL. 1 | | | | | |
| 4 | | IDENTIFY CLASS "1" IN PLAN NUMBER | | | | | |
| 5 | | CLASS "2" IS AN ADDITIONAL SURFACE | | | | | |
| 6 | | THE CLASS "2" IS THE PLAN TO USE | | | | | |
| 7 | | NO. OF POINTS SURROUNDING THE SURFACE | | | | | |
| 8 | | COORDINATES OF FIRST SURROUNDING POINT | | | | | |
| 9 | | COORDINATES OF SECOND SURROUNDING POINT | | | | | |
| 10 | | COORDINATES OF THIRD SURROUNDING POINT | | | | | |
| 11 | | COORDINATES OF FOURTH SURROUNDING POINT | | | | | |
| 12 | | COORDINATES OF FIFTH SURROUNDING POINT | | | | | |
| 13 | | COORDINATES OF SIXTH SURROUNDING POINT | | | | | |
| 14 | | COORDINATES OF SEVENTH SURROUNDING POINT | | | | | |
| 15 | | COORDINATES OF EIGHTH SURROUNDING POINT | | | | | |
| 16 | | COORDINATES OF NINTH SURROUNDING POINT | | | | | |
| 17 | | COORDINATES OF TENTH SURROUNDING POINT | | | | | |
| 18 | | COORDINATES OF ELEVENTH SURROUNDING POINT | | | | | |
| 19 | | COORDINATES OF TWELFTH SURROUNDING POINT | | | | | |
| 20 | | COORDINATES OF THIRTEENTH SURROUNDING POINT | | | | | |
| 21 | | COORDINATES OF FOURTEENTH SURROUNDING POINT | | | | | |
| 22 | | COORDINATES OF FIFTEENTH SURROUNDING POINT | | | | | |
| 23 | | COORDINATES OF SIXTEENTH SURROUNDING POINT | | | | | |
| 24 | | COORDINATES OF SEVENTEENTH SURROUNDING POINT | | | | | |
| 25 | | COORDINATES OF EIGHTEENTH SURROUNDING POINT | | | | | |
| 26 | | COORDINATES OF NINETEENTH SURROUNDING POINT | | | | | |
| 27 | | COORDINATES OF TWENTIETH SURROUNDING POINT | | | | | |
| 28 | | COORDINATES OF TWENTY-FIRST SURROUNDING POINT | | | | | |
| 29 | | COORDINATES OF TWENTY-SECOND SURROUNDING POINT | | | | | |
| 30 | | COORDINATES OF TWENTY-THIRD SURROUNDING POINT | | | | | |
| 31 | | COORDINATES OF TWENTY-FOURTH SURROUNDING POINT | | | | | |
| 32 | | COORDINATES OF TWENTY-FIFTH SURROUNDING POINT | | | | | |
| 33 | | COORDINATES OF TWENTY-SIXTH SURROUNDING POINT | | | | | |
| 34 | | COORDINATES OF TWENTY-SEVENTH SURROUNDING POINT | | | | | |
| 35 | | COORDINATES OF TWENTY-EIGHTH SURROUNDING POINT | | | | | |
| 36 | | COORDINATES OF TWENTY-NINTH SURROUNDING POINT | | | | | |
| 37 | | COORDINATES OF THIRTIETH SURROUNDING POINT | | | | | |
| 38 | | COORDINATES OF THIRTY-FIRST SURROUNDING POINT | | | | | |
| 39 | | COORDINATES OF THIRTY-SECOND SURROUNDING POINT | | | | | |
| 40 | | COORDINATES OF THIRTY-THIRD SURROUNDING POINT | | | | | |
| 41 | | COORDINATES OF THIRTY-FOURTH SURROUNDING POINT | | | | | |
| 42 | | COORDINATES OF THIRTY-FIFTH SURROUNDING POINT | | | | | |
| 43 | | COORDINATES OF THIRTY-SIXTH SURROUNDING POINT | | | | | |
| 44 | | COORDINATES OF THIRTY-SEVENTH SURROUNDING POINT | | | | | |
| 45 | | COORDINATES OF THIRTY-EIGHTH SURROUNDING POINT | | | | | |
| 46 | | COORDINATES OF THIRTY-NINTH SURROUNDING POINT | | | | | |
| 47 | | COORDINATES OF FORTY SURROUNDING POINT | | | | | |
| 48 | | COORDINATES OF FORTY-FIRST SURROUNDING POINT | | | | | |
| 49 | | COORDINATES OF FORTY-SECOND SURROUNDING POINT | | | | | |
| 50 | | COORDINATES OF FORTY-THIRD SURROUNDING POINT | | | | | |
| 51 | | COORDINATES OF FORTY-FOURTH SURROUNDING POINT | | | | | |
| 52 | | COORDINATES OF FORTY-FIFTH SURROUNDING POINT | | | | | |
| 53 | | COORDINATES OF FORTY-SIXTH SURROUNDING POINT | | | | | |
| 54 | | COORDINATES OF FORTY-SEVENTH SURROUNDING POINT | | | | | |
| 55 | | COORDINATES OF FORTY-EIGHTH SURROUNDING POINT | | | | | |
| 56 | | COORDINATES OF FORTY-NINTH SURROUNDING POINT | | | | | |
| 57 | | COORDINATES OF FIFTY SURROUNDING POINT | | | | | |
| 58 | | COORDINATES OF FIFTY-FIRST SURROUNDING POINT | | | | | |
| 59 | | COORDINATES OF FIFTY-SECOND SURROUNDING POINT | | | | | |
| 60 | | COORDINATES OF FIFTY-THIRD SURROUNDING POINT | | | | | |
| 61 | | COORDINATES OF FIFTY-FOURTH SURROUNDING POINT | | | | | |
| 62 | | COORDINATES OF FIFTY-FIFTH SURROUNDING POINT | | | | | |
| 63 | | COORDINATES OF FIFTY-SIXTH SURROUNDING POINT | | | | | |
| 64 | | COORDINATES OF FIFTY-SEVENTH SURROUNDING POINT | | | | | |
| 65 | | COORDINATES OF FIFTY-EIGHTH SURROUNDING POINT | | | | | |
| 66 | | COORDINATES OF FIFTY-NINTH SURROUNDING POINT | | | | | |
| 67 | | COORDINATES OF SIXTY SURROUNDING POINT | | | | | |
| 68 | | COORDINATES OF SIXTY-FIRST SURROUNDING POINT | | | | | |
| 69 | | COORDINATES OF SIXTY-SECOND SURROUNDING POINT | | | | | |
| 70 | | COORDINATES OF SIXTY-THIRD SURROUNDING POINT | | | | | |
| 71 | | COORDINATES OF SIXTY-FOURTH SURROUNDING POINT | | | | | |
| 72 | | COORDINATES OF SIXTY-FIFTH SURROUNDING POINT | | | | | |
| 73 | | COORDINATES OF SIXTY-SIXTH SURROUNDING POINT | | | | | |
| 74 | | COORDINATES OF SIXTY-SEVENTH SURROUNDING POINT | | | | | |
| 75 | | COORDINATES OF SIXTY-EIGHTH SURROUNDING POINT | | | | | |
| 76 | | COORDINATES OF SIXTY-NINTH SURROUNDING POINT | | | | | |
| 77 | | COORDINATES OF SEVENTY SURROUNDING POINT | | | | | |
| 78 | | COORDINATES OF SEVENTY-FIRST SURROUNDING POINT | | | | | |
| 79 | | COORDINATES OF SEVENTY-SECOND SURROUNDING POINT | | | | | |
| 80 | | COORDINATES OF SEVENTY-THIRD SURROUNDING POINT | | | | | |
| 81 | | COORDINATES OF SEVENTY-FOURTH SURROUNDING POINT | | | | | |
| 82 | | COORDINATES OF SEVENTY-FIFTH SURROUNDING POINT | | | | | |
| 83 | | COORDINATES OF SEVENTY-SIXTH SURROUNDING POINT | | | | | |
| 84 | | COORDINATES OF SEVENTY-SEVENTH SURROUNDING POINT | | | | | |
| 85 | | COORDINATES OF SEVENTY-EIGHTH SURROUNDING POINT | | | | | |
| 86 | | COORDINATES OF SEVENTY-NINTH SURROUNDING POINT | | | | | |
| 87 | | COORDINATES OF EIGHTY SURROUNDING POINT | | | | | |
| 88 | | COORDINATES OF EIGHTY-FIRST SURROUNDING POINT | | | | | |
| 89 | | COORDINATES OF EIGHTY-SECOND SURROUNDING POINT | | | | | |
| 90 | | COORDINATES OF EIGHTY-THIRD SURROUNDING POINT | | | | | |
| 91 | | COORDINATES OF EIGHTY-FOURTH SURROUNDING POINT | | | | | |
| 92 | | COORDINATES OF EIGHTY-FIFTH SURROUNDING POINT | | | | | |
| 93 | | COORDINATES OF EIGHTY-SIXTH SURROUNDING POINT | | | | | |
| 94 | | COORDINATES OF EIGHTY-SEVENTH SURROUNDING POINT | | | | | |
| 95 | | COORDINATES OF EIGHTY-EIGHTH SURROUNDING POINT | | | | | |
| 96 | | COORDINATES OF EIGHTY-NINTH SURROUNDING POINT | | | | | |
| 97 | | COORDINATES OF NINETY SURROUNDING POINT | | | | | |
| 98 | | COORDINATES OF NINETY-FIRST SURROUNDING POINT | | | | | |
| 99 | | COORDINATES OF NINETY-SECOND SURROUNDING POINT | | | | | |
| 100 | | COORDINATES OF NINETY-THIRD SURROUNDING POINT | | | | | |
| 101 | | COORDINATES OF NINETY-FOURTH SURROUNDING POINT | | | | | |
| 102 | | COORDINATES OF NINETY-FIFTH SURROUNDING POINT | | | | | |
| 103 | | COORDINATES OF NINETY-SIXTH SURROUNDING POINT | | | | | |
| 104 | | COORDINATES OF NINETY-SEVENTH SURROUNDING POINT | | | | | |
| 105 | | COORDINATES OF NINETY-EIGHTH SURROUNDING POINT | | | | | |
| 106 | | COORDINATES OF NINETY-NINTH SURROUNDING POINT | | | | | |
| 107 | | COORDINATES OF HUNDRED SURROUNDING POINT | | | | | |

FIGURE 10. Class 1 and 2 Surface Input Data Format

FORTRAN F'XSD ID DIGIT DECIMAL DATA

| DECK NO. | FORMAT | PROGRAMMER | E. A. TOPP | DATE 4/24/53 | PAGE | OF | JOB NO. |
|----------|----------------|--------------------------------------|------------------|--------------|------|----|---------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | | | | |
| 1 | F. S. T. T. | NAME OF CLASS 3 SURFACE CODE 1-4 | | | | | |
| 2 | | THE "1" IS CODE 1 TO CREATE IS | | | | | |
| 3 | | INTEGRALLY GENERATED PLANE POLAR | | | | | |
| 4 | | INTEGRAL CODE "2" IS KEY IN SURF | | | | | |
| 5 | | THE CODE "3" IS KEY IN SURF | | | | | |
| 6 | | THE CODE "4" IS FOR CODE TO ALL CODE | | | | | |
| 7 | | NO. OF ACTION POINTS = 3 | | | | | |
| 8 | | | | | | | |
| 9 | | COORDINATES OF CENTER | | | | | |
| 10 | | | | | | | |
| 11 | | X = AXIS RADIOS | | | | | |
| 12 | | Y = AXIS RADIOS | | | | | |
| 13 | | | | | | | |
| 14 | | | | | | | |
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FIGURE 11. Class 3 Surface Specifications Input Data Format

| FORTRAN FIXED 10 DIGIT DECIMAL DATA | | | |
|-------------------------------------|----------------|--|------------------|
| DECK NO. | FORST | PROGRAMMER | F. A. TOPP |
| DATE | 4/24/52 | PAGE | OF |
| JOB NO. | | | |
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH |
| 1 | | NAME OF CLASS 4 OF 5 SURFACE CODE 4 - 6 | |
| 2 | | CLASS 4 - PLATE POSITION, USE "1" TO COL. 1 | |
| 3 | | CLASS 5 - ROOTS OF FUNCTION OF WELD, REV. 3, IN P. 1 | |
| 4 | | INTERVAL CODE WILL BE READY | |
| 5 | | PERIODS TO BE FOR LAMINATION PROPERTIES | |
| 6 | | FOR COLS 7-10 FOR CARD 19, ALL CARDS | |
| 7 | | NO. OF POINTS BETWEEN SURFACE | |
| 8 | | COORDINATES OF FIRST SURFACE POINT | |
| 9 | | COORDINATES OF SECOND SURFACE POINT | |
| 10 | | COORDINATES OF THIRD SURFACE POINT | |
| 11 | | COORDINATES OF SECOND SURFACE POINT | |
| 12 | | COORDINATES OF SECOND SURFACE POINT | |
| 13 | | COORDINATES OF SECOND SURFACE POINT | |
| 14 | | COORDINATES OF SECOND SURFACE POINT | |
| 15 | | COORDINATES OF SECOND SURFACE POINT | |
| 16 | | COORDINATES OF SECOND SURFACE POINT | |
| 17 | | COORDINATES OF SECOND SURFACE POINT | |
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| 30 | | COORDINATES OF SECOND SURFACE POINT | |
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| 32 | | COORDINATES OF SECOND SURFACE POINT | |
| 33 | | COORDINATES OF SECOND SURFACE POINT | |
| 34 | | COORDINATES OF SECOND SURFACE POINT | |
| 35 | | COORDINATES OF SECOND SURFACE POINT | |
| 36 | | COORDINATES OF SECOND SURFACE POINT | |
| 37 | | COORDINATES OF SECOND SURFACE POINT | |
| 38 | | COORDINATES OF SECOND SURFACE POINT | |
| 39 | | COORDINATES OF SECOND SURFACE POINT | |
| 40 | | COORDINATES OF SECOND SURFACE POINT | |
| 41 | | COORDINATES OF SECOND SURFACE POINT | |
| 42 | | COORDINATES OF SECOND SURFACE POINT | |
| 43 | | COORDINATES OF SECOND SURFACE POINT | |
| 44 | | COORDINATES OF SECOND SURFACE POINT | |
| 45 | | COORDINATES OF SECOND SURFACE POINT | |
| 46 | | COORDINATES OF SECOND SURFACE POINT | |
| 47 | | COORDINATES OF SECOND SURFACE POINT | |
| 48 | | COORDINATES OF SECOND SURFACE POINT | |
| 49 | | COORDINATES OF SECOND SURFACE POINT | |
| 50 | | COORDINATES OF SECOND SURFACE POINT | |

FIGURE 12. Class 4 and 5 Surface Input Data format

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | FORMY | PROGRAMMER | F. S. TOPP | DATE | 8/24/51 | PAGE | 1 | JOB NO. |
|----------|----------------|---|------------------|------|---------|------|---|---------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | | | | | |
| C 1 | 1 | NAME OF CLASS 6 SURFACE CODE 1 - 6 | | | | | | |
| C 2 | 2 | THE "X" IN CODE 3 FOR AN INVERTABLE | | | | | | |
| C 3 | 3 | COMPUTED PLANE POSITION OF SURF. WITH COORDINATE DATA | | | | | | |
| C 4 | 4 | COMPUTED CO. OF SURF. FROM SURF. DATA | | | | | | |
| C 5 | 5 | THE CODE 1-10 FOR FUNCTIONAL DESCRIPTION | | | | | | |
| C 6 | 6 | USE CODE 7-10 FOR CODE TO ALL CAPS | | | | | | |
| C 7 | 7 | NO. OF SURFACE CROSS SECTION SPACES 1-3 | | | | | | |
| C 8 | 8 | NO. OF CROSS SECTION SPACES | | | | | | |
| C 9 | 9 | POSITIONS OF FIRST CROSS SECTION CENTER | | | | | | |
| C 10 | 10 | 1-10 SURF. FIRST CROSS SECTION | | | | | | |
| C 11 | 11 | 2-10 SURF. FIRST CROSS SECTION | | | | | | |
| C 12 | 12 | DEPTH (E-CROSS), SECOND CROSS SECTION (IF APPL) | | | | | | |
| C 13 | 13 | 1-10 SURF. " " " " " " | | | | | | |
| C 14 | 14 | 1-10 SURF. " " " " " " | | | | | | |
| C 15 | 15 | DEPTH " " " " " " | | | | | | |
| C 16 | 16 | DEPTH " " " " " " | | | | | | |
| C 17 | 17 | DEPTH " " " " " " | | | | | | |
| C 18 | 18 | DEPTH " " " " " " | | | | | | |
| C 19 | 19 | DEPTH " " " " " " | | | | | | |
| C 20 | 20 | DEPTH " " " " " " | | | | | | |
| C 21 | 21 | DEPTH " " " " " " | | | | | | |
| C 22 | 22 | DEPTH " " " " " " | | | | | | |
| C 23 | 23 | DEPTH " " " " " " | | | | | | |
| C 24 | 24 | DEPTH " " " " " " | | | | | | |
| C 25 | 25 | DEPTH " " " " " " | | | | | | |
| C 26 | 26 | DEPTH " " " " " " | | | | | | |
| C 27 | 27 | DEPTH " " " " " " | | | | | | |
| C 28 | 28 | DEPTH " " " " " " | | | | | | |
| C 29 | 29 | DEPTH " " " " " " | | | | | | |
| C 30 | 30 | DEPTH " " " " " " | | | | | | |
| C 31 | 31 | DEPTH " " " " " " | | | | | | |
| C 32 | 32 | DEPTH " " " " " " | | | | | | |
| C 33 | 33 | DEPTH " " " " " " | | | | | | |
| C 34 | 34 | DEPTH " " " " " " | | | | | | |
| C 35 | 35 | DEPTH " " " " " " | | | | | | |
| C 36 | 36 | DEPTH " " " " " " | | | | | | |
| C 37 | 37 | DEPTH " " " " " " | | | | | | |
| C 38 | 38 | DEPTH " " " " " " | | | | | | |
| C 39 | 39 | DEPTH " " " " " " | | | | | | |
| C 40 | 40 | DEPTH " " " " " " | | | | | | |
| C 41 | 41 | DEPTH " " " " " " | | | | | | |
| C 42 | 42 | DEPTH " " " " " " | | | | | | |
| C 43 | 43 | DEPTH " " " " " " | | | | | | |
| C 44 | 44 | DEPTH " " " " " " | | | | | | |
| C 45 | 45 | DEPTH " " " " " " | | | | | | |
| C 46 | 46 | DEPTH " " " " " " | | | | | | |
| C 47 | 47 | DEPTH " " " " " " | | | | | | |
| C 48 | 48 | DEPTH " " " " " " | | | | | | |
| C 49 | 49 | DEPTH " " " " " " | | | | | | |
| C 50 | 50 | DEPTH " " " " " " | | | | | | |
| C 51 | 51 | DEPTH " " " " " " | | | | | | |
| C 52 | 52 | DEPTH " " " " " " | | | | | | |
| C 53 | 53 | DEPTH " " " " " " | | | | | | |
| C 54 | 54 | DEPTH " " " " " " | | | | | | |
| C 55 | 55 | DEPTH " " " " " " | | | | | | |
| C 56 | 56 | DEPTH " " " " " " | | | | | | |
| C 57 | 57 | DEPTH " " " " " " | | | | | | |
| C 58 | 58 | DEPTH " " " " " " | | | | | | |
| C 59 | 59 | DEPTH " " " " " " | | | | | | |
| C 60 | 60 | DEPTH " " " " " " | | | | | | |
| C 61 | 61 | DEPTH " " " " " " | | | | | | |
| C 62 | 62 | DEPTH " " " " " " | | | | | | |
| C 63 | 63 | DEPTH " " " " " " | | | | | | |
| C 64 | 64 | DEPTH " " " " " " | | | | | | |
| C 65 | 65 | DEPTH " " " " " " | | | | | | |
| C 66 | 66 | DEPTH " " " " " " | | | | | | |
| C 67 | 67 | DEPTH " " " " " " | | | | | | |
| C 68 | 68 | DEPTH " " " " " " | | | | | | |
| C 69 | 69 | DEPTH " " " " " " | | | | | | |
| C 70 | 70 | DEPTH " " " " " " | | | | | | |
| C 71 | 71 | DEPTH " " " " " " | | | | | | |
| C 72 | 72 | DEPTH " " " " " " | | | | | | |
| C 73 | 73 | DEPTH " " " " " " | | | | | | |
| C 74 | 74 | DEPTH " " " " " " | | | | | | |
| C 75 | 75 | DEPTH " " " " " " | | | | | | |
| C 76 | 76 | DEPTH " " " " " " | | | | | | |
| C 77 | 77 | DEPTH " " " " " " | | | | | | |
| C 78 | 78 | DEPTH " " " " " " | | | | | | |
| C 79 | 79 | DEPTH " " " " " " | | | | | | |
| C 80 | 80 | DEPTH " " " " " " | | | | | | |
| C 81 | 81 | DEPTH " " " " " " | | | | | | |
| C 82 | 82 | DEPTH " " " " " " | | | | | | |
| C 83 | 83 | DEPTH " " " " " " | | | | | | |
| C 84 | 84 | DEPTH " " " " " " | | | | | | |
| C 85 | 85 | DEPTH " " " " " " | | | | | | |
| C 86 | 86 | DEPTH " " " " " " | | | | | | |
| C 87 | 87 | DEPTH " " " " " " | | | | | | |
| C 88 | 88 | DEPTH " " " " " " | | | | | | |
| C 89 | 89 | DEPTH " " " " " " | | | | | | |
| C 90 | 90 | DEPTH " " " " " " | | | | | | |
| C 91 | 91 | DEPTH " " " " " " | | | | | | |
| C 92 | 92 | DEPTH " " " " " " | | | | | | |
| C 93 | 93 | DEPTH " " " " " " | | | | | | |
| C 94 | 94 | DEPTH " " " " " " | | | | | | |
| C 95 | 95 | DEPTH " " " " " " | | | | | | |
| C 96 | 96 | DEPTH " " " " " " | | | | | | |
| C 97 | 97 | DEPTH " " " " " " | | | | | | |
| C 98 | 98 | DEPTH " " " " " " | | | | | | |
| C 99 | 99 | DEPTH " " " " " " | | | | | | |
| C 100 | 100 | DEPTH " " " " " " | | | | | | |

FIGURE 13. Class 6 Surface Specifications Input Data Format

Class 7

The sphere radius r entered on the first line, followed by the X, Y, and Z coordinates locating the center of the sphere as shown in Figure 14.

Class 8

The names of the surface (s) which are to be entered under this class are entered together on one card, without regard to order as shown in Figure 15. The card is usually divided into 12 words of six columns each. Each name to be entered must appear identically in a word-space as it appears in the word-space on the data name card.

Class 9

The first point to be transformed is entered on the first line, followed by the X, Y and Z coordinates of the "new" position of the point as shown in Figure 16. The second point to be transformed immediately follows on the fifth line followed by the X-coordinate of the new position of the second point, thus completing the first card. The Y and Z coordinates of the new position of the second point are entered on the first two lines of the second card, followed by the number of the third point to be transformed and its new X, Y, and Z coordinates.

All of the numbers entered in the above data may be entered as fixed or floating point numbers except connections data, which must be entered as decimal integers. If a decimal point is given (fractional numbers must have decimal points given), the floating number may be located anywhere in the field (line); if no decimal point is given, the number must be located to the extreme right of the field (no blanks to the right of the number).

Run Instructions

Six FORTRAN words comprise a set of run instructions; two sets may be entered on one card as shown in Figure 17. The first set starts at column 1 and the second set starts at column 37. Two words (12 columns) comprise one line on the data sheet. The name of the Surface 1 data is entered in the first word (columns 1 - 6) precisely as it appears in the first word of the surface data name card. The name of the Surface 2 data is entered in the second word (columns 8 - 12) precisely as it appears in the first word of the surface data name card. If a primary transformation of Surface 1 is desired, the desired transformation data name is entered in columns 13 - 18, otherwise, it is left blank. If a primary transformation of Surface 2 is desired, the name of the transformation data is entered in the fourth word, columns 19 - 24. If a detailed output is desired, the alphabetical character "D" is entered in column 27, or in column 31. If the "D" appears in either or both locations, a detailed output will result; if a blank is in both locations, a standard output will result. The horizontal naming division "integer" appears in column 30, unless the integer 10 or 11 is used, in which case columns 29 and 30 are utilized. The vertical naming division "integer" appears in column 36, un-

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DEQA NO. 70247 | | PROGRAMMER E. A. SOPE | DATE 6/11/53 | PAGE | OF | JOB NO. |
|----------------|-------------|-----------------------|--|------|----|---------|
| NUMBER | DEFINITION | DESCRIPTION | DO NOT KEY PUNCH | | | |
| 7 | 7 1 1 1 1 1 | | NAME OF CLASS 2 SURFACE, CODE 1-5 | | | |
| 8 | | | FOR 70 25 COL 1 FOR A SPHERE | | | |
| 9 | | | CONTRACT CODE 7-12 MUST BE BLANK | | | |
| 10 | | | THE CODE 13-15 FOR MATERIAL IDENTIFICATION | | | |
| 11 | | | THE CODE 16-18 FOR CODE 25, 45, 60, 75 | | | |
| 12 | | | NUMBER OF SPINES | | | |
| 13 | | | ACCELERATION OF SPIN | | | |
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FIGURE 14. Class 7 Sphere Specification Input Data Format

FORTRAN FIXED 10 DIGIT DECIMAL DATA

FORM NO. FPD11 PROGRAMMER: P. E. TERRY DATE: 12/63 PAGE: 1 JOB NO.

| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH |
|--------|----------------|--|------------------|
| 1 | 1 | TYPE OF CLASS 9 DATA CODE A - 6 | |
| 2 | 2 | EXP. FACTOR CODE B - 12 TRANSFORMATION | |
| 3 | 3 | DATA | |
| 4 | 4 | IS POINT CODE 7-12 MUST BE MARKED | |
| 5 | 5 | EXP. CODE 13-16 FOR ARITHMETICAL OPERATIONS | |
| 6 | 6 | EXP. CODE 17-20 FOR LOGIC OPERATIONS | |
| 7 | 7 | FIRST POINT TO BE TRANSFORMED | |
| 8 | 8 | | |
| 9 | 9 | COORDINATES OF FIRST POINT FROM | |
| 10 | 10 | NON-ORIGINS | |
| 11 | 11 | | |
| 12 | 12 | SECOND POINT TO BE TRANSFORMED | |
| 13 | 13 | | |
| 14 | 14 | COORDINATES OF SECOND POINT FROM REV. ORIGIN | |
| 15 | 15 | | |
| 16 | 16 | THIRD POINT, etc. | |
| 17 | 17 | | |
| 18 | 18 | COORDINATES, etc. | |
| 19 | 19 | | |
| 20 | 20 | | |
| 21 | 21 | DATA 21 & 2 DATA POINTS THE INITIAL POINT IS OFF | |
| 22 | 22 | INTERVAL WHICH MAY BE EXTENDED BY 1000000 | |
| 23 | 23 | TYPE OF POINT | |
| 24 | 24 | DATA POINT BE DELETED FROM A POINT-MARKED | |
| 25 | 25 | REPETITIOUS COMPUTATION SYSTEM | |

FIGURE 16. Class 9 Transformation Data Input Data Format

FORTRAN FIXED IO DIGIT DECIMAL DATA

| DECK NO. | FOUR/F | PROGRAMMER | E. S. MOSE | DATE | 4/24/53 | PAGE | 4 | TOTAL | 40 |
|----------|--------------|---|------------------|------|---------|------|---|-------|----|
| NUMBER | NOTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | | | | | | |
| 1 | | PAGE OF SERVICE 1 | | | | | | | |
| 2 | | PAGE OF SERVICE 1 TRANSFORMATOR DATA, IN LIST | | | | | | | |
| 3 | | PAGE OF SERVICE 2 | | | | | | | |
| 4 | | PAGE OF SERVICE 2 TRANSFORMATOR DATA, IN LIST | | | | | | | |
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FIGURE 17. Run Instructions Input Data Format

less the integer 10 or 11 is used, in which case columns 35 and 36 are utilized. If columns 29 and 30 are both blank, a standard integer 4 meaning 24 horizontal divisions of each naming line is used. If 35 and 36 are both blank, a standard vertical division of 24 will be used. The above format is repeated in the same manner, starting from column 37 on the fourth line, for the second set of run instructions on the card. There is no numerical limit to the number of run instructions which may be entered. The only requirement is, of course, that the data called for has been loaded in under the names used.

SECTION V

PROGRAM OUTPUT

Input data is processed and printed out prior to its use in factor computations for programmer verification. The orientation vector head end is also printed out for all plane surfaces, so that the "active" side used by the program is clearly shown. Class 3 and 6 specifications as read in are printed, along with the surface data generated by the specifications.

A standard "minimum" output is given when the code letter "D" does not appear in the run instructions, consisting of the following:

1. Run number
2. Run instructions
3. The computed form factor
4. The Surface 1 mapping area
5. The exchange coefficient (fA product)
6. The total area of Surface 1
7. If Surface 1 is bisected, the area seen by Surface 2
8. The total area of Surface 2, if Surface 2 area can be computed
9. If Surface 2 is bisected, the area seen by Surface 1, if that area can be computed
10. The time in seconds spent in Subroutine SHIFAC, if utilized

If a detailed output is requested, the minimum output plus the following is printed:

1. The final coordinates of Surface 1 and Surface 2 prior to computation of configuration factors.
2. The X-Left and X-Right coordinates for each Y division of Surface 1 mapping, including horizontal and vertical divisions used.
3. Each configuration factor computed. The output is given in groups of factors easily identified because the last factor in a group occupies a line by itself. Each group contains the configuration factors computed on a mapping line. The first factor in the group is that computed at Y-left and the last factor in the group is that

computed at X-right. The first group represents the first mapping line, the second group the second mapping line, etc.

4. If the silhouette generator was used, the silhouette computed for points selected on each mapping line is printed out. The first numeral given is the mapping line, the second is the point on the mapping line, moving from X-left to X-right. The numbers following represent the silhouette.

SECTION VI

REFERENCES

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APPENDIX A

SAMPLE PROBLEMS

A number of sample problems have been devised to illustrate the capabilities and limitations of CONFAC II. The examples are arranged roughly in order of complexity, beginning with simple plane surfaces and concluding with a complicated "intervening surface" problem involving plane and solid surfaces.

The surface configurations upon which the example problems are based are shown in accompanying illustrations. Each illustration is conveniently grouped separately with the problem description pertaining to the surfaces shown in the illustration, along with the input data sheets, run instructions, program output and a short discussion.

SAMPLE PROBLEM GROUP A

The surfaces shown in Figure 18 are similar to the examples given in CONFAC I. The added CONFAC II capability of bisecting a nonplanar surface is demonstrated. The data sheets are shown in Figure 19 and the results are presented in Figure 20.

Problem 1A

In Figure 18 (A1), the factor between the floor of a circular room (1FLOOR) and an adjacent wall (1WALL) is computed, using standard horizontal and vertical running divisions (24 x 24) on Surface 1. A detailed output is requested.

Note that because no primary or auxiliary transformation occurred, the floor coordinate system is the same as the input data (unrimed) coordinate system. The first running line starts at the origin and extends to point 1 in 1FLOOR.

Problem 2A

In Figure 18 (A1), any plane surface may be used as Surface 1 providing it has been properly entered in data prior to the factor request. To demonstrate, the wall (1WALL) now acts as Surface 1, and the factor to the floor (1FLOOR) is requested.

Note that Surface 1WALL is not in the X-Y plane of its input (unrimed) coordinate system. The program, therefore, had to perform an auxiliary transformation of both surfaces to the rimed system shown, prior to factor computation, to get Surface 1 in the XY plane.

Problem 3A

In Figure 18 (A2), the factor from the floor (1FLOOR) to two adjacent walls taken together (2WALLS) is requested. This is a valid request because the boundary data describing 2WALLS form a valid silhouette of 2WALLS from any point on 1FLOOR. The factor should be twice that to one wall alone.

Problem 4A

The program cannot validly compute the factor from a nonplanar surface. A Class 2 surface is assumed nonplanar. The factor from 2WALLS to 1FLOOR is requested in order to elicit the diagnostic, warning the user of this error.

The program does not test the surface, as in CONFAC I. If a nonplanar surface is erroneously entered as a Class 1 surface, it will not be rejected if used as Surface 1 - the responsibility lay with the user to insure that Surface 1 is planar.

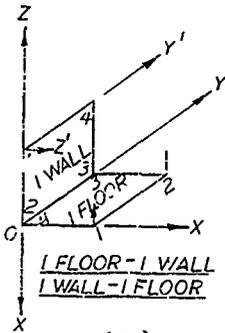
Problem 5A

In Figure 18 (A3), the necessity for proper order in data entry is emphasized. The wall data are deliberately entered in a clockwise direction (IWALLR) looking at the active surface, instead of counterclockwise. Hence, the orientation vector points in the wrong direction. The factor from IFLOOR to IWALLR is requested in order to elicit the diagnostic which alerts the user to a possible error.

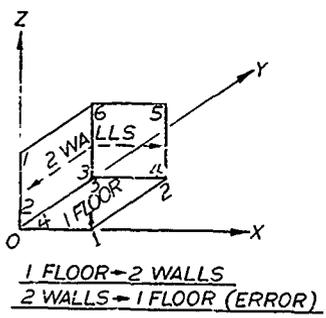
Problem 6A

In Figure 15 (A4), CONFAC II has the capability of bisecting a nonplanar (Class 2) surface. The factor from IFLOOR to 2WALLZ, is requested, with a detailed output, to demonstrate this capability.

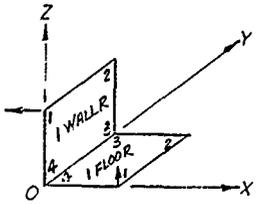
Subroutine IQUIC bisected 2WALLZ at the XY plane, and reconstructed the surface by eliminating points 2, 3, and 4, as shown, and creating new points 2', 3', 4' and 5'. The dashed line 2' 3' divides Surface 1 (IFLOOR) into triangular parts, designated A and B. The view of the reconstructed 2WALLZ from area B reflects a valid silhouette in the proper counterclockwise order. When reconstructed 2WALLZ is viewed from area A, the points still form a valid silhouette, but the order is reversed. This means the computed configuration factor will be to the hemispherical space not occupied by 2WALLZ, and will be negative. So, subroutine FACTOR subtracts this factor from 1.0 to yield the correct factor to 2WALLZ.



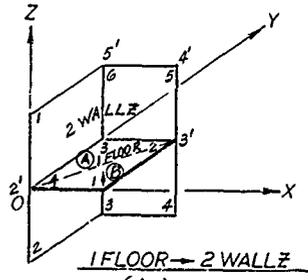
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FIGURE 18. SAMPLE PROBLEMS - GROUP A

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FIGURE 19. Group A Sample Problems Input Data Code Sheets (continued)

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| 26 | | | | | |
| 27 | | | | | |
| 28 | | | | | |
| 29 | | | | | |
| 30 | | | | | |

FORTRAN FIXED IO DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE | OF | JOB NO. |
|----------|----------------|-------------|------------------|----|---------|
| | | | | | |
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | | |
| 1 | | | | | |
| 2 | | | | | |
| 3 | | | | | |
| 4 | | | | | |
| 5 | | | | | |
| 6 | | | | | |
| 7 | | | | | |
| 8 | | | | | |
| 9 | | | | | |
| 10 | | | | | |
| 11 | | | | | |
| 12 | | | | | |
| 13 | | | | | |
| 14 | | | | | |
| 15 | | | | | |
| 16 | | | | | |
| 17 | | | | | |
| 18 | | | | | |
| 19 | | | | | |
| 20 | | | | | |
| 21 | | | | | |
| 22 | | | | | |
| 23 | | | | | |
| 24 | | | | | |
| 25 | | | | | |
| 26 | | | | | |
| 27 | | | | | |
| 28 | | | | | |
| 29 | | | | | |
| 30 | | | | | |

FIGURE 19. Group A Sample Problems Input Data Code Sheets (continued)

NASA SPACE AND INFORMATION SYSTEMS DIVISION
 T-4 PROJECT ADJUNCT-INTERCHANGE CONFIGURATION FACTOR PROGRAM
 C O N F I D

NAA CONTACT II REPORT SAMPLE PROBLEMS FROM FIG. 1A3-A.A.T09P5.11/1/63

I N P U T D A T A

```

***** DATA NAME= *IFLOOR * 1X1 SQUARE
POINT X Y Z POINT X Y Z
1 0.1000000E 01 0. 0.1000000E 01----(INTERNALLY GENERATED ORIENTATION VECTOR) Z
3 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.

***** DATA NAME= *SMALL * 1X1 SQUARE TOUCHING IN WALL
POINT X Y Z POINT X Y Z
1 0.1000000E 01 0. 0.1000000E 01----(INTERNALLY GENERATED ORIENTATION VECTOR) Z
3 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.1000000E 01

***** DATA NAME= *SMALLR * SAME AS SMALL, BUT WITH DATA ENTERED CLOCKWISE
POINT X Y Z POINT X Y Z
1 -0.1000000E 01 0. 0.1000000E 01----(INTERNALLY GENERATED ORIENTATION VECTOR) Z
3 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.1000000E 01

***** DATA NAME= *SMALLS * SIDE AND BACK WALL TAKEN TOGETHER
POINT X Y Z POINT X Y Z
1 0. 0. 0.1000000E 01 0. 0. 0.1000000E 01 0.1000000E 01 0.
3 0.1000000E 01 0.1000000E 01 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.1000000E 01
  
```

FIGURE 20. Group A Sample Problems Program Results
 (24 pages)

VIA COMFAC II REPORT SAMPLE PROBLEMS FROM FIG. (A)-K-KAT UPS, 11/1/63

```

RUN NO. 1 DATA USED FOR THIS RUN= *IFLOOR*SMALL *
      *D *
      * *
      * *
THE FORM FACTOR FROM SURFAC *IFLOOR * TO SURFACE *SMALL * = 0.19996
THE EXCHANGE COEFFICIENT (FA) = 0.19996E+00 SO UNITS
      THE MAPPING AREA = 1.000000E 00 SO UNITS
THE J % OF SURFACE *IFLOOR * = 0.100000E 01 SO UNITS.
THE AREA OF SURFACE *SMALL * = 0.100000E 01 SO UNITS.
THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION=

```

```

***** DATA NAME= *IFLOOR *
POINT X Y Z ORIENT X Y Z
1 0.100000E 01 0. 0. 0.100000E 01----(INTERNALLY GENERATED ORIENTATION VECTORS) Z
3 0. 0. 0.100000E 01 0. 0. 0.100000E 01 0. 0.

```

5

```

***** DATA NAME= *SMALL *
POINT X Y Z ORIENT X Y Z
1 0.100000E 01 0. 0. 0.100000E 01----(INTERNALLY GENERATED ORIENTATION VECTORS) Z
3 0. 0. 0.100000E 01 0. 0. 0.100000E 01 0. 0.
COORDINATES OF POINTS ON BOUNDARY OF SURF *IFLOOR * FOR EACH Y INTERVAL
X-LEFT X-RIGHT Y X-LEFT X-RIGHT Y
0. 0. 0.100000E 01 0. 0.833333E-01 0. 0.100000E 01 0.416666E-01
0. 0. 0.100000E 01 0. 0.100000E 01 0.125000E-00

```

FIGURE 20. Group A. Sample Problems Program Results (continued)

0. 0.100000E 01 0.1666667E-00 C. 0.100000E 01 0.588333E 00
 0. 2.100000E 01 0.200000E-00 0. 1.000000E 01 0.396666E-00
 0. 2.100000E 01 0.333333E-00 0. 0.700000E 01 0.370000E-00
 0. 2.100000E 01 0.500000E-00 0. 1.000000E 01 0.458333E 00
 0. 2.100000E 01 0.500000E-00 0. 1.000000E 01 0.624000E 00
 0. 2.100000E 01 0.583333E 00 0. 1.000000E 01 0.624000E 00
 0. 2.100000E 01 0.750000E-00 0. 1.000000E 01 0.708333E 00
 0. 2.100000E 01 0.833333E 00 0. 1.000000E 01 0.875000E 00
 0. 2.100000E 01 0.100000E-00 0. 1.000000E 01 0.875000E 00
 0. 2.100000E 01 0.100000E-00 0. 1.000000E 01 0.958333E 00

NO. OF HORIZONTAL INCREMENTS: 24 NO. OF VERTICAL INCREMENTS: 24

THE EQUILIBRIUM ARE PLANE ORBIT COMPUTATION FACTORS COMPUTED FOR THIS RUN
 LOWEST GRID LINE FIRST, FROM *LEFT TO *RIGHT.

0.250000E-00 0.238174E-00 0.2264098E-00 0.2147804E-00 0.2033451E-00 0.1921649E-00
 0.1812784E-00 0.170741E-00 0.1605884E-00 0.1508493E-00 0.1415274E-00 0.132575E-00
 0.123948E-00 0.115681E-00 0.1077392E-01 0.1000813E-00 0.9316960E-01 0.8854905E-01
 0.8535426E-01 0.8277592E-01 0.7288377E-01 0.6799038E-01 0.6537979E-01 0.5952419E-01
 0.500000E 00 0.3627648E-00 0.2993818E-00 0.2647417E-00 0.2406935E-00 0.2215649E-00
 0.2075042E-00 0.192678E-00 0.175989E-00 0.1652006E-00 0.1530019E-00 0.1433944E-00
 0.1326074E-00 0.1243870E-00 0.115989E-00 0.1072773E-01 0.9831921E-01 0.89898E-01
 0.820000E 00 0.6131545E-00 0.3466923E-00 0.3096164E-00 0.293848E-00 0.278948E-00
 0.276642E-00 0.2091476E-00 0.1934485E-00 0.1790108E-00 0.1658294E-00 0.1529071E-00
 0.1424899E-00 0.1323837E-00 0.1229162E-00 0.1141671E-00 0.1060798E-00 0.9860413E-01
 0.898712E-01 0.8293921E-01 0.7969921E-01 0.759282E-01 0.699225E-01 0.6427036E-01
 0.500000E 00 0.439534E-00 0.3801883E-00 0.3358659E-00 0.3006194E-00 0.2713642E-00
 0.247673E-00 0.226642E-00 0.208481E-00 0.192681E-00 0.177030E-00 0.163191E-00
 0.1511731E-00 0.139645E-00 0.1282340E-01 0.117324E-01 0.1071948E-01 0.1044978E-01
 0.956537E-01 0.8882340E-01 0.822138E-01 0.772238E-01 0.717948E-01 0.664978E-01
 0.500000E 00 0.4473457E-00 0.3900101E-00 0.3576912E-00 0.3261318E-00 0.295294E-00
 0.247673E-00 0.2415963E-00 0.2216715E-00 0.2035944E-00 0.1872681E-00 0.172924E-00
 0.160603E-00 0.146803E-00 0.1335593E-00 0.1225344E-00 0.1159130E-00 0.107281E-00
 0.100000E 00 0.8209959E-01 0.8542179E-01 0.7929282E-01 0.7366185E-01 0.6848651E-01

FIGURE 20. Group A Sample Problems Program Results
 (continued)

| | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|
| 0.632799E-C1 | 0.454429E-00 | 0.411214E-00 | 0.371896E-00 | 0.336937E-00 | 0.306112E-00 |
| 0.500000E-00 | 0.454429E-00 | 0.411214E-00 | 0.371896E-00 | 0.336937E-00 | 0.306112E-00 |
| 0.166211E-00 | 0.153104E-00 | 0.141148E-00 | 0.130252E-00 | 0.120218E-00 | 0.111026E-00 |
| 0.102740E-00 | 0.950812E-01 | 0.880670E-01 | 0.816376E-01 | 0.757436E-01 | 0.703358E-01 |
| 0.652734E-00 | 0.455000E-00 | 0.413609E-00 | 0.382646E-00 | 0.348622E-00 | 0.317664E-00 |
| 0.172444E-00 | 0.265446E-00 | 0.243009E-00 | 0.222723E-00 | 0.204357E-00 | 0.187664E-00 |
| 0.103032E-00 | 0.156672E-00 | 0.146077E-00 | 0.135488E-00 | 0.124901E-00 | 0.114508E-00 |
| 0.668380E-01 | 0.977475E-01 | 0.904696E-01 | 0.837293E-01 | 0.775264E-01 | 0.719493E-01 |
| 0.500000E-00 | 0.462105E-00 | 0.425206E-00 | 0.390107E-00 | 0.357305E-00 | 0.327048E-00 |
| 0.177777E-00 | 0.279465E-00 | 0.251077E-00 | 0.226091E-00 | 0.203765E-00 | 0.183760E-00 |
| 0.103813E-00 | 0.100057E-00 | 0.927479E-01 | 0.852620E-01 | 0.782057E-01 | 0.713411E-01 |
| 0.681080E-01 | 0.641358E-01 | 0.593492E-01 | 0.546536E-01 | 0.501490E-01 | 0.458376E-01 |
| 0.306725E-00 | 0.280793E-00 | 0.257410E-00 | 0.236009E-00 | 0.216447E-00 | 0.198276E-00 |
| 0.182275E-00 | 0.187401E-00 | 0.174888E-00 | 0.161677E-00 | 0.149424E-00 | 0.139146E-00 |
| 0.110233E-00 | 0.101998E-00 | 0.941801E-01 | 0.870594E-01 | 0.805486E-01 | 0.746029E-01 |
| 0.500000E-00 | 0.465720E-00 | 0.420121E-00 | 0.399384E-00 | 0.368236E-00 | 0.338839E-00 |
| 0.111345E-00 | 0.285833E-00 | 0.262233E-00 | 0.240230E-00 | 0.220165E-00 | 0.202829E-00 |
| 0.118817E-00 | 0.118817E-00 | 0.118817E-00 | 0.118817E-00 | 0.118817E-00 | 0.118817E-00 |
| 0.112237E-01 | 0.105063E-00 | 0.975288E-01 | 0.923074E-01 | 0.873397E-01 | 0.825642E-01 |
| 0.500000E-00 | 0.466742E-00 | 0.423083E-00 | 0.401313E-00 | 0.371292E-00 | 0.342593E-00 |
| 0.113495E-00 | 0.106660E-00 | 0.995013E-01 | 0.935078E-01 | 0.873745E-01 | 0.822263E-01 |
| 0.200000E-00 | 0.467220E-00 | 0.431673E-00 | 0.403160E-00 | 0.375035E-00 | 0.346144E-00 |
| 0.116880E-00 | 0.291346E-00 | 0.267592E-00 | 0.245603E-00 | 0.225334E-00 | 0.206711E-00 |
| 0.189644E-00 | 0.174093E-00 | 0.159752E-00 | 0.146766E-00 | 0.134048E-00 | 0.124094E-00 |
| 0.103713E-01 | 0.102210E-00 | 0.951691E-01 | 0.896069E-01 | 0.843316E-01 | 0.793963E-01 |
| 0.500000E-00 | 0.467395E-00 | 0.432811E-00 | 0.403333E-00 | 0.373666E-00 | 0.344781E-00 |
| 0.119015E-00 | 0.184478E-00 | 0.160134E-00 | 0.147128E-00 | 0.135124E-00 | 0.124371E-00 |
| 0.114445E-00 | 0.105467E-00 | 0.972889E-01 | 0.898113E-01 | 0.829282E-01 | 0.767215E-01 |
| 0.170944E-01 | 0.663734E-00 | 0.631875E-00 | 0.603366E-00 | 0.576310E-00 | 0.546144E-00 |
| 0.316880E-00 | 0.291346E-00 | 0.267592E-00 | 0.245603E-00 | 0.225334E-00 | 0.206711E-00 |
| 0.189644E-00 | 0.174093E-00 | 0.159752E-00 | 0.146766E-00 | 0.134048E-00 | 0.124094E-00 |

FIGURE 20. Group A Sample Problems Program Results
(continued)

| | | | | | |
|----------------|---------------|---------------|---------------|---------------|---------------|
| 0.1142451E+00 | 0.1032704E+00 | 0.9709184E-01 | 0.8963659E-01 | 0.8203786E-01 | 0.7462346E-01 |
| 0.7091130E-01 | 0.6464928E-00 | 0.5130384E-00 | 0.4519190E-00 | 0.3913195E-00 | 0.3421053E-00 |
| 0.3104912E-01 | 0.2893245E-00 | 0.2154029E-00 | 0.2437138E-00 | 0.2213240E-00 | 0.2757093E-00 |
| 0.1881765E-01 | 0.1770316E-00 | 0.1185815E-00 | 0.1456994E-00 | 0.1339545E-00 | 0.1132505E-00 |
| 0.1134928E-00 | 0.1396053E-00 | 0.9650288E-01 | 0.8911444E-01 | 0.8237674E-01 | 0.7629293E-01 |
| 0.5000000E+00 | 0.4657209E-00 | 0.4120121E-00 | 0.3993846E-00 | 0.3622163E-00 | 0.3188398E-00 |
| 0.3113485E-00 | 0.2859181E-00 | 0.2872335E-00 | 0.2405338E-00 | 0.2204169E-00 | 0.2023829E-00 |
| 0.1881765E-01 | 0.1881765E-00 | 0.1881765E-00 | 0.1881765E-00 | 0.1881765E-00 | 0.1881765E-00 |
| 0.1700037E-01 | 0.1039024E-00 | 0.9323895E-01 | 0.8482507E-01 | 0.8080846E-01 | 0.7579582E-01 |
| 0.5000000E+00 | 0.4842592E-00 | 0.4522925E-00 | 0.3955278E-00 | 0.3624870E-00 | 0.3188312E-00 |
| 0.1105385E-00 | 0.1674014E-00 | 0.1178395E-00 | 0.1414715E-00 | 0.1301824E-00 | 0.1199116E-00 |
| 0.1882217E-00 | 0.1882217E-00 | 0.1882217E-00 | 0.1882217E-00 | 0.1882217E-00 | 0.1882217E-00 |
| 0.4881080E-01 | 0.4881080E-00 | 0.4881080E-00 | 0.4881080E-00 | 0.4881080E-00 | 0.4881080E-00 |
| 0.5000000E+00 | 0.4621056E-00 | 0.4252041E-00 | 0.3901042E-00 | 0.3573098E-00 | 0.3270483E-00 |
| 0.2993336E-00 | 0.2740946E-00 | 0.2510378E-00 | 0.2300014E-00 | 0.2110278E-00 | 0.1934706E-00 |
| 0.1778007E-00 | 0.1834541E-00 | 0.1500219E-00 | 0.1393644E-00 | 0.1274298E-00 | 0.1174576E-00 |
| 0.4881080E-01 | 0.4881080E-00 | 0.4881080E-00 | 0.4881080E-00 | 0.4881080E-00 | 0.4881080E-00 |
| 0.5000000E+00 | 0.4590002E-00 | 0.4196697E-00 | 0.3824040E-00 | 0.3486228E-00 | 0.3179568E-00 |
| 0.1037241E-00 | 0.1587859E-00 | 0.1160074E-00 | 0.1155845E-00 | 0.1247419E-00 | 0.1184608E-00 |
| 0.1037241E-00 | 0.9774238E-00 | 0.9028496E-01 | 0.8327293E-01 | 0.7759847E-01 | 0.7198933E-01 |
| 0.5000000E+00 | 0.4564209E-00 | 0.4112148E-00 | 0.3718894E-00 | 0.3360377E-00 | 0.3112395E-00 |
| 0.7890978E-00 | 0.2547786E-00 | 0.2332160E-00 | 0.2118889E-00 | 0.1964444E-00 | 0.1803977E-00 |
| 0.4662118E-00 | 0.1531666E-00 | 0.1411489E-00 | 0.1302521E-00 | 0.1202390E-00 | 0.1111026E-00 |
| 0.8537347E-01 | 0.9390822E-01 | 0.9087095E-01 | 0.8163781E-01 | 0.7574307E-01 | 0.7033538E-01 |
| 0.5000000E+00 | 0.4473857E-00 | 0.3990101E-00 | 0.3570122E-00 | 0.3211835E-00 | 0.2909358E-00 |
| 0.2647635E-00 | 0.2449023E-00 | 0.2261671E-00 | 0.2059942E-00 | 0.1978461E-00 | 0.1821512E-00 |
| 0.5000000E+00 | 0.4290950E-00 | 0.3852179E-01 | 0.3492883E-01 | 0.3166186E-01 | 0.2864652E-01 |
| 0.6372798E-01 | 0.5836354E-00 | 0.5001897E-00 | 0.3584969E-00 | 0.3026195E-00 | 0.2718993E-00 |
| 0.2410220E-00 | 0.2229754E-00 | 0.2030491E-00 | 0.1898457E-00 | 0.1711711E-00 | 0.1503969E-00 |
| 0.15811251E-00 | 0.1398666E-00 | 0.1294859E-00 | 0.1199457E-00 | 0.7137946E-01 | 0.6645701E-01 |
| 0.5564218E-01 | 0.8882341E-01 | 0.8523385E-01 | 0.7872672E-01 | 0.7137946E-01 | 0.6645701E-01 |
| 0.5000000E+00 | 0.4135154E-00 | 0.3499924E-00 | 0.3058146E-00 | 0.2737865E-00 | 0.2486691E-00 |
| 0.2276612E-00 | 0.2005578E-00 | 0.1934858E-00 | 0.1779010E-00 | 0.1659296E-00 | 0.1537498E-00 |

FIGURE 20. Group A, Sample Problems Program Results
(continued)

0.1426349E-00 0.1333835E-00 0.1233164E-00 0.1146371E-00 0.1040789E-00 0.08460314E-01
 0.8169544E-01 0.8531021E-01 0.7940921E-01 0.7395689E-01 0.6892224E-01 0.6427036E-01
 0.5005002E-00 0.3674902E-00 0.2993192E-00 0.2647484E-00 0.2463065E-00 0.2213054E-00
 0.2031992E-00 0.1906359E-00 0.1773294E-00 0.1652008E-00 0.1537009E-00 0.1419594E-00
 0.8725442E-01 0.8187070E-01 0.7611639E-01 0.7102748E-01 0.6631526E-01 0.6195099E-01
 0.376921E-01 0.430171E-00 0.226098E-00 0.2147602E-00 0.2033631E-00 0.1921608E-00
 0.1812704E-00 0.1700000E-00 0.1576081E-00 0.1450681E-00 0.132374E-00 0.130637E-00
 0.1242689E-00 0.1163181E-00 0.108331E-00 0.100341E-00 0.919374E-01 0.836937E-01
 0.8335081E-01 0.7773592E-01 0.7263371E-01 0.6798038E-01 0.6355974E-01 0.5928492E-01

FIGURE 20. Group A Sample Problems Program Results
 (continued)

NAA COIFAC II REPORT SAMPLE PROBLEMS FROM FIG. 1A3-K-A.TOWNS.11/1/63

```

RUN NO. 2 DATA USED FOR THIS RUN= *SMALL *FLOOR*
      *D *
THE FORM FACTOR FROM SURFACE *SMALL * TO SURFACE *FLOOR * = 0.19996
THE EXCHANGE COEFFICIENT (FA)= 0.19996E+00 SQ UNITS
THE MAPPING AREA = 1.000000E 00 SQ UNITS
THE AREA OF SURFACE *SMALL * = 0.100000E 01 SQ UNITS.
THE AREA OF SURFACE *FLOOR * = 0.100000E 01 SQ UNITS.
THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

***** DATA NAME= *SMALL *
POINT  X      Y      Z      PRINT  X      Y      Z
1  -0.      -0.      0.100000E 01---(INTERMEDIATELY GENERATED ORIENTATION VECTOR)
3  0.100000E 01 0.100000E 01 0.      -0.      0.100000E 01 0.

***** DATA NAME= *FLOOR *
POINT  X      Y      Z      PRINT  X      Y      Z
1  0.100000E 01 0.100000E 01---(INTERMEDIATELY GENERATED ORIENTATION VECTOR)
3  0.100000E 01 0.100000E 01 0.      0.100000E 01 -0.100000E 01 0.100000E 01
COORDINATES OF POINTS ON BOUNDARY OF SURF *SMALL * FOR EACH Y INTERVAL
X=LEFT  X=RIGHT  X=LEFT  X=RIGHT  Y
-0.      0.100000E 01 -0.      0.100000E 01 0.150000E-01
-0.      0.100000E 01 0.833333E-01 -0.      0.100000E 01 0.150000E-01

```

FIGURE 20. Group A Sample Problems Program Results (continued)

| | | | | | |
|-----|--------------|--------------|-----|--------------|--------------|
| -0+ | 0.130000E 01 | 0.166667E-00 | -0+ | 0.106730E 01 | 0.208333E-00 |
| -0+ | 0.130000E 01 | 0.250000E-00 | -0+ | 0.100000E 01 | 0.075000E-00 |
| -0+ | 0.130000E 01 | 0.333333E-00 | -0+ | 0.100000E 01 | 0.116667E-00 |
| -0+ | 0.130000E 01 | 0.416667E-00 | -0+ | 0.100000E 01 | 0.158333E-00 |
| -0+ | 0.130000E 01 | 0.500000E-00 | -0+ | 0.100000E 01 | 0.200000E-00 |
| -0+ | 0.130000E 01 | 0.583333E-00 | -0+ | 0.100000E 01 | 0.241667E-00 |
| -0+ | 0.130000E 01 | 0.666667E-00 | -0+ | 0.100000E 01 | 0.283333E-00 |
| -0+ | 0.130000E 01 | 0.750000E-00 | -0+ | 0.100000E 01 | 0.325000E-00 |
| -0+ | 0.130000E 01 | 0.833333E-00 | -0+ | 0.100000E 01 | 0.366667E-00 |
| -0+ | 0.130000E 01 | 0.916667E-00 | -0+ | 0.100000E 01 | 0.408333E-00 |
| -0+ | 0.130000E 01 | 1.000000E-00 | -0+ | 0.100000E 01 | 0.450000E-00 |

NO. OF HORIZONTAL INCREMENTS= 24 NO. OF VERTICAL INCREMENTS= 24

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN
LOWEST GRID LINE FIRST, FROM X=LEFT TO X=RIGHT.

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|
| 0.5573420E-01 | 0.5922419E-01 | 0.6359978E-01 | 0.6798038E-01 | 0.7268577E-01 | 0.7773592E-01 |
| 0.8212665E-01 | 0.8954935E-01 | 0.9515905E-01 | 0.1017698E-00 | 0.1088212E-00 | 0.1163181E-00 |
| 0.1182178E-00 | 0.1924538E-00 | 0.2033545E-00 | 0.2147402E-00 | 0.2260095E-00 | 0.2381714E-00 |
| 0.250000E-00 | 0.3104098E-01 | 0.4633195E-01 | 0.7103713E-01 | 0.7111664E-01 | 0.8456781E-01 |
| 0.8720442E-01 | 0.3318608E-01 | 0.1407129E-00 | 0.1000764E-00 | 0.1159894E-00 | 0.1444870E-00 |
| 0.1330674E-00 | 0.1443284E-00 | 0.1490194E-00 | 0.1622008E-00 | 0.1779282E-00 | 0.1945369E-00 |
| 0.200000E-00 | 0.2215049E-00 | 0.2460958E-00 | 0.2887418E-00 | 0.2993619E-00 | 0.3621491E-00 |
| 0.5997212E-01 | 0.6882255E-01 | 0.6882255E-01 | 0.7395828E-01 | 0.74205E-01 | 0.8330218E-01 |
| 0.7129132E-01 | 0.785076E-01 | 0.1009798E-00 | 0.1140712E-00 | 0.1244857E-00 | 0.1329391E-00 |
| 0.8227642E-00 | 0.8446091E-00 | 0.2777868E-00 | 0.3028146E-00 | 0.3469824E-00 | 0.4133158E-00 |
| 0.900000E-00 | 0.8465870E-00 | 0.7117944E-00 | 0.7612364E-00 | 0.8232188E-00 | 0.8883140E-00 |
| 0.8541175E-00 | 0.1070969E-00 | 0.1111171E-00 | 0.1149457E-00 | 0.1274895E-00 | 0.1398684E-00 |
| 0.9565317E-01 | 0.1070969E-00 | 0.1070969E-00 | 0.1188990E-00 | 0.2083312E-00 | 0.2261750E-00 |
| 0.500000E-00 | 0.2718661E-00 | 0.3006199E-00 | 0.3353059E-00 | 0.3802881E-00 | 0.4495357E-00 |
| 0.6322792E-01 | 0.6148651E-01 | 0.7366849E-01 | 0.7929282E-01 | 0.8542178E-01 | 0.9205042E-01 |
| 0.172814E-00 | 0.172814E-00 | 0.182344E-00 | 0.182344E-00 | 0.1935215E-00 | 0.1668093E-00 |
| 0.354035E-00 | 0.354035E-00 | 0.354035E-00 | 0.354035E-00 | 0.354035E-00 | 0.354035E-00 |
| 0.2647653E-00 | 0.2647653E-00 | 0.2647653E-00 | 0.2647653E-00 | 0.2647653E-00 | 0.2647653E-00 |

FIGURE 20. Group A. Sample Problems Program Results
(continued)

| | | | | | |
|---------------|----------------|---------------|----------------|---------------|---------------|
| 0-31388002-C0 | 0-346-4A9E-00 | 0-3372035C-00 | 0-4033608E-00 | 0-4364795E-00 | 0-4672204E-00 |
| 0-30000002-C0 | 0-1253285E-00 | 0-8237674E-01 | 0-6911441E-01 | 0-9565285E-01 | 0-1040600E-00 |
| 0-1119094E-00 | 0-2325094E-00 | 0-2231728E-00 | 0-2237138E-00 | 0-2550025E-00 | 0-2402024E-00 |
| 0-1884764E-00 | 0-3421913E-00 | 0-3712833E-00 | 0-4019193E-00 | 0-4336335E-00 | 0-4666782E-00 |
| 0-3138422E-00 | 0-7556381E-01 | 0-8166876E-01 | 0-8662974E-01 | 0-9452834E-01 | 0-1030502E-00 |
| 0-7002237E-01 | 0-1235274E-00 | 0-1323804E-00 | 0-1439300E-00 | 0-1565948E-00 | 0-1704894E-00 |
| 0-1225374E-00 | 0-2205470E-00 | 0-2205470E-00 | 0-2405309E-00 | 0-2622733E-00 | 0-2858183E-00 |
| 0-111474E-00 | 0-2324898E-00 | 0-2324898E-00 | 0-2597596E-00 | 0-2810182E-01 | 0-3057280E-00 |
| 0-3000000E-C0 | 0-7402784E-01 | 0-8094605E-01 | 0-8705943E-01 | 0-9241803E-01 | 0-1019848E-00 |
| 0-105390E-C0 | 0-1982776E-00 | 0-2164437E-00 | 0-2360083E-00 | 0-2574191E-00 | 0-2807805E-00 |
| 0-3002503E-C0 | 0-3338684E-00 | 0-3536870E-00 | 0-37055880E-00 | 0-3922233E-00 | 0-4142074E-00 |
| 0-6812603E-C1 | 0-73461175E-01 | 0-7720078E-01 | 0-7554546E-01 | 0-647276E-00 | 5-1000572E-00 |
| 0-158364E-00 | 0-1165376E-00 | 0-1274233E-00 | 0-1383464E-00 | 0-150323E-00 | 5-1634541E-00 |
| 0-2793740E-00 | 0-276049E-00 | 0-114504E-00 | 0-230004E-00 | 0-2210316E-00 | 5-2740546E-00 |
| 0-3000000E-C0 | 0-276049E-00 | 0-157068E-00 | 0-2310104E-00 | 0-4226031E-00 | 5-4810271E-00 |
| 0-053791E-C1 | 0-719333E-01 | 0-775985E-01 | 0-8372935E-01 | 0-9042645E-01 | 0-977473E-01 |
| 0-124943E-00 | 0-1876684E-00 | 0-206354E-00 | 0-2227289E-00 | 0-2430048E-00 | 0-2656470E-00 |
| 0-3002672E-C0 | 0-3179507E-00 | 0-3466224E-00 | 0-3674949E-00 | 0-4194648E-00 | 0-4590002E-00 |
| 0-653734E-C0 | 0-7032587E-01 | 0-757430E-01 | 0-8163780E-01 | 0-8806705E-01 | 0-9564271E-01 |
| 0-1027400E-00 | 0-1111065E-00 | 0-126239E-00 | 0-1302257E-00 | 0-141440E-00 | 0-1531066E-00 |
| 0-278088E-00 | 0-300797E-00 | 0-176244E-00 | 0-2138883E-00 | 0-233234E-00 | 0-2547786E-00 |
| 0-3000000E-C0 | 0-300117E-00 | 0-374799E-00 | 0-2718974E-00 | 0-412119E-00 | 0-4394210E-00 |
| 0-092799E-01 | 0-688609E-01 | 0-736828E-01 | 0-772928E-01 | 0-83421E-01 | 0-9205054E-01 |
| 0-1570750E-C0 | 0-172557E-00 | 0-187280E-00 | 0-203584E-00 | 0-225271E-00 | 0-249003E-00 |
| 0-1646264E-C0 | 0-190338E-00 | 0-213189E-00 | 0-237012E-00 | 0-269701E-00 | 0-304763E-00 |
| 0-492074E-C0 | 0-666270E-01 | 0-713794E-01 | 0-767226E-01 | 0-825238E-01 | 0-8862340E-01 |
| 0-586518E-C1 | 0-1030969E-00 | 0-111171E-00 | 0-119945E-00 | 0-129465E-00 | 0-139664E-00 |
| 0-47172E-C0 | 0-171641E-00 | 0-177034E-00 | 0-1948990E-00 | 0-208561E-00 | 0-2267756E-00 |
| 0-5300000E-C0 | 0-274694E-00 | 0-300019E-00 | 0-3359879E-00 | 0-3801884E-00 | 0-435635E-C0 |
| 0-5894218E-C1 | 0-6447016E-01 | 0-692252E-01 | 0-739582E-01 | 0-794974E-01 | 0-8538941E-01 |
| 0-4369268E-C1 | 0-868041E-01 | 0-106094E-00 | 0-114167E-00 | 0-122816E-00 | 0-133835E-00 |

FIGURE 20. Group A Sample Problems Program Results
(continued)

| | | | | | |
|---------------|----------------|---------------|---------------|----------------|---------------|
| 0.14263492-CU | 0.45316995-00 | 0.1658292E-00 | 0.1790103-00 | 0.3368518E-00 | 0.2306476E-00 |
| 0.14263492-CU | 0.24865091E-00 | 0.2737869E-00 | 0.1058147E-00 | 0.14926924E-00 | 0.4133178E-00 |
| 0.14263492-CU | 0.6195098E-01 | 0.683191E-01 | 0.710372E-01 | 0.761163E-01 | 0.812921E-01 |
| 0.14263492-CU | 0.9736602E-01 | 0.1007149E-00 | 0.1188074E-00 | 0.115874E-00 | 0.1160349E-00 |
| 0.14263492-CU | 0.2231992E-00 | 0.1539020E-00 | 0.165208E-00 | 0.177394E-00 | 0.1460349E-00 |
| 0.14263492-CU | 0.2231992E-00 | 0.4760979E-00 | 0.2887418E-00 | 0.2993620E-00 | 0.327491E-00 |
| 0.14263492-CU | 0.897469E-01 | 0.651098E-01 | 0.679803E-01 | 0.726572E-01 | 0.777359E-01 |
| 0.14263492-CU | 0.128266E-00 | 0.141377E-00 | 0.15068E-00 | 0.15623E-00 | 0.162197E-00 |
| 0.14263492-CU | 0.1172608E-00 | 0.2033451-00 | 0.2147895E-00 | 0.226409E-00 | 0.238174E-00 |
| 0.14263492-CU | 0.1172608E-00 | 0.2033451-00 | 0.2147895E-00 | 0.226409E-00 | 0.238174E-00 |

FIGURE 20. Group A Sample Problems Program Results
(continued)

DATA CO/FAC II REPORT SAMPLE PROBLEMS FROM FIG. (A1)-K-A-TOPS:11 1/63

UN NO. 3 DATA USED FOR THIS RUN= *IFLOOR+Z*ALL*
 *U * * *

THE FURN FACTOR FROM SURFACE =FLOOR * TO SURFACE *Z*ALLS *
 TP EXCHANGE COEFFICIENT (F3)= 0.39492E+60 SO UNITS * = 0.3909Z

THE WAPLING AREA * --0000000E 00 SO UNITS
 EA OF S * = 0.1000000E 01 SO UNITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION=

```

***** DATA NAME= *IFLOOR *
POINT X Y Z POINT X Y Z
1 0.100000E 01 0. 0. 0.100000E 01 0. 0. 0.100000E 01 0. 0. 0.100000E 01 0. 0.
2 0.100000E 01 0.100000E 01 0. 0. 0.100000E 01 0. 0. 0.100000E 01 0. 0.
***** DATA NAME= *Z*ALL *
POINT X Y Z POINT X Y Z
1 0. 0. 0.100000E 01 0. 0. 0. 0. 0. 0. 0. 0.
2 0.100000E 01 0.100000E 01
COORDINATES OF POINTS OF BOUNDARY OF SURF *IFLOOR * FOR EACH Y INTERVAL
X=LEFT X=RIGHT X=LEFT X=RIGHT X=LEFT X=RIGHT X=LEFT X=RIGHT
0. 0.100000E 01 0. 0. 0.100000E 01 0.100000E 01
0. 0.100000E 01 0.333333E-01 0. 0. 0.100000E 01 0.125000E 00

```

FIGURE 20. Group A Sample Problems Program Results (continued)

| | | | | | |
|----|--------------|---------------|----|--------------|--------------|
| G. | 0.100000E 01 | 0.1858667E+00 | 0. | 0.100000E 01 | 0.208333E-00 |
| G. | 0.100000E 01 | 0.2500000E+00 | 0. | 0.100000E 01 | 0.375000E-00 |
| G. | 0.100000E 01 | 0.333333E+00 | 0. | 0.100000E 01 | 0.458333E-00 |
| G. | 0.100000E 01 | 0.416666E+00 | 0. | 0.100000E 01 | 0.541666E-00 |
| G. | 0.100000E 01 | 0.500000E+00 | 0. | 0.100000E 01 | 0.625000E-00 |
| G. | 0.100000E 01 | 0.583333E+00 | 0. | 0.100000E 01 | 0.708333E-00 |
| G. | 0.100000E 01 | 0.666666E+00 | 0. | 0.100000E 01 | 0.791666E-00 |
| G. | 0.100000E 01 | 0.750000E+00 | 0. | 0.100000E 01 | 0.875000E-00 |
| G. | 0.100000E 01 | 0.833333E+00 | 0. | 0.100000E 01 | 0.958333E-00 |
| G. | 0.100000E 01 | 0.916666E+00 | 0. | | |
| G. | 0.100000E 01 | 0.100000E 01 | 0. | | |

42. OF HORIZONTAL INCREMENTS= 2% NOS. OF VERTICAL INCREMENTS= 2%

THE FOLLOWING ARE PLATE DRAIN COMPARISON FACTORS COMPUTED FOR THIS RUN
 L3%-ST-RED LINE FIRST FROM X-LEFT TO X-RIGHT.

| | | | | | |
|---------------|---------------|---------------|---------------|--------------|---------------|
| 0.100000E 01 | 0.2760740E-00 | 0.2463870E-00 | 0.2173754E-00 | 0.210000E 01 | 0.208333E-00 |
| 0.246117E+00 | 0.2288541E-00 | 0.2297537E-00 | 0.2208467E-00 | 0.212113E+00 | 0.207276E-00 |
| 0.192809E-00 | 0.174216E-00 | 0.174216E-00 | 0.171771E-00 | 0.165661E+00 | 0.157037E-00 |
| 0.114685E+00 | 0.1159418E-00 | 0.1159418E-00 | 0.115719E-00 | 0.114262E+00 | 0.114262E-00 |
| 0.4246099E-00 | 0.393632E-00 | 0.393632E-00 | 0.393178E-00 | 0.392420E+00 | 0.391902E-00 |
| 0.27244E+00 | 0.240746E-00 | 0.240746E-00 | 0.231225E-00 | 0.220594E+00 | 0.220594E-00 |
| 0.173463E+00 | 0.162211E-00 | 0.162211E-00 | 0.157897E-00 | 0.15389E+00 | 0.15389E-00 |
| 0.135159E+00 | 0.1446049E-00 | 0.1446049E-00 | 0.1374897E-00 | 0.134645E+00 | 0.134645E-00 |
| 0.292249E+00 | 0.4498349E-00 | 0.4498349E-00 | 0.371940E-00 | 0.244200E+00 | 0.237632E-00 |
| 0.152337E+00 | 0.248754E-00 | 0.248754E-00 | 0.2606191E-00 | 0.244200E+00 | 0.244200E-00 |
| 0.123517E+00 | 0.181932E-00 | 0.181932E-00 | 0.1453177E-00 | 0.137863E+00 | 0.137863E-00 |
| 0.33786E+00 | 0.530663E-00 | 0.530663E-00 | 0.4428845E-00 | 0.379122E+00 | 0.3535010E-00 |
| 0.246934E+00 | 0.215503E-00 | 0.215503E-00 | 0.250149E-00 | 0.261494E+00 | 0.253155E-00 |
| 0.173351E+00 | 0.176464E-00 | 0.176464E-00 | 0.166034E-00 | 0.153337E+00 | 0.153337E-00 |
| 0.357583E+00 | 0.52249E+00 | 0.52249E+00 | 0.4494135E-00 | 0.439330E+00 | 0.435763E-00 |
| 0.353123E+00 | 0.316376E-00 | 0.316376E-00 | 0.2701128E-00 | 0.263780E+00 | 0.263780E-00 |
| 0.180702E+00 | 0.187901E-00 | 0.187901E-00 | 0.220952E-00 | 0.220952E-00 | 0.220952E-00 |
| | 0.116061E-00 | 0.116061E-00 | 0.161810E-00 | 0.153710E+00 | 0.144602E-00 |

FIGURE 20. Group A Sample Problems Program Results
 (continued)

| | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|
| 0.578644E CO | 0.447350E 00 | 0.456781E 00 | 0.456179E 00 | 0.513301E 00 | 0.438325E 00 |
| 0.511160E CO | 0.496524E 00 | 0.478470E 00 | 0.478470E 00 | 0.478470E 00 | 0.478470E 00 |
| 0.286368E CO | 0.584650E 00 |
| 0.664109E CO | 0.633743E 00 | 0.712871E 00 | 0.700373E 00 | 0.685041E 00 | 0.675987E 00 |
| 0.601203E CO | 0.571703E 00 | 0.562647E 00 | 0.573762E 00 | 0.564931E 00 | 0.559018E 00 |
| 0.292579E CO | 0.516018E 00 | 0.523482E 00 | 0.506688E 00 | 0.476834E 00 | 0.442697E 00 |
| 0.502000E CO | 0.733174E 00 | 0.724629E 00 | 0.714780E 00 | 0.703245E 00 | 0.632140E 00 |
| 0.621278E CO | 0.670421E 00 | 0.660584E 00 | 0.650843E 00 | 0.641527E 00 | 0.632077E 00 |
| 0.583150E CO | 0.577739E 00 | 0.572698E 00 | 0.567786E 00 | 0.561149E 00 | 0.558944E 00 |
| 0.305734E CO | 0.577739E 00 | 0.572698E 00 | 0.567786E 00 | 0.561149E 00 | 0.559224E 00 |

FIGURE 20. Group A Sample Problems Program Results
(continued)

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (A)-K.A.TOUPS.1/1/63

RUN NO. 4 DATA USED FOR THIS RUN= *2MALLS*1FLDOR*
* * * * *

A NONPLANAR SURFACE CANNOT BE USED AS SURFACE 1-THIS RUN ABORTED.

FIGURE 20. Group A Sample Problems Program Results
(continued)

NAA COMFAC II REPORT SAMPLE PROBLEMS FROM FIG. (A) M. A. TOWNSHILL/703

RUN NO. 5 DATA USED FOR THIS RUN- *IFLOOS*+MALLR*
* * * * *

NOV. OF SURFACE *IFLOUP * IS SEEN BY SURFACE *MALLR *
IF THE ABOVE RESULT IS UNEXPECTED, OR NOT BECOME ALARMED- IT HAPPENS TO THE BEST OF CM- JUST CHECK YOUR
DATA AND BE ESPECIALLY BE SURE THAT YOU ENTERED ALL POINTS IN COUNT-CLOCKWISE ORDER, AS THEY APPEAR WHEN
FACING THE ACTIVE SIDE OF THE SURFACE, AND DERIVED FROM A RIGHT-HANDED COORDINATE SYSTEM.

FIGURE 20. Group A Sample Problems Program Results
(continued)

NAA CONFAC II REPORT SIMPLE PROBLEMS FROM FIG. 1A1-KA-17C/PS.11/1/63

RUN NO. 6 DATA USED FOR THIS RUN= *IFLOOR*2MALLZ*
 *D * * *

THE FORM FACTOR FROM SURFACE *IFLOOR * TO SURFACE *2MALLZ * = 0.39932

THE EXCHANGE COEFFICIENT (FA)= 0.39932E-00 SQ UNITS

THE MAPPING AREA = 1.0000000E 00 SQ UNITS

THE AREA OF SURFACE *IFLOOR * = 0.1000000E 01 SQ UNITS.

ONLY A PART OF SURFACE *2MALLZ * SEES SURFACE *IFLOOR *

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

***** DATA NAME= *IFLOOR *

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|---------------|---------------|---------------|-------|---------------|---------------|----|
| 1 | 0.1000000E 01 | 0. | 0.1000000E 01 | 2 | 0. | 0. | 0. |
| 3 | 0. | 0.1000000E 01 | 0. | 4 | 0.1000000E 01 | 0.1000000E 01 | 0. |

***** DATA NAME= *2MALLZ *

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|---------------|---------------|---------------|-------|---------------|---------------|---------------|
| 1 | 0. | 0.1000000E 01 | 0.1000000E 01 | 2 | 0. | 0. | 0. |
| 3 | 0.1000000E 01 | 0.1000000E 01 | 0.1000000E 01 | 4 | 0.1000000E 01 | 0.1000000E 01 | 0.1000000E 01 |
| 5 | 0. | 0.1000000E 01 | 0.1000000E 01 | | | | |

COORDINATES OF POINTS ON BOUNDARY OF SUR* *IFLOOR * FOR EACH Y INTERVAL

X-LEFT X-RIGHT Y X-LEFT X-RIGHT Y

FIGURE 20. Group A Sample Problems Program Results
 (continued)

| | | | | | |
|--------------|---------------|--------------|---------------|---------------|---------------|
| 0.355423E+00 | 0.333750E+00 | 0.315651E+00 | 0.279112E+00 | 0.269376E+00 | 0.260007E+00 |
| 0.189700E+00 | 0.180163E+00 | 0.170843E+00 | 0.161810E+00 | 0.153071E+00 | 0.144602E+00 |
| 0.135413E+00 | 0.125885E+00 | 0.116565E+00 | 0.107390E+00 | 0.990337E+00 | 0.901831E+00 |
| 0.77773E+00 | 0.730302E+00 | 0.682207E+00 | 0.633795E+00 | 0.585034E+00 | 0.536041E+00 |
| 3.217044E+00 | 0.2583770E+00 | 0.445749E+00 | 0.237324E+00 | 0.222222E+00 | 0.211601E+00 |
| 0.209894E+00 | 0.190164E+00 | 0.180162E+00 | 0.170061E+00 | 0.161052E+00 | 0.151933E+00 |
| 0.581350E+00 | 0.5462346E+00 | 0.511164E+00 | 0.476159E+00 | 0.4412050E+00 | 0.406298E+00 |
| 0.368378E+00 | 0.378007E+00 | 0.353477E+00 | 0.328461E+00 | 0.302944E+00 | 0.277034E+00 |
| 0.222870E+00 | 0.2064874E+00 | 0.189762E+00 | 0.173143E+00 | 0.156792E+00 | 0.140881E+00 |
| 0.149689E+00 | 0.137825E+00 | 0.126180E+00 | 0.114831E+00 | 0.103801E+00 | 0.931508E+00 |
| 0.119423E+00 | 0.107511E+00 | 0.973922E+00 | 0.893101E+00 | 0.814459E+00 | 0.737654E+00 |
| 0.302378E+00 | 0.285489E+00 | 0.271522E+00 | 0.260298E+00 | 0.247321E+00 | 0.234915E+00 |
| 0.222870E+00 | 0.211160E+00 | 0.199754E+00 | 0.188639E+00 | 0.177810E+00 | 0.167271E+00 |
| 0.551446E+00 | 0.565963E+00 | 0.535309E+00 | 0.506729E+00 | 0.479299E+00 | 0.454204E+00 |
| 0.704378E+00 | 0.402091E+00 | 0.387609E+00 | 0.368897E+00 | 0.349244E+00 | 0.329728E+00 |
| 0.234623E+00 | 0.222222E+00 | 0.211093E+00 | 0.198262E+00 | 0.186625E+00 | 0.175188E+00 |
| 0.164314E+00 | 0.157703E+00 | 0.146192E+00 | 0.139108E+00 | 0.129566E+00 | 0.120045E+00 |
| 0.451924E+00 | 0.424607E+00 | 0.402319E+00 | 0.384408E+00 | 0.366315E+00 | 0.349431E+00 |
| 0.717175E+00 | 0.717256E+00 | 0.702297E+00 | 0.287660E+00 | 0.273874E+00 | 0.260198E+00 |
| 0.333833E+00 | 0.233732E+00 | 0.220850E+00 | 0.208186E+00 | 0.195779E+00 | 0.183602E+00 |
| 0.058213E+00 | 0.582687E+00 | 0.556746E+00 | 0.531405E+00 | 0.508719E+00 | 0.493481E+00 |
| 0.081195E+00 | 0.458257E+00 | 0.419409E+00 | 0.392374E+00 | 0.287192E+00 | 0.273570E+00 |
| 0.255772E+00 | 0.245749E+00 | 0.234095E+00 | 0.218600E+00 | 0.205199E+00 | 0.1922130E+00 |
| 0.174235E+00 | 0.161707E+00 | 0.148702E+00 | 0.136233E+00 | 0.119864E+00 | 0.107251E+00 |
| 0.455351E+00 | 0.454603E+00 | 0.434934E+00 | 0.416027E+00 | 0.398037E+00 | 0.380744E+00 |
| 0.364224E+00 | 0.346007E+00 | 0.334786E+00 | 0.318255E+00 | 0.302109E+00 | 0.285489E+00 |
| 0.187808E+00 | 0.258376E+00 | 0.245901E+00 | 0.229750E+00 | 0.215227E+00 | 0.201148E+00 |
| 0.424689E+00 | 0.401003E+00 | 0.378668E+00 | 0.5520126E+00 | 0.534081E+00 | 0.510937E+00 |
| 0.700479E+00 | 0.659531E+00 | 0.610232E+00 | 0.562781E+00 | 0.517098E+00 | 0.473098E+00 |
| 0.238589E+00 | 0.271704E+00 | 0.250339E+00 | 0.240786E+00 | 0.225427E+00 | 0.210379E+00 |
| 0.192362E+00 | | | | | |

FIGURE 20. Group A Sample Problems Program Results
(continued)

| | | | | | |
|---------------|--------------|--------------|--------------|--------------|--------------|
| 0.432637E+00 | 0.610244E+00 | 0.388625E+00 | 0.366882E+00 | 0.545522E+00 | 0.224742E+00 |
| 0.396493E+00 | 0.380725E+00 | 0.364666E+00 | 0.340149E+00 | 0.331765E+00 | 0.317765E+00 |
| 0.401914E+00 | 0.428998E+00 | 0.426907E+00 | 0.425135E+00 | 0.226368E+00 | 0.220027E+00 |
| 0.203570E+00 | 0.626403E+00 | 0.439640E+00 | 0.378993E+00 | 0.595569E+00 | 0.513623E+00 |
| 0.414920E+00 | 0.360334E+00 | 0.482046E+00 | 0.464370E+00 | 0.447144E+00 | 0.443042E+00 |
| 0.513197E+00 | 0.396037E+00 | 0.382733E+00 | 0.396316E+00 | 0.370388E+00 | 0.334278E+00 |
| 0.211843E+00 | 0.301030E+00 | 0.423768E+00 | 0.426818E+00 | 0.246893E+00 | 0.230212E+00 |
| 0.450843E+00 | 0.430720E+00 | 0.411024E+00 | 0.391283E+00 | 0.514803E+00 | 0.532228E+00 |
| 0.317079E+00 | 0.212927E+00 | 0.408271E+00 | 0.384406E+00 | 0.463387E+00 | 0.450218E+00 |
| 0.227574E+00 | 0.441645E+00 | 0.279112E+00 | 0.280149E+00 | 0.260490E+00 | 0.240744E+00 |
| 0.220897E+00 | 0.441645E+00 | 0.464271E+00 | 0.401910E+00 | 0.505344E+00 | 0.567173E+00 |
| 0.450223E+00 | 0.434934E+00 | 0.419440E+00 | 0.403705E+00 | 0.442604E+00 | 0.446165E+00 |
| 0.327574E+00 | 0.335225E+00 | 0.315651E+00 | 0.295465E+00 | 0.274034E+00 | 0.251958E+00 |
| 0.467074E+00 | 0.654745E+00 | 0.434723E+00 | 0.416879E+00 | 0.599212E+00 | 0.581824E+00 |
| 0.264780E+00 | 0.244104E+00 | 0.231823E+00 | 0.215909E+00 | 0.500310E+00 | 0.495018E+00 |
| 0.371869E+00 | 0.354936E+00 | 0.351475E+00 | 0.312317E+00 | 0.288743E+00 | 0.264688E+00 |
| 0.2376501E+00 | 0.564706E+00 | 0.447130E+00 | 0.430145E+00 | 0.413388E+00 | 0.264646E+00 |
| 0.290553E+00 | 0.447076E+00 | 0.444232E+00 | 0.431009E+00 | 0.451018E+00 | 0.264646E+00 |
| 0.492543E+00 | 0.376637E+00 | 0.460049E+00 | 0.444592E+00 | 0.441034E+00 | 0.413442E+00 |
| 0.432160E+00 | 0.672467E+00 | 0.654823E+00 | 0.644376E+00 | 0.647834E+00 | 0.612227E+00 |
| 0.390895E+00 | 0.581608E+00 | 0.561117E+00 | 0.552728E+00 | 0.530833E+00 | 0.524445E+00 |
| 0.444730E+00 | 0.474842E+00 | 0.460476E+00 | 0.449350E+00 | 0.444942E+00 | 0.443442E+00 |
| 0.420658E+00 | 0.403105E+00 | 0.376027E+00 | 0.353502E+00 | 0.334320E+00 | 0.291907E+00 |
| 0.257532E+00 | 0.694012E+00 | 0.672796E+00 | 0.657826E+00 | 0.645693E+00 | 0.629738E+00 |
| 0.203331E+00 | 0.451684E+00 | 0.430678E+00 | 0.414502E+00 | 0.404599E+00 | 0.394552E+00 |
| 0.541261E+00 | 0.474842E+00 | 0.460476E+00 | 0.449350E+00 | 0.444942E+00 | 0.444599E+00 |
| 0.444730E+00 | 0.474842E+00 | 0.460476E+00 | 0.449350E+00 | 0.444942E+00 | 0.444599E+00 |
| 0.714764E+00 | 0.702397E+00 | 0.686002E+00 | 0.671737E+00 | 0.657631E+00 | 0.643760E+00 |
| 0.432160E+00 | 0.616677E+00 | 0.603970E+00 | 0.591283E+00 | 0.578933E+00 | 0.566688E+00 |
| 0.252324E+00 | 0.244222E+00 | 0.231402E+00 | 0.217303E+00 | 0.207139E+00 | 0.197184E+00 |
| 0.447813E+00 | 0.466260E+00 | 0.447588E+00 | 0.441238E+00 | 0.427839E+00 | 0.413194E+00 |

FIGURE 20. Group A Sample Problems Program Results
(continued)

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|
| 0-2767014E-C0 | 0-7158712E-2C | 0-5923166E 00 | 0-6650028E 00 | 0-6717976E 00 | 0-6598238E C0 |
| 0-7264088E C0 | 0-6771908E C0 | 0-5257154E 00 | 0-5410762E 00 | 0-5353098E C0 | 0-7338470E C0 |
| 0-5771898E C0 | 0-5671908E C0 | 0-4784192E-00 | 0-4541662E-00 | 0-4186147E-00 | 0-5353632E-00 |
| 0-5111622E C0 | 0-4962319E-70 | 0-4784192E-00 | 0-4541662E-00 | 0-4186147E-00 | 0-5353632E-00 |
| 0-5683708E C0 | 0-7254978E 00 | 0-7128372E 00 | 0-703737E C0 | 0-6458013E 00 | 0-6378982E C0 |
| 0-5283708E C0 | 0-6441968E 00 | 0-5416435E 00 | 0-6339207E C0 | 0-6205803E C0 | 0-6100144E 00 |
| 0-6010038E C0 | 0-5917073E 00 | 0-5886476E 00 | 0-5737962E 00 | 0-5479632E C0 | 0-5459971E C0 |
| 0-6216182E C0 | 0-5517432E 00 | 0-5239422E 00 | 0-5058692E 00 | 0-4776348E-00 | 0-4246997E-00 |
| 0-2860746E-C0 | 0-7581714E 00 | 0-7264088E C0 | 0-7147804E C0 | 0-7033515E C0 | 0-6211008E C0 |
| 0-7500000E C0 | 0-6101038E C0 | 0-6050431E 00 | 0-6057962E 00 | 0-591372E C0 | 0-5818972E C0 |
| 0-6817288E C0 | 0-6101038E C0 | 0-6050431E 00 | 0-6057962E 00 | 0-591372E C0 | 0-5818972E C0 |
| 0-5831526E C0 | 0-3777359E 00 | 0-3746888E 00 | 0-3679804E 00 | 0-3635088E C0 | 0-3595742E C0 |
| 0-1807342E-00 | | | | | |

FIGURE 20. Group 1 Sample Problems Program Results
(continued)

SYNTH. PROGRAM GROUP B

The geometrical relationships used in this example are presented in Figure 21. The data sheets are shown in Figure 22 with results in Figure 23.

Problem 1B

The use of the surface generator and double bisection of surfaces is demonstrated. The plane Surface 1PLAT1 is entered as usual in the data, but the octagonal disk 3DISK is created by specifications to the surface generator. Note that no connections data are created for a Class 3 surface, but would be if the disk were named CDISK.

The double bisection is easily seen in side view of 1PLAT1 and 3DISK. The results of the factor request from 1PLAT1 and 3DISK is shown in Run #1 output, indicating the areas in each surface seen by the other. The number of points defining 3DISK has been reduced to 7 and reorganized because of the bisection, as seen along the dotted line.

Problem 2B

The converse factor, 3DISK to 1PLAT1, is requested as Run #2. Because the disk is now Surface 1, the final coordinate system in 3DISK is aligned so that the XY plane is the plane of the disk. Point 1 becomes the origin, and line segment 1 2 the X axis. Note that the exchange coefficients (f_A) are very nearly equal, as they should be because of the reciprocity theorem.

Notice that the factor from one surface to the other along the line of bisection is, in reality, zero, but the output is, in some cases, non-zero though quite small (10^{-8} order of magnitude). This is caused by accumulated internal truncation error, and is not significant enough to warrant concern here. (This is not the case, however, with some silhouette generator computations).

Problem 3B

The capability of coordinate transformation is illustrated. Run #3 requests the factor from 1PLAT1 to 3DISK transformed to the position shown by the transformation data 9TDISK. The program detected, after transforming 3DISK, that it bisected 1PLAT1. As the output shows, the part of 1PLAT1 actually named was the trapezoid indicated in the top view, and in the output final coordinate data.

Problem 4B

It is quite feasible to generate or manually input a surface, transform the surface to a different location, and then ask for the factor between the original surface and the transformed surface. This is shown by Run #4, where 3DISK is used as Surface 1, and 3DISK transformed by 9TDISK is used as

Surface 2. The output shows a bisection of 3DISK, removing the 4th boundary point, and therefore adding a point to the final 3DISK surface boundaries, making it 9 instead of 8.

Problem 5B

The factor from the transformed disk, 3DISK9TDICK, to 1PLAT1 is requested as Run #5, demonstrating program flexibility in that Surface 1 is now transformed. The resulting exchange coefficient is very nearly equal to Run #3, as it should be.

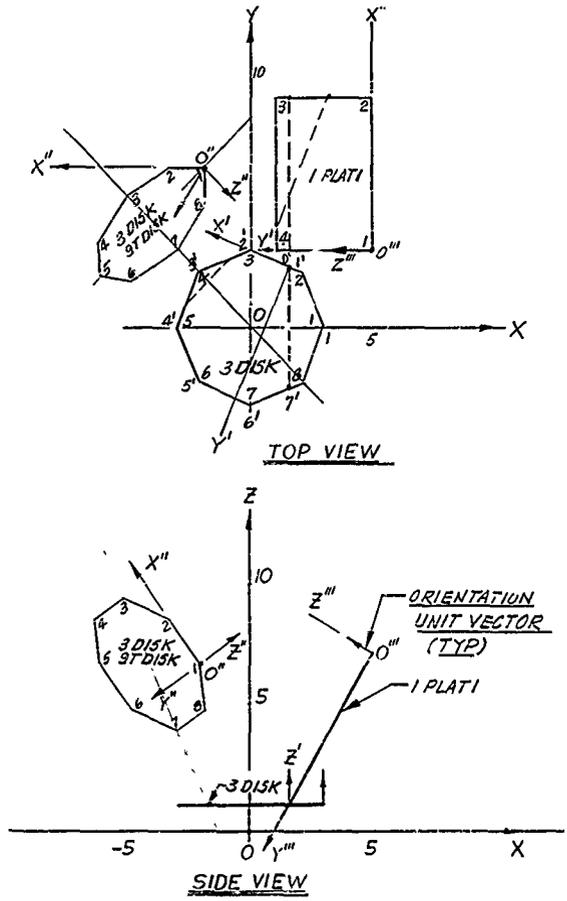


FIGURE 21. GROUP B SAMPLE PROBLEMS GEOMETRY

FORTRAN FIXED IO DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 3 of 3 | JOB NO. 252-20 |
|----------|----------------|-------------|------------------|----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | 1 | 1 | | |
| 2 | 2 | 2 | | |
| 3 | 3 | 3 | | |
| 4 | 4 | 4 | | |
| 5 | 5 | 5 | | |
| 6 | 6 | 6 | | |
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| 11 | 11 | 11 | | |
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| 36 | 36 | 36 | | |
| 37 | 37 | 37 | | |
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| 100 | 100 | 100 | | |

FORTRAN FIXED IO DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 10 of 31 | JOB NO. 252-20 |
|----------|----------------|-------------|------------------|----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | 1 | 1 | | |
| 2 | 2 | 2 | | |
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FIGURE 22. Group B Sample Problems Input Data Code Sheets

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. PROGRAMMER DATE PAGE 11 of 31 JOB NO. 255-32

| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH |
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FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. PROGRAMMER DATE PAGE 12 of 31 JOB NO. 255-32

| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH |
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FIGURE 22. Group B Sample Problems Input Data Code Sheets (continued)

NAA SPACE AND INFORMATION SYSTEMS DIVISION
 T-4 PROJECT AUGMENT-INTERCHANGE CONFIGURATION FACTOR PROGRAM
 C O N F A C I
 NAA COFAC II REPORT SAMPLE PROBLEMS FROM FIG. (81)-K-4-100P-511/1/63

I N P L T O A T A

**** DATA NAME= *SPLATE * A SKEWED RECTANGULAR SURFACE
 POINT X Y Z POINT X Y Z
 1 0.4131776 01 0.3000000 01 0.7490139 01 --- (INTERNALLY GENERATED ORIENTATION VECTOR) Z
 2 0.1000000 01 0.7000000 01 0. 0.1000000 01 0.9000000 01 0.7000000 01
 3 0.4100000 01 0.3000000 01 0. 0.1000000 01 0.3000000 01 0.7000000 01

**** DATA NAME= *3DISK * OCTAGONAL DISK
 SURFACE SPECIFICATIONS=
 NO OF X-SECTIONS = 1 NO OF Z-SECTION BOUNDARY DIVISIONS = 8
 LOCATION OF VERTICAL CENTRALLINE, X= 0. Y= 0.
 X-SECTION NO. X-RADIUS Y-RADIUS ELEVATION ABOVE XY PLANE
 1 0.3000000 01 0.3000000 01 0.1000000 01

THE FOLLOWING INTERNALLY GENERATED SURFACE DATA RESULTED FROM THE ABOVE SPECIFICATIONS-

POINT X Y Z POINT X Y Z
 1 0.5000000 01 0. 0.2000000 01 --- (INTERNALLY GENERATED ORIENTATION VECTOR) Z
 2 0.3000000 01 0. 0.3000000 01 0.2000000 01 0.1000000 01 0.1000000 01
 3 0.5879331-07 0.3000000 01 0.1000000 01 4 -0.2121320 01 0.2121320 01 0.1000000 01
 4 0.5879331-07 0.3000000 01 0.1000000 01 5 -0.2121320 01 0.2121320 01 0.1000000 01
 5 0.5879331-07 0.3000000 01 0.1000000 01 6 -0.2121320 01 0.2121320 01 0.1000000 01
 6 0.5879331-07 0.3000000 01 0.1000000 01 7 0.2121320 01 -0.2121320 01 0.1000000 01
 7 0.5879331-07 0.3000000 01 0.1000000 01 8 0.2121320 01 -0.2121320 01 0.1000000 01

**** DATA NAME= *9YDISK * TRANSFORMS 3DISK TO SKEWED POSITION IN II QUADRANT
 TRANSFORMATION DATA=

FIGURE 23. Group B Sample Problems Program Results
 (27 pages)

```

POINT X Y POINT X Y
1 -0.193840E 01 0.618190E 01 0.458070E 01 0.511130E 01 0.917610E 01
7 -0.300000E 01 0.300000E 01 0.400000E 01

```

FIGURE 23. Group B Sample Problems Program Results
(continued)

IMA 50 IFAC II REPORT SAMPLE PROBLEMS FROM FIG. (P)-6-A-TIUPS-11/7/63

```

RUN NO. 1 CASE USED FOR THIS RUN= *IPLATI=3DISK *
          *
          *
THE FORM FACTOR FROM SURFACE *IPLATI * TO SURFACE *3DISK * = 0.00994
THE EXCHANGE COEFFICIENT (EAF)= 0.46132E+00 SO UNITS
          *
          *
          *
          *
THE MAGNITUDE AREA = 0.4140363E 02 SO UNITS
          *
          *
ONLY A PART OF SURFACE *IPLATI * COMPRISING AN AREA OF 0.4140363E 02 SO UNITS,
SEES SURFACE *3DISK
          *
          *
THE AREA OF SURFACE *IPLATI * = 0.4037355E 02 SO UNITS.
          *
          *
ONLY A PART OF SURFACE *3DISK * COMPRISING AN AREA OF 0.2113364E 02 SO UNITS,
SEES SURFACE *IPLATI *
          *
          *
THE AREA OF SURFACE *3DISK * = 0.2544558E 02 SO UNITS.
          *
          *
THE FOLLOWING ARE THE GLOBAL SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION=

***** DATA NAME= *IPLATI *
POINT 0. X -0. Y 0. POINT X INTERNALLY GENERATED ORIENTATION VECTOR Z
1 0. -0. -0. 0.100000E 01---1
2 0.600000E 01 0. 0.
3 0.000000E 01 0.6940597E 01 0. 0. 0. 0.6940597E 01 0.

***** DATA NAME= *3DISK *
POINT 0. X 0. Y 0. POINT X INTERNALLY GENERATED ORIENTATION VECTOR Z
1 0.6559591E 00 0.6740501E 01 0. 0. 0. 0.6559591E 00 0.6740501E 01 0.
2 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
3 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.

```

FIGURE 23. Group B Sample Problems Program Results
(continued)

3 -0.8786792E 00 0.8742623E 01 0.1262026E 01 4 -0.1000000E 01 0.9186278E 01 0.4000132E 01
 5 -0.5121320E 01 0.8742623E 01 0.3502024E 01 6 -0.1000000E 01 0.7500156E 01 0.2100182E 01
 7 -0.5534939E 01 0.6310337E 01 0.

COORDINATES OF POINTS ON BOUNDARY OF SURF *18PLATE * FOR EACH Y INTERVAL

| X-LEFT | X-RIGHT | Y | X-LEFT | X-RIGHT | Y |
|--------|--------------|---------------|--------|--------------|---------------|
| 0. | 0.600000E 01 | -0. | 0. | 0.600000E 01 | 0.4879378E-00 |
| 0. | 0.600000E 01 | 0.1189546E 02 | 0. | 0.600000E 01 | 0.4939138E 00 |
| 0. | 0.600000E 01 | 0.1181752E 01 | 0. | 0.600000E 01 | 0.5000000E 00 |
| 0. | 0.600000E 01 | 0.1172728E 01 | 0. | 0.600000E 01 | 0.5059862E 00 |
| 0. | 0.600000E 01 | 0.1163704E 01 | 0. | 0.600000E 01 | 0.5119724E 00 |
| 0. | 0.600000E 01 | 0.1154680E 01 | 0. | 0.600000E 01 | 0.5179586E 00 |
| 0. | 0.600000E 01 | 0.1145656E 01 | 0. | 0.600000E 01 | 0.5239448E 00 |
| 0. | 0.600000E 01 | 0.1136632E 01 | 0. | 0.600000E 01 | 0.5299310E 00 |
| 0. | 0.600000E 01 | 0.1127608E 01 | 0. | 0.600000E 01 | 0.5359172E 00 |
| 0. | 0.600000E 01 | 0.1118584E 01 | 0. | 0.600000E 01 | 0.5419034E 00 |
| 0. | 0.600000E 01 | 0.1109560E 01 | 0. | 0.600000E 01 | 0.5478896E 00 |
| 0. | 0.600000E 01 | 0.1100536E 01 | 0. | 0.600000E 01 | 0.5538758E 00 |
| 0. | 0.600000E 01 | 0.1091512E 01 | 0. | 0.600000E 01 | 0.5598620E 00 |
| 0. | 0.600000E 01 | 0.1082488E 01 | 0. | 0.600000E 01 | 0.5658482E 00 |
| 0. | 0.600000E 01 | 0.1073464E 01 | 0. | 0.600000E 01 | 0.5718344E 00 |
| 0. | 0.600000E 01 | 0.1064440E 01 | 0. | 0.600000E 01 | 0.5778206E 00 |
| 0. | 0.600000E 01 | 0.1055416E 01 | 0. | 0.600000E 01 | 0.5838068E 00 |
| 0. | 0.600000E 01 | 0.1046392E 01 | 0. | 0.600000E 01 | 0.5897930E 00 |
| 0. | 0.600000E 01 | 0.1037368E 01 | 0. | 0.600000E 01 | 0.5957792E 00 |
| 0. | 0.600000E 01 | 0.1028344E 01 | 0. | 0.600000E 01 | 0.6017654E 00 |
| 0. | 0.600000E 01 | 0.1019320E 01 | 0. | 0.600000E 01 | 0.6077516E 00 |
| 0. | 0.600000E 01 | 0.1010296E 01 | 0. | 0.600000E 01 | 0.6137378E 00 |
| 0. | 0.600000E 01 | 0.1001272E 01 | 0. | 0.600000E 01 | 0.6197240E 00 |
| 0. | 0.600000E 01 | 0.0992248E 01 | 0. | 0.600000E 01 | 0.6257102E 00 |
| 0. | 0.600000E 01 | 0.0983224E 01 | 0. | 0.600000E 01 | 0.6316964E 00 |
| 0. | 0.600000E 01 | 0.0974200E 01 | 0. | 0.600000E 01 | 0.6376826E 00 |
| 0. | 0.600000E 01 | 0.0965176E 01 | 0. | 0.600000E 01 | 0.6436688E 00 |
| 0. | 0.600000E 01 | 0.0956152E 01 | 0. | 0.600000E 01 | 0.6496550E 00 |
| 0. | 0.600000E 01 | 0.0947128E 01 | 0. | 0.600000E 01 | 0.6556412E 00 |
| 0. | 0.600000E 01 | 0.0938104E 01 | 0. | 0.600000E 01 | 0.6616274E 00 |
| 0. | 0.600000E 01 | 0.0929080E 01 | 0. | 0.600000E 01 | 0.6676136E 00 |
| 0. | 0.600000E 01 | 0.0920056E 01 | 0. | 0.600000E 01 | 0.6735998E 00 |
| 0. | 0.600000E 01 | 0.0911032E 01 | 0. | 0.600000E 01 | 0.6795860E 00 |
| 0. | 0.600000E 01 | 0.0902008E 01 | 0. | 0.600000E 01 | 0.6855722E 00 |
| 0. | 0.600000E 01 | 0.0892984E 01 | 0. | 0.600000E 01 | 0.6915584E 00 |
| 0. | 0.600000E 01 | 0.0883960E 01 | 0. | 0.600000E 01 | 0.6975446E 00 |
| 0. | 0.600000E 01 | 0.0874936E 01 | 0. | 0.600000E 01 | 0.7035308E 00 |
| 0. | 0.600000E 01 | 0.0865912E 01 | 0. | 0.600000E 01 | 0.7095170E 00 |
| 0. | 0.600000E 01 | 0.0856888E 01 | 0. | 0.600000E 01 | 0.7155032E 00 |
| 0. | 0.600000E 01 | 0.0847864E 01 | 0. | 0.600000E 01 | 0.7214894E 00 |
| 0. | 0.600000E 01 | 0.0838840E 01 | 0. | 0.600000E 01 | 0.7274756E 00 |
| 0. | 0.600000E 01 | 0.0829816E 01 | 0. | 0.600000E 01 | 0.7334618E 00 |
| 0. | 0.600000E 01 | 0.0820792E 01 | 0. | 0.600000E 01 | 0.7394480E 00 |
| 0. | 0.600000E 01 | 0.0811768E 01 | 0. | 0.600000E 01 | 0.7454342E 00 |
| 0. | 0.600000E 01 | 0.0802744E 01 | 0. | 0.600000E 01 | 0.7514204E 00 |
| 0. | 0.600000E 01 | 0.0793720E 01 | 0. | 0.600000E 01 | 0.7574066E 00 |
| 0. | 0.600000E 01 | 0.0784696E 01 | 0. | 0.600000E 01 | 0.7633928E 00 |
| 0. | 0.600000E 01 | 0.0775672E 01 | 0. | 0.600000E 01 | 0.7693790E 00 |
| 0. | 0.600000E 01 | 0.0766648E 01 | 0. | 0.600000E 01 | 0.7753652E 00 |
| 0. | 0.600000E 01 | 0.0757624E 01 | 0. | 0.600000E 01 | 0.7813514E 00 |
| 0. | 0.600000E 01 | 0.0748600E 01 | 0. | 0.600000E 01 | 0.7873376E 00 |
| 0. | 0.600000E 01 | 0.0739576E 01 | 0. | 0.600000E 01 | 0.7933238E 00 |
| 0. | 0.600000E 01 | 0.0730552E 01 | 0. | 0.600000E 01 | 0.7993100E 00 |
| 0. | 0.600000E 01 | 0.0721528E 01 | 0. | 0.600000E 01 | 0.8052962E 00 |
| 0. | 0.600000E 01 | 0.0712504E 01 | 0. | 0.600000E 01 | 0.8112824E 00 |
| 0. | 0.600000E 01 | 0.0703480E 01 | 0. | 0.600000E 01 | 0.8172686E 00 |
| 0. | 0.600000E 01 | 0.0694456E 01 | 0. | 0.600000E 01 | 0.8232548E 00 |
| 0. | 0.600000E 01 | 0.0685432E 01 | 0. | 0.600000E 01 | 0.8292410E 00 |
| 0. | 0.600000E 01 | 0.0676408E 01 | 0. | 0.600000E 01 | 0.8352272E 00 |
| 0. | 0.600000E 01 | 0.0667384E 01 | 0. | 0.600000E 01 | 0.8412134E 00 |
| 0. | 0.600000E 01 | 0.0658360E 01 | 0. | 0.600000E 01 | 0.8471996E 00 |
| 0. | 0.600000E 01 | 0.0649336E 01 | 0. | 0.600000E 01 | 0.8531858E 00 |
| 0. | 0.600000E 01 | 0.0640312E 01 | 0. | 0.600000E 01 | 0.8591720E 00 |
| 0. | 0.600000E 01 | 0.0631288E 01 | 0. | 0.600000E 01 | 0.8651582E 00 |
| 0. | 0.600000E 01 | 0.0622264E 01 | 0. | 0.600000E 01 | 0.8711444E 00 |
| 0. | 0.600000E 01 | 0.0613240E 01 | 0. | 0.600000E 01 | 0.8771306E 00 |
| 0. | 0.600000E 01 | 0.0604216E 01 | 0. | 0.600000E 01 | 0.8831168E 00 |
| 0. | 0.600000E 01 | 0.0595192E 01 | 0. | 0.600000E 01 | 0.8891030E 00 |
| 0. | 0.600000E 01 | 0.0586168E 01 | 0. | 0.600000E 01 | 0.8950892E 00 |
| 0. | 0.600000E 01 | 0.0577144E 01 | 0. | 0.600000E 01 | 0.9010754E 00 |
| 0. | 0.600000E 01 | 0.0568120E 01 | 0. | 0.600000E 01 | 0.9070616E 00 |
| 0. | 0.600000E 01 | 0.0559096E 01 | 0. | 0.600000E 01 | 0.9130478E 00 |
| 0. | 0.600000E 01 | 0.0550072E 01 | 0. | 0.600000E 01 | 0.9190340E 00 |
| 0. | 0.600000E 01 | 0.0541048E 01 | 0. | 0.600000E 01 | 0.9250202E 00 |
| 0. | 0.600000E 01 | 0.0532024E 01 | 0. | 0.600000E 01 | 0.9310064E 00 |
| 0. | 0.600000E 01 | 0.0523000E 01 | 0. | 0.600000E 01 | 0.9369926E 00 |
| 0. | 0.600000E 01 | 0.0513976E 01 | 0. | 0.600000E 01 | 0.9429788E 00 |
| 0. | 0.600000E 01 | 0.0504952E 01 | 0. | 0.600000E 01 | 0.9489650E 00 |
| 0. | 0.600000E 01 | 0.0495928E 01 | 0. | 0.600000E 01 | 0.9549512E 00 |
| 0. | 0.600000E 01 | 0.0486904E 01 | 0. | 0.600000E 01 | 0.9609374E 00 |
| 0. | 0.600000E 01 | 0.0477880E 01 | 0. | 0.600000E 01 | 0.9669236E 00 |
| 0. | 0.600000E 01 | 0.0468856E 01 | 0. | 0.600000E 01 | 0.9729098E 00 |
| 0. | 0.600000E 01 | 0.0459832E 01 | 0. | 0.600000E 01 | 0.9788960E 00 |
| 0. | 0.600000E 01 | 0.0450808E 01 | 0. | 0.600000E 01 | 0.9848822E 00 |
| 0. | 0.600000E 01 | 0.0441784E 01 | 0. | 0.600000E 01 | 0.9908684E 00 |
| 0. | 0.600000E 01 | 0.0432760E 01 | 0. | 0.600000E 01 | 0.9968546E 00 |
| 0. | 0.600000E 01 | 0.0423736E 01 | 0. | 0.600000E 01 | 1.0028408E 00 |
| 0. | 0.600000E 01 | 0.0414712E 01 | 0. | 0.600000E 01 | 1.0088270E 00 |
| 0. | 0.600000E 01 | 0.0405688E 01 | 0. | 0.600000E 01 | 1.0148132E 00 |
| 0. | 0.600000E 01 | 0.0396664E 01 | 0. | 0.600000E 01 | 1.0207994E 00 |
| 0. | 0.600000E 01 | 0.0387640E 01 | 0. | 0.600000E 01 | 1.0267856E 00 |
| 0. | 0.600000E 01 | 0.0378616E 01 | 0. | 0.600000E 01 | 1.0327718E 00 |
| 0. | 0.600000E 01 | 0.0369592E 01 | 0. | 0.600000E 01 | 1.0387580E 00 |
| 0. | 0.600000E 01 | 0.0360568E 01 | 0. | 0.600000E 01 | 1.0447442E 00 |
| 0. | 0.600000E 01 | 0.0351544E 01 | 0. | 0.600000E 01 | 1.0507304E 00 |
| 0. | 0.600000E 01 | 0.0342520E 01 | 0. | 0.600000E 01 | 1.0567166E 00 |
| 0. | 0.600000E 01 | 0.0333496E 01 | 0. | 0.600000E 01 | 1.0627028E 00 |
| 0. | 0.600000E 01 | 0.0324472E 01 | 0. | 0.600000E 01 | 1.0686890E 00 |
| 0. | 0.600000E 01 | 0.0315448E 01 | 0. | 0.600000E 01 | 1.0746752E 00 |
| 0. | 0.600000E 01 | 0.0306424E 01 | 0. | 0.600000E 01 | 1.0806614E 00 |
| 0. | 0.600000E 01 | 0.0297400E 01 | 0. | 0.600000E 01 | 1.0866476E 00 |
| 0. | 0.600000E 01 | 0.0288376E 01 | 0. | 0.600000E 01 | 1.0926338E 00 |
| 0. | 0.600000E 01 | 0.0279352E 01 | 0. | 0.600000E 01 | 1.0986200E 00 |
| 0. | 0.600000E 01 | 0.0270328E 01 | 0. | 0.600000E 01 | 1.1046062E 00 |
| 0. | 0.600000E 01 | 0.0261304E 01 | 0. | 0.600000E 01 | 1.1105924E 00 |
| 0. | 0.600000E 01 | 0.0252280E 01 | 0. | 0.600000E 01 | 1.1165786E 00 |
| 0. | 0.600000E 01 | 0.0243256E 01 | 0. | 0.600000E 01 | 1.1225648E 00 |
| 0. | 0.600000E 01 | 0.0234232E 01 | 0. | 0.600000E 01 | 1.1285510E 00 |
| 0. | 0.600000E 01 | 0.0225208E 01 | 0. | 0.600000E 01 | 1.1345372E 00 |
| 0. | 0.600000E 01 | 0.0216184E 01 | 0. | 0.600000E 01 | 1.1405234E 00 |
| 0. | 0.600000E 01 | 0.0207160E 01 | 0. | 0.600000E 01 | 1.1465096E 00 |
| 0. | 0.600000E 01 | 0.0198136E 01 | 0. | 0.600000E 01 | 1.1524958E 00 |
| 0. | 0.600000E 01 | 0.0189112E 01 | 0. | 0.600000E 01 | 1.1584820E 00 |
| 0. | 0.600000E 01 | 0.0180088E 01 | 0. | 0.600000E 01 | 1.1644682E 00 |
| 0. | 0.600000E 01 | 0.0171064E 01 | 0. | 0.600000E 01 | 1.1704544E 00 |
| 0. | 0.600000E 01 | 0.0162040E 01 | 0. | 0.600000E 01 | 1.1764406E 00 |
| 0. | 0.600000E 01 | 0.0153016E 01 | 0. | 0.600000E 01 | 1.1824268E 00 |
| 0. | 0.600000E 01 | 0.0143992E 01 | 0. | 0.600000E 01 | 1.1884130E 00 |
| 0. | 0.600000E 01 | 0.0134968E 01 | 0. | 0.600000E 01 | 1.1943992E 00 |
| 0. | 0.600000E 01 | 0.0125944E 01 | 0. | 0.600000E 01 | 1.2003854E 00 |
| 0. | 0.600000E 01 | 0.0116920E 01 | 0. | 0.600000E 01 | 1.2063716E 00 |
| 0. | 0.600000E 01 | 0.0107896E 01 | 0. | 0.600000E 01 | 1.2123578E 00 |
| 0. | 0.600000E 01 | 0.0098872E 01 | 0. | 0.600000E 01 | 1.2183440E 00 |
| 0. | 0.600000E 01 | 0.0089848E 01 | 0. | 0.600000E 01 | 1.2243302E 00 |
| 0. | 0.600000E 01 | 0.0080824E 01 | 0. | 0.600000E 01 | 1.2303164E 00 |
| 0. | 0.600000E 01 | 0.0071800E 01 | 0. | 0.600000E 01 | 1.2363026E 00 |
| 0. | 0.600000E 01 | 0.0062776E 01 | 0. | 0.600000E 01 | 1.2422888E 00 |
| 0. | 0.600000E 01 | 0.0053752E 01 | 0. | 0.600000E 01 | 1.2482750E 00 |
| 0. | 0.600000E 01 | 0.0044728E 01 | 0. | 0.600000E 01 | 1.2542612E 00 |
| 0. | 0.600000E 01 | 0.0035704E 01 | 0. | 0.600000E 01 | 1.2602474E 00 |
| 0. | 0.600000E 01 | 0.0026680E 01 | 0. | 0.600000E 01 | 1.2662336E 00 |
| 0. | 0.600000E 01 | 0.0017656E 01 | 0. | 0.600000E 01 | 1.2722198E 00 |
| 0. | 0.600000E 01 | 0.0008632E 01 | 0. | 0.600000E 01 | 1.2782060E 00 |
| 0. | 0.600000E 01 | 0.000000E 01 | 0. | 0.600000E 01 | 1.2841922E 00 |

NO. OF HORIZONTAL INCREMENTS* 24 NO. OF VERTICAL INCREMENTS* 24

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN
 LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|
| 3-1059382E-01 | 0.1024098E-01 | 0.9877514E-02 | 0.8904486E-02 | 0.9105181E-02 | 0.8724486E-02 |
| 0.6226105E-02 | 0.2970133E-0 | | | | |

| | | | | | |
|----------------|----------------|---------------|---------------|---------------|---------------|
| 0.7689145E-02 | 0.6518462E-02 | 0.3723891E-02 | 0.4912825E-02 | 0.4318709E-02 | 0.3801149E-02 |
| 0.1603004E-02 | 0.2791624E-02 | 0.2816741E-02 | 0.2324252E-02 | 0.2621631E-02 | 0.1618187E-02 |
| 0.688902E-01 | 2.338135E-01 | 0.4311004E-01 | 0.3456716E-01 | 0.2782889E-01 | 0.2253429E-01 |
| 0.8483701E-02 | 0.1191910E-02 | 0.1021812E-01 | 0.1021812E-01 | 0.6702071E-02 | 0.7353897E-02 |
| 0.2827103E-02 | 0.3397031E-02 | 0.4586717E-02 | 0.1816831E-02 | 0.1616176E-02 | 0.1444296E-04 |
| 0.2827103E-02 | 0.2322661E-02 | 0.2049683E-02 | 0.1816831E-02 | 0.1616176E-02 | 0.1444296E-04 |
| 0.1462100E-01 | 0.6489092E-01 | 0.3710365E-01 | 0.2827619E-01 | 0.2431815E-01 | 0.1770876E-01 |
| 0.1413178E-01 | 0.1114164E-01 | 0.1315322E-02 | 0.7627754E-02 | 0.6339031E-02 | 0.5121207E-02 |
| 0.1413178E-01 | 0.1413178E-01 | 0.1205016E-02 | 0.2803375E-02 | 0.2423884E-02 | 0.2108234E-02 |
| 0.8974109E-03 | 2.165...0E-01 | 0.1411018E-02 | 0.4423668E-02 | 0.1111521E-02 | 0.9932162E-03 |
| 0.6833051E-01 | 0.3144928E-01 | 0.2402315E-01 | 0.1770897E-01 | 0.1235339E-01 | 0.1027880E-01 |
| 0.2351119E-02 | 0.702...5E-04 | 0.1719458E-02 | 0.1412160E-02 | 0.1208491E-02 | 0.1058190E-02 |
| 0.3956210E-03 | 0.8354910E-03 | 0.7330130E-03 | 0.6485291E-03 | 0.5744472E-03 | 0.5150864E-03 |
| 0.17525398E-01 | 0. | 0. | 0.2984492E-09 | 0. | 0.2223369E-08 |
| 0. | 0.1167971E-28 | 0. | 0. | 0. | 0. |
| 0. | 0.24644...E-33 | 0. | 0.1133461E-08 | 0. | 0.1482246E-09 |
| 0. | | | | | |

FIGURE 2j. Group 3 Sample Problems Program Results
(continued)

| | | | | | |
|----------------|---------------|---------------|---------------|---------------|---------------|
| 0.25116385-01 | 0.34065432-02 | 0.12492465-01 | 0.17978461-01 | 0.23020667-01 | 0.28950431-01 |
| 0.23107788-01 | 3.3835682E-01 | 0.4235710E-01 | 0.45889701-01 | 0.4602106E-01 | 0.5147768E-01 |
| 0.2964788E-01 | 3.5526535E-01 | 0.5975338E-01 | 0.5782531E-01 | 0.5965110E-01 | 0.5983353E-01 |
| 0.3518891E-01 | 3.5956989E-01 | 0.5975338E-01 | 0.5975338E-01 | 0.5975338E-01 | 0.5983353E-01 |
| 0.1165797E-08 | 0.34065432-02 | 0.1070951E-01 | 0.1060445E-01 | 0.1122598E-01 | 0.2392350E-01 |
| 0.14849001E-01 | 0.5030265E-01 | 0.3191771E-01 | 0.3237318E-01 | 0.3308718E-01 | 0.3326254E-01 |
| 0.3502837E-01 | 3.5312068E-01 | 0.5189368E-01 | 0.5338180E-01 | 0.532839E-01 | 0.5284491E-01 |
| 0.25116385-01 | 0.4807717E-02 | 0.3750069E-02 | 0.1440818E-01 | 0.1907938E-01 | 0.2344060E-01 |
| 0.2755781E-01 | 0.3123704E-01 | 0.3459314E-01 | 0.3750069E-01 | 0.4213482E-01 | 0.4233942E-01 |
| 0.4393571E-01 | 0.4458292E-01 | 0.4982778E-01 | 0.4461503E-01 | 0.432340E-01 | 0.4477860E-01 |
| 0.4726644E-01 | 0.4458292E-01 | 0.4807717E-02 | 0.1374784E-01 | 0.1727168E-01 | 0.2156224E-01 |
| 0.2509313E-01 | 0.4087500E-01 | 0.4807717E-02 | 0.4365868E-01 | 0.4432189E-01 | 0.4455244E-01 |
| 0.4402121E-01 | 0.4469633E-01 | 0.4453623E-01 | 0.4442505E-01 | 0.4438570E-01 | 0.4337353E-01 |
| 0.4200819E-01 | 0.4039820E-02 | 0.807422E-02 | 0.1205408E-01 | 0.1590848E-01 | 0.1957911E-01 |
| 0.231153E-01 | 0.4087500E-01 | 0.502765E-01 | 0.312582E-01 | 0.337469E-01 | 0.350175E-01 |
| 0.380167E-01 | 0.331010E-01 | 0.427431E-01 | 0.400408E-01 | 0.3509770E-01 | 0.3948055E-01 |
| 0.223128E-09 | 0.330536E-01 | 0.320536E-01 | 0.3904407E-01 | 0.301105E-01 | 0.3140771E-01 |
| 0.3323287E-01 | 0.4460045E-01 | 0.3108731E-01 | 0.3646265E-01 | 0.3762463E-01 | 0.3739862E-01 |
| 0.3308802E-01 | 0.3764540E-01 | 0.3108731E-01 | 0.3735348E-01 | 0.3704662E-01 | 0.3665411E-01 |
| 0.178978E-01 | 0.3076318E-02 | 0.6169942E-02 | 0.822371E-02 | 0.1223350E-01 | 0.1512836E-01 |
| 0.345488E-01 | 0.3076318E-02 | 0.243578E-01 | 0.352539E-01 | 0.4060716E-01 | 0.4866733E-01 |
| 0.338797E-01 | 0.3467526E-01 | 0.3467849E-01 | 0.345664E-01 | 0.3435408E-01 | 0.3405386E-01 |
| 0.1502011E-01 | 0.3216574E-02 | 0.545814E-02 | 0.8110911E-02 | 0.1082776E-01 | 0.1342385E-01 |
| 0.475581E-01 | 0.686284E-01 | 0.4294708E-01 | 0.3020191E-01 | 0.4243135E-01 | 0.3284768E-01 |
| 0.310618E-01 | 0.3197279E-01 | 0.328771E-01 | 0.5101194E-01 | 0.3095198E-01 | 0.3143937E-01 |
| 0.1185797E-08 | 0.4409344E-02 | 0.644601E-02 | 0.7260942E-02 | 0.2948307E-02 | 0.110714E-01 |
| 0.1541404E-01 | 0.1333607E-01 | 0.1333607E-01 | 0.2018312E-01 | 0.2189155E-01 | 0.2388311E-01 |
| 0.242337E-01 | 0.168889E-01 | 0.168889E-01 | 0.2570939E-01 | 0.2835175E-01 | 0.2888891E-01 |

FIGURE 23. Group B Sample Problems Program Results
(continued)

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|
| 0.2920585E-C1 | 0.2951442E-01 | 0.2964031E-01 | 0.2967188E-01 | 0.2970304E-0A | 0.2945001E-01 |
| 0.2921380E-C8 | 0.2952031E-02 | 0.2953198E-02 | 0.2954324E-02 | 0.2955450E-02 | 0.2956576E-01 |
| 0.2226379E-01 | 0.2227505E-01 | 0.2228631E-01 | 0.2229757E-01 | 0.2230883E-01 | 0.2232009E-01 |
| 0.2248494E-C1 | 0.2249620E-01 | 0.2250746E-01 | 0.2251872E-01 | 0.2252998E-01 | 0.2254124E-01 |
| 0.2724232E-C1 | 0.2725358E-01 | 0.2726484E-01 | 0.2727610E-01 | 0.2728736E-01 | 0.2729862E-01 |
| 0.1118597E-C8 | 0.1119723E-02 | 0.1120849E-02 | 0.1121975E-02 | 0.1123101E-02 | 0.1124227E-01 |
| 0.1153976E-C1 | 0.1155102E-01 | 0.1156228E-01 | 0.1157354E-01 | 0.1158480E-01 | 0.1159606E-01 |
| 0.2463032E-C1 | 0.2464158E-01 | 0.2465284E-01 | 0.2466410E-01 | 0.2467536E-01 | 0.2468662E-01 |
| 0.2357472E-C8 | 0.2358598E-02 | 0.2359724E-02 | 0.2360850E-02 | 0.2361976E-02 | 0.2363102E-01 |
| 0.1041595E-C1 | 0.1042721E-01 | 0.1043847E-01 | 0.1044973E-01 | 0.1046099E-01 | 0.1047225E-01 |
| 0.1878939E-C1 | 0.1880065E-01 | 0.1881191E-01 | 0.1882317E-01 | 0.1883443E-01 | 0.1884569E-01 |
| 0.2317424E-C1 | 0.2318550E-01 | 0.2319676E-01 | 0.2320802E-01 | 0.2321928E-01 | 0.2323054E-01 |
| 0.1778692E-C8 | 0.1779818E-02 | 0.1780944E-02 | 0.1782070E-02 | 0.1783196E-02 | 0.1784322E-01 |
| 0.1878939E-C1 | 0.1880065E-01 | 0.1881191E-01 | 0.1882317E-01 | 0.1883443E-01 | 0.1884569E-01 |
| 0.2115823E-C1 | 0.2116949E-01 | 0.2118075E-01 | 0.2119201E-01 | 0.2120327E-01 | 0.2121453E-01 |
| 0.2384492E-C8 | 0.2385618E-02 | 0.2386744E-02 | 0.2387870E-02 | 0.2388996E-02 | 0.2390122E-01 |
| 0.1978692E-C1 | 0.1979818E-01 | 0.1980944E-01 | 0.1982070E-01 | 0.1983196E-01 | 0.1984322E-01 |
| 0.2078692E-C1 | 0.2079818E-01 | 0.2080944E-01 | 0.2082070E-01 | 0.2083196E-01 | 0.2084322E-01 |
| 0.2078692E-C1 | 0.2079818E-01 | 0.2080944E-01 | 0.2082070E-01 | 0.2083196E-01 | 0.2084322E-01 |
| 0.1833015E-C1 | 0.1834141E-01 | 0.1835267E-01 | 0.1836393E-01 | 0.1837519E-01 | 0.1838645E-01 |
| 0.1453128E-C1 | 0.1454254E-01 | 0.1455380E-01 | 0.1456506E-01 | 0.1457632E-01 | 0.1458758E-01 |
| 0.1105797E-C8 | 0.1106923E-02 | 0.1108049E-02 | 0.1109175E-02 | 0.1110301E-02 | 0.1111427E-01 |
| 0.4494358E-C2 | 0.4495484E-02 | 0.4496610E-02 | 0.4497736E-02 | 0.4498862E-02 | 0.4499988E-01 |
| 0.1625738E-C1 | 0.1626864E-01 | 0.1627990E-01 | 0.1629116E-01 | 0.1630242E-01 | 0.1631368E-01 |
| 0.1887754E-C1 | 0.1888880E-01 | 0.1890006E-01 | 0.1891132E-01 | 0.1892258E-01 | 0.1893384E-01 |
| 0.2384492E-C8 | 0.2385618E-02 | 0.2386744E-02 | 0.2387870E-02 | 0.2388996E-02 | 0.2390122E-01 |
| 0.1161132E-C1 | 0.1162258E-01 | 0.1163384E-01 | 0.1164510E-01 | 0.1165636E-01 | 0.1166762E-01 |
| 0.1322288E-C1 | 0.1323414E-01 | 0.1324540E-01 | 0.1325666E-01 | 0.1326792E-01 | 0.1327918E-01 |
| 0.1893384E-C2 | 0.1894510E-02 | 0.1895636E-02 | 0.1896762E-02 | 0.1897888E-02 | 0.1899014E-01 |
| 0.4619575E-C2 | 0.4620701E-02 | 0.4621827E-02 | 0.4622953E-02 | 0.4624079E-02 | 0.4625205E-01 |

FIGURE 23. Group B Sample Problems Program Results
(continued)

COORDINATES OF POINTS ON BOUNDARY OF SURF * * * FOR EACH Y INTERVAL

| X-LEFT | X-RI,INT | Y | X-LEFT | X-RIGHT | Y |
|--------|--------------|--------------|--------|--------------|---------------|
| 0. | 0.600000E-01 | 0. | 0. | 0.600000E-01 | 0.3359274E-00 |
| 0. | 0.600000E-01 | 0.371648E-00 | 0. | 0.600000E-01 | 0.3359274E-00 |
| 0. | 0.600000E-01 | 0.114717E-01 | 0. | 0.600000E-01 | 0.1030792E-01 |
| 0. | 0.600000E-01 | 0.201564E-01 | 0. | 0.600000E-01 | 0.1030792E-01 |
| 0. | 0.600000E-01 | 0.318527E-01 | 0. | 0.600000E-01 | 0.2351149E-01 |
| 0. | 0.600000E-01 | 0.318527E-01 | 0. | 0.600000E-01 | 0.302347E-01 |
| 0. | 0.551732E-01 | 0.453112E-01 | 0. | 0.600000E-01 | 0.476709E-01 |
| 0. | 0.551732E-01 | 0.517281E-01 | 0. | 0.518294E-01 | 0.476709E-01 |
| 0. | 0.517281E-01 | 0.654693E-01 | 0. | 0.517281E-01 | 0.503931E-01 |
| 0. | 0.517281E-01 | 0.654693E-01 | 0. | 0.517281E-01 | 0.638202E-01 |
| 0. | 0.517281E-01 | 0.718042E-01 | 0. | 0.517281E-01 | 0.638202E-01 |
| 0. | 0.517281E-01 | 0.718042E-01 | 0. | 0.517281E-01 | 0.762472E-01 |
| 0. | 0.734015E-00 | 0.368225E-01 | 0. | 0.115382E-01 | 0.772633E-01 |

NO. OF HORIZONTAL INCREMENTS= 24 NO. OF VERTICAL INCREMENTS= 24

THE FOLLOWING ARC PLANE POINT COORDINATION FACTORS COMPUTED FOR THIS RUN
 LONGEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

| | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|
| 0.550079E-01 | 0.551698E-01 | 0.554651E-01 | 0.537728E-01 | 0.628153E-01 | 0.514817E-01 |
| 0.553816E-01 | 0.577624E-01 | 0.535050E-01 | 0.535250E-01 | 0.517050E-01 | 0.514809E-01 |
| 0.553816E-01 | 0.551402E-01 | 0.231505E-01 | 0.212328E-01 | 0.193907E-01 | 0.176280E-01 |
| 0.577624E-01 | 0.574517E-01 | 0.560004E-01 | 0.559473E-01 | 0.545014E-01 | 0.531816E-01 |
| 0.577624E-01 | 0.593721E-01 | 0.484592E-01 | 0.479747E-01 | 0.450832E-01 | 0.429079E-01 |
| 0.577624E-01 | 0.620166E-01 | 0.330084E-01 | 0.340316E-01 | 0.337597E-01 | 0.324804E-01 |
| 0.577624E-01 | 0.601000E-01 | 0.490200E-01 | 0.479747E-01 | 0.450832E-01 | 0.429079E-01 |
| 0.577624E-01 | 0.522505E-01 | 0.530775E-01 | 0.537800E-01 | 0.548824E-01 | 0.559031E-01 |
| 0.577624E-01 | 0.592009E-01 | 0.426404E-01 | 0.424244E-01 | 0.418027E-01 | 0.414800E-01 |
| 0.577624E-01 | 0.484806E-01 | 0.228404E-01 | 0.205228E-01 | 0.185047E-01 | 0.159246E-01 |
| 0.610037E-01 | 0.610037E-01 | 0.638248E-01 | 0.598160E-01 | 0.568312E-01 | 0.531329E-01 |
| 0.550079E-01 | 0.550079E-01 | 0.517507E-01 | 0.493868E-01 | 0.470650E-01 | 0.446351E-01 |

FIGURE 23. Group B Sample Problems Program Results
 (continued)

| | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|
| 0.421232E+01 | 0.395553E+01 | 0.369281E+01 | 0.343658E+01 | 0.317754E+01 | 0.292358E+01 |
| 0.253795E+01 | 0.243576E+01 | 0.225030E+01 | 0.197463E+01 | 0.177558E+01 | 0.157836E+01 |
| 0.619211E+01 | 0.613474E+01 | 0.624665E+01 | 0.613979E+01 | 0.605607E+01 | 0.584791E+01 |
| 0.560782E+01 | 0.560320E+01 | 0.547998E+01 | 0.501239E+01 | 0.471280E+01 | 0.440248E+01 |
| 0.201034E+01 | 0.200617E+01 | 0.242062E+01 | 0.189901E+01 | 0.167995E+01 | 0.147612E+01 |
| 0.128771E+01 | 0.128771E+01 | 0.653414E+01 | 0.626631E+01 | 0.611923E+01 | 0.590122E+01 |
| 0.655468E+01 | 0.652465E+01 | 0.352282E+01 | 0.344938E+01 | 0.302210E+01 | 0.278424E+01 |
| 0.271403E+01 | 0.272571E+01 | 0.225271E+01 | 0.177859E+01 | 0.155638E+01 | 0.135158E+01 |
| 0.411742E+01 | 0.650580E+01 | 0.646267E+01 | 0.635212E+01 | 0.619004E+01 | 0.600939E+01 |
| 0.665926E+01 | 0.652589E+01 | 0.526284E+01 | 0.504218E+01 | 0.476113E+01 | 0.446440E+01 |
| 0.218623E+01 | 0.218623E+01 | 0.252058E+01 | 0.182513E+01 | 0.162508E+01 | 0.149412E+01 |
| 0.191413E+01 | 0.664401E+01 | 0.654219E+01 | 0.639192E+01 | 0.622044E+01 | 0.602160E+01 |
| 0.652949E+01 | 0.647407E+01 | 0.374071E+01 | 0.311133E+01 | 0.280409E+01 | 0.250272E+01 |
| 0.573653E+01 | 0.175863E+01 | 0.175863E+01 | 0.163982E+01 | 0.123864E+01 | 0.101195E+01 |
| 0.622380E+01 | 0.615643E+01 | 0.652116E+01 | 0.637311E+01 | 0.619283E+01 | 0.597803E+01 |
| 0.573653E+01 | 0.378198E+01 | 0.328205E+01 | 0.448679E+01 | 0.426671E+01 | 0.442432E+01 |
| 0.618642E+01 | 0.618642E+01 | 0.149600E+01 | 0.148282E+01 | 0.163004E+01 | 0.161823E+02 |
| 0.612345E+01 | 0.600768E+01 | 0.647261E+01 | 0.630432E+01 | 0.610491E+01 | 0.587603E+01 |
| 0.317124E+01 | 0.317124E+01 | 0.104006E+01 | 0.276319E+01 | 0.238746E+01 | 0.208442E+01 |
| 0.443811E+02 | 0.443811E+02 | 0.152561E+01 | 0.103884E+01 | 0.824661E+02 | 0.824661E+02 |
| 0.543717E+01 | 0.514621E+01 | 0.646786E+01 | 0.641560E+01 | 0.631643E+01 | 0.570784E+01 |
| 0.356837E+01 | 0.311007E+01 | 0.276355E+01 | 0.449789E+01 | 0.411640E+01 | 0.380937E+01 |
| 0.211594E+01 | 0.162820E+01 | 0.101691E+01 | 0.243801E+01 | 0.211978E+01 | 0.181704E+01 |
| 0.664721E+01 | 0.618328E+01 | 0.615308E+01 | 0.592854E+01 | 0.573023E+01 | 0.547327E+01 |
| 0.315131E+01 | 0.280372E+01 | 0.455146E+01 | 0.421171E+01 | 0.386510E+01 | 0.350286E+01 |
| 0.173957E+01 | 0.173957E+01 | 0.743207E+02 | 0.526440E+01 | 0.336403E+01 | 0.154327E+02 |
| 0.999979E+01 | 0.999979E+01 | 0.591914E+01 | 0.572791E+01 | 0.556007E+01 | 0.526444E+01 |

FIGURE 23. Group B Sample Problems Program Results
(continued)

FIGURE 23. Group B Sample Problems Program Results (continued)

| | | | | | |
|----------------|----------------|----------------|----------------|----------------|----------------|
| 0.499653E-C1 | 0.470854E-C1 | 0.440356E-F-01 | 0.440844E-F-01 | 0.352166E-01 | 0.382874E-01 |
| 0.125511E-C1 | 0.659040E-01 | 0.742339E-02 | 0.742339E-02 | 0.364170E-01 | 0.163814E-02 |
| 0.455462E-C8 | 0.577813E-C1 | 0.259176E-01 | 0.352641E-01 | 0.565245E-01 | 0.789370E-01 |
| 0.321005E-C1 | 0.267714E-C1 | 0.237325E-F-01 | 0.237325E-F-01 | 0.178664E-01 | 0.131243E-01 |
| 0.289516E-C1 | 0.160026E-01 | 0.787766E-F-02 | 0.531190E-F-02 | 0.350940E-F-02 | 0.167273E-02 |
| 0.114922E-C1 | 0.541267E-C1 | 0.525676E-01 | 0.508049E-01 | 0.448546E-01 | 0.467114E-01 |
| 0.354743E-C1 | 0.419132E-01 | 0.339248E-01 | 0.382216E-01 | 0.339740E-01 | 0.311764E-01 |
| 0.444100E-C1 | 0.252231E-01 | 0.760576E-02 | 0.592974E-02 | 0.530072E-02 | 0.166493E-02 |
| 0.446673E-C8 | 0.499162E-01 | 0.494172E-F-01 | 0.467475E-01 | 0.449372E-01 | 0.429752E-01 |
| 0.312608E-C1 | 0.239022E-01 | 0.213727E-01 | 0.188913E-01 | 0.164381E-01 | 0.140970E-01 |
| 0.266520E-C1 | 0.951366E-02 | 0.728761E-02 | 0.536841E-02 | 0.346094E-02 | 0.167071E-02 |
| 0.117752E-C1 | 0.452031E-C1 | 0.438271E-F-01 | 0.422820E-02 | 0.406180E-F-01 | 0.388415E-F-01 |
| 0.440512E-C8 | 0.349624E-C1 | 0.334244E-C1 | 0.362374E-01 | 0.289235E-01 | 0.264413E-01 |
| 0.319628E-C1 | 0.235975E-01 | 0.177238E-C1 | 0.174831E-01 | 0.152870E-01 | 0.131208E-01 |
| 0.220297E-C1 | 0.858979E-02 | 0.781978E-02 | 0.573131E-02 | 0.352474E-02 | 0.181929E-02 |
| 0.414661E-C1 | 0.462639E-02 | 0.339483E-C1 | 0.375044E-01 | 0.360027E-01 | 0.344228E-01 |
| 0.252139E-C8 | 0.151075E-01 | 0.177608E-01 | 0.181909E-01 | 0.138970E-01 | 0.119842E-01 |
| 0.191813E-C1 | 0.828732E-02 | 0.656573E-02 | 0.478319E-C2 | 0.312115E-02 | 0.122403E-02 |
| 0.271379E-C8 | 0.856612E-01 | 0.330084E-01 | 0.325483E-01 | 0.312243E-F-01 | 0.298412E-F-01 |
| 0.244027E-01 | 0.269174E-01 | 0.233844E-01 | 0.236435E-01 | 0.221224E-01 | 0.205450E-01 |
| 0.189358E-C1 | 0.172958E-01 | 0.150443E-01 | 0.139509E-C1 | 0.132394E-F-01 | 0.107316E-F-01 |
| 0.168224E-C8 | 0.743061E-C2 | 0.585893E-02 | 0.483309E-02 | 0.284772E-02 | 0.139762E-02 |
| 0.307924E-C1 | 0.296712E-01 | 0.286439E-01 | 0.275452E-01 | 0.264023E-01 | 0.242224E-01 |
| 0.140171E-C1 | 0.647581E-01 | 0.271595E-01 | 0.195071E-01 | 0.164711E-01 | 0.148697E-01 |
| 0.781454E-C2 | 0.665762E-02 | 0.511809E-F-02 | 0.379920E-F-02 | 0.230453E-F-02 | 0.137178E-C2 |
| 0.528284E-C9 | 0.246531E-01 | 0.217004E-F-01 | 0.163307E-01 | 0.144644E-01 | 0.104820E-01 |
| 0.162700E-C1 | 0.118640E-01 | 0.117400E-F-01 | 0.105346E-01 | 0.114534E-01 | 0.143597E-01 |
| 0.112337E-C1 | 0.141397E-F-01 | 0.110194E-F-01 | 0.989465E-02 | 0.877038E-02 | 0.164616E-02 |
| 0.652236E-F-02 | 0.541035E-02 | 0.443034E-F-01 | 0.332860E-02 | 0.212259E-F-02 | 0.135308E-F-02 |

FIGURE 23. Group B Sample Problems Program Results
(continued)

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|
| 0.201026_E-C4 | 0.193419E-01 | 0.1884237E-01 | 0.178843E-01 | 0.17143E-01 | 0.161921E-01 |
| 0.152576E-01 | 0.147119E-01 | 0.1438477E-01 | 0.1350473E-01 | 0.1224039E-01 | 0.113642E-01 |
| 0.457349E-02 | 0.431587E-02 | 0.415224E-02 | 0.3859230E-02 | 0.3497891E-02 | 0.3097267E-02 |
| 0. | 0.433894E-02 | 0.415699E-02 | 0.359021E-02 | 0.1718535E-02 | 0.834594E-03 |
| 0.111800E-01 | 0.109266E-01 | 0.100788E-01 | 0.134537E-01 | 0.1284228E-01 | 0.112434E-01 |
| 0.735677E-02 | 0.716228E-02 | 0.650311E-02 | 0.590774E-02 | 0.52722E-02 | 0.469902E-02 |
| 0.393784E-02 | 0.327994E-02 | 0.2841180E-02 | 0.196349E-02 | 0.1367028E-02 | 0.651337E-03 |
| 0.1051084E-01 | 0.04274E-01 | 0.970507E-02 | 0.934320E-02 | 0.891454E-02 | 0.841081E-02 |
| 0.805458E-02 | 0.763205E-02 | 0.719849E-02 | 0.675301E-02 | 0.617344E-02 | 0.551210E-02 |
| 0.273549E-02 | 0.228644E-02 | 0.1825368E-02 | 0.499369E-02 | 0.368222E-02 | 0.28814E-02 |
| 0. | 0.228644E-02 | 0.1825368E-02 | 0.1369939E-02 | 0.9126860E-03 | 0.453272E-03 |
| 0.441084E-02 | 0.414274E-02 | 0.389676E-02 | 0.342224E-02 | 0.323245E-02 | 0.311363E-02 |
| 0.346308E-02 | 0.259483E-02 | 0.212375E-02 | 0.145500E-02 | 0.118197E-02 | 0.135035E-02 |
| 0.184211E-02 | 0.1329680E-02 | 0.1098564E-02 | 0.823284E-03 | 0.3400740E-03 | 0.274609E-04 |

FIGURE 23. Group B Sample Problems Program Results
(continued)

HAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (61)-K.A."DUPS", 1/63

RUN NO. 4 DATA USED FOR THIS RUN= *DISK *DISK*
DISK
DISK

*THE FORM FACTOR FROM SURFACE *DISK * TO SURFACE *DISK *DISK* = 0.0.901

*THE EXCHANGE COEFFICIENT (FA) = 0.50423E 00 50 UNITS

*THE MAPPING AREA = 0.2467100E 02 50 UNITS

*ONLY A PART OF SURFACE *DISK * * COMPRISING AN AREA OF 0.2467100E 02 50 UNITS,
SEES SURFACE *DISK *DISK*

*THE AREA OF SURFACE *DISK * = 0.2545584E 02 50 UNITS.

*THE AREA OF SURFACE *DISK *DISK* = 0.2545584E 02 50 UNITS.

*THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION=

***** DATA NAME= *DISK *

| POINT | Z | X | Y | Z | X | Y |
|-------|----------------|---------------|-----|----------------|---------------|----|
| 1 | -0. | 0.999997E 00 | -0. | 0.999997E 00 | 0. | 0. |
| 2 | -0. | 0.1433588E 01 | -0. | 0.226902E 01 | -0.246800E 01 | 0. |
| 3 | 0. | 0.3015382E 01 | 0. | 0.226902E 01 | 0.246800E 01 | 0. |
| 4 | 0. | 0.1433588E 01 | 0. | 0.226902E 01 | 0.246800E 01 | 0. |
| 5 | 0. | 0.1433588E 01 | 0. | 0.226902E 01 | 0.246800E 01 | 0. |
| 6 | 0. | 0.1433588E 01 | 0. | 0.226902E 01 | 0.246800E 01 | 0. |
| 7 | 0. | 0.1433588E 01 | 0. | 0.226902E 01 | 0.246800E 01 | 0. |
| 8 | 0. | 0.1433588E 01 | 0. | 0.226902E 01 | 0.246800E 01 | 0. |
| 9 | -0.1623231E 01 | 0.1422558E 01 | 0. | -0.1623231E 01 | 0.1422558E 01 | 0. |

***** DATA NAME= *DISK *DISK*

| POINT | Z | X | Y | Z | X | Y |
|-------|------------|--------------|------------|------------|--------------|------------|
| 1 | 0.6402E 01 | 0.344509E 01 | 0.6402E 01 | 0.6402E 01 | 0.344509E 01 | 0.6402E 01 |
| 2 | 0.6402E 01 | 0.344509E 01 | 0.6402E 01 | 0.6402E 01 | 0.344509E 01 | 0.6402E 01 |
| 3 | 0.6402E 01 | 0.344509E 01 | 0.6402E 01 | 0.6402E 01 | 0.344509E 01 | 0.6402E 01 |

FIGURE 23. Group B Sample Problems Program Results
(continued)

5 0.4505811E 01 0.3746827E 01 0.5620974E 01 8 0.4451845E 01 0.4623187E 01 0.3760598E 01
 7 0.5007741E 01 0.4495225E 01 0.3999999E 01 8 0.4288433E 01 0.2603110E 01 0.3760598E 01

COORDINATES OF POINTS ON BOUNDARY OF SUMF *SDISK * FOR EACH Y INTERVAL

| X-LEFT | X-RL-INT | Y | X-LEFT | X-RIGHT | Y |
|----------------|---------------|----------------|----------------|---------------|---------------|
| -0.4431392E+00 | 0.2265101E 01 | -0.4419397E+00 | -0.2309697E+00 | 0.2527073E 01 | 0.2309698E+00 |
| 0.233795E+00 | 0.221998E 01 | 0.933876E 00 | -0.6521802E+00 | 0.228901E 01 | 0.6940951E 00 |
| 0.2248418E+01 | 0.3919897E 01 | 0.1847758E 01 | -0.1154658E 01 | 0.349095E 01 | 0.1154658E 01 |
| -0.1622588E 01 | 0.3919897E 01 | 0.1847758E 01 | -0.1233588E 01 | 0.391989E 01 | 0.2078182E 01 |
| 0.1622588E 01 | 0.3919897E 01 | 0.3307698E 01 | -0.1233588E 01 | 0.391989E 01 | 0.2506448E 01 |
| -0.1622588E 01 | 0.3919897E 01 | 0.3307698E 01 | -0.1233588E 01 | 0.391989E 01 | 0.3444548E 01 |
| 0.1622588E 01 | 0.3442812E 01 | 0.393517E 01 | -0.1618789E 01 | 0.337134E 04 | 0.394687E 01 |
| -0.1622588E 01 | 0.3442812E 01 | 0.393517E 01 | -0.1618789E 01 | 0.337134E 04 | 0.4818018E 01 |
| 0.4451937E+00 | 0.2756033E 01 | 0.558137E 01 | -0.6286095E 00 | 0.228901E 01 | 0.4818018E 01 |
| -0.4451937E+00 | 0.2756033E 01 | 0.558137E 01 | -0.2309698E+00 | 0.2527073E 01 | 0.3312104E 01 |
| 0.1933684E+01 | 0.1724156E 01 | 0.1724156E 01 | 0.1926895E+01 | 0.1979181E 01 | 0.2081821E 01 |
| 0.2248418E+01 | 0.2055435E 01 | 0.2055435E 01 | 0.2052390E+01 | 0.2056623E 01 | 0.2043350E 01 |
| 0.2545374E+01 | 0.2755923E 01 | 0.2755923E 01 | 0.2012630E+01 | 0.1998499E 01 | 0.1981900E 01 |
| 0.1931100E+01 | 0.1959094E 01 | 0.1979181E 01 | 0.1997421E 01 | 0.2015736E 01 | 0.2032980E 01 |
| 0.2545374E+01 | 0.260478E 01 | 0.260478E 01 | 0.2088937E 01 | 0.2098885E 01 | 0.210709E 01 |
| 0.2074949E+01 | 0.260478E 01 | 0.260478E 01 | 0.2088937E 01 | 0.2098885E 01 | 0.210709E 01 |
| 0.1904251E+01 | 0.260478E 01 | 0.260478E 01 | 0.2088937E 01 | 0.2098885E 01 | 0.210709E 01 |
| 0.1904251E+01 | 0.1724156E 01 | 0.1724156E 01 | 0.2088937E 01 | 0.2098885E 01 | 0.210709E 01 |
| 0.2248418E+01 | 0.2182481E 01 | 0.2182481E 01 | 0.2180481E 01 | 0.2173744E 01 | 0.2163597E 01 |
| 0.2248418E+01 | 0.2182481E 01 | 0.2182481E 01 | 0.2180481E 01 | 0.2173744E 01 | 0.2163597E 01 |
| 0.1926936E+01 | 0.2122233E 01 | 0.2122233E 01 | 0.2085366E 01 | 0.2056003E 01 | 0.1979822E 01 |

NO. OF HORIZONTAL INCREMENTS= 24 NO. OF VERTICAL INCREMENTS= 24

THE FOLLOWING ARE PLANE PLIGHT CONFIGURATION FACTORS COMPUTED FOR THIS RUN
 LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|
| 0.1926936E+01 | 0.1933684E+01 | 0.1724156E 01 | 0.1926895E+01 | 0.1979181E 01 | 0.2081821E 01 |
| 0.2248418E+01 | 0.2248418E+01 | 0.2055435E 01 | 0.2052390E+01 | 0.2056623E 01 | 0.2043350E 01 |
| 0.2545374E+01 | 0.2545374E+01 | 0.2755923E 01 | 0.2012630E+01 | 0.1998499E 01 | 0.1981900E 01 |
| 0.1931100E+01 | 0.1959094E 01 | 0.1979181E 01 | 0.1997421E 01 | 0.2015736E 01 | 0.2032980E 01 |
| 0.2545374E+01 | 0.260478E 01 | 0.260478E 01 | 0.2088937E 01 | 0.2098885E 01 | 0.210709E 01 |
| 0.2074949E+01 | 0.260478E 01 | 0.260478E 01 | 0.2088937E 01 | 0.2098885E 01 | 0.210709E 01 |
| 0.1904251E+01 | 0.260478E 01 | 0.260478E 01 | 0.2088937E 01 | 0.2098885E 01 | 0.210709E 01 |
| 0.1904251E+01 | 0.1724156E 01 | 0.1724156E 01 | 0.2088937E 01 | 0.2098885E 01 | 0.210709E 01 |
| 0.2248418E+01 | 0.2182481E 01 | 0.2182481E 01 | 0.2180481E 01 | 0.2173744E 01 | 0.2163597E 01 |
| 0.2248418E+01 | 0.2182481E 01 | 0.2182481E 01 | 0.2180481E 01 | 0.2173744E 01 | 0.2163597E 01 |
| 0.1926936E+01 | 0.2122233E 01 | 0.2122233E 01 | 0.2085366E 01 | 0.2056003E 01 | 0.1979822E 01 |

FIGURE 23. Group B Sample Problems Program Results
 (continued)

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|
| 0.1939185E-01 | 0.1973327E-01 | 0.2006445E-04 | 0.2038035E-01 | 0.2050977E-01 | 0.2095514E-01 |
| 0.217290E-01 | 0.2154005E-01 | 0.2176337E-01 | 0.2166931E-01 | 0.2214272E-01 | 0.222396E-01 |
| 0.228277E-01 | 0.227560E-01 | 0.2281225E-01 | 0.2280495E-01 | 0.2300935E-01 | 0.230877E-01 |
| 0.1887365E-02 | 0.1927445E-01 | 0.190658E-01 | 0.190446E-01 | 0.1928486E-01 | 0.193541E-01 |
| 0.197244E-01 | 0.196958E-01 | 0.1970778E-01 | 0.195446E-01 | 0.195446E-01 | 0.215446E-01 |
| 0.215700E-01 | 0.2153144E-01 | 0.2105468E-01 | 0.2194175E-01 | 0.227296E-01 | 0.225087E-01 |
| 0.2215305E-01 | 0.216330E-01 | 0.2104065E-01 | 0.2027011E-01 | 0.1930594E-01 | 0.193323E-01 |
| 0.190769E-01 | 0.1956216E-01 | 0.2004024E-01 | 0.205599E-01 | 0.209470E-01 | 0.214084E-01 |
| 0.218278E-01 | 0.222013E-01 | 0.225737E-01 | 0.228966E-01 | 0.231608E-01 | 0.232768E-01 |
| 0.222601E-01 | 0.222601E-01 | 0.220769E-01 | 0.215799E-01 | 0.2182969E-01 | 0.215799E-01 |
| 0.149936E-01 | 0.149936E-01 | 0.150169E-01 | 0.150431E-01 | 0.150961E-01 | 0.15111E-01 |
| 0.220117E-01 | 0.224977E-01 | 0.230605E-01 | 0.232863E-01 | 0.236014E-01 | 0.238107E-01 |
| 0.240244E-01 | 0.240871E-01 | 0.240261E-01 | 0.238373E-01 | 0.234728E-01 | 0.229446E-01 |
| 0.221037E-01 | 0.212064E-01 | 0.196844E-01 | 0.1844100E-01 | 0.166105E-01 | 0.145039E-01 |
| 0.188479E-01 | 0.191009E-01 | 0.197229E-01 | 0.203431E-01 | 0.209357E-01 | 0.215446E-01 |
| 0.221592E-01 | 0.227294E-01 | 0.231768E-01 | 0.230773E-01 | 0.230974E-01 | 0.229392E-01 |
| 0.233333E-01 | 0.233333E-01 | 0.233333E-01 | 0.233333E-01 | 0.233333E-01 | 0.233333E-01 |
| 0.218623E-01 | 0.203176E-01 | 0.180578E-01 | 0.167039E-01 | 0.147315E-01 | 0.111700E-01 |
| 0.773514E-02 | 0.193403E-01 | 0.190849E-01 | 0.200364E-01 | 0.215446E-01 | 0.248793E-01 |
| 0.226477E-01 | 0.230478E-01 | 0.234493E-01 | 0.240084E-01 | 0.243949E-01 | 0.246651E-01 |
| 0.242678E-01 | 0.244082E-01 | 0.247817E-01 | 0.245574E-01 | 0.242698E-01 | 0.240214E-01 |
| 0.219128E-01 | 0.204432E-01 | 0.185580E-01 | 0.162376E-01 | 0.134450E-01 | 0.101009E-01 |
| 0.189107E-01 | 0.197569E-01 | 0.202256E-01 | 0.208800E-01 | 0.215446E-01 | 0.221898E-01 |
| 0.227644E-01 | 0.233444E-01 | 0.238102E-01 | 0.243800E-01 | 0.247774E-01 | 0.250184E-01 |
| 0.242678E-01 | 0.242678E-01 | 0.242678E-01 | 0.242678E-01 | 0.242678E-01 | 0.242678E-01 |
| 0.218900E-01 | 0.202945E-01 | 0.181944E-01 | 0.156930E-01 | 0.125890E-01 | 0.888280E-02 |
| 0.460256E-02 | 0.095159E-01 | 0.205385E-01 | 0.210914E-01 | 0.215446E-01 | 0.223078E-01 |
| 0.230106E-01 | 0.235914E-01 | 0.241586E-01 | 0.246641E-01 | 0.249917E-01 | 0.252750E-01 |
| 0.235289E-01 | 0.235289E-01 | 0.235289E-01 | 0.244000E-01 | 0.244105E-01 | 0.243008E-01 |
| 0.217240E-01 | 0.199325E-01 | 0.176712E-01 | 0.168912E-01 | 0.151331E-01 | 0.125934E-02 |
| 0.192336E-01 | 0.199119E-01 | 0.205890E-01 | 0.212654E-01 | 0.219272E-01 | 0.225396E-01 |
| 0.232389E-01 | 0.237965E-01 | 0.243344E-01 | 0.248806E-01 | 0.251107E-01 | 0.252008E-01 |
| 0.244444E-01 | 0.244444E-01 | 0.244444E-01 | 0.244444E-01 | 0.244444E-01 | 0.244444E-01 |
| 0.214278E-01 | 0.194434E-01 | 0.159362E-01 | 0.119304E-01 | 0.102753E-01 | 0.556343E-02 |

FIGURE 23. Group B Sample Problems Program Results (continued)

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|
| 0.18712231-C1 | 0.1469667E-01 | 0.1774026E-01 | 0.1020759E-01 | 0.7262815E-01 | 0.3871211E-02 |
| 0.2052241E-01 | 0.2083680E-01 | 0.2112693E-01 | 0.2138755E-01 | 0.2167895E-01 | 0.2175445E-01 |
| 0.2593095E-01 | 0.252891E-01 | 0.250366E-01 | 0.2192205E-01 | 0.2179115E-01 | 0.2154058E-01 |
| 0.3150240E-01 | 0.3137866E-01 | 0.3178401E-01 | 0.2465712E-01 | 0.2810302E-01 | 0.3735103E-02 |
| 0.3869137E-01 | 0.569374E-01 | 0.2086409E-01 | 0.2102354E-01 | 0.2114125E-01 | 0.2129295E-01 |
| 0.4726642E-01 | 0.212424E-01 | 0.2117964E-01 | 0.2104035E-01 | 0.2082875E-01 | 0.2032748E-01 |
| 0.2013817E-01 | 0.1964205E-01 | 0.1903066E-01 | 0.1828974E-01 | 0.1740607E-01 | 0.1636316E-01 |
| 0.1912164E-01 | 0.1374866E-01 | 0.1213976E-01 | 0.1030898E-01 | 0.8722335E-02 | 0.5898336E-02 |
| 0.2017882E-01 | 0.2629373E-01 | 0.203835E-01 | 0.2044466E-01 | 0.2047341E-01 | 0.2046622E-01 |
| 0.2041981E-01 | 0.2032884E-01 | 0.2018871E-01 | 0.1997440E-01 | 0.1976029E-01 | 0.192641E-01 |
| 0.1934875E-01 | 0.186168E-01 | 0.182354E-01 | 0.180429E-01 | 0.178281E-01 | 0.174241E-01 |
| 0.5385244E-01 | 0.136106E-01 | 0.123254E-01 | 0.108429E-01 | 0.937837E-02 | 0.7615011E-02 |
| 0.5395244E-01 | 0.192763E-01 | 0.185631E-01 | 0.186205E-01 | 0.1857915E-01 | 0.180828E-01 |
| 0.5394875E-01 | 0.172675E-01 | 0.169297E-01 | 0.163331E-01 | 0.1574735E-01 | 0.1504665E-01 |
| 0.1188168E-01 | 0.174057E-01 | 0.169297E-01 | 0.163331E-01 | 0.1574735E-01 | 0.1504665E-01 |
| 0.1826082E-01 | 0.1146081E-01 | 0.1144359E-01 | 0.1137003E-01 | 0.1023466E-01 | 0.8970473E-02 |
| 0.1391819E-01 | | | | | |

FIGURE 23. Group B Sample Problems Program Results
(continued)

NAA COMPAC II REPORT SAMPLE PROBLEMS FROM FIG. 10)-P-A-TOUPS,11/1/63

```

RUN NO. 5 DATA USED FOR THIS RUN= *3DISK *1PLAT1*
          *91DISK*
          *D
          *
THE FORM FACTOR FROM SURFACE *3DISK *91DISK* TO SURFACE *1PLAT1 * = 0.04739
THE EXCHANGE COEFFICIENT (FA) = 0.12034E 01 30 UNITS
          THE MAPPING AREA = 0.2542277E 01 30 UNITS
THE AREA OF SURFACE *3DISK *91DISK* = 6.2545584E 02 30 UNITS.
ONLY A PART OF SURFACE *1PLAT1
SEE SURFACE *3DISK *91DISK*
          *, COMPRISING AN AREA OF 0.3688701E 02 30 UNITS.
THE AREA OF SURFACE *1PLAT1 * = 0.4937355E 02 30 UNITS.

```

THE FOLLOWING ARE THE (FIRIAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

```

***** DATA NAME= *3DISK *91DISK*
POINT X Y Z POINT X Y Z
1 0. 0. -0. 1.100000E 01---(INTERNALLY GENERATED ORIENTATION VECTOR) Z
2 0.254964E 01 0.4223588E 01 0. 4 0.3919687E 01 0.3919687E 01 0.
3 0.254964E 01 0.4223588E 01 0. 5 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
7 -0.1623567E 01 0.3919688E 01 0. 6 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
          8 -0.1623567E 01 0.3919687E 01 0.1623588E 01 0.

```

```

***** DATA NAME= *1PLAT1. *
POINT X Y Z POINT X Y Z
1 -0.1608478E 01 -0.911003E 00 0.631531E 01---(INTERNALLY GENERATED ORIENTATION VECTOR) Z
2 -0.4021187E 01 -0.4218442E 01 0.6399990E 01 2 -0.3664935E 01 -0.5074852E 01 0.2774745E 0
3 -0.2115526E 01 -0.3395928E 01 0. 4 -0.7171818E 01 0.2545583E 01 0.
7 -0.3771257E 01 0.313543E 01 0.4664098E 00

```

FIGURE 13. Group B Sample Problems Program Results
(continued)

| | | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 0.154452E-01 | 0.458152E-01 | 0.453254E-01 | 0.453761E-01 | 0.451415E-01 | 0.451402E-01 | 0.451402E-01 |
| 0.255044E-01 | 0.455044E-01 | 0.453254E-01 | 0.453761E-01 | 0.451415E-01 | 0.451402E-01 | 0.451402E-01 |
| 0.110934E-01 | 0.402714E-00 | 0.399101E-01 | 0.404230E-01 | 0.404230E-01 | 0.404230E-01 | 0.404230E-01 |
| 0.271234E-01 | 0.456338E-01 | 0.454733E-01 | 0.454634E-01 | 0.454634E-01 | 0.454634E-01 | 0.454634E-01 |
| 0.444562E-01 | 0.422393E-01 | 0.410950E-01 | 0.418228E-01 | 0.418228E-01 | 0.418228E-01 | 0.418228E-01 |
| 0.113264E-01 | 0.101285E-00 | 0.101394E-00 | 0.095760E-01 | 0.094834E-01 | 0.094834E-01 | 0.095102E-01 |
| 0.400213E-01 | 0.764027E-01 | 0.744140E-01 | 0.668225E-01 | 0.646331E-01 | 0.646331E-01 | 0.611604E-01 |
| 0.278212E-01 | 0.548105E-01 | 0.513254E-01 | 0.499393E-01 | 0.486361E-01 | 0.486361E-01 | 0.442255E-01 |
| 0.108314E-01 | 0.398603E-01 | 0.370938E-01 | 0.373761E-01 | 0.373761E-01 | 0.373761E-01 | 0.325293E-01 |
| 0.115538E-01 | 0.109712E-00 | 0.102724E-00 | 0.962274E-01 | 0.905404E-01 | 0.905404E-01 | 0.891380E-01 |
| 0.398460E-01 | 0.227757E-01 | 0.497820E-01 | 0.662756E-01 | 0.644444E-01 | 0.644444E-01 | 0.418837E-01 |
| 0.397614E-01 | 0.374137E-01 | 0.353872E-01 | 0.334872E-01 | 0.334872E-01 | 0.334872E-01 | 0.300326E-01 |
| 0.116893E-01 | 0.109310E-00 | 0.104450E-00 | 0.962084E-01 | 0.901781E-01 | 0.901781E-01 | 0.845330E-01 |
| 0.244631E-01 | 0.402970E-01 | 0.476657E-01 | 0.446010E-01 | 0.413091E-01 | 0.413091E-01 | 0.373376E-01 |
| 0.284772E-01 | 0.354825E-01 | 0.334216E-01 | 0.314236E-01 | 0.294666E-01 | 0.294666E-01 | 0.278160E-01 |
| 0.110399E-01 | 0.104660E-01 | 0.973492E-01 | 0.914036E-01 | 0.858219E-01 | 0.858219E-01 | 0.803816E-01 |
| 0.330848E-01 | 0.477443E-01 | 0.602537E-01 | 0.631814E-01 | 0.607782E-01 | 0.607782E-01 | 0.484039E-01 |
| 0.367444E-01 | 0.342405E-01 | 0.324897E-01 | 0.303869E-01 | 0.286890E-01 | 0.286890E-01 | 0.271066E-01 |
| 0.232002E-01 | 0.377253E-01 | 0.373540E-01 | 0.465162E-01 | 0.419384E-01 | 0.419384E-01 | 0.365829E-01 |
| 0.308848E-01 | 0.677161E-01 | 0.637532E-01 | 0.596878E-01 | 0.564535E-01 | 0.564535E-01 | 0.531377E-01 |
| 0.260928E-01 | 0.331172E-01 | 0.312748E-01 | 0.295490E-01 | 0.279328E-01 | 0.279328E-01 | 0.264183E-01 |
| 0.374465E-01 | 0.410788E-01 | 0.466691E-01 | 0.481719E-01 | 0.477034E-01 | 0.477034E-01 | 0.428113E-01 |
| 0.428482E-01 | 0.450794E-01 | 0.479793E-01 | 0.460324E-01 | 0.440127E-01 | 0.440127E-01 | 0.392265E-01 |
| 0.339462E-01 | 0.310938E-01 | 0.304331E-01 | 0.287010E-01 | 0.271600E-01 | 0.271600E-01 | 0.257134E-01 |
| 0.443688E-01 | 0.461100E-01 | 0.511842E-01 | 0.470268E-01 | 0.427649E-01 | 0.427649E-01 | 0.408303E-01 |
| 0.445262E-01 | 0.410938E-01 | 0.376764E-01 | 0.344506E-01 | 0.316257E-01 | 0.316257E-01 | 0.481346E-01 |
| 0.498280E-01 | 0.434006E-01 | 0.410013E-01 | 0.386237E-01 | 0.367000E-01 | 0.367000E-01 | 0.347024E-01 |
| 0.231016E-01 | 0.310597E-01 | 0.294607E-01 | 0.278410E-01 | 0.262375E-01 | 0.262375E-01 | 0.249974E-01 |
| 0.451402E-01 | 0.407815E-01 | 0.365225E-01 | 0.324745E-01 | 0.286150E-01 | 0.286150E-01 | 0.449445E-01 |

FIGURE 23. Group B Sample Problems Program Results
(continued)

SAMPLE PROBLEM GROUP C

The geometrical relationships for this sample problem are shown in Figure 24. The data sheets are presented in Figure 25 and the results are shown in Figure 26.

Problem 1C

In this problem, a solid surface which could not be created by the program surface generator is entered manually along with the necessary connections data. A cube with four truncated corners, named SCURF, is entered in data from a convenient location in its coordinate system, i.e., at the origin, as shown in Figure 24. Only three points were computed and entered as 9TCUBE transformation data to move the surface to the desired position shown over Surface 1, 1PLATS. The factor from 1PLATS to SCURB9TCUBE is requested as Run #1.

The silhouette generator was used to compute the silhouette from each point in 1PLATS, and because a detailed output was requested with 6 horizontal and 6 vertical divisions of 1PLATS, 49 silhouettes were computed as shown in Figure 26. The numbers following each identifying naming line and naming point number are the boundary point numbers which form the silhouette when connected together. It was not possible, since there are no crossovers in the silhouette, to run this problem in the simple mode in SURFAC at greater speed. The naming divisions were deliberately set at 6 x 6 to reduce the output. Some experimentation is required to determine how many divisions are required to yield the factor to the accuracy desired.

Problem 2C

The silhouette generator requires that all points in Surface 2 be above the plane of Surface 1 when operating in either the simple or complex mode. A view of SCUBE in its original position from 1PLATS clearly shows part of SCUBE below the surface of 1PLATS; the run is therefore rejected with a diagnostic indicating this condition.

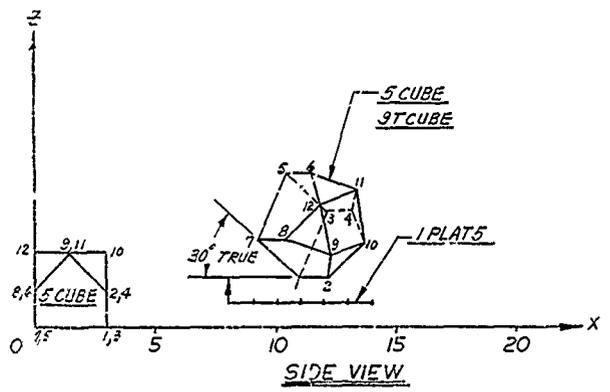
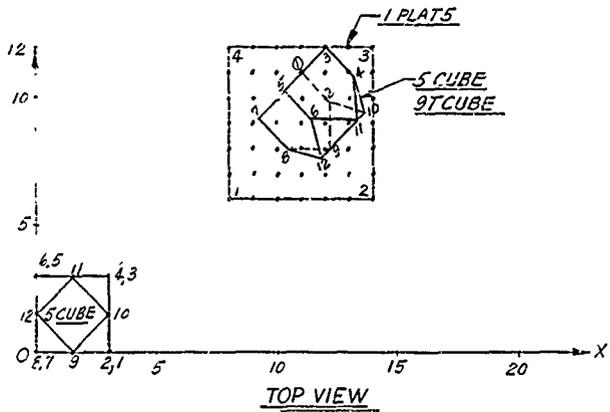


FIGURE 24. GROUP C SAMPLE PROBLEM'S GEOMETRY

FORTRAN FIXED IO DIGIT DECIMAL DATA

| CODE NO. | PROGRAMMER | DATE | PAGE 11 of 36 | JOB NO. 2424-30 |
|----------|-------------------------------|-------------|------------------|-----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | 1 1 1 1 1 1 1 1 1 1 | | | |
| 2 | 2 2 2 2 2 2 2 2 2 2 | | | |
| 3 | 3 3 3 3 3 3 3 3 3 3 | | | |
| 4 | 4 4 4 4 4 4 4 4 4 4 | | | |
| 5 | 5 5 5 5 5 5 5 5 5 5 | | | |
| 6 | 6 6 6 6 6 6 6 6 6 6 | | | |
| 7 | 7 7 7 7 7 7 7 7 7 7 | | | |
| 8 | 8 8 8 8 8 8 8 8 8 8 | | | |
| 9 | 9 9 9 9 9 9 9 9 9 9 | | | |
| 10 | 10 10 10 10 10 10 10 10 10 10 | | | |
| 11 | 11 11 11 11 11 11 11 11 11 11 | | | |
| 12 | 12 12 12 12 12 12 12 12 12 12 | | | |
| 13 | 13 13 13 13 13 13 13 13 13 13 | | | |
| 14 | 14 14 14 14 14 14 14 14 14 14 | | | |
| 15 | 15 15 15 15 15 15 15 15 15 15 | | | |
| 16 | 16 16 16 16 16 16 16 16 16 16 | | | |
| 17 | 17 17 17 17 17 17 17 17 17 17 | | | |
| 18 | 18 18 18 18 18 18 18 18 18 18 | | | |
| 19 | 19 19 19 19 19 19 19 19 19 19 | | | |
| 20 | 20 20 20 20 20 20 20 20 20 20 | | | |
| 21 | 21 21 21 21 21 21 21 21 21 21 | | | |
| 22 | 22 22 22 22 22 22 22 22 22 22 | | | |
| 23 | 23 23 23 23 23 23 23 23 23 23 | | | |
| 24 | 24 24 24 24 24 24 24 24 24 24 | | | |
| 25 | 25 25 25 25 25 25 25 25 25 25 | | | |
| 26 | 26 26 26 26 26 26 26 26 26 26 | | | |
| 27 | 27 27 27 27 27 27 27 27 27 27 | | | |
| 28 | 28 28 28 28 28 28 28 28 28 28 | | | |
| 29 | 29 29 29 29 29 29 29 29 29 29 | | | |
| 30 | 30 30 30 30 30 30 30 30 30 30 | | | |
| 31 | 31 31 31 31 31 31 31 31 31 31 | | | |
| 32 | 32 32 32 32 32 32 32 32 32 32 | | | |
| 33 | 33 33 33 33 33 33 33 33 33 33 | | | |
| 34 | 34 34 34 34 34 34 34 34 34 34 | | | |
| 35 | 35 35 35 35 35 35 35 35 35 35 | | | |
| 36 | 36 36 36 36 36 36 36 36 36 36 | | | |
| 37 | 37 37 37 37 37 37 37 37 37 37 | | | |
| 38 | 38 38 38 38 38 38 38 38 38 38 | | | |
| 39 | 39 39 39 39 39 39 39 39 39 39 | | | |
| 40 | 40 40 40 40 40 40 40 40 40 40 | | | |
| 41 | 41 41 41 41 41 41 41 41 41 41 | | | |
| 42 | 42 42 42 42 42 42 42 42 42 42 | | | |
| 43 | 43 43 43 43 43 43 43 43 43 43 | | | |
| 44 | 44 44 44 44 44 44 44 44 44 44 | | | |
| 45 | 45 45 45 45 45 45 45 45 45 45 | | | |
| 46 | 46 46 46 46 46 46 46 46 46 46 | | | |
| 47 | 47 47 47 47 47 47 47 47 47 47 | | | |
| 48 | 48 48 48 48 48 48 48 48 48 48 | | | |
| 49 | 49 49 49 49 49 49 49 49 49 49 | | | |
| 50 | 50 50 50 50 50 50 50 50 50 50 | | | |

FORTRAN FIXED IO DIGIT DECIMAL DATA

| CODE NO. | PROGRAMMER | DATE | PAGE 11 of 36 | JOB NO. 2424-30 |
|----------|-------------------------------|-------------|------------------|-----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | 1 1 1 1 1 1 1 1 1 1 | | | |
| 2 | 2 2 2 2 2 2 2 2 2 2 | | | |
| 3 | 3 3 3 3 3 3 3 3 3 3 | | | |
| 4 | 4 4 4 4 4 4 4 4 4 4 | | | |
| 5 | 5 5 5 5 5 5 5 5 5 5 | | | |
| 6 | 6 6 6 6 6 6 6 6 6 6 | | | |
| 7 | 7 7 7 7 7 7 7 7 7 7 | | | |
| 8 | 8 8 8 8 8 8 8 8 8 8 | | | |
| 9 | 9 9 9 9 9 9 9 9 9 9 | | | |
| 10 | 10 10 10 10 10 10 10 10 10 10 | | | |
| 11 | 11 11 11 11 11 11 11 11 11 11 | | | |
| 12 | 12 12 12 12 12 12 12 12 12 12 | | | |
| 13 | 13 13 13 13 13 13 13 13 13 13 | | | |
| 14 | 14 14 14 14 14 14 14 14 14 14 | | | |
| 15 | 15 15 15 15 15 15 15 15 15 15 | | | |
| 16 | 16 16 16 16 16 16 16 16 16 16 | | | |
| 17 | 17 17 17 17 17 17 17 17 17 17 | | | |
| 18 | 18 18 18 18 18 18 18 18 18 18 | | | |
| 19 | 19 19 19 19 19 19 19 19 19 19 | | | |
| 20 | 20 20 20 20 20 20 20 20 20 20 | | | |
| 21 | 21 21 21 21 21 21 21 21 21 21 | | | |
| 22 | 22 22 22 22 22 22 22 22 22 22 | | | |
| 23 | 23 23 23 23 23 23 23 23 23 23 | | | |
| 24 | 24 24 24 24 24 24 24 24 24 24 | | | |
| 25 | 25 25 25 25 25 25 25 25 25 25 | | | |
| 26 | 26 26 26 26 26 26 26 26 26 26 | | | |
| 27 | 27 27 27 27 27 27 27 27 27 27 | | | |
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| 33 | 33 33 33 33 33 33 33 33 33 33 | | | |
| 34 | 34 34 34 34 34 34 34 34 34 34 | | | |
| 35 | 35 35 35 35 35 35 35 35 35 35 | | | |
| 36 | 36 36 36 36 36 36 36 36 36 36 | | | |
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| 38 | 38 38 38 38 38 38 38 38 38 38 | | | |
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| 41 | 41 41 41 41 41 41 41 41 41 41 | | | |
| 42 | 42 42 42 42 42 42 42 42 42 42 | | | |
| 43 | 43 43 43 43 43 43 43 43 43 43 | | | |
| 44 | 44 44 44 44 44 44 44 44 44 44 | | | |
| 45 | 45 45 45 45 45 45 45 45 45 45 | | | |
| 46 | 46 46 46 46 46 46 46 46 46 46 | | | |
| 47 | 47 47 47 47 47 47 47 47 47 47 | | | |
| 48 | 48 48 48 48 48 48 48 48 48 48 | | | |
| 49 | 49 49 49 49 49 49 49 49 49 49 | | | |
| 50 | 50 50 50 50 50 50 50 50 50 50 | | | |

FIGURE 25. Group C Sample Problems Input Data Code Sheets

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 11 OF 20 | JOB NO. 2424-10 |
|----------|----------------|-------------|------------------|-----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | 1 | | | |
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FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 11 OF 20 | JOB NO. 2424-10 |
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| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | | | | |
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FIGURE 25. Group C Sample Problems Input Data Code Sheets (continued)

FORTRAN FIXED IO DIGIT DECIMAL DATA

| DEC. NO. | PROGRAMMER | DATE | PAGE 27 of 36 | JOB NO. 285-30 |
|----------|----------------|-------------|------------------|----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | C | | | |
| 2 | C | | | |
| 3 | C | | | |
| 4 | C | | | |
| 5 | C | | | |
| 6 | C | | | |
| 7 | C | | | |
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| 9 | C | | | |
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| 74 | C | | | |
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| 91 | C | | | |
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| 94 | C | | | |
| 95 | C | | | |
| 96 | C | | | |
| 97 | C | | | |
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| 99 | C | | | |
| 100 | C | | | |

FIGURE 25. Group C Sample Problems Input Data Code Sheets (continued)

MMA SPACE AND INFORMATION SYSTEMS DIVISION,
 T-4 PROJECT RADIAN-INTERCHANGE CONFIGURATION FACTOR PROGRAM

C O N F A C I I
 MMA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (C)-M.A.T.O.U.P.S., 1/1/63

I N P U T D A T A

***** DATA NAME= *IPLATS * 6X6 PLATE PARALLEL TO XY PLANE, Z=1
 POINT X Y Z POINT X Y Z
 1 0.800000E 01 0.400000E 01 0.200000E 01 1 0.100000E 01 0.100000E 01 0.100000E 01
 2 0.800000E 01 0.400000E 01 0.100000E 01 2 0.140000E 01 0.140000E 01 0.140000E 01
 3 0.110000E 02 0.110000E 02 0.110000E 02 4 0.800000E 01 0.800000E 01 0.800000E 01

***** DATA NAME= *SCUBE * 3 UNITS ON A SIDE, WITH FOUR ADJACENT CORNERS INDICATED
 POINT X Y Z POINT X Y Z
 1 0.300000E 01 0.300000E 01 0.300000E 01 4 0.300000E 01 0.300000E 01 0.300000E 01
 2 0.300000E 01 0.300000E 01 0.300000E 01 5 0.300000E 01 0.300000E 01 0.300000E 01
 3 0.300000E 01 0.300000E 01 0.300000E 01 6 0.300000E 01 0.300000E 01 0.300000E 01
 4 0.300000E 01 0.300000E 01 0.300000E 01 7 0.300000E 01 0.300000E 01 0.300000E 01
 5 0.300000E 01 0.300000E 01 0.300000E 01 8 0.300000E 01 0.300000E 01 0.300000E 01
 6 0.300000E 01 0.300000E 01 0.300000E 01 9 0.300000E 01 0.300000E 01 0.300000E 01
 7 0.300000E 01 0.300000E 01 0.300000E 01 10 0.300000E 01 0.300000E 01 0.300000E 01
 8 0.300000E 01 0.300000E 01 0.300000E 01 11 0.300000E 01 0.300000E 01 0.300000E 01
 9 0.300000E 01 0.300000E 01 0.300000E 01 12 0.300000E 01 0.300000E 01 0.300000E 01

POINT CONNECTING POINTS POINT CONNECTING POINTS POINT CONNECTING POINTS
 1 3 7 2 1 9 10 -0 3 5 1 8 -0 4 7 9 11 2 -0
 2 4 8 3 2 10 11 0 4 6 2 7 8 -0 5 10 11 12 -0
 3 5 9 4 3 11 12 0 5 10 11 12 0 6 11 12 1 -0
 4 6 10 5 4 12 1 0 6 11 12 1 0 7 9 12 -0
 5 7 11 6 5 1 12 0 7 9 12 1 0 8 1 11 0
 6 8 12 7 6 1 12 0 8 1 11 0 9 1 11 0

***** DATA NAME= *SCURC * TRANSFORMS SCUBE TO SKEWED POSITION IN 15° QUAD.
 TRANSFORMATION-DATA
 POINT X Y Z POINT X Y Z
 1 0.110000E 02 0.110000E 02 0.200000E 01 2 0.120000E 02 0.999310E 01 0.200000E 01

FIGURE 26. Group C Sample Problems Program Results;
 (7 pages)

7 0.91626831 01 0.9.65269E 01 0.15000004 0.

FIGURE 26. Group C Sample Problems Program Results
(continued)

IAA CONFIDENTIAL II REPORT SAMPLE PROBLEMS FROM FIG. (C)-K.A.-TROUPS, II/1/63

RUN NO. 1 DATA USED FOR THIS RUN - DISPLAY SCURE *
 *OTICURE *
 *U 1 *
 *I *

MAPPING SURFACE 2 SILICOLITE COMPUTED FROM MAPPING POINT SHOWN

| LINE # | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|--------|----|----|---|---|---|---|---|---|---|----|----|----|
| 1 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 2 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 3 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 4 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 5 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 6 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 7 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 8 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 9 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 10 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 11 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |
| 12 | 12 | 10 | 7 | 5 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 12 |

FIGURE 26. Group C Sample Problems Program Results
 (continued)

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1 7 9 10 1 3 1 7 0 9
6 2 9 2 1 3 3 7 8 9
6 3 9 2 1 3 3 7 8 9
6 5 9 2 1 3 3 7 8 9
6 6 9 10 4 3 1 7 8 9
6 7 1 9 2 1 3 3 1 4 9
7 2 9 2 1 3 3 7 8 9
7 4 9 2 10 4 3 3 7 8 9
7 5 9 2 4 3 3 7 8 9
7 6 9 10 4 3 1 2 9

```

TOTAL TIME IN SILFAC = 1.089 SECONDS.

THE FURN FACTOR FROM SURFACE *PLATS * TO SURFACE *SCUBE 9TCUBE* = 0.20965

THE EXCHANGE COEFFICIENT (EFA)* = 0.75475E 01 SQ UNITS

THE AREA OF SURFACE *PLATS * = 0.36400000E 02 SQ UNITS

THE AREA OF SL * = 0.36000000E 02 SQ UNITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

NIITS.

***** DATA NAME= *PLATS * *

```

POINT 3. X 0. Y 0. Z 0.000000E 01---(INITIALLY ORIGINATES ORIENTATION VECTOR) Z
4 3. X 0. Y 0. Z 0.000000E 01
5 0.000000E 01 0.000000E 01 0.
4 0.
0.000000E 01 0.000000E 01 0.

```

***** DATA NAME= *SCUBE 9TCUBE*

FIGURE 26. Group C Sample Problems Program Results
(continued)

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|-------------|-----|-------------|-------|------------|-----|-------------|
| 1 | 3.30000002 | 0.1 | 0.00000000 | 0.0 | 0.40000000 | 0.1 | 0.3038400 |
| 2 | 3.40000002 | 0.1 | 0.30000000 | 1 | 0.40000000 | 0.1 | 0.50000000 |
| 3 | 3.50000002 | 0.1 | 0.60000000 | 2 | 0.40000000 | 0.1 | 0.70000000 |
| 4 | 3.60000002 | 0.1 | 0.90000000 | 3 | 0.40000000 | 0.1 | 0.90000000 |
| 5 | 3.70000002 | 0.1 | 1.20000000 | 4 | 0.40000000 | 0.1 | 1.10000000 |
| 6 | 3.80000002 | 0.1 | 1.50000000 | 5 | 0.40000000 | 0.1 | 1.30000000 |
| 7 | 3.90000002 | 0.1 | 1.80000000 | 6 | 0.40000000 | 0.1 | 1.50000000 |
| 8 | 4.00000002 | 0.1 | 2.10000000 | 7 | 0.40000000 | 0.1 | 1.70000000 |
| 9 | 4.10000002 | 0.1 | 2.40000000 | 8 | 0.40000000 | 0.1 | 1.90000000 |
| 10 | 4.20000002 | 0.1 | 2.70000000 | 9 | 0.40000000 | 0.1 | 2.10000000 |
| 11 | 4.30000002 | 0.1 | 3.00000000 | 10 | 0.40000000 | 0.1 | 2.30000000 |
| 12 | 4.40000002 | 0.1 | 3.30000000 | 11 | 0.40000000 | 0.1 | 2.50000000 |
| 13 | 4.50000002 | 0.1 | 3.60000000 | 12 | 0.40000000 | 0.1 | 2.70000000 |
| 14 | 4.60000002 | 0.1 | 3.90000000 | 13 | 0.40000000 | 0.1 | 2.90000000 |
| 15 | 4.70000002 | 0.1 | 4.20000000 | 14 | 0.40000000 | 0.1 | 3.10000000 |
| 16 | 4.80000002 | 0.1 | 4.50000000 | 15 | 0.40000000 | 0.1 | 3.30000000 |
| 17 | 4.90000002 | 0.1 | 4.80000000 | 16 | 0.40000000 | 0.1 | 3.50000000 |
| 18 | 5.00000002 | 0.1 | 5.10000000 | 17 | 0.40000000 | 0.1 | 3.70000000 |
| 19 | 5.10000002 | 0.1 | 5.40000000 | 18 | 0.40000000 | 0.1 | 3.90000000 |
| 20 | 5.20000002 | 0.1 | 5.70000000 | 19 | 0.40000000 | 0.1 | 4.10000000 |
| 21 | 5.30000002 | 0.1 | 6.00000000 | 20 | 0.40000000 | 0.1 | 4.30000000 |
| 22 | 5.40000002 | 0.1 | 6.30000000 | 21 | 0.40000000 | 0.1 | 4.50000000 |
| 23 | 5.50000002 | 0.1 | 6.60000000 | 22 | 0.40000000 | 0.1 | 4.70000000 |
| 24 | 5.60000002 | 0.1 | 6.90000000 | 23 | 0.40000000 | 0.1 | 4.90000000 |
| 25 | 5.70000002 | 0.1 | 7.20000000 | 24 | 0.40000000 | 0.1 | 5.10000000 |
| 26 | 5.80000002 | 0.1 | 7.50000000 | 25 | 0.40000000 | 0.1 | 5.30000000 |
| 27 | 5.90000002 | 0.1 | 7.80000000 | 26 | 0.40000000 | 0.1 | 5.50000000 |
| 28 | 6.00000002 | 0.1 | 8.10000000 | 27 | 0.40000000 | 0.1 | 5.70000000 |
| 29 | 6.10000002 | 0.1 | 8.40000000 | 28 | 0.40000000 | 0.1 | 5.90000000 |
| 30 | 6.20000002 | 0.1 | 8.70000000 | 29 | 0.40000000 | 0.1 | 6.10000000 |
| 31 | 6.30000002 | 0.1 | 9.00000000 | 30 | 0.40000000 | 0.1 | 6.30000000 |
| 32 | 6.40000002 | 0.1 | 9.30000000 | 31 | 0.40000000 | 0.1 | 6.50000000 |
| 33 | 6.50000002 | 0.1 | 9.60000000 | 32 | 0.40000000 | 0.1 | 6.70000000 |
| 34 | 6.60000002 | 0.1 | 9.90000000 | 33 | 0.40000000 | 0.1 | 6.90000000 |
| 35 | 6.70000002 | 0.1 | 10.20000000 | 34 | 0.40000000 | 0.1 | 7.10000000 |
| 36 | 6.80000002 | 0.1 | 10.50000000 | 35 | 0.40000000 | 0.1 | 7.30000000 |
| 37 | 6.90000002 | 0.1 | 10.80000000 | 36 | 0.40000000 | 0.1 | 7.50000000 |
| 38 | 7.00000002 | 0.1 | 11.10000000 | 37 | 0.40000000 | 0.1 | 7.70000000 |
| 39 | 7.10000002 | 0.1 | 11.40000000 | 38 | 0.40000000 | 0.1 | 7.90000000 |
| 40 | 7.20000002 | 0.1 | 11.70000000 | 39 | 0.40000000 | 0.1 | 8.10000000 |
| 41 | 7.30000002 | 0.1 | 12.00000000 | 40 | 0.40000000 | 0.1 | 8.30000000 |
| 42 | 7.40000002 | 0.1 | 12.30000000 | 41 | 0.40000000 | 0.1 | 8.50000000 |
| 43 | 7.50000002 | 0.1 | 12.60000000 | 42 | 0.40000000 | 0.1 | 8.70000000 |
| 44 | 7.60000002 | 0.1 | 12.90000000 | 43 | 0.40000000 | 0.1 | 8.90000000 |
| 45 | 7.70000002 | 0.1 | 13.20000000 | 44 | 0.40000000 | 0.1 | 9.10000000 |
| 46 | 7.80000002 | 0.1 | 13.50000000 | 45 | 0.40000000 | 0.1 | 9.30000000 |
| 47 | 7.90000002 | 0.1 | 13.80000000 | 46 | 0.40000000 | 0.1 | 9.50000000 |
| 48 | 8.00000002 | 0.1 | 14.10000000 | 47 | 0.40000000 | 0.1 | 9.70000000 |
| 49 | 8.10000002 | 0.1 | 14.40000000 | 48 | 0.40000000 | 0.1 | 9.90000000 |
| 50 | 8.20000002 | 0.1 | 14.70000000 | 49 | 0.40000000 | 0.1 | 10.10000000 |
| 51 | 8.30000002 | 0.1 | 15.00000000 | 50 | 0.40000000 | 0.1 | 10.30000000 |
| 52 | 8.40000002 | 0.1 | 15.30000000 | 51 | 0.40000000 | 0.1 | 10.50000000 |
| 53 | 8.50000002 | 0.1 | 15.60000000 | 52 | 0.40000000 | 0.1 | 10.70000000 |
| 54 | 8.60000002 | 0.1 | 15.90000000 | 53 | 0.40000000 | 0.1 | 10.90000000 |
| 55 | 8.70000002 | 0.1 | 16.20000000 | 54 | 0.40000000 | 0.1 | 11.10000000 |
| 56 | 8.80000002 | 0.1 | 16.50000000 | 55 | 0.40000000 | 0.1 | 11.30000000 |
| 57 | 8.90000002 | 0.1 | 16.80000000 | 56 | 0.40000000 | 0.1 | 11.50000000 |
| 58 | 9.00000002 | 0.1 | 17.10000000 | 57 | 0.40000000 | 0.1 | 11.70000000 |
| 59 | 9.10000002 | 0.1 | 17.40000000 | 58 | 0.40000000 | 0.1 | 11.90000000 |
| 60 | 9.20000002 | 0.1 | 17.70000000 | 59 | 0.40000000 | 0.1 | 12.10000000 |
| 61 | 9.30000002 | 0.1 | 18.00000000 | 60 | 0.40000000 | 0.1 | 12.30000000 |
| 62 | 9.40000002 | 0.1 | 18.30000000 | 61 | 0.40000000 | 0.1 | 12.50000000 |
| 63 | 9.50000002 | 0.1 | 18.60000000 | 62 | 0.40000000 | 0.1 | 12.70000000 |
| 64 | 9.60000002 | 0.1 | 18.90000000 | 63 | 0.40000000 | 0.1 | 12.90000000 |
| 65 | 9.70000002 | 0.1 | 19.20000000 | 64 | 0.40000000 | 0.1 | 13.10000000 |
| 66 | 9.80000002 | 0.1 | 19.50000000 | 65 | 0.40000000 | 0.1 | 13.30000000 |
| 67 | 9.90000002 | 0.1 | 19.80000000 | 66 | 0.40000000 | 0.1 | 13.50000000 |
| 68 | 10.00000002 | 0.1 | 20.10000000 | 67 | 0.40000000 | 0.1 | 13.70000000 |
| 69 | 10.10000002 | 0.1 | 20.40000000 | 68 | 0.40000000 | 0.1 | 13.90000000 |
| 70 | 10.20000002 | 0.1 | 20.70000000 | 69 | 0.40000000 | 0.1 | 14.10000000 |
| 71 | 10.30000002 | 0.1 | 21.00000000 | 70 | 0.40000000 | 0.1 | 14.30000000 |
| 72 | 10.40000002 | 0.1 | 21.30000000 | 71 | 0.40000000 | 0.1 | 14.50000000 |
| 73 | 10.50000002 | 0.1 | 21.60000000 | 72 | 0.40000000 | 0.1 | 14.70000000 |
| 74 | 10.60000002 | 0.1 | 21.90000000 | 73 | 0.40000000 | 0.1 | 14.90000000 |
| 75 | 10.70000002 | 0.1 | 22.20000000 | 74 | 0.40000000 | 0.1 | 15.10000000 |
| 76 | 10.80000002 | 0.1 | 22.50000000 | 75 | 0.40000000 | 0.1 | 15.30000000 |
| 77 | 10.90000002 | 0.1 | 22.80000000 | 76 | 0.40000000 | 0.1 | 15.50000000 |
| 78 | 11.00000002 | 0.1 | 23.10000000 | 77 | 0.40000000 | 0.1 | 15.70000000 |
| 79 | 11.10000002 | 0.1 | 23.40000000 | 78 | 0.40000000 | 0.1 | 15.90000000 |
| 80 | 11.20000002 | 0.1 | 23.70000000 | 79 | 0.40000000 | 0.1 | 16.10000000 |
| 81 | 11.30000002 | 0.1 | 24.00000000 | 80 | 0.40000000 | 0.1 | 16.30000000 |
| 82 | 11.40000002 | 0.1 | 24.30000000 | 81 | 0.40000000 | 0.1 | 16.50000000 |
| 83 | 11.50000002 | 0.1 | 24.60000000 | 82 | 0.40000000 | 0.1 | 16.70000000 |
| 84 | 11.60000002 | 0.1 | 24.90000000 | 83 | 0.40000000 | 0.1 | 16.90000000 |
| 85 | 11.70000002 | 0.1 | 25.20000000 | 84 | 0.40000000 | 0.1 | 17.10000000 |
| 86 | 11.80000002 | 0.1 | 25.50000000 | 85 | 0.40000000 | 0.1 | 17.30000000 |
| 87 | 11.90000002 | 0.1 | 25.80000000 | 86 | 0.40000000 | 0.1 | 17.50000000 |
| 88 | 12.00000002 | 0.1 | 26.10000000 | 87 | 0.40000000 | 0.1 | 17.70000000 |
| 89 | 12.10000002 | 0.1 | 26.40000000 | 88 | 0.40000000 | 0.1 | 17.90000000 |
| 90 | 12.20000002 | 0.1 | 26.70000000 | 89 | 0.40000000 | 0.1 | 18.10000000 |
| 91 | 12.30000002 | 0.1 | 27.00000000 | 90 | 0.40000000 | 0.1 | 18.30000000 |
| 92 | 12.40000002 | 0.1 | 27.30000000 | 91 | 0.40000000 | 0.1 | 18.50000000 |
| 93 | 12.50000002 | 0.1 | 27.60000000 | 92 | 0.40000000 | 0.1 | 18.70000000 |
| 94 | 12.60000002 | 0.1 | 27.90000000 | 93 | 0.40000000 | 0.1 | 18.90000000 |
| 95 | 12.70000002 | 0.1 | 28.20000000 | 94 | 0.40000000 | 0.1 | 19.10000000 |
| 96 | 12.80000002 | 0.1 | 28.50000000 | 95 | 0.40000000 | 0.1 | 19.30000000 |
| 97 | 12.90000002 | 0.1 | 28.80000000 | 96 | 0.40000000 | 0.1 | 19.50000000 |
| 98 | 13.00000002 | 0.1 | 29.10000000 | 97 | 0.40000000 | 0.1 | 19.70000000 |
| 99 | 13.10000002 | 0.1 | 29.40000000 | 98 | 0.40000000 | 0.1 | 19.90000000 |
| 100 | 13.20000002 | 0.1 | 29.70000000 | 99 | 0.40000000 | 0.1 | 20.10000000 |
| 101 | 13.30000002 | 0.1 | 30.00000000 | 100 | 0.40000000 | 0.1 | 20.30000000 |
| 102 | 13.40000002 | 0.1 | 30.30000000 | 101 | 0.40000000 | 0.1 | 20.50000000 |
| 103 | 13.50000002 | 0.1 | 30.60000000 | 102 | 0.40000000 | 0.1 | 20.70000000 |
| 104 | 13.60000002 | 0.1 | 30.90000000 | 103 | 0.40000000 | 0.1 | 20.90000000 |
| 105 | 13.70000002 | 0.1 | 31.20000000 | 104 | 0.40000000 | 0.1 | 21.10000000 |
| 106 | 13.80000002 | 0.1 | 31.50000000 | 105 | 0.40000000 | 0.1 | 21.30000000 |
| 107 | 13.90000002 | 0.1 | 31.80000000 | 106 | 0.40000000 | 0.1 | 21.50000000 |
| 108 | 14.00000002 | 0.1 | 32.10000000 | 107 | 0.40000000 | 0.1 | 21.70000000 |
| 109 | 14.10000002 | 0.1 | 32.40000000 | 108 | 0.40000000 | 0.1 | 21.90000000 |
| 110 | 14.20000002 | 0.1 | 32.70000000 | 109 | 0.40000000 | 0.1 | 22.10000000 |
| 111 | 14.30000002 | 0.1 | 33.00000000 | 110 | 0.40000000 | 0.1 | 22.30000000 |
| 112 | 14.40000002 | 0.1 | 33.30000000 | 111 | 0.40000000 | 0.1 | 22.50000000 |
| 113 | 14.50000002 | 0.1 | 33.60000000 | 112 | 0.40000000 | 0.1 | 22.70000000 |
| 114 | 14.60000002 | 0.1 | 33.90000000 | 113 | 0.40000000 | 0.1 | 22.90000000 |
| 115 | 14.70000002 | 0.1 | 34.20000000 | 114 | 0.40000000 | 0.1 | 23.10000000 |

MAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (CI-K-A) (JPS-11/1/63)

RUN NO. 2 DATA USED FOR THIS RUN *PLAYS+SCUBE *
*D 1 * 1 *

MAPPING SURFACE 2 SILHOUETTE COMPUTED FROM MAPPING POINT SHOWN
LINE PT

SURF 1 HAS A 0 OR - 2-03340 FEL TO SURF 1-THIS RUN ABORTED.

FIGURE 26. Group C Sample Problems Program Results
(continued)

YAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (C)-K.A.-TOWPS-11/1/63

RUN NO. 3 DATA USED FOR THIS RUN- *SCUBE *PLATIS*
* * * * *

A NONPLANAR SURFACE CANNOT BE USED AS SURFACE 1-THIS RUN ABORTED.

FIGURE 26. Group C Sample Problems Program Results
(continued)

SAMPLE PROBLEM GROUP D

The geometrical relationship for this sample problem are presented in Figure 27. The data sheets are shown in Figure 28 and the results are presented in Figure 29.

Problem 1D

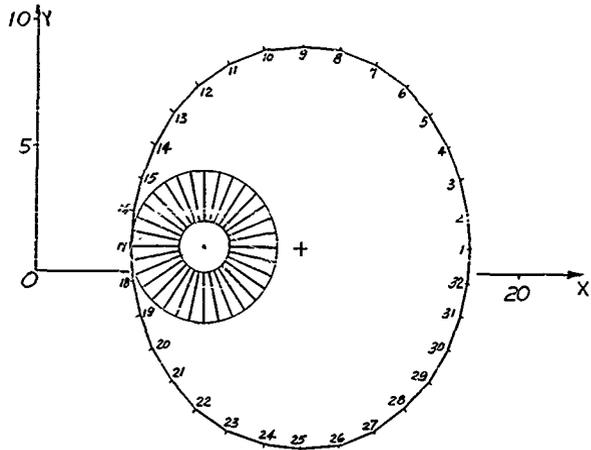
The referenced figure, Figure 27, shows a truncated-cone-on-cylinder and a disk, skewed with respect to the cylinder-cone centerline. The cylinder-cone is created by the surface generator as GCYTR, a 32-sided solid in its final position in the unprimed coordinate system. The disk is also internally generated, but because the generator (in its present version) is limited to cross sections parallel to XY plane, the disk, ZDISK, had to be transformed to the skewed position by transformation data 9TDSK. The results are shown in Figure 29. The simple mode was used for processing because no line segment crossovers are present, which enabled the use of transformations to construct the problem. The warning note concerning the difference between the mapping area and the actual 3DISK surface area is supplied to attract attention to possible errors in Surface 1 data entry of the choice of mapping increments. As indicated in the comments on Problem 1 of Sample Problem Group C, the coarse increment 6 x 6 was selected to reduce output. A finer increment should probably be used to insure accuracy to the third place, if such is desired. It must be emphasized that the form factor obtained in Run #1 is the factor to the solid figure, 6CYLTR, which, of course, includes the bases. Since the factor to the skin is the desired number, it is necessary to subtract the factors to the ends. The upper end is obviously not seen ($f = 0$), so the factor to the base only must be obtained. The base is easily created by the surface generator (3DISKB), but it is created with the orientation vector pointing toward the +Z axis--the wrong way. It is necessary to turn it around by a primary transformation--(9TDSK). Thus, the full capability of the primary transformation feature is utilized and exemplified, shown by Run #2. The factor to the skin of 6CYLTR is obtained by subtracting the results of Run #2 from Run #1, or

$$f_{\text{skin}} = f_{\text{total}} - f_{\text{base}}$$

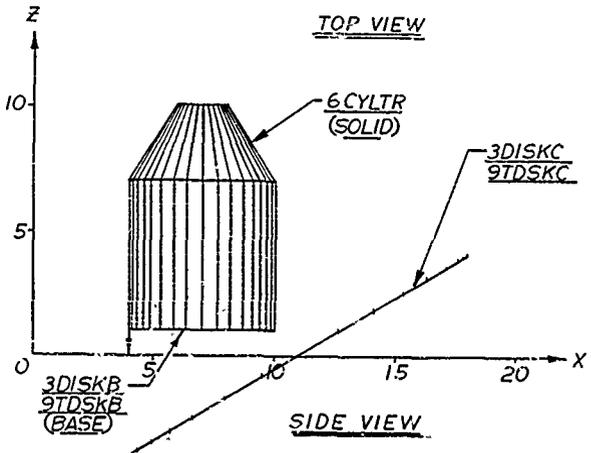
$$f = 0.18946 - 0.09955$$

$$f = .08991$$

The exchange coefficient is computed in a similar manner.



TOP VIEW



SIDE VIEW

FIGURE 27. GROUP D SAMPLE PROBLEMS GEOMETRY

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 30 of 36 | JOB NO. 2521-30 |
|----------|----------------|-------------|------------------|-----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | | | | |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |
| 6 | | | | |
| 7 | | | | |
| 8 | | | | |
| 9 | | | | |
| 10 | | | | |
| 11 | | | | |
| 12 | | | | |
| 13 | | | | |
| 14 | | | | |
| 15 | | | | |
| 16 | | | | |
| 17 | | | | |
| 18 | | | | |
| 19 | | | | |
| 20 | | | | |
| 21 | | | | |
| 22 | | | | |
| 23 | | | | |
| 24 | | | | |
| 25 | | | | |
| 26 | | | | |
| 27 | | | | |
| 28 | | | | |
| 29 | | | | |
| 30 | | | | |

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 31 of 36 | JOB NO. 2521-30 |
|----------|----------------|-------------|------------------|-----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | | | | |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |
| 6 | | | | |
| 7 | | | | |
| 8 | | | | |
| 9 | | | | |
| 10 | | | | |
| 11 | | | | |
| 12 | | | | |
| 13 | | | | |
| 14 | | | | |
| 15 | | | | |
| 16 | | | | |
| 17 | | | | |
| 18 | | | | |
| 19 | | | | |
| 20 | | | | |
| 21 | | | | |
| 22 | | | | |
| 23 | | | | |
| 24 | | | | |
| 25 | | | | |
| 26 | | | | |
| 27 | | | | |
| 28 | | | | |
| 29 | | | | |
| 30 | | | | |

FIGURE 28. Group D Sample Problems Input Data, Code Sheets (continued)

MAA SPACE AND INFORMATION SYSTEMS DIVISION
 IFA PROJECT RADIANT-INTERCHANGE COMPUTATION FACILITY PROGRAM

C O H F A C I I

MAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (D)-K.A.TODPS.11/1/65

I N P U T D A T A

***** DATA NAME = 3DISK * B UNIT RADIUS DISK

SURFACE SPECIFICATIONS =

NO OF X-SECTIONS = 1 NO OF K-SECTION BOUNDARY DIVISIONS = 32

LOCATION OF VERTICAL CENTERLINE, X = 0. * Y = 0.

X-SECTION NO. X-AXIS RADIUS Y AXIS RADIUS ELEVATION ABOVE XY .LANE

1 0.8000000E 01 0.8000000E 01 0.

THE FOLLOWING INTERNALLY GENERATED SURFACE DATA RESULTED FROM THE ABOVE SPECIFICATIONS-

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|---------------|--------------|----|--------------|--------------|---|----|
| 1 | 0.800000E 01 | 0. | 0. | 0.100000E 01 | ---- | INTERNALY GENERATED ORIENTATION VECTOR) | |
| 2 | 0.739103E 01 | 0. | 0. | 4 | 0.766278E 01 | 0. | 0. |
| 3 | 0.739103E 01 | 0.306180E 01 | 0. | 5 | 0.665175E 01 | 0. | 0. |
| 4 | 0.508487E 01 | 0.739103E 01 | 0. | 6 | 0.484453E 01 | 0.402175E 01 | 0. |
| 5 | 0.306180E 01 | 0.739103E 01 | 0. | 7 | 0.306180E 01 | 0.739103E 01 | 0. |
| 6 | 0.289027E -07 | 0.799999E 01 | 0. | 8 | 0.150072E 01 | 0.784628E 01 | 0. |
| 7 | 0.289027E -07 | 0.799999E 01 | 0. | 9 | 0.150072E 01 | 0.784628E 01 | 0. |
| 8 | 0.150072E 01 | 0.784628E 01 | 0. | 10 | 0.150072E 01 | 0.784628E 01 | 0. |
| 9 | 0.150072E 01 | 0.784628E 01 | 0. | 11 | 0.150072E 01 | 0.784628E 01 | 0. |
| 10 | 0.150072E 01 | 0.784628E 01 | 0. | 12 | 0.150072E 01 | 0.784628E 01 | 0. |
| 11 | 0.150072E 01 | 0.784628E 01 | 0. | 13 | 0.150072E 01 | 0.784628E 01 | 0. |
| 12 | 0.150072E 01 | 0.784628E 01 | 0. | 14 | 0.150072E 01 | 0.784628E 01 | 0. |
| 13 | 0.150072E 01 | 0.784628E 01 | 0. | 15 | 0.150072E 01 | 0.784628E 01 | 0. |
| 14 | 0.150072E 01 | 0.784628E 01 | 0. | 16 | 0.150072E 01 | 0.784628E 01 | 0. |
| 15 | 0.150072E 01 | 0.784628E 01 | 0. | 17 | 0.150072E 01 | 0.784628E 01 | 0. |
| 16 | 0.150072E 01 | 0.784628E 01 | 0. | 18 | 0.150072E 01 | 0.784628E 01 | 0. |
| 17 | 0.150072E 01 | 0.784628E 01 | 0. | 19 | 0.150072E 01 | 0.784628E 01 | 0. |
| 18 | 0.150072E 01 | 0.784628E 01 | 0. | 20 | 0.150072E 01 | 0.784628E 01 | 0. |
| 19 | 0.150072E 01 | 0.784628E 01 | 0. | 21 | 0.150072E 01 | 0.784628E 01 | 0. |
| 20 | 0.150072E 01 | 0.784628E 01 | 0. | 22 | 0.150072E 01 | 0.784628E 01 | 0. |
| 21 | 0.150072E 01 | 0.784628E 01 | 0. | 23 | 0.150072E 01 | 0.784628E 01 | 0. |
| 22 | 0.150072E 01 | 0.784628E 01 | 0. | 24 | 0.150072E 01 | 0.784628E 01 | 0. |
| 23 | 0.150072E 01 | 0.784628E 01 | 0. | 25 | 0.150072E 01 | 0.784628E 01 | 0. |
| 24 | 0.150072E 01 | 0.784628E 01 | 0. | 26 | 0.150072E 01 | 0.784628E 01 | 0. |
| 25 | 0.150072E 01 | 0.784628E 01 | 0. | 27 | 0.150072E 01 | 0.784628E 01 | 0. |
| 26 | 0.150072E 01 | 0.784628E 01 | 0. | 28 | 0.150072E 01 | 0.784628E 01 | 0. |
| 27 | 0.150072E 01 | 0.784628E 01 | 0. | 29 | 0.150072E 01 | 0.784628E 01 | 0. |
| 28 | 0.150072E 01 | 0.784628E 01 | 0. | 30 | 0.665175E 01 | 0.484453E 01 | 0. |
| 29 | 0.306180E 01 | 0.739103E 01 | 0. | 31 | 0.766278E 01 | 0.150072E 01 | 0. |
| 30 | 0.508487E 01 | 0.739103E 01 | 0. | | | | |
| 31 | 0.739103E 01 | 0.306180E 01 | 0. | | | | |

FIGURE 29. Group D Sample Problems Program Results
 (14 pages)

| POINT | CONNECTING POINTS | POINT | CONNECTING POINTS | POINT | CONNECTING POINTS | POINT | CONNECTING POINTS |
|-------|-------------------|----------------|-------------------|-------|-------------------|----------------|-------------------|
| 57 | 0.67642E 01 | -0.41590E 02 | 0.10000E 02 | 58 | 0.45535E 01 | -0.6657102E 00 | 0.70000E 01 |
| 58 | 0.45535E 01 | -0.6657102E 00 | 0.70000E 01 | 59 | 0.61683E 01 | -0.44200E 00 | 0.10000E 02 |
| 59 | 0.61683E 01 | -0.44200E 00 | 0.10000E 01 | 60 | 0.57798E 01 | -0.111120E 01 | 0.70000E 01 |
| 60 | 0.57798E 01 | -0.111120E 01 | 0.70000E 01 | 61 | 0.59798E 01 | -0.111120E 01 | 0.70000E 01 |
| 61 | 0.59798E 01 | -0.111120E 01 | 0.70000E 01 | 62 | 0.54444E 01 | -0.165307E 00 | 0.10000E 02 |
| 62 | 0.54444E 01 | -0.165307E 00 | 0.10000E 02 | 63 | 0.58115E 01 | -0.17168E 01 | 0.70000E 01 |
| 63 | 0.58115E 01 | -0.17168E 01 | 0.70000E 01 | 64 | 0.68847E 01 | -0.197570E 01 | 0.10000E 02 |
| 64 | 0.68847E 01 | -0.197570E 01 | 0.10000E 02 | 65 | 0.70000E 01 | -0.145699E 01 | 0.70000E 01 |
| 65 | 0.70000E 01 | -0.145699E 01 | 0.70000E 01 | 66 | 0.71500E 01 | -0.197570E 01 | 0.10000E 01 |
| 66 | 0.71500E 01 | -0.197570E 01 | 0.10000E 01 | 67 | 0.70000E 01 | -0.145699E 01 | 0.70000E 01 |
| 67 | 0.70000E 01 | -0.145699E 01 | 0.70000E 01 | 68 | 0.69607E 01 | -0.15999E 01 | 0.10000E 01 |
| 68 | 0.69607E 01 | -0.15999E 01 | 0.10000E 01 | 69 | 0.81480E 01 | -0.17167E 01 | 0.70000E 01 |
| 69 | 0.81480E 01 | -0.17167E 01 | 0.70000E 01 | 70 | 0.71213E 01 | -0.112130E 01 | 0.70000E 01 |
| 70 | 0.71213E 01 | -0.112130E 01 | 0.70000E 01 | 71 | 0.71213E 01 | -0.112130E 01 | 0.70000E 01 |
| 71 | 0.71213E 01 | -0.112130E 01 | 0.70000E 01 | 72 | 0.94940E 01 | -0.665709E 00 | 0.10000E 01 |
| 72 | 0.94940E 01 | -0.665709E 00 | 0.10000E 01 | 73 | 0.94940E 01 | -0.665709E 00 | 0.10000E 01 |
| 73 | 0.94940E 01 | -0.665709E 00 | 0.10000E 01 | 74 | 0.72119E 01 | -0.146840E 00 | 0.70000E 01 |
| 74 | 0.72119E 01 | -0.146840E 00 | 0.70000E 01 | 75 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 75 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 76 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 76 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 77 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 77 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 78 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 78 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 79 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 79 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 80 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 80 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 81 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 81 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 82 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 82 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 83 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 83 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 84 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 84 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 85 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 85 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 86 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 86 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 87 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 87 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 88 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 88 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 89 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 89 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 90 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 90 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 91 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 91 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 92 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 92 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 93 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 93 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 94 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 94 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 95 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 95 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 96 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 96 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 97 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 97 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 98 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 98 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 99 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |
| 99 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 | 100 | 0.99423E 01 | -0.146840E 00 | 0.70000E 01 |

FIGURE 26. Group D Sample Problems Program Results
(continued)

```

61 84, 0, 78, 60      82 85, 83, 79, 0      83 84, 84, 80, 62      84 81, 0, 81, 83
62 80, 38, 82, 0      86 80, 81, 83, 85      87 90, 0, 84, 86      88 91, 80, 85, 90
63 90, 0, 90, 82      94 9, 0, 81, 89      91 94, 82, 88, 92      92 95, 83, 89, 91
93 90, 0, 90, 82      94 9, 0, 81, 89      91 94, 82, 88, 92      92 95, 83, 89, 91

```

```

***** DATA NAME= *DISK0 * BASE OF CYLINDER-CREATED WITH ACTIVE SIDE TOWARD +Z AXIS
SURFACE SPECIFICATIONS-

```

```

NO OF X-SECTIONS = 1          NO OF X-SECTION BOUNDARY DIVISIONS = 32
LOCATION OF VERTICAL CENTERLINE, X= 0.          * Y= 0.
X-SECTION NO.      X-AXIS RADIUS      Y-AXIS RADIUS      ELEVATION ABOVE XY PLANE
1                  0.300000E 01      0.300000E 01      0.

```

```

THE FOLLOWING INTERNALLY GENERATED SURFACE DATA RESULTED FROM THE ABOVE SPECIFICATIONS-

```

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|--------------|--------------|----|-------|--------------|--------------|----|
| 1 | 0.30000E 01 | 0. | 0. | 1 | 0.100000E 01 | 0. | 0. |
| 2 | 0.277161E 01 | 0. | 0. | 2 | 0.282250E 01 | 0. | 0. |
| 3 | 0.277161E 01 | 0.118050E 01 | 0. | 3 | 0.282250E 01 | 0.158527E 00 | 0. |
| 4 | 0.212120E 01 | 0.212120E 01 | 0. | 4 | 0.164671E 01 | 0.289440E 01 | 0. |
| 5 | 0.118050E 01 | 0.300000E 01 | 0. | 5 | 0.164671E 01 | 0.289440E 01 | 0. |
| 6 | 0.118050E 01 | 0.300000E 01 | 0. | 6 | 0.164671E 01 | 0.289440E 01 | 0. |
| 7 | 0.118050E 01 | 0.300000E 01 | 0. | 7 | 0.164671E 01 | 0.289440E 01 | 0. |
| 8 | 0.118050E 01 | 0.300000E 01 | 0. | 8 | 0.164671E 01 | 0.289440E 01 | 0. |
| 9 | 0.118050E 01 | 0.300000E 01 | 0. | 9 | 0.164671E 01 | 0.289440E 01 | 0. |
| 10 | 0.118050E 01 | 0.300000E 01 | 0. | 10 | 0.164671E 01 | 0.289440E 01 | 0. |
| 11 | 0.118050E 01 | 0.277161E 01 | 0. | 11 | 0.164671E 01 | 0.289440E 01 | 0. |
| 12 | 0.118050E 01 | 0.277161E 01 | 0. | 12 | 0.164671E 01 | 0.289440E 01 | 0. |
| 13 | 0.118050E 01 | 0.277161E 01 | 0. | 13 | 0.164671E 01 | 0.289440E 01 | 0. |
| 14 | 0.118050E 01 | 0.277161E 01 | 0. | 14 | 0.164671E 01 | 0.289440E 01 | 0. |
| 15 | 0.118050E 01 | 0.277161E 01 | 0. | 15 | 0.164671E 01 | 0.289440E 01 | 0. |
| 16 | 0.118050E 01 | 0.277161E 01 | 0. | 16 | 0.164671E 01 | 0.289440E 01 | 0. |
| 17 | 0.118050E 01 | 0.277161E 01 | 0. | 17 | 0.164671E 01 | 0.289440E 01 | 0. |
| 18 | 0.118050E 01 | 0.277161E 01 | 0. | 18 | 0.164671E 01 | 0.289440E 01 | 0. |
| 19 | 0.118050E 01 | 0.277161E 01 | 0. | 19 | 0.164671E 01 | 0.289440E 01 | 0. |
| 20 | 0.118050E 01 | 0.277161E 01 | 0. | 20 | 0.164671E 01 | 0.289440E 01 | 0. |
| 21 | 0.118050E 01 | 0.277161E 01 | 0. | 21 | 0.164671E 01 | 0.289440E 01 | 0. |
| 22 | 0.118050E 01 | 0.277161E 01 | 0. | 22 | 0.164671E 01 | 0.289440E 01 | 0. |
| 23 | 0.118050E 01 | 0.277161E 01 | 0. | 23 | 0.164671E 01 | 0.289440E 01 | 0. |
| 24 | 0.118050E 01 | 0.277161E 01 | 0. | 24 | 0.164671E 01 | 0.289440E 01 | 0. |
| 25 | 0.118050E 01 | 0.277161E 01 | 0. | 25 | 0.164671E 01 | 0.289440E 01 | 0. |
| 26 | 0.118050E 01 | 0.277161E 01 | 0. | 26 | 0.164671E 01 | 0.289440E 01 | 0. |
| 27 | 0.118050E 01 | 0.277161E 01 | 0. | 27 | 0.164671E 01 | 0.289440E 01 | 0. |
| 28 | 0.118050E 01 | 0.277161E 01 | 0. | 28 | 0.164671E 01 | 0.289440E 01 | 0. |
| 29 | 0.118050E 01 | 0.277161E 01 | 0. | 29 | 0.164671E 01 | 0.289440E 01 | 0. |
| 30 | 0.118050E 01 | 0.277161E 01 | 0. | 30 | 0.164671E 01 | 0.289440E 01 | 0. |
| 31 | 0.277161E 01 | 0.118050E 01 | 0. | 31 | 0.282250E 01 | 0.158527E 00 | 0. |
| 32 | 0.277161E 01 | 0.118050E 01 | 0. | 32 | 0.282250E 01 | 0.158527E 00 | 0. |

```

***** DATA NAME= *PTD5MC * MOVES JOIASC TO SKEMED POSITION ON X-AXIS
TRANSFERMATION DATA-

```

FIGURE 29. Group D Sample Problems Program Results
(continued)

```

POINT  X      Y      Z      POINT  X      Y      Z
  1  0.172800E 02  0.160000E 01  0.400000E 01  0.          0.          0.
  2  0.160000E 02 -0.700000E 01  0.          0.          0.          0.
***** DATA NAME= *PTDISK * FLIPS 3CISKD AROUND SO THAT ACTIVE SIDE SEES 3D13NC*PTDISK
INFORMATION DATA-
POINT  X      Y      Z      POINT  X      Y      Z
  1  0.300000E 01  0.160000E 01  0.100000E 01  0.700000E 01  0.400000E 01  0.100000E 01
  2  0.700000E 01 -0.200000E 01  0.100000E 01

```

FIGURE 29. Group D Sample Problems Program Results
(continued)

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. 101-1-A.TOURS.11/1/63

RUN NO. 1 DATA USED FOR THIS RUN= 0103040506070809101112131415161718192021222324252627282930313233343536373839404142434445464748495051525354555657585960616263646566676869707172737475767778798081828384858687888990919293949596

| MAPPING LINE PT | SURFACE 2 SILHOUETTE COMPUTED FROM MAPPING POINT SHOWN | |
|-----------------|--|---|
| 1 1 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 76 77 |
| 1 2 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83 |
| 1 3 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83 |
| 1 4 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83 |
| 1 5 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83 |
| 1 6 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83 |
| 1 7 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83 |
| 2 1 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 76 75 78 81 |
| 2 2 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 76 75 78 81 |
| 2 3 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 76 75 78 81 |
| 2 4 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 76 75 78 81 |
| 2 5 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83 |
| 2 6 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83 |
| 2 7 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83 |
| 3 1 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 76 75 78 81 |
| 3 2 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 76 75 78 81 |
| 3 3 | 0 | 12 15 18 21 20 22 19 16 13 10 7 4 1 94 91 88 85 82 79 76 75 78 81 |

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FIGURE 29. Group D Jump's Problems Program Results (continued)


```

6 1 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64 67 70
73 76 79 82 85 88 91 94 97 100 103 106 109 112 115 118 121 124 127 130 133 136 139 142 145
6 6 67 70 73 76 79 82 85 88 91 94 97 100 103 106 109 112 115 118 121 124 127 130 133 136 139 142 145
6 7 1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64
2 1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64
7 2 67 70 73 76 79 82 85 88 91 94 97 100 103 106 109 112 115 118 121 124 127 130 133 136 139 142 145
7 3 1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64
7 4 67 70 73 76 79 82 85 88 91 94 97 100 103 106 109 112 115 118 121 124 127 130 133 136 139 142 145
7 5 1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64
7 6 67 70 73 76 79 82 85 88 91 94 97 100 103 106 109 112 115 118 121 124 127 130 133 136 139 142 145
7 7 73 76 79 82 85 88 91 94 97 100 103 106 109 112 115 118 121 124 127 130 133 136 139 142 145

```

```

TOTAL TIME IN SILENCE = 9.837 SECONDS.
THE FORM FACTOR FROM SURFACE *DISKCOFDSKC* TO SURFACE *OCYLTR * = 0.16946
THE EXCHANGE COEFFICIENT (EAF) = 0.378491 02 SU UNITS
THE MAPPING AREA = 0.18904446 03 SU UNITS
THE AREA OF SURFACE *DISKCOFDSKC* = 0.19977256 03 SU UNITS.
THE AREA OF SURFACE *OCYLTR * = 0.11927926 03 SU UNITS.
WARNING-VARIABLE IS MORE THAN 1 PERCENT DIFFERENCE FROM THE AREA IN SURFACE *DISKCOFDSKC* SEEN BY SURFACE *OCYLTR *. THIS MAY BE CAUSED BY WRONG SURFACE DATA FOR THE FACTOR COMPUTATION. THE FACTOR MAY BE INCORRECT.
THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-
***** DATA NAME= *DISKCOFDSKC*

```

FIGURE 59. Group D Sample Problems Program Results
(continued)

| NO | X-LEFT | X-RIGHT | Y | X-LEFT | X-RIGHT | Y |
|----|--------------|--------------|--------------|--------------|--------------|--------------|
| 39 | 0.130724E 01 | 0.607378E 01 | 0.110189E 02 | 0.294507E 01 | 0.129075E 02 | 0.411530E 02 |
| 41 | 0.265161E 01 | 0.991910E 01 | 0.241191E 02 | 0.152437E 01 | 0.709607E 01 | 0.110759E 02 |
| 43 | 0.282242E 01 | 0.118730E 02 | 0.425191E 01 | 0.152437E 01 | 0.709607E 01 | 0.110759E 02 |
| 45 | 0.101280E 01 | 0.154370E 01 | 0.111215E 02 | 0.135908E 01 | 0.135908E 02 | 0.438727E 01 |
| 47 | 0.132935E 01 | 0.134668E 02 | 0.316102E 01 | 0.712598E 01 | 0.725982E 01 | 0.111506E 02 |
| 49 | 0.417007E 00 | 0.792538E 01 | 0.211602E 02 | 0.241550E 00 | 0.135111E 02 | 0.135111E 02 |
| 51 | 0.167895E 00 | 0.124238E 02 | 0.221219E 01 | 0.224687E 00 | 0.729703E 01 | 0.111564E 02 |
| 53 | 0.204151E 00 | 0.266818E 01 | 0.111219E 02 | 0.372409E 00 | 0.127553E 02 | 0.094603E 01 |
| 55 | 0.416386E 00 | 0.126028E 02 | 0.037417E 01 | 0.112474E 00 | 0.127553E 02 | 0.110759E 02 |
| 57 | 0.131420E 01 | 0.711189E 01 | 0.116139E 02 | 0.126292E 01 | 0.795152E 01 | 0.112606E 01 |
| 59 | 0.212385E 00 | 0.711189E 01 | 0.695354E 01 | 0.146243E 00 | 0.916678E 01 | 0.112606E 01 |
| 61 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 63 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 65 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 67 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 69 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 71 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 73 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 75 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 77 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 79 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 81 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 83 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 85 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 87 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 89 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 91 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 93 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |
| 95 | 0.115841E 01 | 0.123172E 01 | 0.105159E 02 | 0.126292E 01 | 0.699278E 01 | 0.109340E 02 |

COORDINATES OF POINTS ON BOUNDARY OF SUNF *DISKCYTORC= FJR EACH Y INTERVAL

| NO. | X-LEFT | X-RIGHT | Y | X-LEFT | X-RIGHT | Y |
|-----|--------------|--------------|--------------|--------------|--------------|--------------|
| -1 | 0.077405E 01 | 0.830239E 01 | 0.510758E 01 | 0.315027E 01 | 0.675716E 01 | 0.265882E 01 |
| -2 | 0.077405E 01 | 0.830239E 01 | 0.100151E 02 | 0.315027E 01 | 0.675716E 01 | 0.265882E 01 |
| 0 | 0.077405E 01 | 0.830239E 01 | 0.100151E 02 | 0.315027E 01 | 0.675716E 01 | 0.265882E 01 |

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 6

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN

FIGURE 29. Group D Sample Problems Program Results
(continued)

LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

| | | | | | |
|--------------|---------------|---------------|--------------|----------------|---------------|
| C.709322E-01 | 0.712180E-01 | C.7153884E-01 | 0.716875E-01 | 0.7167783E-01 | 0.715095E-01 |
| C.710784E-01 | 0.958000E-01 | 0.1100715E-00 | 0.128763E-00 | 0.117009E-00 | 0.971640E-01 |
| C.78257E-01 | 0.1211815E-00 | 0.181047E-00 | 0.217763E-00 | 0.1844521E-00 | 0.122625E-00 |
| C.790000E-01 | 0.183289E-00 | 0.2610136E-00 | 0.365596E-00 | 0.27761501E-00 | 0.1528916E-00 |
| C.779010E-01 | 0.156527E-00 | 0.3057494E-00 | 0.522031E 00 | 0.36920741E-00 | 0.167698E-00 |
| C.815078E-01 | 0.830074E-00 | 0.2374699E-00 | 0.319074E-00 | 0.2106811E-00 | 0.1554562E-00 |
| C.965181E-01 | 0.1160692E-00 | 0.1155315E-00 | 0.116652E-00 | 0.1171803E-00 | 0.116966E-00 |
| C.112201E-00 | | | | | |
| C.116109E-00 | | | | | |

FIGURE 29. Group D Sample Problems Program Results
(continued)

NMA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. 10D-K.A.TROUPS-11/17/63

RUN NO. 2 DATA USED FOR THIS RUN= *DISKCOVDISK*
 DISKCOVDISK
 DISKCOVDISK
 DISKCOVDISK

THE FORM FACTOR FROM SURFACE *DISKCOVDISK* TO SURFACE *DISKCOVDISK* = 0.00955

THE EXCHANGE COEFFICIENT (FAI) = 0.19888E 02 SQ UNITS

THE MAPPING AREA = 0.123045HE 03 SQ UNITS

ONLY A PART OF SURFACE *DISKCOVDISK*, COMPRISING AN AREA OF 0.13145HE 03 SQ UNITS,

SEES SURFACE *DISKCOVDISK*

THE AREA OF SURFACE *DISKCOVDISK* = 0.1907725E 01 SQ UNITS.

THE AREA OF SURFACE *DISKCOVDISK* = 0.2809301E 02 SQ UNITS.

WARNING-WARNING

THE MAPPING AREA IS MORE THAN 1 PERCENT DIFFERENT FROM THE AREA IN SURFACE *DISKCOVDISK*. SEE BY
 CROSSING A MAPPING LINE IN MORE THAN TWO PLACES), OR TOO COARSE INCREMENTS. THE FACTOR MAY BE INCORRECT.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

***** DATA NAME= *DISKCOVDISK*

| POINT | Z | X | Y | Z | X | Y | Z |
|-------|----|---------------|----|---------------|---------------|----|----|
| 1 | 0. | 0. | 0. | 0.1000000E 01 | 0.0000000E 00 | 0. | 0. |
| 2 | 0. | 0.0000000E 00 | 0. | 0. | 0.4501800E 00 | 0. | 0. |
| 3 | 0. | 0.0000000E 00 | 0. | 0. | 0.3860200E 01 | 0. | 0. |
| 4 | 0. | 0.0000000E 00 | 0. | 0. | 0.1770000E 01 | 0. | 0. |
| 5 | 0. | 0.0000000E 00 | 0. | 0. | 0.4190300E 01 | 0. | 0. |
| 6 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 7 | 0. | 0.0000000E 00 | 0. | 0. | 0.7650200E 01 | 0. | 0. |
| 8 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 9 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 10 | 0. | 0.0000000E 00 | 0. | 0. | 0.7650200E 01 | 0. | 0. |
| 11 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 12 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 13 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 14 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 15 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 16 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 17 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |
| 18 | 0. | 0.0000000E 00 | 0. | 0. | 0.1730000E 01 | 0. | 0. |

FIGURE 29. Group D Sample Problems Program Results
 (continued)

10 -0.348379E 01 0.154080E 02 0.
 21 -0.4487729E 01 0.1146319E 02 0.
 20 -0.4096129E 01 0.1501695E 02 0.

***** DATA NAME= *DISK8VDSK8*

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|---------------|----------------|---------------|-------|---------------|----------------|---------------|
| 1 | 0.4855979E 01 | 0.0721171E 01 | 0.350088E 01 | 1 | 0.4855979E 01 | 0.0721171E 01 | 0.350088E 01 |
| 2 | 0.490749E 01 | 0.0540025E 01 | 0.4304102E 01 | 2 | 0.5118021E 01 | 0.0501168E 01 | 0.4304102E 01 |
| 3 | 0.4855979E 01 | 0.0721171E 01 | 0.350088E 01 | 3 | 0.5002319E 01 | 0.0785379E 01 | 0.4113300E 01 |
| 4 | 0.4855979E 01 | 0.0721171E 01 | 0.350088E 01 | 4 | 0.5002319E 01 | 0.0785379E 01 | 0.4113300E 01 |
| 5 | 0.4855979E 01 | 0.0721171E 01 | 0.350088E 01 | 5 | 0.490749E 01 | 0.0540025E 01 | 0.4304102E 01 |
| 6 | 0.4855979E 01 | 0.0721171E 01 | 0.350088E 01 | 6 | 0.490749E 01 | 0.0540025E 01 | 0.4304102E 01 |
| 7 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 7 | 0.490749E 01 | 0.0540025E 01 | 0.4304102E 01 |
| 8 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 8 | 0.490749E 01 | 0.0540025E 01 | 0.4304102E 01 |
| 9 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 9 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 |
| 10 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 10 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 11 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 11 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 12 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 12 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 13 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 13 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 14 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 14 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 15 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 15 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 16 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 16 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 17 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 17 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 18 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 18 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 19 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 19 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 20 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 20 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 21 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 21 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 22 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 22 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 23 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 23 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 24 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 24 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 25 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 25 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 26 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 26 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 27 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 27 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 28 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 28 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 29 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 29 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 30 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 30 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 31 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 31 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |
| 32 | 0.4282297E 01 | 0.04528167E 01 | 0.3440105E 01 | 32 | 0.280401E 01 | 0.0585057E 01 | 0.2534455E 01 |

COORDINATES OF POINTS ON BOUNDARY OF SURF *DISK8VDSK8* FOR EACH Y INTERVAL

| X-LEFT | X-RIGHT | Y | Z | X-LEFT | X-RIGHT | Y | Z |
|----------------|---------------|-----|---------------|----------------|---------------|-----|---------------|
| -0.1610034E 01 | 0.4855979E 01 | 0.0 | 0.5007672E 01 | -0.1610034E 01 | 0.4855979E 01 | 0.0 | 0.5007672E 01 |
| -0.1610034E 01 | 0.4855979E 01 | 0.0 | 0.5007672E 01 | -0.1610034E 01 | 0.4855979E 01 | 0.0 | 0.5007672E 01 |
| -0.1610034E 01 | 0.4855979E 01 | 0.0 | 0.5007672E 01 | -0.1610034E 01 | 0.4855979E 01 | 0.0 | 0.5007672E 01 |

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 6

THE FOLLOWING ARE PLATE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN
 PLATEX AXIS LINE FROM X-LEFT TO X-RIGHT.

0.4372995E-08 0.1424607E-03 0.2406906E-05 0.3767027E-05 0.5002467E-03 0.6486831E-03

FIGURE 29. Group b Sample Problems Program Results
 (continued)

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|
| C-725304E-03 | 0.6225217E-02 | 0.1501604E-01 | 0.2430070E-01 | 0.3101297E-01 | 0.3531677E-01 |
| C-716654E-08 | 0.3716789E-01 | 0.1252211E-00 | 0.1871291E-00 | 0.1659108E-00 | 0.1140264E-00 |
| C-220133E-07 | 0.1054518E-00 | 0.4651275E-00 | 0.5039026E 00 | 0.3690750E-00 | 0.2116433E-00 |
| C-774422E-01 | 0.8896273E-01 | 0.2592187E-00 | 0.4122213E-00 | 0.3477288E-00 | 0.2200286E-00 |
| C-1074407E-00 | 0.905752E-02 | 0.5687903E-01 | 0.8732407E-01 | 0.1281295E-00 | 0.1282457E-00 |
| C-219328E-07 | 0.1210962E-01 | 0.1161268E-01 | 0.1572363E-01 | 0.1600011E-01 | 0.1663135E-01 |
| C-011170E-09 | | | | | |
| C-925839E-01 | | | | | |
| C-023869E-01 | | | | | |
| C-023869E-01 | | | | | |

FIGURE 29. Group D Sample Problems Program Results
(continued)

SAMPLE PROBLEM GROUP F.

The capability of obtaining form factors to spheres in any position relative to Surface 1 is demonstrated, Figure 30. Closed form configuration factor solutions are utilized, enabling very rapid computations. The data sheets are presented in Figure 31 and the results in Figure 32.

Problem 1E

The factor from a rectangle, 1PLAT8, to a sphere, 7SPH1, fully above the plane of 1PLAT8 (Case I) is requested as Run #1. The configuration factor solution in this case is extremely simple (see Appendix E), which, in addition to the coarse mapping of 1PLAT8, accounts for the short computational time.

Problem 2E

The factor from 1PLAT8 to 7SPH2 is requested. The sphere is the same size as 7SPH1, except part of the lower half of the sphere is below, and outside of, the surface of 1PLAT8 (Case II). The results are shown as Run #2.

Problem 3E

A larger sphere, 7SPH3, is located with part of the upper half of the sphere below the surface of 1PLAT8 (Case III). The results are shown as Run #3.

Problem 4E

The program will also compute the factor to a sphere which is embedded in Surface 1, illustrated by 7SPH2 and 1PLAT7. However, no attempt is made to determine what part of 1PLAT7 sees the sphere; when a mapping point on Surface 1 appears inside the sphere, a configuration factor of zero is returned and integrated along with the other computed factors. Therefore, in Run #4 we see no indication that 1PLAT7 is bisected by 7SPH2, although in reality it is. The problem is handled in this way because of the extreme complexity of the general determination of that part of Surface 1 not seen by the sphere.

Problem 5E

The trivial case of the sphere completely below Surface 1 is illustrated by Run #5.

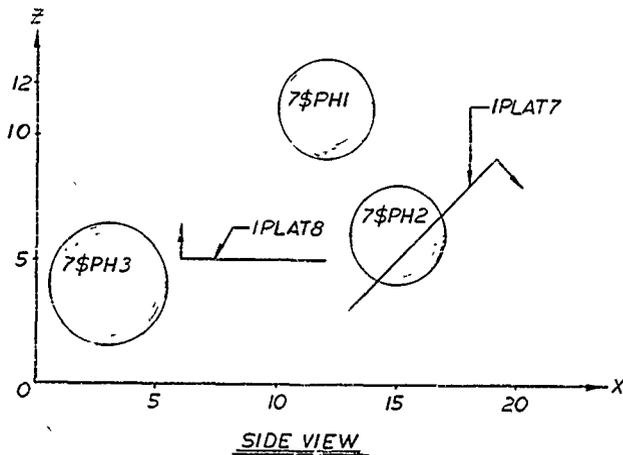
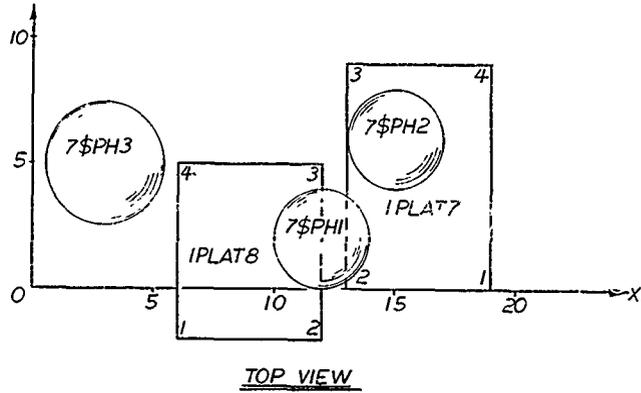


FIGURE 30. Group E Sample Problems Geometry
1.50

FORTRAN FIXED IO DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 23 of 34 | JOB NO. 2522-20 |
|----------|----------------|-------------|------------------|-----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
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FIGURE 31. Group E Sample Problems Input Data Code Sheets

FORTPAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 21 of 36 | JOB NO. 222 X |
|----------|----------------|-------------|------------------|---------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
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FORTTRAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 21 of 36 | JOB NO. 222 X |
|----------|----------------|-------------|------------------|---------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1.0 | | | | |
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FIGURE 31. Group E Sample Problems Input Data Codo Sheets (continued)

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | | PROGRAMMER | SITE | PAGE 35 OF 38 | JOB NO. 2522-31 |
|----------|-------------------|------------------------------|------|---------------|-----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION DO NOT KEY PUNCH | | | |
| 1 | 1.5.1.1.1.7.P.P.2 | | | | |
| 2 | 1.5.1.1.1.7.P.P.2 | | | | |
| 3 | 1.5.1.1.1.7.P.P.2 | | | | |
| 4 | 1.5.1.1.1.7.P.P.2 | | | | |
| 5 | 1.5.1.1.1.7.P.P.2 | | | | |
| 6 | 1.5.1.1.1.7.P.P.2 | | | | |
| 7 | 1.5.1.1.1.7.P.P.2 | | | | |
| 8 | 1.5.1.1.1.7.P.P.2 | | | | |
| 9 | 1.5.1.1.1.7.P.P.2 | | | | |
| 10 | 1.5.1.1.1.7.P.P.2 | | | | |
| 11 | 1.5.1.1.1.7.P.P.2 | | | | |
| 12 | 1.5.1.1.1.7.P.P.2 | | | | |
| 13 | 1.5.1.1.1.7.P.P.2 | | | | |
| 14 | 1.5.1.1.1.7.P.P.2 | | | | |
| 15 | 1.5.1.1.1.7.P.P.2 | | | | |
| 16 | 1.5.1.1.1.7.P.P.2 | | | | |
| 17 | 1.5.1.1.1.7.P.P.2 | | | | |
| 18 | 1.5.1.1.1.7.P.P.2 | | | | |
| 19 | 1.5.1.1.1.7.P.P.2 | | | | |
| 20 | 1.5.1.1.1.7.P.P.2 | | | | |
| 21 | 1.5.1.1.1.7.P.P.2 | | | | |
| 22 | 1.5.1.1.1.7.P.P.2 | | | | |
| 23 | 1.5.1.1.1.7.P.P.2 | | | | |
| 24 | 1.5.1.1.1.7.P.P.2 | | | | |
| 25 | 1.5.1.1.1.7.P.P.2 | | | | |
| 26 | 1.5.1.1.1.7.P.P.2 | | | | |
| 27 | 1.5.1.1.1.7.P.P.2 | | | | |
| 28 | 1.5.1.1.1.7.P.P.2 | | | | |
| 29 | 1.5.1.1.1.7.P.P.2 | | | | |
| 30 | 1.5.1.1.1.7.P.P.2 | | | | |
| 31 | 1.5.1.1.1.7.P.P.2 | | | | |
| 32 | 1.5.1.1.1.7.P.P.2 | | | | |
| 33 | 1.5.1.1.1.7.P.P.2 | | | | |
| 34 | 1.5.1.1.1.7.P.P.2 | | | | |
| 35 | 1.5.1.1.1.7.P.P.2 | | | | |
| 36 | 1.5.1.1.1.7.P.P.2 | | | | |
| 37 | 1.5.1.1.1.7.P.P.2 | | | | |
| 38 | 1.5.1.1.1.7.P.P.2 | | | | |
| 39 | 1.5.1.1.1.7.P.P.2 | | | | |
| 40 | 1.5.1.1.1.7.P.P.2 | | | | |
| 41 | 1.5.1.1.1.7.P.P.2 | | | | |
| 42 | 1.5.1.1.1.7.P.P.2 | | | | |
| 43 | 1.5.1.1.1.7.P.P.2 | | | | |
| 44 | 1.5.1.1.1.7.P.P.2 | | | | |
| 45 | 1.5.1.1.1.7.P.P.2 | | | | |
| 46 | 1.5.1.1.1.7.P.P.2 | | | | |
| 47 | 1.5.1.1.1.7.P.P.2 | | | | |
| 48 | 1.5.1.1.1.7.P.P.2 | | | | |
| 49 | 1.5.1.1.1.7.P.P.2 | | | | |
| 50 | 1.5.1.1.1.7.P.P.2 | | | | |

FIGURE 31. Group E Sample Problems Input Data Code Sheets
(continued)

NAA SPACE AND INFORMATION SYSTEMS DIVISION
 T-8 PROJECT RADIANT-INTERCHANGE CONFIGURATION FACTOR PROGRAM
 C O N F A C I I

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (E)-K-A-T-0-U-P-5, II/11/63

I N P U T D A T A

```

***** DATA NAME= *IPLAT7 * SKewed RECTANGULAR PLATE IN 1ST QUADRANT.
POINT 0.197011E 02 0. 0. 0.824091E 01----- (INTERMEDIATELY GENERATED ORIENTATION VECTORS)
1 0.190000E 02 0. 0.000000E 01 0.000000E 02 0.190000E 01 0.000000E 01 0.000000E 01 0.000000E 01
3 0.190000E 02 0.960000E 01 0.300000E 01 0.300000E 02 0.190000E 01 0.900000E 01 0.900000E 01 0.900000E 01

***** DATA NAME= *IPLAT8 * RECT PLATE PARALLEL TO XY PLANE, 1ST AND 4TH QUADRANTS.
POINT 0.000000E 01 -0.200000E 01 0.000000E 01 0.000000E 01----- (INTERMEDIATELY GENERATED ORIENTATION VECTORS)
1 0.000000E 01 0.000000E 01
3 0.000000E 01 0.000000E 01

***** DATA NAME= *IPLAT9 * 2 UNIT RADIUS FULLY SEEN BY IPLAT8 NOT SEEN BY IPLAT7 (CASE II)
SPHERE SPECIFICATIONS=
RADIUS = 0.200000E 01
COORDINATES OF CENTER----- X = 0.100000E 02 Y = 0.200000E 01 Z = 0.100000E 02

***** DATA NAME= *IPLAT10 * 2 UNIT SPHERE PARTLY SEEN BY IPLAT7 AND IPLAT8 (CASE II)
SPHERE SPECIFICATIONS=
RADIUS = 0.200000E 01
COORDINATES OF CENTER----- X = 0.150000E 02 Y = 0.600000E 01 Z = 0.600000E 01
  
```

FIGURE 30. Group E Sample Problems Program Results
 (13 pages)

***** DATA NAME= *TSPH3
SPHERE SPECIFICATIONS-
RADIUS = 0.250000E 01
COORDINATES OF CENTER= X = 0.300000E 01 Y = 0.500000E 01 Z = 0.400000E 01

FIGURE 32. Group E Sample Problems Program Results
(continued)

MA CONVAC II REPORT SAMPLE PROBLEMS FROM FIG. (E)-G.A.TROUPS, 11/1/63

```

RUN# 01 1 DATA USED FOR THIS RUN= *IPLATB*7SPH1 *
      *D 1* 1*
TOTAL TIME IS SILEAC = 0.021 SECONDS.
THE FORM FACTOR FROM SURFACE *IPLATB * TO SURFACE *7SPH1 * = 0.08339
THE EXCHANGE COEFFICIENT (FA)= 0.28807E 01 SQ UNITS
THE MAPPING AREA = 0.4200000E 02 SQ UNITS
THE AREA OF SURFACE *IPLATB * = 0.4200000E 02 SQ UNITS.
THE AREA OF SURFACE *7SPH1 * = 0.5026548E 02 SQ UNITS.
THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION=

***** DATA NAME= *IPLATB *
POINT 0. X Y Z POINT X Y Z
      1 0.000000E 01 0.700000E 01 0. 0. 0. 0.1000000E 01 --- (INTERMEDIATELY GENERATED ORIENTATION VECTOR) Z
      2 0.600000E 01 0.700000E 01 0. 0. 0. 0.6000000E 01 -D.
      3 0.600000E 01 0.700000E 01 0. 0. 0. 0.7000000E 01 0.

***** DATA NAME= *7SPH1 *
POINT 0. X Y Z POINT X Y Z
      1 0.600000E 01 0.400000E 01 0.400000E 01 0.600000E 01 0.600000E 01 0.600000E 01
COORDINATES OF POINTS ON BOUNDARY OF SURF *IPLATB * FOR EACH Y INTERVAL
      X-LEFT X-RIGHT Y X-LEFT X-RIGHT Y
0. 0.600000E 01 -0. 0. 0.600000E 01 0.1166667E 01
  
```

FIGURE 32. Group E Sample Problems Program Results (continued)

0. 0.6000000E 0. 0.2333333E 01 0. 0. 0.6000000E 01 0.3500000E 01
 0. 0.6000000E 01 0.4666667E 01 0. 0. 0.6000000E 01 0.3933333E 01
 0. 0.6000000E 01 0.7000000E 01

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 6

THE FOLLOWING ARE PLANE PRINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN
 LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

| | | | | |
|---------------|---------------|---------------|---------------|---------------|
| 0.3007282E-01 | 0.4280040E-02 | 0.5037517E-01 | 0.5727027E-01 | 0.6220101E-01 |
| 0.4400397E-01 | 0.5160394E-01 | 0.5215214E-01 | 0.7210018E-01 | 0.7943108E-01 |
| 0.4323366E-01 | 0.5919787E-01 | 0.7267287E-01 | 0.8577958E-01 | 0.9586443E-01 |
| 0.3711525E-01 | 0.5006368E-01 | 0.6334500E-01 | 0.7884667E-01 | 0.9398584E-01 |
| 0.9938965E-01 | 0.4982959E-01 | 0.6319198E-01 | 0.7683417E-01 | 0.9330887E-01 |
| 0.1009637E-01 | 0.4648105E-01 | 0.5826450E-01 | 0.7136197E-01 | 0.8405444E-01 |
| 0.3922746E-01 | 0.4097927E-01 | 0.5037517E-01 | 0.6048123E-01 | 0.6997084E-01 |
| 0.3608817E-01 | | | | |
| 0.3718746E-01 | | | | |
| 0.3221845E-01 | | | | |
| 0.7735068E-01 | | | | |

FIGURE 32. Group 3 Sample Problems Program Results
 (continued)

| X-LEFT | X-RIGHT | Y | X-LEFT | X-RIGHT | Y |
|--------|--------------|--------------|--------|--------------|--------------|
| 0. | 0.600000E 01 | 0.233333E 01 | 0. | 0.600000E 01 | 0.116666E 01 |
| 0. | 0.600000E 01 | 0.466666E 01 | 0. | 0.600000E 01 | 0.350000E 01 |
| 0. | 0.600000E 01 | 0.700000E 01 | 0. | 0.600000E 01 | 0.583333E 01 |

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 6

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS PUN
 LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

| | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|
| 0.265234E-02 | 0.297608E-02 | 0.359173E-02 | 0.427204E-02 | 0.508021E-02 | 0.597181E-02 |
| 0.281754E-02 | 0.337257E-02 | 0.436101E-02 | 0.566610E-02 | 0.700287E-02 | 0.854221E-02 |
| 0.299842E-02 | 0.385304E-02 | 0.501172E-02 | 0.755987E-02 | 0.980659E-02 | 0.126323E-01 |
| 0.317746E-02 | 0.451498E-02 | 0.737242E-02 | 0.100292E-01 | 0.138289E-01 | 0.191558E-01 |
| 0.359234E-02 | 0.655658E-02 | 0.909130E-02 | 0.110394E-01 | 0.192640E-01 | 0.292897E-01 |
| 0.419331E-02 | 0.746095E-02 | 0.107423E-01 | 0.161638E-01 | 0.235695E-01 | 0.433351E-01 |
| 0.458210E-02 | 0.802771E-02 | 0.119347E-01 | 0.165889E-01 | 0.311208E-01 | 0.575082E-01 |
| 0.518210E-02 | | | | | |
| 0.578210E-02 | | | | | |
| 0.638210E-02 | | | | | |
| 0.698210E-02 | | | | | |
| 0.758210E-02 | | | | | |
| 0.818210E-02 | | | | | |
| 0.878210E-02 | | | | | |
| 0.938210E-02 | | | | | |
| 0.998210E-02 | | | | | |
| 0.105821E-01 | | | | | |
| 0.111821E-01 | | | | | |
| 0.117821E-01 | | | | | |
| 0.123821E-01 | | | | | |
| 0.129821E-01 | | | | | |
| 0.135821E-01 | | | | | |
| 0.141821E-01 | | | | | |
| 0.147821E-01 | | | | | |
| 0.153821E-01 | | | | | |
| 0.159821E-01 | | | | | |
| 0.165821E-01 | | | | | |
| 0.171821E-01 | | | | | |
| 0.177821E-01 | | | | | |
| 0.183821E-01 | | | | | |
| 0.189821E-01 | | | | | |
| 0.195821E-01 | | | | | |
| 0.201821E-01 | | | | | |
| 0.207821E-01 | | | | | |
| 0.213821E-01 | | | | | |
| 0.219821E-01 | | | | | |
| 0.225821E-01 | | | | | |
| 0.231821E-01 | | | | | |
| 0.237821E-01 | | | | | |
| 0.243821E-01 | | | | | |
| 0.249821E-01 | | | | | |
| 0.255821E-01 | | | | | |
| 0.261821E-01 | | | | | |
| 0.267821E-01 | | | | | |
| 0.273821E-01 | | | | | |
| 0.279821E-01 | | | | | |
| 0.285821E-01 | | | | | |
| 0.291821E-01 | | | | | |
| 0.297821E-01 | | | | | |
| 0.303821E-01 | | | | | |
| 0.309821E-01 | | | | | |
| 0.315821E-01 | | | | | |
| 0.321821E-01 | | | | | |
| 0.327821E-01 | | | | | |
| 0.333821E-01 | | | | | |
| 0.339821E-01 | | | | | |
| 0.345821E-01 | | | | | |
| 0.351821E-01 | | | | | |
| 0.357821E-01 | | | | | |
| 0.363821E-01 | | | | | |
| 0.369821E-01 | | | | | |
| 0.375821E-01 | | | | | |
| 0.381821E-01 | | | | | |
| 0.387821E-01 | | | | | |
| 0.393821E-01 | | | | | |
| 0.399821E-01 | | | | | |
| 0.405821E-01 | | | | | |
| 0.411821E-01 | | | | | |
| 0.417821E-01 | | | | | |
| 0.423821E-01 | | | | | |
| 0.429821E-01 | | | | | |
| 0.435821E-01 | | | | | |
| 0.441821E-01 | | | | | |
| 0.447821E-01 | | | | | |
| 0.453821E-01 | | | | | |
| 0.459821E-01 | | | | | |
| 0.465821E-01 | | | | | |
| 0.471821E-01 | | | | | |
| 0.477821E-01 | | | | | |
| 0.483821E-01 | | | | | |
| 0.489821E-01 | | | | | |
| 0.495821E-01 | | | | | |
| 0.501821E-01 | | | | | |
| 0.507821E-01 | | | | | |
| 0.513821E-01 | | | | | |
| 0.519821E-01 | | | | | |
| 0.525821E-01 | | | | | |
| 0.531821E-01 | | | | | |
| 0.537821E-01 | | | | | |
| 0.543821E-01 | | | | | |
| 0.549821E-01 | | | | | |
| 0.555821E-01 | | | | | |
| 0.561821E-01 | | | | | |
| 0.567821E-01 | | | | | |
| 0.573821E-01 | | | | | |
| 0.579821E-01 | | | | | |
| 0.585821E-01 | | | | | |
| 0.591821E-01 | | | | | |
| 0.597821E-01 | | | | | |
| 0.603821E-01 | | | | | |
| 0.609821E-01 | | | | | |
| 0.615821E-01 | | | | | |
| 0.621821E-01 | | | | | |
| 0.627821E-01 | | | | | |
| 0.633821E-01 | | | | | |
| 0.639821E-01 | | | | | |
| 0.645821E-01 | | | | | |
| 0.651821E-01 | | | | | |
| 0.657821E-01 | | | | | |
| 0.663821E-01 | | | | | |
| 0.669821E-01 | | | | | |
| 0.675821E-01 | | | | | |
| 0.681821E-01 | | | | | |
| 0.687821E-01 | | | | | |
| 0.693821E-01 | | | | | |
| 0.699821E-01 | | | | | |
| 0.705821E-01 | | | | | |
| 0.711821E-01 | | | | | |
| 0.717821E-01 | | | | | |
| 0.723821E-01 | | | | | |
| 0.729821E-01 | | | | | |
| 0.735821E-01 | | | | | |
| 0.741821E-01 | | | | | |
| 0.747821E-01 | | | | | |
| 0.753821E-01 | | | | | |
| 0.759821E-01 | | | | | |
| 0.765821E-01 | | | | | |
| 0.771821E-01 | | | | | |
| 0.777821E-01 | | | | | |
| 0.783821E-01 | | | | | |
| 0.789821E-01 | | | | | |
| 0.795821E-01 | | | | | |
| 0.801821E-01 | | | | | |
| 0.807821E-01 | | | | | |
| 0.813821E-01 | | | | | |
| 0.819821E-01 | | | | | |
| 0.825821E-01 | | | | | |
| 0.831821E-01 | | | | | |
| 0.837821E-01 | | | | | |
| 0.843821E-01 | | | | | |
| 0.849821E-01 | | | | | |
| 0.855821E-01 | | | | | |
| 0.861821E-01 | | | | | |
| 0.867821E-01 | | | | | |
| 0.873821E-01 | | | | | |
| 0.879821E-01 | | | | | |
| 0.885821E-01 | | | | | |
| 0.891821E-01 | | | | | |
| 0.897821E-01 | | | | | |
| 0.903821E-01 | | | | | |
| 0.909821E-01 | | | | | |
| 0.915821E-01 | | | | | |
| 0.921821E-01 | | | | | |
| 0.927821E-01 | | | | | |
| 0.933821E-01 | | | | | |
| 0.939821E-01 | | | | | |
| 0.945821E-01 | | | | | |
| 0.951821E-01 | | | | | |
| 0.957821E-01 | | | | | |
| 0.963821E-01 | | | | | |
| 0.969821E-01 | | | | | |
| 0.975821E-01 | | | | | |
| 0.981821E-01 | | | | | |
| 0.987821E-01 | | | | | |
| 0.993821E-01 | | | | | |
| 0.999821E-01 | | | | | |

FIGURE 32. Group 2 Sample Problems Program Results
 (continued)

ALA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (E)-K.A. ...JPS,11/1/63

```

RUN NO. 3 DATA USED FOR THIS RUN- *PLAT8*7SPH3 *
      *0 1* 1*

TOTAL TIME IN SELFAC = 0.058 SECONDS.
THE FIRM FACTOR FROM SURFACE *PLAT8 * TO SURFACE *7SPH3 * = 0.00502
THE EXCHANGE COEFFICIENT (FAJ)= 0.21089E-00 50 UNITS
THE AREA OF SURFACE *PLAT8 * = 0.4200000E 02 50 UNITS.

ONLY A PART OF SURFACE *7SPH3 *
SEES SURFACE *PLAT8 * *; COMPRISING AN AREA OF 0.2335619E 02 50 UNITS.

THE AREA OF SURFACE *7SPH3 * = 0.7853982E 02 50 UNITS.

THE FOLLOWING ARE THE (FICIAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

***** DATA NAME= *PLAT8 *
POINT 0. X Y Z POINT X Y Z
1 0. 0. 0. 0.1000000E 01---(INTERNALLY GENERATED ORIENTATION VECTOR) Z
2 0. 0. 0. 0.6000000E 01 0. 0. 0.7000000E 01 0.
3 0.6000000E 01 0.7000000E 02 0.

***** DATA NAME= *7SPH3 *
POINT X Y Z POINT X Y Z
1 -0.3000000E 01 0.7000000E 01 -0.1000000E 01 POINT X Y Z
COORDINATES OF POINTS ON BOUNDARY OF SURF *PLAT8 * FOR EACH Y INTERVAL

```

FIGURE 32. Group E Sample Problems Program Results
(continued)

| | | | | | |
|---------------|---------------|---------------|---------------|---------------|----------------|
| 0.1116397E-C0 | 0.7366526E-01 | 0.4711763E-01 | 0.3059036E-01 | 0.2040013E-01 | 0.1-004648E-01 |
| 0.317209E-C2 | 0.6744630E-02 | 0.6155096E-02 | 0.4118316E-02 | 0.148811E-01 | 0.140024E-01 |
| 0.4031624E-C1 | 0.2778631E-01 | 0.3712033E-01 | 0.4680320E-01 | 0.318151E-01 | 0.108843E-01 |
| 0.468510E-01 | 0.3712032E-01 | 0.277863E-01 | 0.2031023E-01 | 0.148024E-01 | 0.108843E-01 |
| 0.322088E-C2 | 0.4060008E-02 | 0.5123229E-02 | 0.6525123E-02 | 0.8375038E-02 | 0.1078054E-01 |
| 0.138556E-C1 | 0.175374E-01 | 0.2153340E-01 | 0.2513747E-01 | 0.2734619E-01 | 0.2734619E-01 |
| 0.852312E-C2 | 0.2153340E-01 | 0.175374E-01 | 0.1385566E-04 | 0.1078036E-01 | 0.8375805E-02 |

Figure 32. Group E Sample Problems Program Results
(continued)

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (E)-K.A.YOUPS,11/1/63

ADJ NO. 5 DATA USED FOR THIS RUN= *PLATT7*7SPH1 *

NONE OF SURFACE *PLATT7 *

* IS SEEN BY SURFACE *7SPH1 *

IF THE ABOVE RESULT IS UNEXPECTED, DO NOT BECOME ALARMED. IT HAPPENS TO THE BEST OF US. JUST CHECK YOUR DATA ESPECIALLY BE SURE THAT YOU ARE ON THE CORRECT SURFACE AND THAT YOU ARE FACING THE ACTIVE SIDE OF THE SURFACE, AND DERIVED FROM A RIGHT-HANDED COORDINATE SYSTEM.

Figure 32. Group E Sample Problems Program Results
(continued)

SAMPLE PROBLEM GROUP F

The capability of computing factors to surfaces which are occluded by intervening surfaces is demonstrated as shown in Figure 33. The data sheets are presented in Figure 34 and the results in Figure 35.

Problem 1F

The factor from 1PLA10 to 1PLA9 is desired with surface 1PLA11 intervening. The surface 5COPLA, representing the boundary points of 1PLA9 including connections, and the boundary points of 1PLA11 including connections is entered in data. Because the silhouette is complex, the surface 5COPLA must be reentered as 8COPLA to enable the silhouette generator to operate in the complex mode. The factor to 8COPLA from 1PLA10 is requested as Run #1. Then, the factor from 1PLA10 to 1PLA11 is requested as Run #2. The factor from 1PLA10 to 1PLA9 is merely the difference between the two,

$$f = 0.26787 - 0.20146$$

$$f = 0.06641$$

Problem 2F

This problem also illustrates the capability of determining factors to occluded surfaces, but data is entered and handled in a different manner. The factor from 1PLA10 to 6PIPE2 is desired, taking into account the flux interceded by 5PIPE1.

The coordinates defining 6PIPE2 are internally generated. 5PIPE1 is entered manually, and the two surfaces are combined for complex processing as 820FEN.

Notice that 5PIPE1 includes a line segment--a "bridge" line--connecting point 7 in 5PIPE1 to 6PIPE2. If this line or any other suitably oriented line serving the purpose were not present, then the silhouette generator would not include 6PIPE2 in any of the silhouettes computed from points on mapping lines 6 and 7 on 1PLA10. The line does not have to actually be in any surface--it need only appear to intersect both surfaces in the silhouette.

The form factor to 820FEN is 0.28139 (Run #3); to 5PIPE1 alone is 0.21556 (Run #4); therefore, the form factor to 6PIPE2 is the difference or 0.06583.

Problem 3F

This problem illustrates improper use of the program, and in particular, the silhouette generator. The factor from 1PLA12 to 5COPLA is requested as Run #5. Note that the data 5COPLA is in reality two surfaces. These surfaces when viewed from 1PLA10 or 1PLA12 present a complex silhouette, and therefore, must be processed in the complex mode. However, when a class 4, 5 or 6 surface is specified as Surface 2, the simple mode is always used. The

silhouette generator consequently saw only IPLA11 sometimes and only IPLA9 sometimes; this condition would not be relieved by use of a bridge line, because the total silhouette is complex, and must be processed as complex.

Problem 4F

When a class 8 surface is used as Surface 2, Surface 1 must be in the XY plane of the Surface 2 coordinate system, with its orientation vector pointing toward the +Z axis. The results of Run #6 show the diagnostic resulting from a request for the factor from IPLA12 to SCOPLA.

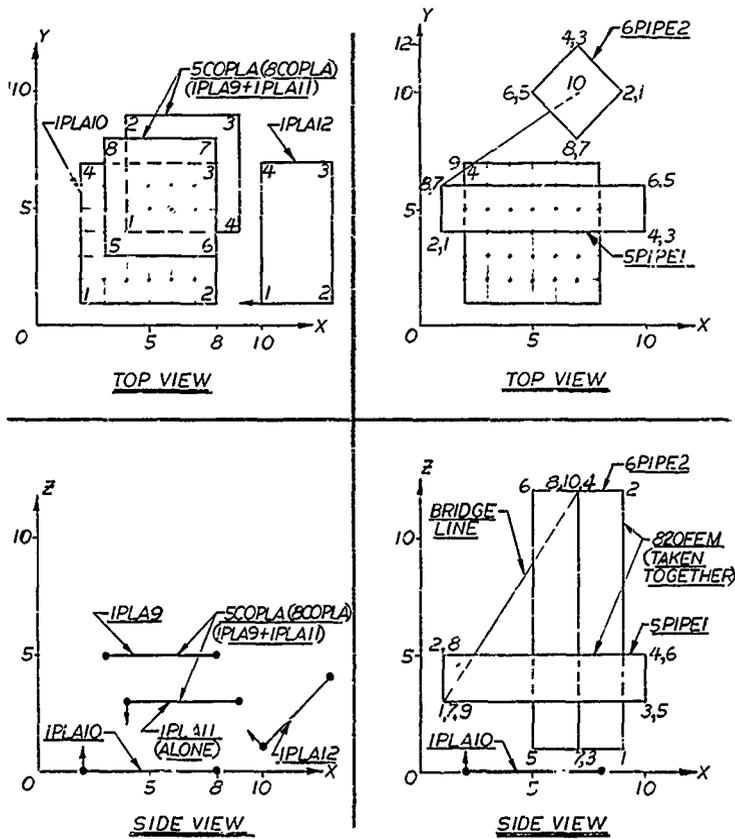


FIGURE 33. Group F Sample Problems Geometry

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| CODE NO. | PROGRAMMER | DATE | PAGE 27 of 31 | JOB NO. 2029 30 |
|----------|----------------|-------------|------------------|-----------------|
| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | | | | |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |
| 6 | | | | |
| 7 | | | | |
| 8 | | | | |
| 9 | | | | |
| 0 | | | | |
| 1 | | | | |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |
| 6 | | | | |
| 7 | | | | |
| 8 | | | | |
| 9 | | | | |
| 0 | | | | |
| 1 | | | | |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |
| 6 | | | | |
| 7 | | | | |
| 8 | | | | |
| 9 | | | | |
| 0 | | | | |
| 1 | | | | |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |
| 6 | | | | |
| 7 | | | | |
| 8 | | | | |
| 9 | | | | |
| 0 | | | | |
| 1 | | | | |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |
| 6 | | | | |
| 7 | | | | |
| 8 | | | | |
| 9 | | | | |
| 0 | | | | |
| 1 | | | | |
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| 9 | F. 1. 1. 9 | | | |
| 10 | F. 1. 1. 0 | | | |
| 11 | F. 1. 1. 1 | | | |
| 12 | F. 1. 1. 2 | | | |
| 13 | F. 1. 1. 3 | | | |
| 14 | F. 1. 1. 4 | | | |
| 15 | F. 1. 1. 5 | | | |
| 16 | F. 1. 1. 6 | | | |
| 17 | F. 1. 1. 7 | | | |
| 18 | F. 1. 1. 8 | | | |
| 19 | F. 1. 1. 9 | | | |
| 20 | F. 1. 1. 0 | | | |
| 21 | F. 1. 1. 1 | | | |
| 22 | F. 1. 1. 2 | | | |
| 23 | F. 1. 1. 3 | | | |
| 24 | F. 1. 1. 4 | | | |
| 25 | F. 1. 1. 5 | | | |
| 26 | F. 1. 1. 6 | | | |
| 27 | F. 1. 1. 7 | | | |
| 28 | F. 1. 1. 8 | | | |
| 29 | F. 1. 1. 9 | | | |
| 30 | F. 1. 1. 0 | | | |
| 31 | F. 1. 1. 1 | | | |
| 32 | F. 1. 1. 2 | | | |
| 33 | F. 1. 1. 3 | | | |
| 34 | F. 1. 1. 4 | | | |
| 35 | F. 1. 1. 5 | | | |
| 36 | F. 1. 1. 6 | | | |
| 37 | F. 1. 1. 7 | | | |
| 38 | F. 1. 1. 8 | | | |
| 39 | F. 1. 1. 9 | | | |
| 40 | F. 1. 1. 0 | | | |

FORTRAN FIXED 10 DIGIT DECIMAL DATA

| DECK NO. | PROGRAM# | DATE | PAGE 32 OF 32 | JOB NO. 2252-32 |
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| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
| 1 | F. 1. 1. 1 | | | |
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| 3 | F. 1. 1. 3 | | | |
| 4 | F. 1. 1. 4 | | | |
| 5 | F. 1. 1. 5 | | | |
| 6 | F. 1. 1. 6 | | | |
| 7 | F. 1. 1. 7 | | | |
| 8 | F. 1. 1. 8 | | | |
| 9 | F. 1. 1. 9 | | | |
| 10 | F. 1. 1. 0 | | | |
| 11 | F. 1. 1. 1 | | | |
| 12 | F. 1. 1. 2 | | | |
| 13 | F. 1. 1. 3 | | | |
| 14 | F. 1. 1. 4 | | | |
| 15 | F. 1. 1. 5 | | | |
| 16 | F. 1. 1. 6 | | | |
| 17 | F. 1. 1. 7 | | | |
| 18 | F. 1. 1. 8 | | | |
| 19 | F. 1. 1. 9 | | | |
| 20 | F. 1. 1. 0 | | | |
| 21 | F. 1. 1. 1 | | | |
| 22 | F. 1. 1. 2 | | | |
| 23 | F. 1. 1. 3 | | | |
| 24 | F. 1. 1. 4 | | | |
| 25 | F. 1. 1. 5 | | | |
| 26 | F. 1. 1. 6 | | | |
| 27 | F. 1. 1. 7 | | | |
| 28 | F. 1. 1. 8 | | | |
| 29 | F. 1. 1. 9 | | | |
| 30 | F. 1. 1. 0 | | | |
| 31 | F. 1. 1. 1 | | | |
| 32 | F. 1. 1. 2 | | | |
| 33 | F. 1. 1. 3 | | | |
| 34 | F. 1. 1. 4 | | | |
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| 36 | F. 1. 1. 6 | | | |
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| 38 | F. 1. 1. 8 | | | |
| 39 | F. 1. 1. 9 | | | |
| 40 | F. 1. 1. 0 | | | |

Figure 34. Group F Sample Problems Input Data Code Sheets
(continued)

FORTRAN: FIXED IO DIGIT DECIMAL DATA

| DECK NO. | PROGRAMMER | DATE | PAGE 33 of 36 | JOB NO. 257-30 |
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| DECK NO. | PROGRAMMER | DATE | PAGE 31 of 32 | JOB NO. 222-30 |
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| NUMBER | IDENTIFICATION | DESCRIPTION | DO NOT KEY PUNCH | |
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Figure 34. Group F Sample Problems Input Data Code Sheets
(continued)

MAA SPACE AND INFORMATION SYSTEMS DIVISION
 IFA PROJECT RADIANT-INTERCHANGE CONFIGURATION FACTOR PROGRAM

C O N F A C T I

MAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (F)-K.A.T.O.U.P.S.11/1/63

I N P U T D A T A

***** DATA NAME- *IPLA10 * 6X6 PLATE IN XY PLANE
 POINT X Y Z POINT X Y Z
 1 0.300000E 01 0.100000E 01 0.100000E 01 1 0.100000E 01 0.100000E 01 0.100000E 01
 2 0.200000E 01 0.100000E 01 0.100000E 01 2 0.200000E 01 0.100000E 01 0.100000E 01
 3 0.400000E 01 0.700000E 01 0.100000E 01 3 0.200000E 01 0.700000E 01 0.100000E 01

***** DATA NAME- *IPLA11 * 5X5 SQUARE, Z=3, LOOKING AT IPLA10
 POINT X Y Z POINT X Y Z
 1 0.400000E 01 0.400000E 01 0.200000E 01 1 0.400000E 01 0.400000E 01 0.200000E 01
 2 0.200000E 01 0.400000E 01 0.200000E 01 2 0.200000E 01 0.400000E 01 0.200000E 01
 3 0.200000E 01 0.200000E 01 0.300000E 01 3 0.200000E 01 0.200000E 01 0.300000E 01

***** DATA NAME- *SCOPLA * IPLA11 COMBINED WITH IPLA0
 POINT X Y Z POINT X Y Z
 1 0.400000E 01 0.400000E 01 0.300000E 01 1 0.400000E 01 0.400000E 01 0.300000E 01
 2 0.200000E 01 0.400000E 01 0.300000E 01 2 0.200000E 01 0.400000E 01 0.300000E 01
 3 0.200000E 01 0.200000E 01 0.500000E 01 3 0.200000E 01 0.200000E 01 0.500000E 01
 4 0.200000E 01 0.200000E 01 0.500000E 01 4 0.200000E 01 0.200000E 01 0.500000E 01
 5 0.200000E 01 0.200000E 01 0.300000E 01 5 0.200000E 01 0.200000E 01 0.300000E 01
 6 0.200000E 01 0.200000E 01 0.300000E 01 6 0.200000E 01 0.200000E 01 0.300000E 01
 7 0.200000E 01 0.200000E 01 0.300000E 01 7 0.200000E 01 0.200000E 01 0.300000E 01

POINT CONNECTING POINTS POINT CONNECTING POINTS POINT CONNECTING POINTS
 1 2, 4, 6, 8, 10, 12 2 5, 7, 9, 11 3 1, 3, 5, 7, 9, 11, 13
 4 1, 3, 5, 7, 9, 11 5 2, 4, 6, 8, 10 6 1, 3, 5, 7, 9, 11, 13
 7 2, 4, 6, 8, 10 8 1, 3, 5, 7, 9, 11, 13

***** DATA NAME- *IPLA12 *

Figure 35. Group F Sample Problems Program Results
 (18 pages)

SHEMED RECTANGLE LOOKING AT SCOPLA

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|--------------|--------------|--------------|-------|--------------|--------------|--------------|
| 1 | 0.100000E 01 | 0.100000E 01 | 0.120000E 01 | 1 | 0.100000E 01 | 0.100000E 01 | 0.100000E 01 |
| 2 | 0.100000E 02 | 0.100000E 01 | 0.100000E 01 | 2 | 0.100000E 02 | 0.100000E 01 | 0.100000E 01 |
| 3 | 0.130000E 02 | 0.750000E 01 | 0.400000E 01 | 3 | 0.100000E 02 | 0.700000E 01 | 0.100000E 01 |

**** DATA NAME= *SPIPE1 * HORIZONTAL PARALLELEPIPED WITH LINE N=100 TO SPIPEZ

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|--------------|--------------|--------------|-------|--------------|--------------|--------------|
| 1 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 1 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 2 | 0.100000E 02 | 0.400000E 01 | 0.100000E 01 | 2 | 0.100000E 02 | 0.400000E 01 | 0.100000E 01 |
| 3 | 0.100000E 02 | 0.400000E 01 | 0.100000E 01 | 3 | 0.100000E 02 | 0.400000E 01 | 0.100000E 01 |
| 4 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 4 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 5 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 5 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 6 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 6 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 7 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 7 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 8 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 8 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 9 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 9 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 10 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 10 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|--------------|--------------|--------------|-------|--------------|--------------|--------------|
| 1 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 1 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 2 | 0.100000E 02 | 0.400000E 01 | 0.100000E 01 | 2 | 0.100000E 02 | 0.400000E 01 | 0.100000E 01 |
| 3 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 3 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 4 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 4 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 5 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 5 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 6 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 6 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 7 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 7 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 8 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 8 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 9 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 9 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |
| 10 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 | 10 | 0.100000E 01 | 0.400000E 01 | 0.100000E 01 |

**** DATA NAME= *SPIPE2 * VERTICAL PARALLELEPIPED

SURFACE SPECIFICATIONS=

ID OF X-SECTIONS = 2

NO OF X-SECTION BOUNDARY DIVISIONS = 4

LOCATION OF VERTICAL CENTERLINE, X= 0.700000E 01, Y= 0.100000E 02

| X-SECTION #0. | X-AXIS RADIUS | Y-AXIS RADIUS | ELEVATION ABOVE XY PLANE |
|---------------|---------------|---------------|--------------------------|
| 1 | 0.200000E 01 | 0.200000E 01 | 0.100000E 01 |
| 2 | 0.200000E 01 | 0.200000E 01 | 0.100000E 02 |

THE FOLLOWING INTERNALLY GENERATED SURFACE DATA RESULT FROM THE ABOVE SPECIFICATIONS=

| POINT | X | Y | Z | POINT | X | Y | Z |
|-------|--------------|--------------|--------------|-------|--------------|--------------|--------------|
| 1 | 0.600000E 01 | 0.100000E 02 | 0.100000E 01 | 1 | 0.600000E 01 | 0.100000E 02 | 0.100000E 01 |
| 2 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 | 2 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 |
| 3 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 | 3 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 |
| 4 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 | 4 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 |
| 5 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 | 5 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 |
| 6 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 | 6 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 |
| 7 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 | 7 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 |
| 8 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 | 8 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 |
| 9 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 | 9 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 |
| 10 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 | 10 | 0.100000E 01 | 0.100000E 02 | 0.100000E 01 |

Figure 35. Group F Sample Problems Program Results
(continued)

| POINT | CONNECTING POINTS |
|-------|-------------------|-------|-------------------|-------|-------------------|-------|-------------------|
| 1 | 3, 2, 7, 0 | 4 | 1, 0, 8, 1 | 5 | 1, 8, 2, 0 | 6 | 2, 0, 5, 7 |
| 2 | 7, 0, 5, 0 | 5 | 8, 0, 6, 5 | 6 | 1, 8, 2, 0 | 7 | 2, 0, 5, 7 |

***** DATA NAME= *SCOPLA * TO RUN SCOPLA IN COMPLEX MODE IN SILFAC

MULTISURFACE DATA=

SCOPLA, *

***** DATA NAME= *RZOFEM

MULTISURFACE DATA=

SPIPE1, SPIPE2, *

Figure 35. Group F Sample Problems Program Results
(continued)


```

0 7 1 2 3 4 5 6 7 8 9 10 11
1 2 3 4 5 6 7 8 9 10 11
2 3 4 5 6 7 8 9 10 11
3 4 5 6 7 8 9 10 11
4 5 6 7 8 9 10 11
5 6 7 8 9 10 11
6 7 8 9 10 11
7 8 9 10 11
8 9 10 11
9 10 11
10 11
11

```

```

TOTAL TIME IN SELFAC = 3.066 SECONDS.
THE ORAM FACTOR FROM SURFACE *IPLAIC* * TO SURFACE *8C0PLA * = 0.2733**
THE EXCHANGE COEFFICIENT (FBI) * 0.9811E 01 50 UNITS
THE MAPPING AREA * 0.360000E 02 50 UNITS
THE AREA OF SURFACE *IPLAIO * = 0.360000E 02 50 UNITS.
THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION=

```

```

***** DATA NAME= *IPLAIO *
POINT X Y Z
0.200000E 01 0.100000E 01 0.100000E 01 ***IPLAIC* OPERATED ORIGIN VECTOR Z
1 0.200000E 01 0.100000E 01 0.
2 0.300000E 01 0.200000E 01 0.
3 0.400000E 01 0.300000E 01 0.
COORDINATES OF POINTS ON BOUNDARY OF SURF *IPLAIO * FOR EACH Y INTERVAL
X=LEFT X=RIGHT X=1/4HT X=Y
0.200000E 01 0.800000E 01 0.100000E 01
0.200000E 01 0.200000E 01 0.800000E 01
0.200000E 01 0.400000E 01 0.600000E 01
0.200000E 01 0.600000E 01 0.400000E 01
0.200000E 01 0.800000E 01 0.200000E 01

```

Figure 35. Group F Sample Problems Program Results
(continued)

NAA CONFAC II REPORT SAMPLE PROFILES FROM FIG. (F)-K-A-10UPS,11/ /63

RUN NO. 7 DATA USED FOR THIS RUN- *IPLAIO=IPLAII*
 D 1
 * 3*

TH FORM FACTOR FROM SURFACE *IPLAIC * TO SURFACE *IPLAII * = 0.21136

THE EXCHANGE COEFFICIENT (FA) = 0.76088E 01 SQ UNITS

THE MAPPING AREA = 0.3600000E 02 SQ UNITS

THE AREA OF SURFACE *IPLAIO * = 0.3603000E 02 SQ UNITS.

THE AREA OF SURFACE *IPLAII * = 0.2500000E 02 SQ UNITS.

THE FOLLOWING ARE THE FINAL SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

***** DATA NAME= *IPLAIO *
 POINT X Y Z
 1 0.2000000E 01 0.1000000E 01 0.1000000E 01
 2 0.8000000E 01 0.1000000E 01 0.
 3 0.8000000E 01 0.7000000E 01 0.

***** DATA NAME= *IPLAII *
 POINT X Y Z
 1 0.4000000E 01 0.4000000E 01 0.3000000E 01
 2 0.4000000E 01 0.4000000E 01 0.3000000E 01
 3 0.9000000E 01 0.9000000E 01 0.3000000E 01
 COORDINATES OF POINTS ON BOUNDARY OF SURF *IPLAIO * FOR EACH Y INTERVAL

| | X-LEFT | X-RIGHT | Y | X-LEFT | X-RIGHT | Y |
|---|---------------|---------------|---------------|---------------|---------------|---------------|
| 1 | 0.2000000E 01 | 0.8000000E 01 | 0.1000000E 01 | 0.2000000E 01 | 0.8000000E 01 | 0.2000000E 01 |
| 2 | 0.2000000E 01 | 0.8000000E 01 | 0.3000000E 01 | 0.2000000E 01 | 0.8000000E 01 | 0.4000000E 01 |
| 3 | 0.9000000E 01 | 0.9000000E 01 | 0.3000000E 01 | 0.9000000E 01 | 0.9000000E 01 | 0.3000000E 01 |

Figure 35. Group F Sample Problems Program Results (continued)

0.2000000E 01 0.8000000E 01 0.5000000E 01 0.2000000E 01 0.6000000E 01
 0.2000000E 01 0.8000000E 01 0.7000000E 01 0.2000000E 01 0.6000000E 01

NO. OF HORIZONTAL INCREMENTS* 6 NO. OF VERTICAL INCREMENTS* 6

THE FOLLOWING ARE PLANE POIT CONFIGURATIVE FACTORS COMPUTED FOR THIS RUN
 LOWEST GRID LINE FIRST, FROM X=LEFT TO X=RIGHT.

| | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|
| 0.257112E-01 | 0.347105E-01 | 0.448790E-01 | 0.534622E-01 | 0.584075E-01 | 0.584075E-01 |
| 0.391952E-01 | 0.557620E-01 | 0.759500E-01 | 0.939483E-01 | 0.104539E-01 | 0.104539E-01 |
| 0.939483E-01 | 0.871659E-01 | 0.120462E-00 | 0.162442E-00 | 0.183005E-00 | 0.183005E-00 |
| 0.175228E-00 | 0.120462E-00 | 0.192473E-00 | 0.255910E-00 | 0.291052E-00 | 0.291052E-00 |
| 0.255910E-00 | 0.162442E-00 | 0.255910E-00 | 0.324691E-00 | 0.392766E-00 | 0.392766E-00 |
| 0.324691E-00 | 0.183005E-00 | 0.291052E-00 | 0.291052E-00 | 0.449616E-00 | 0.449616E-00 |
| 0.449616E-00 | 0.183005E-00 | 0.291052E-00 | 0.392766E-00 | 0.449616E-00 | 0.449616E-00 |
| 0.104539E-00 | 0.183005E-00 | 0.291052E-00 | 0.392766E-00 | 0.449616E-00 | 0.449616E-00 |
| 0.104539E-00 | 0.183005E-00 | 0.291052E-00 | 0.392766E-00 | 0.449616E-00 | 0.449616E-00 |
| 0.392766E-00 | 0.183005E-00 | 0.291052E-00 | 0.392766E-00 | 0.449616E-00 | 0.449616E-00 |

Figure 35. Group F Sample Problems Program Results
 (continued)


```

5 7 1 3 5 19 12 11 13 15 20 9 1 15 16 22 9 1
6 1 1 3 5 19 20 7 21 14 17 11 13 15 16 22 9 1
6 3 1 3 5 19 20 7 21 14 17 11 13 15 16 22 9 1
6 4 1 3 5 19 20 7 21 14 17 11 13 15 16 22 9 1
6 6 1 3 5 19 20 7 21 14 17 11 13 15 16 22 9 1
6 7 1 3 5 19 20 7 21 14 17 11 13 15 16 22 9 1
7 2 1 3 5 6 19 20 18 17 11 13 21 14 16 22 43 8 7 1
7 3 1 3 5 6 8 7 19 18 17 11 13 15 16 20 9 1
7 4 1 3 5 6 8 7 19 18 17 11 13 15 16 20 9 1
7 6 1 3 5 6 8 7 19 18 12 10 11 13 15 16 20 9 1
7 7 1 3 5 6 8 7 19 16 18 17 11 13 15 17 20 9 1

```

TOTAL TIME IN SILFAL = 15.570 SECONDS.

THE FORM FACTOR FROM SURFACE = 1PLAIG * TO SURFACE * 020FEM * = C.228750

THE EXCHANGE COEFFICIENT (EFA3) = 0.10171E 02 50 UNITS

THE MAPPING AREA = C.9400002L 02 50 UNITS

THE AREA OF SURFACE = 1PLAID * = C.3600000E 02 50 UNITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

```

***** DATA NAME= *1PLAID *
POINT X Y Z POINT X Y Z
1 0.200000E 01 0.100000E 01 0.100000E 01-- (INTERMEDIATE ORIENTATION VECTOR)
2 0.200000E 01 0.100000E 01 0.100000E 01
3 0.200000E 01 0.100000E 01 0.100000E 01
COORDINATES OF POINTS ON BOUNDARY OF SURF *1PLAID * F3D EACH Y INTERVAL
X=LEFT X=RIGHT Y X=LEFT X=RIGHT Y
3.200000E 01 0.800000E 01 0.100000E 01 0.200000E 01 0.200000E 01 0.200000E 01

```

Figure 35. Group F Sample Problems Program Results
(continued)

0.200000E 01 0.800000E 01 0.300000E 01 0.300000E 01 0.800000E 01 0.800000E 01
 0.200000E 01 0.800000E 01 0.200000E 01 0.200000E 01 0.800000E 01 0.800000E 01
 0.200000E 01 0.800000E 01 0.700000E 01 0.700000E 01 0.800000E 01 0.800000E 01

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 6

THE FOLLOWING ARE FRAME PRINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN
 LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

| | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|
| C-114509E-00 | 0.132940E-00 | 0.185789E-00 | 0.152594E-00 | 0.153566E-00 | 0.188571E-00 |
| C-117203E-00 | 0.175849E-00 | 0.193505E-00 | 0.202820E-00 | 0.204504E-00 | 0.198288E-00 |
| C-189934E-00 | 0.225935E-00 | 0.280959E-00 | 0.231254E-00 | 0.204209E-00 | 0.257806E-00 |
| C-190098E-00 | 0.267809E-00 | 0.295793E-00 | 0.311554E-00 | 0.317054E-00 | 0.311072E-00 |
| C-276133E-00 | 0.316139E-00 | 0.349205E-00 | 0.340828E-00 | 0.394524E-00 | 0.394036E-00 |
| C-368845E-00 | 0.316606E-00 | 0.349205E-00 | 0.365619E-00 | 0.380977E-00 | 0.378775E-00 |
| C-368845E-00 | 0.303433E-00 | 0.350173E-00 | 0.384522E-00 | 0.346277E-00 | 0.386827E-00 |
| C-240001E-00 | | | | | |
| C-352801E-00 | | | | | |

Figure 35. Group F Sample Problems Program Results
 (continued)


```

5 7 1 3 5 7 1 1 7 1
6 2 1 3 5 6 8 7 1
0 2 1 3 5 6 8 7 1
0 2 1 3 5 6 8 7 1
0 5 1 3 5 6 8 7 1
0 6 1 3 5 6 8 7 1
7 1 1 3 5 6 8 7 1
7 2 1 3 5 6 8 7 1
7 3 1 3 5 6 8 7 1
7 4 1 3 5 6 8 7 1
7 5 1 3 5 6 8 7 1
7 6 1 3 5 6 8 7 1
7 7 1 3 5 6 8 7 1

```

```

TOTAL TIME IN SILFAC = 1.484 SECONDS.
THE FORM FACTOR FROM SURFACE *IPLAIO * TO SURFACE *SP1PEI * = 0.421672
LX EXCHANGE COEFFICIENT (FAI) = 0.77299E 01 SC UNITS
THE MAPPING AREA = 0.3660000E 02 SQ UNITS
THE AREA OF SURFACE *IPLAIO * = 0.3660000E 02 SQ UNITS.

```

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION*

```

***** DATA NAME= *IPLAIO *
PRINT
  1 0.00000E 01 0.100000E 01 0.100000E 01-----INTERMALLY GENERATED ORIENTATION VECTORS X Y Z
  2 0.000000E 01 0.000000E 01 0.000000E 01 0.
  3 0.000000E 01 0.000000E 01 0.
***** DATA NAME= *SP1PEI *

```

Figure 35. Group F Sample Problems Program Results
(continued)

NIA CONVAC II REPORT SAMPLE PROBLEMS FROM FIG. 1(F)-K...TOUPS:11/1763

RUN NO. 5 DATA USED FOR THIS RUN = *SPLA12+SCOLA*
 D 1 1*

SURFACE 2 SILHOUETTE COMPUTED FROM MAPPING POINT SHOW

| | | | | | |
|---------|---|---|---|---|---|
| MAPPING | 5 | 6 | 7 | 8 | 5 |
| LINE | 0 | 1 | 0 | 1 | 0 |
| PI | 1 | 2 | 3 | 4 | 5 |
| 1 | 1 | 2 | 3 | 4 | 5 |
| 2 | 1 | 2 | 3 | 4 | 5 |
| 3 | 1 | 2 | 3 | 4 | 5 |
| 4 | 1 | 2 | 3 | 4 | 5 |
| 5 | 1 | 2 | 3 | 4 | 5 |
| 6 | 1 | 2 | 3 | 4 | 5 |
| 7 | 1 | 2 | 3 | 4 | 5 |
| 8 | 1 | 2 | 3 | 4 | 5 |
| 9 | 1 | 2 | 3 | 4 | 5 |
| 10 | 1 | 2 | 3 | 4 | 5 |
| 11 | 1 | 2 | 3 | 4 | 5 |
| 12 | 1 | 2 | 3 | 4 | 5 |
| 13 | 1 | 2 | 3 | 4 | 5 |
| 14 | 1 | 2 | 3 | 4 | 5 |
| 15 | 1 | 2 | 3 | 4 | 5 |
| 16 | 1 | 2 | 3 | 4 | 5 |
| 17 | 1 | 2 | 3 | 4 | 5 |
| 18 | 1 | 2 | 3 | 4 | 5 |
| 19 | 1 | 2 | 3 | 4 | 5 |
| 20 | 1 | 2 | 3 | 4 | 5 |
| 21 | 1 | 2 | 3 | 4 | 5 |
| 22 | 1 | 2 | 3 | 4 | 5 |
| 23 | 1 | 2 | 3 | 4 | 5 |
| 24 | 1 | 2 | 3 | 4 | 5 |
| 25 | 1 | 2 | 3 | 4 | 5 |
| 26 | 1 | 2 | 3 | 4 | 5 |
| 27 | 1 | 2 | 3 | 4 | 5 |
| 28 | 1 | 2 | 3 | 4 | 5 |
| 29 | 1 | 2 | 3 | 4 | 5 |
| 30 | 1 | 2 | 3 | 4 | 5 |
| 31 | 1 | 2 | 3 | 4 | 5 |
| 32 | 1 | 2 | 3 | 4 | 5 |
| 33 | 1 | 2 | 3 | 4 | 5 |
| 34 | 1 | 2 | 3 | 4 | 5 |
| 35 | 1 | 2 | 3 | 4 | 5 |
| 36 | 1 | 2 | 3 | 4 | 5 |
| 37 | 1 | 2 | 3 | 4 | 5 |
| 38 | 1 | 2 | 3 | 4 | 5 |
| 39 | 1 | 2 | 3 | 4 | 5 |
| 40 | 1 | 2 | 3 | 4 | 5 |
| 41 | 1 | 2 | 3 | 4 | 5 |
| 42 | 1 | 2 | 3 | 4 | 5 |
| 43 | 1 | 2 | 3 | 4 | 5 |
| 44 | 1 | 2 | 3 | 4 | 5 |
| 45 | 1 | 2 | 3 | 4 | 5 |
| 46 | 1 | 2 | 3 | 4 | 5 |
| 47 | 1 | 2 | 3 | 4 | 5 |
| 48 | 1 | 2 | 3 | 4 | 5 |
| 49 | 1 | 2 | 3 | 4 | 5 |
| 50 | 1 | 2 | 3 | 4 | 5 |

Figure 35. Group F Sample Problems Program Results
 (continued)

```

5 7 4 1 3 2 1 4
6 1 3 2 1 4
0 3 4 3 2 1 4
0 3 4 3 2 1 4
0 3 4 3 2 1 4
7 1 4 3 2 1 4
7 1 4 3 2 1 4
7 1 4 3 2 1 4
7 1 4 3 2 1 4
7 1 4 3 2 1 4

```

```

TOTAL TIME IN SILFAC = 1.119 SECONDS.
THE FORM FACTOR FROM SURFACE *IPLA12 * TO SURFACF *SCOPLA * = 0.00882
THE EXCHANGE COEFFICIENT (EAF) = 0.10501E 01 SQ UNITS
THE MAPPING AREA = 0.255559E 02 SQ UNITS
THE AREA OF SURFACE *IPLA12 * = 0.255559E 02 SQ UNITS.
THE AREA OF * S SQ UNITS.

```

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

```

***** DATA NAME= *IPLA12 *
POINT 0. X Y Z
1 0. 0. 0.100000E 01---(INITIALLY GENERATED ORIENTATION VECTOR)
3 0.000000E 01 0.000000E 01 0.
***** DATA NAME= *SCOPLA *

```

Figure 35. Group F Sample Problems Program Results
(continued)

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (F)-K-A-TOPS+11/1/66

PUN NO. 6 DATA USED FOR THIS RUN= *IPLA12*BCPLA*
D 1 1*

SURFACE 1 MUST BE IN THE XY PLANE OF ITS CS WHEN SURFACE 2 IS CLASS B-THE PUN ABORTED.

Figure 35. Group F Sample Problems Program Results
(continued)

APPENDIX B

PROGRAM DECK SETUP, LISTINGS, AND MAPS

The program deck arrangement shown in Figure 36 contains a main program and six subprograms which are listed in this appendix. A listing of the main program, 7J360, is shown in Figure 37 followed by a map of the core storage locations in Figure 38.

The first subprogram in the deck setup is subroutine UNIVFC which is shown in Figure 39 and the map of core storage in Figure 40. The transformation subroutine, TAPRI, is presented in Figure 41 and the map of core storage in Figure 42. The listing and map of subroutine DFIGU is presented in Figures 43 and 44. The listing and map of subroutine MAP, is presented in Figure 45 and 46. The listing of the subroutine FACTOR is presented in Figure 47 and the map of core storage in Figure 48. Subroutine SILFAC listing and core storage is presented in Figure 49. Figure 51 shows the variable formats used by this program.

This IBM FORTRAN II program uses two input-output statements which must be modified for computing systems other than the MAA Monitor, FIB III, system. These are

```
READ N, List
PRINT N, List
```

A convenient FAP assembled program is included which will convert the READ-PRINT statement to,

```
READ INPUT TAPE 5, N, List
WRITE OUTPUT TAPE 6, N, List
```

This assembly is listed in Figure 52. The convert to any other computing system using peripheral equipment and not using the same tape designations, the last three EOU cards are simply changed to read

```
MIN EOU A (Input statement tape number)
MOUT EOU B (Output statement tape number)
MPUNCH EOU C (Punch statement tape number)
```

For computing centers using attached printing equipment, the FAP assembly can be removed and the program will execute in that system.

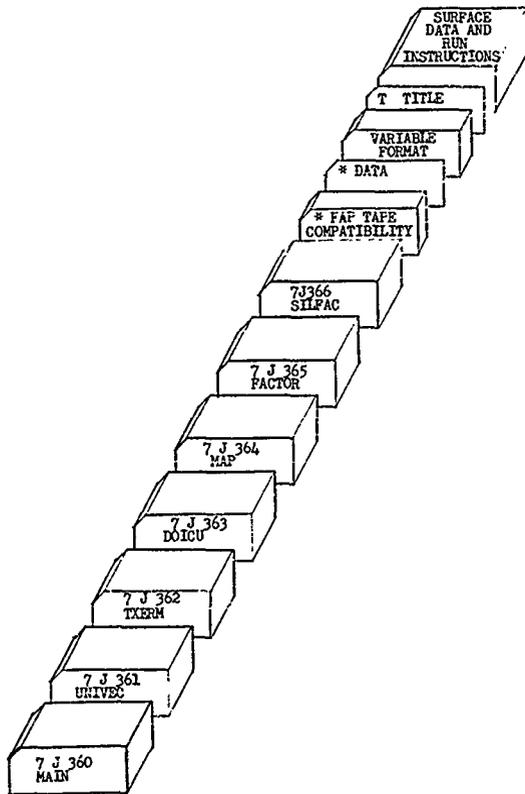


FIGURE 36. PROGRAM DECK SETUP

```

C CONFAC II-MAIN PROG-ANALYSIS AND PROG BY K.A.TOUPS,MAA SID. 11/1/63 36000100
C FACTORS BETWEEN SUGGESTS THE COMPUTATION OF CONFIGURATION AND TORN 36000200
C FORTRAN SUBROUTINES USED ARE UNIVCG, XFRMNDJGCMAP, FACTOR, AND SILFAC 36000300
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C F(1557),F(1558),F(1559),F(1560),F(1561),F(1562),F(1563),F(1564),F(1565), 36016800
C F(1566),F(1567),F(1568),F(1569),F(1570),F(1571),F(1572),F(1573),F(1574), 36016900
C F(1575),F(1576),F(1577),F(1578),F(1579),F(1580),F(1581),F(1582),F(1583), 36017000
C F(1584),F(1585),F(1586),F(1587),F(1588),F(1589),F(1590),F(1591),F(1592), 36017100
C F(1593),F(1594),F(1595),F(1596),F(1597),F(1598),F(1599),F(1600),F(1601), 36017200
C F(1602),F(1603),F(1604),F(1605),F(1606),F(1607),F(1608),F(1609),F(1610), 36017300
C F(1611),F(1612),F(1613),F(1614),F(1615),F(1616),F(1617),F(1618),F(1
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73300  C=MFAC II-MAIN PROG-ANALYSIS AND PROG BY K.A.TOURP,MAA SID, 11/1/63
12200  F1 (E1-F111D)
C SELECT 13 18400
C READ REMAINDER OF THIS SURFACE DATA
12400  M=PP11
      F5=PI(3,2,1);(P(K,M,1),K=1,3),M=3,MP)
      GO TO 22200
C READ CLASS 5 DATA-INTERNAL PLANE POLYGON-CONSTANT SILUET BOUNDARY PTS. 3016300
13000  M=PP11
      F5= SI(4,5,10,15,1),M=11,MP11)
C PRINT SPECIFICATIONS
13100  M=SID
      GO TO 10500
C READ DATA FOR A PLANE SURFACE W/CONNECTION DATA-CLASS 4
13200  M=PP11
      F5= SI(4,5,10,15,1),M=11,MP11)
C ALYAGE COUNTER LOCATING CONNECTIONS DATA
15000  I=1;I=1;1114600,14600,14500
      I=5000 PRINT
      GO TO 13400
C ERASE SURFACE DATA LOCATION TO CONNECTIONS
14600  ACI(1)=1
C READ SENSE LIGHT 1
14800  M=PP11
C BOUNDARY LINE 0
      READ
      I=1;I=1;M=1
C TEST AGAINST MAX ALLOWABLE
C READ FFC(PP11-100 115200,15200 12220
15200  M=PP11
      F 7*PI(2-2,1),P(3,2,1),PP11,2,1,C1,M=1,4),
      GO TO 42000
C READ CLASS 6 DATA TO GENERATE A PLANE POLYGON OR MULTIFACETED SURFACE
16000  M=PP11
      W/CONNECTION DATA
      GO TO SENSE LIGHT 1
3015700
3015800
3015900
3016000
3016100
3016200
3016300
3016400
3016500
3016600
3016700
3016800
3016900
3017000
3017100
3017200
3017300
3017400
3017500
3017600
3017700
3017800
3017900
3018000
3018100
3018200
3018300
3018400
3018500
3018600
3018700
3018800
3018900
3019000
3019100
3019200
3019300
3019400
3019500
3019600
3019700
3019800
3019900

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Figure 37. Main Program Listing (continued)


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73300  COMPAC II-MAIN PROG-ANALYSIS AND PROG BY K.A.-TOUPS,MAA SID, 11/71/83
41800  PPI(1,1)=P(1,1,1)
PPI(2,1)=P(2,1,1)
PPI(3,1)=P(3,1,1)
462100  PPI(1,1)=P(1,1,1)
462200  PPI(2,1)=P(2,1,1)
462300  PPI(3,1)=P(3,1,1)
C TRANSLATE TO GENERATE CONNECTIONS DATA
C CLAS TO 40000
C CLAS TO SURFACE TO FACILITATE AREA AND FACTOR COMPUTATION--CLASS 1-2
22000  K=0*1
P11(K)=P(1,1,1)
P12(K)=P(2,1,1)
P13(K)=P(3,1,1)
P14(K)=P(4,1,1)
P15(K)=P(5,1,1)
22400  IF(ASC(1))4000,44000,22500
C GENERATE ORIENTATION VECTOR OCCS FOR CLASSES 1-6
22600  ORIENT=ORIENT+P11(K)
ORIENT=ORIENT+P12(K)
ORIENT=ORIENT+P13(K)
ORIENT=ORIENT+P14(K)
ORIENT=ORIENT+P15(K)
SENSE LIGHT 3
SENSE LIGHT 4
SENSE LIGHT 5
SENSE LIGHT 6
IF(SENSE LIGHT 3)22700,21500
IF(SENSE LIGHT 4)22800,21500
IF(SENSE LIGHT 5)22900,21500
IF(SENSE LIGHT 6)23000,21500
22700  IF(ABS(FVIM))=-.1123000,25000,24700
23000  IF(ABS(FVIM))=-.1123000,25000,24700
24000  IF(SENSE LIGHT 4)24000,24500
24000  IF(SENSE LIGHT 5)24000,24500
24500  GO TO 26000
24500  GO TO 26000
C IF PFS 1-2 AND LAST FORM A TRIANGLE LYING IN THE SURFACE, THE ORIENTA-
C THE SURFACE AREA OF THE TRIANGLE AND THE SURFACE AREA OF THE TRIANGLE
C THE "ANGLE" ARE AREAS COMPUTED ON THE XY AND XZ PLANES, AND ARE
C OPPOSITE IN SIGN ON XZ PLANE. THE SIGN OF THE DC IS HEREFOR REVERSED
C TO YIELD A POSITIVE NUMBER FOR AREA.
25000  DC=-VIM1
25000  DC=-VIM1
25000  GO TO 26000
25000  GO TO 26000
26000  GO TO 26000
C PUT IN COORDINATE OF CLOSURE POINT TEMPORARILY IN NO.1 SPOT IN ARRAY
C PP CALLING FOR COMPUTATION.
C PP CALLING FOR COMPUTATION.
C COMPUTE PROJECTED AREA ON PRINCIPAL PLANE N1#2
36027400
36027500
36027600
36027700
36027800
36027900
36028000
36028100
36028200
36028300
36028400
36028500
36028600
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36029000
36029100
36029200
36029300
36029400
36029500
36029600
36029700
36029800
36029900
36030000
36030100
36030200
36030300
36030400
36030500
36030600
36030700
36030800
36030900
36031000
36031100
36031200

```

Figure 37. Main Program Listing (continued)

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36031300
36031400
36031500
36031600
36031700
36031800
36031900
36032000
36032100
36032200
36032300
36032400
36032500
36032600
36032700
36032800
36032900
36033000
36033100
36033200
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36034200
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36034400
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36034700
36034800
36034900
36035000

```

GO 26500 M=Z
 26500 ARK(1)=ARK(1)
 C IF ARK(1)=ARK(1)/DC/2
 C IF THE AREA IS NEGATIVE, THE ORIENTATION VECTOR MUST BE REVERSED. THE
 C AREA IS NEGATIVE WHEN THE ANGLE OUTSIDE THE SURFACE
 C PRIMER WHEN THE X-PRODUCT WAS TAKEN TO CALCULATE THE ORIENTATION VECTOR.
 IF AREA(1) IS 127000, 27500, 27500
 24000
 V(1)=V(1)
 V(2)=V(2)
 V(3)=V(3)
 C ERRECT UNIT ORIENTATION VECTOR
 27500 P(1)=P(1)
 P(2)=P(2)
 P(3)=P(3)
 GO TO 44000
 L, CIRCULAR IF X-SECTIONS ARE SIMILAR, AND IF CIRCULAR OR ELLIPTICAL
 30000 GO 31500 WITH=SEC
 RAL=ARK(1)/V(1)
 RAL=ARK(2)/V(2)
 RAL=ARK(3)/V(3)
 C SL3 IS USED TO GO TO 30000, 30500
 30500 IF=SENSE LIGHT 3134000, 32000
 L, GO TO 44000 TOLERANCE FOR NON-SIMILARITY
 X(1)=X(1)-.005*RAF
 C TEST CIRCULARITY
 31000 IF=SENSE LIGHT 3134000, 31500, 32000
 C THIS SECTION IS CIRCULAR WITH TOLERANCE -.SL4 ON
 31500 SENSE LIGHT 4
 C IF SIMILAR, CONTINUE WITH NEXT SECTION
 34000 IF=TRANSFIRAF=HALJ-R(1) 33000, 33000, 40000
 35000 IF=SENSE LIGHT 33000, 33000, 40000
 C THEY ARE CIRCULAR
 C THE AREA OF ONE FACE ONLY THROUGH ALL X-SECTIONS NEED BE COMPUTED
 C THE AREA OF ALL FACES THROUGH ALL X-SECTIONS, ALL MUST BE COMPUTED
 L FOR ELLIPTICAL X-SECTIONS EXCEPT FOR AN EVEN NO. OF SIDES WHEN ONLY

Figure 37. Main Program Listing (continued)


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73800  CONCAC II, MAIN PROC-ANALYSIS AND PH00 BY K.A.TOUSS-MAA SID, 11/1/63
C TEST FOR NAME=MEANS NO TXFRM NEG0- LOAD NO IN LP(WP) FOR NO TXFRM
C IF FILE(LPZ)36000-59500-58000
C IF THE WORD IN LOCATION KPZ IS NOT BLANK, VERIFY PROPER CLASS--9.
58000 IF(LC(17)+9358500-59000-58500
      FZ2
58500 PRINT 015000
C IF THE DATA CLASS IS BELOW 6, TXFRM THE DATA. THE MEM LOCATION OF THE
C TXFRM COORDINATES IS ESTABLISHED IN SUB TXFRM THROUGH ARRAY LP(6P)
59000 IF(XABS(FINSC(1))-6159500-59300+59200
      FZ3
59200 GO TO 61000
C SL4 IS USED TO INDICATE A PRIMARY TXFRM
59300 CALL TXFRM
      FZ4
59500 GO TO 60000
C TXFRM IS CALLED IN SUB TXFRM
60000 INITIALIZE SUBSECTION FLAGS
60200 LINKP=1
C IF SURFACE 2 IS A SPHERE, TRANSFER SPHERE COORDINATES TO LOC 6 IN P
60200 P(1+1,61)=SP(1,61)
      FZ5
      FZ6
      FZ7
      FZ8
      FZ9
      FZ10
      FZ11
      FZ12
      FZ13
      FZ14
      FZ15
      FZ16
      FZ17
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66000 CONTINUE
C PROCEED TO NEXT RUN
67000
67500 IF IN(0,167520,67550,67600
77500 IF IN(0,167520,67550,67520
67530 PRINT '(4)167540,67540,67530
      PRINT
      F3
C IF GO TO 81000
67540 IF IN(5,167525,67525,67545
67545 PRINT
67550 IF IN(5,167525,67525,67545
C ALL ON BEANS O OR NEG Z CORRD IN CLASS 8 SURFACE-PRINT DIAGNOSTIC
67540 OR TO 81000
67600 CALL FACTOR
67700 PRINT
C PRINT THE AREA INDICATING AREA OF EACH SURFACE SEEN, IF NOT ALL.
D0 70000 NP=1,2
  J3=LDLKP)
  *7800 NP=1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23,24,25,26,27,28,29,30,31,32,33,34,35,36,37,38,39,40,41,42,43,44,45,46,47,48,49,50,51,52,53,54,55,56,57,58,59,60,61,62,63,64,65,66,67,68,69,70,71,72,73,74,75,76,77,78,79,80,81,82,83,84,85,86,87,88,89,90,91,92,93,94,95,96,97,98,99,100,101,102,103,104,105,106,107,108,109,110,111,112,113,114,115,116,117,118,119,120,121,122,123,124,125,126,127,128,129,130,131,132,133,134,135,136,137,138,139,140,141,142,143,144,145,146,147,148,149,150,151,152,153,154,155,156,157,158,159,160,161,162,163,164,165,166,167,168,169,170,171,172,173,174,175,176,177,178,179,180,181,182,183,184,185,186,187,188,189,190,191,192,193,194,195,196,197,198,199,200,201,202,203,204,205,206,207,208,209,210,211,212,213,214,215,216,217,218,219,220,221,222,223,224,225,226,227,228,229,230,231,232,233,234,235,236,237,238,239,240,241,242,243,244,245,246,247,248,249,250,251,252,253,254,255,256,257,258,259,260,261,262,263,264,265,266,267,268,269,270,271,272,273,274,275,276,277,278,279,280,281,282,283,284,285,286,287,288,289,290,291,292,293,294,295,296,297,298,299,300,301,302,303,304,305,306,307,308,309,310,311,312,313,314,315,316,317,318,319,320,321,322,323,324,325,326,327,328,329,330,331,332,333,334,335,336,337,338,339,340,341,342,343,344,345,346,347,348,349,350,351,352,353,354,355,356,357,358,359,360,361,362,363,364,365,366,367,368,369,370,371,372,373,374,375,376,377,378,379,380,381,382,383,384,385,386,387,388,389,390,391,392,393,394,395,396,397,398,399,400,401,402,403,404,405,406,407,408,409,410,411,412,413,414,415,416,417,418,419,420,421,422,423,424,425,426,427,428,429,430,431,432,433,434,435,436,437,438,439,440,441,442,443,444,445,446,447,448,449,450,451,452,453,454,455,456,457,458,459,460,461,462,463,464,465,466,467,468,469,470,471,472,473,474,475,476,477,478,479,480,481,482,483,484,485,486,487,488,489,490,491,492,493,494,495,496,497,498,499,500,501,502,503,504,505,506,507,508,509,510,511,512,513,514,515,516,517,518,519,520,521,522,523,524,525,526,527,528,529,530,531,532,533,534,535,536,537,538,539,540,541,542,543,544,545,546,547,548,549,550,551,552,553,554,555,556,557,558,559,560,561,562,563,564,565,566,567,568,569,570,571,572,573,574,575,576,577,578,579,580,581,582,583,584,585,586,587,588,589,590,591,592,593,594,595,596,597,598,599,600,601,602,603,604,605,606,607,608,609,610,611,612,613,614,615,616,617,618,619,620,621,622,623,624,625,626,627,628,629,630,631,632,633,634,635,636,637,638,639,640,641,642,643,644,645,646,647,648,649,650,651,652,653,654,655,656,657,658,659,660,661,662,663,664,665,666,667,668,669,670,671,672,673,674,675,676,677,678,679,680,681,682,683,684,685,686,687,688,689,690,691,692,693,694,695,696,697,698,699,700,701,702,703,704,705,706,707,708,709,710,711,712,713,714,715,716,717,718,719,720,721,722,723,724,725,726,727,728,729,730,731,732,733,734,735,736,737,738,739,740,741,742,743,744,745,746,747,748,749,750,751,752,753,754,755,756,757,758,759,760,761,762,763,764,765,766,767,768,769,770,771,772,773,774,775,776,777,778,779,780,781,782,783,784,785,786,787,788,789,790,791,792,793,794,795,796,797,798,799,800,801,802,803,804,805,806,807,808,809,810,811,812,813,814,815,816,817,818,819,820,821,822,823,824,825,826,827,828,829,830,831,832,833,834,835,836,837,838,839,840,841,842,843,844,845,846,847,848,849,850,851,852,853,854,855,856,857,858,859,860,861,862,863,864,865,866,867,868,869,870,871,872,873,874,875,876,877,878,879,880,881,882,883,884,885,886,887,888,889,890,891,892,893,894,895,896,897,898,899,900,901,902,903,904,905,906,907,908,909,910,911,912,913,914,915,916,917,918,919,920,921,922,923,924,925,926,927,928,929,930,931,932,933,934,935,936,937,938,939,940,941,942,943,944,945,946,947,948,949,950,951,952,953,954,955,956,957,958,959,960,961,962,963,964,965,966,967,968,969,970,971,972,973,974,975,976,977,978,979,980,981,982,983,984,985,986,987,988,989,990,991,992,993,994,995,996,997,998,999,1000,1001,1002,1003,1004,1005,1006,1007,1008,1009,1010,1011,1012,1013,1014,1015,1016,1017,1018,1019,1020,1021,1022,1023,1024,1025,1026,1027,1028,1029,1030,1031,1032,1033,1034,1035,1036,1037,1038,1039,1040,1041,1042,1043,1044,1045,1046,1047,1048,1049,1050,1051,1052,1053,1054,1055,1056,1057,1058,1059,1060,1061,1062,1063,1064,1065,1066,1067,1068,1069,1070,1071,1072,1073,1074,1075,1076,1077,1078,1079,1080,1081,1082,1083,1084,1085,1086,1087,1088,1089,1090,1091,1092,1093,1094,1095,1096,1097,1098,1099,1100,1101,1102,1103,1104,1105,1106,1107,1108,1109,1110,1111,1112,1113,1114,1115,1116,1117,1118,1119,1120,1121,1122,1123,1124,1125,1126,1127,1128,1129,1130,1131,1132,1133,1134,1135,1136,1137,1138,1139,1140,1141,1142,1143,1144,1145,1146,1147,1148,1149,1150,1151,1152,1153,1154,1155,1156,1157,1158,1159,1160,1161,1162,1163,1164,1165,1166,1167,1168,1169,1170,1171,1172,1173,1174,1175,1176,1177,1178,1179,1180,1181,1182,1183,1184,1185,1186,1187,1188,1189,1190,1191,1192,1193,1194,1195,1196,1197,1198,1199,1200,1201,1202,1203,1204,1205,1206,1207,1208,1209,1210,1211,1212,1213,1214,1215,1216,1217,1218,1219,1220,1221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,2222,2223,2224,2225,2226,2227,2228,2229,2230,2231,2232,2233,2234,2235,2236,2237,2238,2239,2240,2241,2242,2243,2244,2245,2246,2247,2248,2249,2250,2251,2252,2253,2254,2255,2256,2257,2258,2259,2260,2261,2262,2263,2264,2265,2266,2267,2268,2269,2270,2271,2272,2273,2274,2275,2276,2277,2278,2279,2280,2281,2282,2283,2284,2285,2286,2287,2288,2289,2290,2291,2292,2293,2294,2295,2296,2297,2298,2299,2300,2301,2302,2303,2304,2305,2306,2307,2308,2309,2310,2311,2312,2313,2314,2315,2316,2317,2318,2319,2320,2321,2322,2323,2324,2325,2326,2327,2328,2329,2330,2331,2332,2333,2334,2335,2336,2337,2338,2339,2340,2341,2342,2343,2344,2345,2346,2347,2348,2349,2350,2351,2352,2353,2354,2355,2356,2357,2358,2359,2360,2361,2362,2363,2364,2365,2366,2367,2368,2369,2370,2371,2372,2373,2374,2375,2376,2377,2378,2379,2380,2381,2382,2383,2384,2385,2386,2387,2388,2389,2390,2391,2392,2393,2394,2395,2396,2397,2398,2399,2400,2401,2402,2403,2404,2405,2406,2407,2408,2409,2410,2411,2412,2413,2414,2415,2416,2417,2418,2419,2420,2421,2422,2423,2424,2425,2426,2427,2428,2429,2430,2431,2432,2433,2434,2435,2436,2437,2438,2439,2440,2441,2442,2443,2444,2445,2446,2447,2448,2449,2450,2451,2452,2453,2454,2455,2456,2457,2458,2459,2460,2461,2462,2463,2464,2465,2466,2467,2468,2469,2470,2471,2472,2473,2474,2475,2476,2477,2478,2479,2480,2481,2482,2483,2484,2485,2486,2487,2488,2489,2490,2491,2492,2493,2494,2495,2496,2497,2498,2499,2500,2501,2502,2503,2504,2505,2506,2507,2508,2509,2510,2511,2512,2513,2514,2515,2516,2517,2518,2519,2520,2521,2522,2523,2524,2525,2526,2527,2528,2529,2530,2531,2532,2533,2534,2535,2536,2537,2538,2539,2540,2541,2542,2543,2544,2545,2546,2547,2548,2549,2550,2551,2552,2553,2554,2555,2556,2557,2558,2559,2560,2561,2562,2563,2564,2565,2566,2567,2568,2569,2570,2571,2572,2573,2574,2575,2576,2577,2578,2579,2580,2581,2582,2583,2584,2585,2586,2587,2588,2589,2590,2591,2592,2593,2594,2595,2596,2597,2598,2599,2600,2601,2602,2603,2604,2605,2606,2607,2608,2609,2610,2611,2612,2613,2614,2615
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STORAGE NOT USED BY PROGRAM

| DEC | DEC | DEC | DEC |
|------------|-------------|-----|-----|
| 4006 07646 | 14613 34425 | | |

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

| DEC | DEC | DEC | DEC |
|-------------------|-------------------|-------------------|-------------------|
| AMAP 13169 35501 | AREA 21067 51113 | AREAX 21011 51023 | CL 22094 31116 |
| C2 21945 22671 | C3 21795 52443 | CL 16140 37414 | OK 22154 2212 |
| FO 12132 51126 | FO 15746 35216 | OP 15179 35313 | SI 15037 18295 |
| F 15180 35514 | FV 14950 35146 | INC 14449 14471 | RC 20976 0740 |
| AD 22154 53112 | FP 15492 36204 | KX 15492 36205 | LD 16125 32401 |
| MSVSS 12023 35257 | MSVSS 15018 35312 | NOA 22100 53124 | MOD 22112 53140 |
| NOL 21157 51245 | NON 22114 53142 | ND3 15168 35503 | ND 75493 18205 |
| NOM 21402 52376 | NOR 21174 51750 | ND 15493 35203 | ND 51215 5098 |
| MSID 22101 53125 | MSL 25217 61201 | NSN 21269 51435 | NTILE 21293 51435 |
| NV 15182 35216 | NVL 15491 35215 | PAF 16131 37427 | PP 32763 27461 |
| AV 20968 51006 | NS 15182 35215 | SP 16445 40075 | TDA 22100 53124 |
| TD 22116 53142 | TSID 22101 53125 | VA 22094 53113 | Y 16154 37422 |
| ZS 20987 50273 | U 14889 35051 | V1 15368 36010 | Y 14768 34681 |

212

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

| DEC | DEC | DEC | DEC |
|----------------|----------------|----------------|----------------|
| FO 1993 07631 | F10 3777 07701 | F11 3753 07251 | F12 3741 02235 |
| F17 3650 07125 | F18 3657 07111 | F19 3633 07081 | F20 3621 07045 |
| F21 3597 07015 | F22 3565 07001 | F23 3573 08765 | F24 3577 08511 |
| F25 3409 06411 | F26 3474 06361 | F27 3451 06261 | F28 3427 06211 |
| F30 3345 06471 | F31 3321 06371 | F32 3285 06325 | F33 3271 06311 |
| F34 3269 06261 | F35 3237 06245 | F36 3214 06210 | F37 3202 06202 |
| F38 3189 06185 | F39 3165 06155 | F40 3141 06125 | F41 3117 06095 |
| F42 4006 05845 | F43 3897 07471 | F44 3865 07455 | F45 3833 07425 |

Figure 58. Main Program Core Storage Map

TJ380 CONFAC II-MAIN PROG-ANALYSIS AND PROC BY K.A.T.OUPS-NMA SID, 11/1/63 02/06/64 PAGE 19
 F7 3861 07425 F8 3849 07411 F9 3801 07331 FX 4003 07643

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS

| SYMBOL | LOC | SYMBOL | LOC | SYMBOL | LOC | SYMBOL | LOC |
|--------|------------|--------|------------|--------|------------|--------|------------|
| ANC | 3138 06102 | IC | 3137 06101 | COSB | 3130 06100 | DEC | 3129 06099 |
| IF | 3134 06076 | J1 | 3133 06075 | J2 | 3132 06074 | J3 | 3131 06073 |
| K | 3126 06066 | K5 | 3125 06065 | MM | 3124 06064 | N | 3123 06063 |
| N1 | 3122 06062 | N2 | 3121 06061 | NBLNK | 3120 06060 | NB | 3119 06059 |
| NK | 3118 06055 | NW | 3117 06054 | NX | 3116 06053 | NZ | 3115 06052 |
| NIC | 3110 06046 | NFS | 3109 06045 | NFT | 3108 06044 | NY | 3107 06043 |
| SCZ | 3100 06042 | SH | 3100 06041 | RAL | 3104 06040 | RJOL | 3103 06039 |
| STHC | 3098 06032 | XB | 3097 06031 | YR | 3096 06030 | Z | 3095 06029 |

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

| SYMBOL | LOC | SYMBOL | LOC | SYMBOL | LOC | SYMBOL | LOC |
|--------|-----|--------|-------|--------|-----|--------|-----|
| 831 | EFY | 1 | 05742 | EFN | LOC | EFN | LOC |

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

| | | | | | | | |
|------|------------|------|------------|------|-------------|------|------------|
| 33 | 3043 05763 | DEC | 3041 05761 | 43 | 32767 73777 | DEC | 3040 05760 |
| 61 | 3036 05734 | A100 | 2829 05415 | A104 | 2842 05432 | A107 | 2851 05443 |
| A102 | 2838 05426 | A106 | 2821 05421 | A108 | 2834 05426 | A109 | 2923 05611 |
| A104 | 2806 05432 | A108 | 2821 05421 | A1GC | 2934 05506 | A1GJ | 2935 05611 |
| A1GC | 2868 05530 | A1C1 | 2883 05647 | C1G0 | 3047 05747 | C1G2 | 3049 05750 |
| C1G7 | 3053 05755 | C1G8 | 3050 05752 | C1G5 | 3051 05753 | C1G6 | 3052 05754 |
| C1G9 | 3057 05761 | C1G0 | 3050 05752 | C1G0 | 3059 05763 | C1G1 | 3060 05764 |
| C1G1 | 3061 05765 | C1G2 | 3062 05766 | C1G4 | 3063 05767 | C1G1 | 3064 05770 |
| C1G4 | 3069 05775 | C105 | 3070 05776 | C107 | 3071 05777 | C108 | 3072 06000 |
| C1G5 | 3073 06001 | C1G0 | 3074 06002 | C1G7 | 3075 06003 | C1G8 | 3076 06004 |
| C1G6 | 3082 06002 | C1G1 | 3083 06003 | C1G2 | 3084 06004 | C1G3 | 3085 06005 |
| C1G0 | 3081 06011 | C1G1 | 3082 06012 | C1G2 | 3083 06013 | C1G3 | 3084 06014 |

Figure 36. Main Program Core Storage Map (continued)

| | | | | | | | |
|-------|------------|-------|------------|-------|------------|-------|------------|
| C11GH | 3085 06015 | C11G1 | 3086 06016 | C1201 | 3097 06017 | C209 | 3088 06020 |
| C120P | 3089 06021 | C120C | 3090 06022 | C120I | 3091 06023 | C20J | 3092 06024 |
| C1112 | 511 00777 | C1118 | 595 01123 | D112D | 944 01682 | D112C | 949 01685 |
| D112F | 957 01675 | D112U | 1183 02237 | D1131 | 1201 02363 | D113V | 1515 02153 |
| D1146 | 209 0313 | D1149 | 095 02602 | D1177 | 2598 05946 | D117U | 2602 05952 |
| D1233 | 1472 02760 | D123U | 1478 02768 | D124F | 1724 03274 | D1251 | 1974 03666 |
| D125W | 1985 03704 | D1264 | 2112 04100 | D1269 | 2135 04127 | D126A | 2159 04182 |
| D1265 | 2293 04365 | D1270 | 2560 05000 | D127R | 2588 05034 | D1282 | 2638 03116 |
| D178L | 2821 05405 | D1312 | 510 00776 | D1318 | 594 01122 | D1370 | 943 01681 |
| D1320 | 186 01178 | D1324 | 147 01179 | D138C | 2320 05406 | D147G | 705 00312 |
| D1404 | 221 00335 | D142L | 1077 02065 | D143F | 1376 02249 | D1440 | 1539 03003 |
| D1442 | 1667 05113 | D1443 | 2012 03250 | D145H | 765 03370 | D1470 | 2314 04242 |
| D1473 | 2491 04673 | D1479 | 2563 05003 | D147K | 2586 05032 | D1503 | 2014 00311 |
| D1512 | 508 00774 | D152F | 1956 01674 | D1540 | 1538 03002 | D1547 | 1577 03051 |
| D152L | 1976 03670 | D1555 | 2050 03767 | D1603 | 198 00366 | D1604 | 220 00334 |
| D162L | 1076 02064 | D164F | 1223 03273 | D165P | 2013 03735 | D1655 | 2292 04364 |
| D170E | 1732 03271 | D170J | 1440 00445 | D1750 | 2007 03727 | D1767 | 2215 02767 |
| E10 | 576 00602 | E134 | 1277 02375 | E135 | 1281 02401 | E137 | 1298 02422 |
| E130 | 1313 02441 | E139 | 1409 02601 | E13M | 1618 02612 | E140 | 1537 03001 |
| E13E | 1927 03657 | E161 | 2246 04306 | E177 | 2412 04834 | E17M | 2522 04732 |
| E170 | 2562 05012 | E17P | 2567 05007 | E17Q | 2573 05015 | E137R | 2590 05036 |

LOCATIONS OF NAMES IN TRANSFER VECTOR

| | | | | | | | |
|-------|----------|--------|----------|-------|---------|---------|----------|
| DEC | 001 | DEC | 002 | DEC | 003 | DEC | 004 |
| C05 | 00012 | C01CU | 13 00017 | EX11 | 7 00007 | FACT04 | 14 00070 |
| HAP | 14 00016 | S16FAC | 15 00017 | S1N | 9 00011 | SORT | 11 00013 |
| TRFR4 | 12 00014 | UNIVEC | 8 00010 | IC5H | 1 00001 | 5-00005 | 5-00005 |
| ESPH1 | 4 00004 | TRPH1 | 3 00003 | 3(L1) | 2 00002 | 15(L1) | 6 00006 |

Figure 30. Main Program Core Storage Map
(continued)

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

| COS NUM (SPH) | DSICH UNITEC | EXIT (CSP) | FACTOR (FEL) | MAP (MPT) | CELEN (CEN) | SEN (SEL) | SRC (SCP) |
|---------------------|-----------------|---------------|-----------------|--------------|----------------|--------------|--------------|
| 100 | 18 | 00340 | EFN | IFN | LDC | IFN | LCC |
| 200 | 19 | 00342 | 2500 | 19 | 00342 | 1000 | 32 |
| 300 | 34 | 00456 | 4000 | 36 | 00463 | 4100 | 37 |
| 400 | 56 | 00564 | 4250 | 57 | 00567 | 4500 | 78 |
| 500 | 79 | 00721 | 11000 | 80 | 00732 | 12000 | 81 |
| 600 | 87 | 01003 | 13000 | 88 | 01044 | 14000 | 103 |
| 700 | 109 | 01445 | 16000 | 109 | 01442 | 17000 | 121 |
| 800 | 176 | 01570 | 19000 | 188 | 01641 | 19200 | 191 |
| 900 | 193 | 01676 | 19000 | 195 | 01705 | 20000 | 219 |
| 1000 | 246 | 02260 | 22400 | 250 | 02307 | 22500 | 251 |
| 1100 | 258 | 02373 | 23000 | 259 | 02377 | 24000 | 260 |
| 1200 | 274 | 02470 | 24000 | 274 | 02470 | 25000 | 274 |
| 1300 | 281 | 02500 | 27000 | 284 | 02527 | 27500 | 278 |
| 1400 | 282 | 02566 | 31000 | 287 | 02566 | 31500 | 290 |
| 1500 | 315 | 03077 | 6732 | 316 | 03094 | 7232 | 317 |
| 1600 | 324 | 03117 | 9232 | 329 | 03176 | 10232 | 334 |
| 1700 | 335 | 03453 | 18232 | 336 | 03442 | 18732 | 340 |
| 1800 | 355 | 03503 | 19432 | 366 | 03507 | 19532 | 368 |
| 1900 | 371 | 03575 | 20232 | 370 | 03574 | 20732 | 371 |
| 2000 | 384 | 03633 | 24232 | 385 | 03640 | 24232 | 381 |
| 2100 | 382 | 03702 | 24332 | 393 | 03701 | 24432 | 396 |
| 2200 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 2300 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 2400 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 2500 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 2600 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 2700 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 2800 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 2900 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3000 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3100 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3200 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3300 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3400 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3500 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3600 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3700 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3800 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 3900 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4000 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4100 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4200 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4300 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4400 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4500 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4600 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4700 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4800 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 4900 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5000 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5100 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5200 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5300 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5400 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5500 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5600 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5700 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5800 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 5900 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6000 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6100 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6200 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6300 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6400 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6500 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6600 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6700 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6800 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 6900 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7000 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7100 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7200 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7300 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7400 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7500 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7600 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7700 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7800 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 7900 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8000 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8100 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8200 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8300 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8400 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8500 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8600 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8700 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8800 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 8900 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9000 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9100 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9200 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9300 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9400 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9500 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9600 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9700 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9800 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 9900 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |
| 10000 | 408 | 04011 | 24832 | 410 | 04017 | 25232 | 416 |

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND ACTUAL LOCATIONS

Figure 38. Main Program Core Storage Map
(continued)

02/08/84 PAGE 22

| TJ300 | CONFAC II MAIN PROG-ANALYSIS AND PROG BY K.-A.TROUPS, NMA SID+ 11/1/63 | 02/08/84 | PAGE 22 |
|-------|--|----------|------------|
| 26732 | 420 04101 | 26732 | 426 04124 |
| 26732 | 420 04130 | 26732 | 435 04164 |
| 26732 | 420 04171 | 26732 | 446 04216 |
| 26732 | 420 04174 | 26732 | 456 04267 |
| 26732 | 420 04180 | 26732 | 462 04313 |
| 26732 | 420 04182 | 26732 | 468 04360 |
| 26732 | 420 04185 | 26732 | 474 04407 |
| 26732 | 420 04188 | 26732 | 480 04454 |
| 26732 | 420 04191 | 26732 | 486 04501 |
| 26732 | 420 04194 | 26732 | 492 04548 |
| 26732 | 420 04197 | 26732 | 498 04595 |
| 26732 | 420 04200 | 26732 | 504 04642 |
| 26732 | 420 04203 | 26732 | 510 04689 |
| 26732 | 420 04206 | 26732 | 516 04736 |
| 26732 | 420 04209 | 26732 | 522 04783 |
| 26732 | 420 04212 | 26732 | 528 04830 |
| 26732 | 420 04215 | 26732 | 534 04877 |
| 26732 | 420 04218 | 26732 | 540 04924 |
| 26732 | 420 04221 | 26732 | 546 04971 |
| 26732 | 420 04224 | 26732 | 552 05018 |
| 26732 | 420 04227 | 26732 | 558 05065 |
| 26732 | 420 04230 | 26732 | 564 05112 |
| 26732 | 420 04233 | 26732 | 570 05159 |
| 26732 | 420 04236 | 26732 | 576 05206 |
| 26732 | 420 04239 | 26732 | 582 05253 |
| 26732 | 420 04242 | 26732 | 588 05300 |
| 26732 | 420 04245 | 26732 | 594 05347 |
| 26732 | 420 04248 | 26732 | 600 05394 |
| 26732 | 420 04251 | 26732 | 606 05441 |
| 26732 | 420 04254 | 26732 | 612 05488 |
| 26732 | 420 04257 | 26732 | 618 05535 |
| 26732 | 420 04260 | 26732 | 624 05582 |
| 26732 | 420 04263 | 26732 | 630 05629 |
| 26732 | 420 04266 | 26732 | 636 05676 |
| 26732 | 420 04269 | 26732 | 642 05723 |
| 26732 | 420 04272 | 26732 | 648 05770 |
| 26732 | 420 04275 | 26732 | 654 05817 |
| 26732 | 420 04278 | 26732 | 660 05864 |
| 26732 | 420 04281 | 26732 | 666 05911 |
| 26732 | 420 04284 | 26732 | 672 05958 |
| 26732 | 420 04287 | 26732 | 678 06005 |
| 26732 | 420 04290 | 26732 | 684 06052 |
| 26732 | 420 04293 | 26732 | 690 06099 |
| 26732 | 420 04296 | 26732 | 696 06146 |
| 26732 | 420 04299 | 26732 | 702 06193 |
| 26732 | 420 04302 | 26732 | 708 06240 |
| 26732 | 420 04305 | 26732 | 714 06287 |
| 26732 | 420 04308 | 26732 | 720 06334 |
| 26732 | 420 04311 | 26732 | 726 06381 |
| 26732 | 420 04314 | 26732 | 732 06428 |
| 26732 | 420 04317 | 26732 | 738 06475 |
| 26732 | 420 04320 | 26732 | 744 06522 |
| 26732 | 420 04323 | 26732 | 750 06569 |
| 26732 | 420 04326 | 26732 | 756 06616 |
| 26732 | 420 04329 | 26732 | 762 06663 |
| 26732 | 420 04332 | 26732 | 768 06710 |
| 26732 | 420 04335 | 26732 | 774 06757 |
| 26732 | 420 04338 | 26732 | 780 06804 |
| 26732 | 420 04341 | 26732 | 786 06851 |
| 26732 | 420 04344 | 26732 | 792 06898 |
| 26732 | 420 04347 | 26732 | 798 06945 |
| 26732 | 420 04350 | 26732 | 804 06992 |
| 26732 | 420 04353 | 26732 | 810 07039 |
| 26732 | 420 04356 | 26732 | 816 07086 |
| 26732 | 420 04359 | 26732 | 822 07133 |
| 26732 | 420 04362 | 26732 | 828 07180 |
| 26732 | 420 04365 | 26732 | 834 07227 |
| 26732 | 420 04368 | 26732 | 840 07274 |
| 26732 | 420 04371 | 26732 | 846 07321 |
| 26732 | 420 04374 | 26732 | 852 07368 |
| 26732 | 420 04377 | 26732 | 858 07415 |
| 26732 | 420 04380 | 26732 | 864 07462 |
| 26732 | 420 04383 | 26732 | 870 07509 |
| 26732 | 420 04386 | 26732 | 876 07556 |
| 26732 | 420 04389 | 26732 | 882 07603 |
| 26732 | 420 04392 | 26732 | 888 07650 |
| 26732 | 420 04395 | 26732 | 894 07697 |
| 26732 | 420 04398 | 26732 | 900 07744 |
| 26732 | 420 04401 | 26732 | 906 07791 |
| 26732 | 420 04404 | 26732 | 912 07838 |
| 26732 | 420 04407 | 26732 | 918 07885 |
| 26732 | 420 04410 | 26732 | 924 07932 |
| 26732 | 420 04413 | 26732 | 930 07979 |
| 26732 | 420 04416 | 26732 | 936 08026 |
| 26732 | 420 04419 | 26732 | 942 08073 |
| 26732 | 420 04422 | 26732 | 948 08120 |
| 26732 | 420 04425 | 26732 | 954 08167 |
| 26732 | 420 04428 | 26732 | 960 08214 |
| 26732 | 420 04431 | 26732 | 966 08261 |
| 26732 | 420 04434 | 26732 | 972 08308 |
| 26732 | 420 04437 | 26732 | 978 08355 |
| 26732 | 420 04440 | 26732 | 984 08402 |
| 26732 | 420 04443 | 26732 | 990 08449 |
| 26732 | 420 04446 | 26732 | 996 08496 |
| 26732 | 420 04449 | 26732 | 1002 08543 |
| 26732 | 420 04452 | 26732 | 1008 08590 |
| 26732 | 420 04455 | 26732 | 1014 08637 |
| 26732 | 420 04458 | 26732 | 1020 08684 |
| 26732 | 420 04461 | 26732 | 1026 08731 |
| 26732 | 420 04464 | 26732 | 1032 08778 |
| 26732 | 420 04467 | 26732 | 1038 08825 |
| 26732 | 420 04470 | 26732 | 1044 08872 |
| 26732 | 420 04473 | 26732 | 1050 08919 |
| 26732 | 420 04476 | 26732 | 1056 08966 |
| 26732 | 420 04479 | 26732 | 1062 09013 |
| 26732 | 420 04482 | 26732 | 1068 09060 |
| 26732 | 420 04485 | 26732 | 1074 09107 |
| 26732 | 420 04488 | 26732 | 1080 09154 |
| 26732 | 420 04491 | 26732 | 1086 09201 |
| 26732 | 420 04494 | 26732 | 1092 09248 |
| 26732 | 420 04497 | 26732 | 1098 09295 |
| 26732 | 420 04500 | 26732 | 1104 09342 |
| 26732 | 420 04503 | 26732 | 1110 09389 |
| 26732 | 420 04506 | 26732 | 1116 09436 |
| 26732 | 420 04509 | 26732 | 1122 09483 |
| 26732 | 420 04512 | 26732 | 1128 09530 |
| 26732 | 420 04515 | 26732 | 1134 09577 |
| 26732 | 420 04518 | 26732 | 1140 09624 |
| 26732 | 420 04521 | 26732 | 1146 09671 |
| 26732 | 420 04524 | 26732 | 1152 09718 |
| 26732 | 420 04527 | 26732 | 1158 09765 |
| 26732 | 420 04530 | 26732 | 1164 09812 |
| 26732 | 420 04533 | 26732 | 1170 09859 |
| 26732 | 420 04536 | 26732 | 1176 09906 |
| 26732 | 420 04539 | 26732 | 1182 09953 |
| 26732 | 420 04542 | 26732 | 1188 10000 |
| 26732 | 420 04545 | 26732 | 1194 10047 |
| 26732 | 420 04548 | 26732 | 1200 10094 |
| 26732 | 420 04551 | 26732 | 1206 10141 |
| 26732 | 420 04554 | 26732 | 1212 10188 |
| 26732 | 420 04557 | 26732 | 1218 10235 |
| 26732 | 420 04560 | 26732 | 1224 10282 |
| 26732 | 420 04563 | 26732 | 1230 10329 |
| 26732 | 420 04566 | 26732 | 1236 10376 |
| 26732 | 420 04569 | 26732 | 1242 10423 |
| 26732 | 420 04572 | 26732 | 1248 10470 |
| 26732 | 420 04575 | 26732 | 1254 10517 |
| 26732 | 420 04578 | 26732 | 1260 10564 |
| 26732 | 420 04581 | 26732 | 1266 10611 |
| 26732 | 420 04584 | 26732 | 1272 10658 |
| 26732 | 420 04587 | 26732 | 1278 10705 |
| 26732 | 420 04590 | 26732 | 1284 10752 |
| 26732 | 420 04593 | 26732 | 1290 10799 |
| 26732 | 420 04596 | 26732 | 1296 10846 |
| 26732 | 420 04599 | 26732 | 1302 10893 |
| 26732 | 420 04602 | 26732 | 1308 10940 |
| 26732 | 420 04605 | 26732 | 1314 10987 |
| 26732 | 420 04608 | 26732 | 1320 11034 |
| 26732 | 420 04611 | 26732 | 1326 11081 |
| 26732 | 420 04614 | 26732 | 1332 11128 |
| 26732 | 420 04617 | 26732 | 1338 11175 |
| 26732 | 420 04620 | 26732 | 1344 11222 |
| 26732 | 420 04623 | 26732 | 1350 11269 |
| 26732 | 420 04626 | 26732 | 1356 11316 |
| 26732 | 420 04629 | 26732 | 1362 11363 |
| 26732 | 420 04632 | 26732 | 1368 11410 |
| 26732 | 420 04635 | 26732 | 1374 11457 |
| 26732 | 420 04638 | 26732 | 1380 11504 |
| 26732 | 420 04641 | 26732 | 1386 11551 |
| 26732 | 420 04644 | 26732 | 1392 11598 |
| 26732 | 420 04647 | 26732 | 1398 11645 |
| 26732 | 420 04650 | 26732 | 1404 11692 |
| 26732 | 420 04653 | 26732 | 1410 11739 |
| 26732 | 420 04656 | 26732 | 1416 11786 |
| 26732 | 420 04659 | 26732 | 1422 11833 |
| 26732 | 420 04662 | 26732 | 1428 11880 |
| 26732 | 420 04665 | 26732 | 1434 11927 |
| 26732 | 420 04668 | 26732 | 1440 11974 |
| 26732 | 420 04671 | 26732 | 1446 12021 |
| 26732 | 420 04674 | 26732 | 1452 12068 |
| 26732 | 420 04677 | 26732 | 1458 12115 |
| 26732 | 420 04680 | 26732 | 1464 12162 |
| 26732 | 420 04683 | 26732 | 1470 12209 |
| 26732 | 420 04686 | 26732 | 1476 12256 |
| 26732 | 420 04689 | 26732 | 1482 12303 |
| 26732 | 420 04692 | 26732 | 1488 12350 |
| 26732 | 420 04695 | 26732 | 1494 12397 |
| 26732 | 420 04698 | 26732 | 1500 12444 |
| 26732 | 420 04701 | 26732 | 1506 12491 |
| 26732 | 420 04704 | 26732 | 1512 12538 |
| 26732 | 420 04707 | 26732 | 1518 12585 |
| 26732 | 420 04710 | 26732 | 1524 12632 |
| 26732 | 420 04713 | 26732 | 1530 12679 |
| 26732 | 420 04716 | 26732 | 1536 12726 |
| 26732 | 420 04719 | 26732 | 1542 12773 |
| 26732 | 420 04722 | 26732 | 1548 12820 |
| 26732 | 420 04725 | 26732 | 1554 12867 |
| 26732 | 420 04728 | 26732 | 1560 12914 |
| 26732 | 420 04731 | 26732 | 1566 12961 |
| 26732 | 420 04734 | 26732 | 1572 13008 |
| 26732 | 420 04737 | 26732 | 1578 13055 |
| 26732 | 420 04740 | 26732 | 1584 13102 |
| 26732 | 420 04743 | 26732 | 1590 13149 |
| 26732 | 420 04746 | 26732 | 1596 13196 |
| 26732 | 420 04749 | 26732 | 1602 13243 |
| 26732 | 420 04752 | 26732 | 1608 13290 |
| 26732 | 420 04755 | 26732 | 1614 13337 |
| 26732 | 420 04758 | 26732 | 1620 13384 |
| 26732 | 420 04761 | 26732 | 1626 13431 |
| 26732 | 420 04764 | 26732 | 1632 13478 |
| 26732 | 420 04767 | 26732 | 1638 13525 |
| 26732 | 420 04770 | 26732 | 1644 13572 |
| 26732 | 420 04773 | 26732 | 1650 13619 |
| 26732 | 420 04776 | 26732 | 1656 13666 |
| 26732 | 420 04779 | 26732 | 1662 13713 |
| 26732 | 420 04782 | 26732 | 1668 13760 |
| 26732 | 420 04785 | 26732 | 1674 13807 |
| 26732 | 420 04788 | 26732 | 1680 13854 |
| 26732 | 420 04791 | 26732 | 1686 13901 |
| 26732 | 420 04794 | 26732 | 1692 13948 |
| 26732 | 420 04797 | 26732 | 1698 13995 |
| 26732 | 420 04800 | 26732 | 1704 14042 |
| 26732 | 420 04803 | 26732 | 1710 14089 |
| 26732 | 420 04806 | 26732 | 1716 14136 |
| 26732 | 420 04809 | 26732 | 1722 14183 |
| 26732 | 420 04812 | 26732 | 1728 14230 |
| 26732 | 420 04815 | 26732 | 1734 14277 |
| 26732 | 420 04818 | 26732 | 1740 14324 |
| 26732 | 420 04821 | 26732 | 1746 14371 |
| 26732 | 420 04824 | 26732 | 1752 14418 |
| 26732 | 420 04827 | 26732 | 1758 14465 |
| 26732 | 420 04830 | 26732 | 1764 14512 |
| 26732 | 420 04833 | 26732 | 1770 14559 |
| 26732 | 420 04836 | 26732 | 1776 14606 |
| 26732 | 420 04839 | 26732 | 1782 14653 |
| 26732 | 420 04842 | 26732 | 1788 14700 |
| 26732 | 420 04845 | 26732 | 1794 14747 |
| 26732 | 420 04848 | 26732 | 1800 14794 |
| 26732 | 420 | | |

STORAGE NOT USED BY PROGRAM

| | | | | | | | |
|-----------|-----------|-------------|-----|-----|-----|-----|-----|
| DEC | DEC | DEC | DEC | DEC | DEC | DEC | DEC |
| 206 00316 | 206 00316 | 14637 34453 | | | | | |

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

| | | | | | | | |
|------------------|-------|-------------|-------------------|-------------------|------------------|-------------|------|
| AMAP 15269 35501 | DEC | DEC | DEC | DEC | DEC | DEC | DEC |
| DT 22102 51126 | DT | 21067 51113 | AREA 21067 51113 | ARFAT 21067 51023 | CL | 22102 51126 | CL |
| FHP 16119 37387 | FH | 15011 35263 | DX 15246 35616 | OT 15179 35513 | DA | 22102 51126 | DA |
| KX 15973 36208 | KX | 15973 36208 | LD 16129 37401 | LI 16121 37371 | FAP 15185 35521 | 15973 36208 | FAP |
| MP 20942 50716 | MSDL | 15167 35477 | MSNGS 15023 32227 | NDI 22102 51126 | FL 14900 37106 | 15973 36208 | FL |
| MGA 22160 51126 | MOC | 15167 35477 | NSID 22101 51125 | NMN 21101 51125 | LP 16123 37373 | 15973 36208 | LP |
| NP 15493 38203 | MSC | 21113 51332 | NTP 32228 77426 | NP 21101 51125 | NCLD 15178 35512 | 15973 36208 | NCLD |
| PAF 16151 37427 | NITEL | 16151 37427 | RY 20978 51006 | PI 16274 37622 | NH 15184 35520 | 15973 36208 | NH |
| RA 16454 40106 | TDX | 16159 37432 | SL 21609 52275 | PI 16274 37622 | NOP 21101 51125 | 15973 36208 | NOP |
| VA 32902 33112 | Y | 14769 34661 | TL 15184 35520 | PI 16274 37622 | NML 15184 35517 | 15973 36208 | NML |
| YL 15368 36010 | Y | 14769 34661 | TL 15184 35520 | PI 16274 37622 | NML 15184 35517 | 15973 36208 | NML |

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

| | | | | | | | |
|-----------|-----|-----------|-----|-----|-----|-----|-----|
| D | DEC | DEC | DEC | DEC | DEC | DEC | DEC |
| 205 00315 | D | 205 00315 | | | | | |

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS

| | | | | | | | |
|--------------|-----|-----------|-----|-----|-----|-----|-----|
| DEC | DEC | DEC | DEC | DEC | DEC | DEC | DEC |
| 11 199 00307 | VL | 198 00306 | | | | | |

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

Figure 40. Subroutine UNIVEG Core Storage Map

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| | | | | | | | |
|-------|-----------|-------|-----------|-------|-----------|-------|-----------|
| DEC | OCT | DEC | OCT | DEC | OCT | DEC | OCT |
| 13 | 189 00275 | 21 | 178 00262 | 61 | 183 00257 | C11C0 | 153 00301 |
| C1100 | 13 00105 | C1100 | 175 00175 | C1102 | 136 00154 | C11C0 | 137 00305 |
| 13 | 00105 | E11 | 30 00036 | E12 | 17 00055 | D1XTP | 123 00173 |
| C1703 | 70 00106 | | | | | | |

LOCATIONS OF NAMES IN TRANSFER VECTOR

| | | | | | |
|-----|-------|-----|-----|-----|-----|
| DEC | OCT | DEC | OCT | DEC | OCT |
| 0 | 00000 | | | | |

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

SORT

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

| | | | | | | | | |
|-----|-----|-------|-----|-----|-------|-----|-----|-------|
| EFN | IFN | LOC | EFN | IFN | LOC | EFN | IFN | LOC |
| 10 | 8 | 00032 | 20 | 10 | 00046 | 25 | 11 | 00111 |
| 35 | 14 | 00102 | 40 | 15 | 00174 | 30 | 13 | 00173 |

Figure 40. Subroutine UNIVETC Core Storage Map (continued)

STORAGE NOT USED BY PROGRAM

| | | | |
|-----|-------|-------|-------|
| DEC | OCY | DEC | OCY |
| 702 | 01276 | 14637 | 34455 |

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

| | | | | |
|------------------|-------------------|-------------------|-------------------|-------------------|
| ANAP 15169 35701 | DEC | OCY | DEC | OCY |
| C2 21945 32971 | AREA 21067 51113 | AREAK 21011 51023 | CL 21024 53116 | CI 21024 53116 |
| CP 16119 37165 | C3 21795 52443 | CL 16140 37414 | DK 21154 53212 | DK 21154 53212 |
| FMP 16119 37165 | DM 15169 35701 | DM 15169 35701 | EV 14928 34204 | EV 14928 34204 |
| IMP 14649 34471 | FH 15011 32243 | F 13180 35315 | KP 14928 34204 | KP 14928 34204 |
| MP 20842 30215 | KC 20976 50760 | ND 22154 53212 | NCLP 19123 31373 | NCLP 19123 31373 |
| MP 20842 30215 | MD 15169 35701 | MSNS 19023 31247 | MON 22114 53142 | MON 22114 53142 |
| NOA 22100 53124 | MDC 22122 53140 | NOL 21157 51245 | NPI 15186 35520 | NPI 15186 35520 |
| NOI 15168 35500 | ND 15494 36206 | NOT 22102 53126 | NVL 15181 35515 | NVL 15181 35515 |
| NSM 22269 51425 | NSC 21413 51335 | NSIO 22101 53125 | NSL 22117 61201 | NSL 22117 61201 |
| PA 16454 40106 | NTILL 21493 51435 | NT 15182 35516 | SL 31658 52242 | SL 31658 52242 |
| SP 16445 40073 | PA 16454 40106 | RY 20998 51006 | TMSID 22101 53125 | TMSID 22101 53125 |
| VI 15348 36010 | RD 22120 53124 | RY 20998 51006 | | |
| | Y 16149 37432 | ZS 20947 50173 | | |
| | Y 16149 37432 | | | |

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

| | | | | |
|----------------|--------------|-------------|-------------|-----|
| CO5A 686 01256 | DEC | OCY | DEC | OCY |
| | DI 677 01245 | R 698 01272 | T 701 01275 | |

STORAGE LOCATIONS FOR VARIABLE'S NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS,

| | | | | |
|--------------|--------------|--------------|-------------|-------------|
| A 668 01234 | B 667 01233 | CD 666 01232 | DEC | OCY |
| D 664 01230 | DY 657 01227 | E 662 01226 | F 661 01225 | F 661 01225 |
| JZ 660 01224 | J 659 01223 | KN 658 01222 | K 657 01221 | K 657 01221 |
| M 656 01220 | NC 655 01217 | N 654 01216 | | |

Figure 42. Subroutine TXFRM Core Storage Map

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

| | | | | | |
|-------|-----------|-------|-----------|-------|-----------|
| DEC | OCT | DEC | OCT | DEC | OCT |
| 11 | 613 01145 | 21 | 595 01223 | 31 | 564 01124 |
| A1121 | 626 01162 | A1122 | 627 01163 | A1123 | 628 01164 |
| C1G6 | 630 01166 | C1G7 | 631 01167 | C1G8 | 632 01170 |
| C1108 | 638 01176 | C1109 | 639 01177 | C1110 | 641 01201 |
| C11G0 | 642 01202 | C11G1 | 643 01203 | C11G2 | 644 01204 |
| C11G5 | 649 01212 | C1202 | 651 01213 | C1203 | 652 01214 |
| D1109 | 150 02276 | D1120 | 221 00335 | D110E | 234 03352 |
| D1278 | 122 00172 | D120H | 230 00567 | D120I | 239 00567 |
| D160H | 259 00403 | D1614 | 514 01002 | D170H | 258 00402 |
| E1E | 254 00354 | E1C | 244 00365 | E1M | 357 00545 |
| E110L | 537 01053 | E110L | 272 00420 | | |

LOCATIONS OF NAMES IN TRANSFER VECTOR

| | | | | | |
|-------|---------|--------|---------|-----|-----|
| DEC | OCT | DEC | OCT | DEC | OCT |
| *SORT | 0 00000 | UNIVEC | 1 00001 | | |

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

SORT UNIVEC

| | | | | | | | |
|-----|----------|-----|----------|-----|----------|-----|----------|
| EFN | IFN | LCG | IFN | LCG | EFN | IFN | LCG |
| 10 | 8 00030 | 12 | 9 00042 | 13 | 13 03107 | 15 | 16 00150 |
| 28 | 22 00173 | 30 | 32 00326 | 40 | 35 00326 | 60 | 37 00360 |
| 150 | 50 00407 | 190 | 51 00570 | 200 | 56 00376 | 300 | 51 00350 |
| 310 | 65 00760 | 320 | 68 00715 | 330 | 70 00721 | 335 | 72 00737 |
| 460 | 78 01023 | 480 | 79 01030 | 500 | 80 01033 | 705 | 81 01056 |

Figure 42. Subroutine TFRH Core Storage Map
(continued)

```

C D3ICUCONFAC III ANALYSIS AND PROGRAMMING BY K.A.TROUPS,HAASID,11/1/63 36300100
C THIS SUBROUTINE DETERMINES WHETHER THE SURFACES SEE EACH OTHER IN 36300200
C WHOLE OR IN PART, AND IF I PART, COMPUTES THE COORDINATE AND AREA OF 36300300
C THE DIMENSION WHICH SURFACE IS IN THE OTHER. 36300400
1AR=1.5674E-05,NOP13=PI*1.02347E-011,PI11=PI*11,PI13=PI*13, 36300500
2PI=PI*2,PI1=PI,PI3=PI*3,PI11=PI*11,PI13=PI*13,PI111=PI*111, 36300600
4AREAKL=PI*HCL(1)*HCL(2)*HCL(3),HCL(1)=HCL(2)=HCL(3)=HCL(12)= 36300700
5MSDS(12)=FM(11)*FM(11)*FM(11)*FM(11)*FM(11)*FM(11)*FM(11)* 36300800
6SQUVALERGE=IP*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI* 36300900
7.0DA1=NSLL(1)*PR(12)*531,INDH(13)=NDC(11),I=VAL(11)*C(11), 36301000
8GDOPN=NI(11)*NSN,NOM=NSC,NL=SD,PP=AREA,AREAX=RY,ZS=KC,MP= 36301100
1KA,SP=NMS,AG=PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI*PI* 36301200
3DR,FAP,WH=HML,NV1=HML,F,DY,NCL=NS(10),ANA=HDD,MSCL=MSHDS,MSL 36301300
4=HDD,MSCL=MSHDS,MSL=HDD,MSCL=MSHDS,MSL=HDD,MSCL=MSHDS,MSL= 36301400
5IFF=SAFE LIGHT *1400*450 36301500
400 KL=10 34000 36301600
450 KL=2 36301700
C INITIATE THE LIGHTS 36301800
C IF SURFACE KP IS NONPLANAR, DO NOT CHECK BISECTION OF SURFACE KL 36301900
IF(LONG(1)SQD00-.0001500 36302000
JPL=JPL+KPY 36302100
C DO NOT CHECK FOR SURFACE KL 36302200
C SELECT POSITION OF SURFACE KP IN ARRAY P 36302300
C DO J=1,3 36302400
JL=LP+KJL OR SURFACE KL 36302500
C VP= Y0-OF POINTS DEFINING SURFACE JL 36302600
C COMPUTE COMPONENTS OF UNIT VECTOR IN SURFACE KP 36302700
DIR=PP(11,1)-PP(11,2),JPI 36302800
DIR=PP(11,2)-PP(11,3),JPI 36302900
DIR=PP(11,3)-PP(11,1),JPI 36303000
36303100
36303200
36303300
36303400
36303500
36303600
36303700
36303800
36303900
36304000

```

Figure 43. Subroutine D3ICU Listing


```

C ORDERED TO RESPECT SURFACE KL IF REQUIRED
15700 IF(LI,ML)12000,7000,24000
C PICKUP SUBSCRIPTS OF SURFACES IN ARRAY P
16000 NP=NP+1
C TEST Z-COORDINATES OF SURFACE KL. COMPUTE X,Y AT TRANSITION AND RETURN=36332200
C 8th POINTS ABOVE HORIZON.
DO 22000 N=1,NP
SENSE LIGHT 0
C IF 22000 N=1,NP
IF(P13,M1,J1)71000,18000,10000
C IF NEXT POINT IS - OR 0,CONTINUE. IF +,GO TO COMPUTE X,Y AT HORIZON. 36318000
DO 23000 M=1,ML
18000 SENSE LIGHT 0
C ADVANCE TO THE NEXT SUBSCRIPT TO NEW POSITION IN KP OF ARRAY P.
19000 K=K+1
PI,K,AL)=P(LI,M,JLI)
PI,K,AL)=P(LI,M,JLI)
C TEST FOR SIGN OF SENSE LIGHT. IF NEG,TEST SLL=IF ZERO OR POSITIVE. 36313000
C GO TO CONTINUE THE LOOP TO PICKUP ON NEXT GO ROUND.
IF(P13,M1,J1)20000,22000,22000
C IF SENSE LIGHT POINT WAS NOT ZERO, THE VALUE OF X,Y AT THE HORIZON MUST
C BE COMPUTED.
20000 IF(SENSE LIGHT)22000,21000
C COMPUTE X,Y AT HORIZON(Z=0) FROM TRACE OF LINE SEGMENT M=M+1 ON XZ AXIS.
C YZ PLANE.
ZC=P13,M,JLI)/P13,M+1,JLI=P13,P,JLI)
21500 P13,K,AL)=0.
22000 P13,K,AL)=P(LI,M,JLI)-C*(P13,M+1,JLI)-P(LI,M,JLI)
C M+1,K,L)=K
NVP13)=K
C COMPUTE VECTOR COMPONENTS FROM 8th POINT TO 8th POINT. JLI AND
C USE THE VECTOR COMPONENTS IN ARRAY M AND EQU LIST IN AREA COMP. 36315000
C USE ICM= ADD POINT (+1 EQUAL TO POINT I FOR USE LATER.
36315000

```

Figure 4.3. Subroutine MOICU Listing
(continued)

```

<MKS>
SENSE LIGHT 1
DO 32000 M=1,3
  V(P)=APPFM(I,J,L)-PP(M,Z,JL)
  PP(I,J,L)=PP(M,Z,KL)+V(M)
  IF SENSE LIGHT 1)126000,28000
32000 IF ABS(F(V(I)))-.1127000,27000,31000
28000 IF SENSE LIGHT 2)129000,30000
29000 M=P
36000 M2=M+32000
C3 TO 32600
33000 DO V(M)
34000 CONTINUE
C
  AREA(KL)=0.
  C SAVE P,PP(NL,I,KL)
  C PUT COORDINATE OF LAST POINT IN THIS SPOT FOR AREA COMPUTATION
  C COMPUTE PRINCIPAL AXIS ANGLES AND PRINCIPAL PLANE
  DO 33000 M=2,K
    AREA(KL)=AREA(KL)+PP(M,Z,I)*PP(NL,M=1,KL)-PP(NL,M=1,KL)
    C FINISH AREA COMPUTATION
  C RESTORE COORDINATE IN UNIT VECTOR
  C GO TO SURFACE 2 BISECTION IF READ
34000 RP=1
35000 IF KL=4)35500,36000,36000
35500 AL=2
  GO TO 10500
36000 ENOT(1,0,0,0,0,1,0,0,1,0,0,0,0,0,0,0)
3615000
3615700
3615800
3615900
3616000
3616100
3616200
3616300
3616400
3616500
3616600
3616700
3616800
3616900
3617000
3617100
3617200
3617300
3617400
3617500
3617600
3617700
3617800
3617900
3618000
3618100
3618200
3618300
3618400
3618500
3618600
3618700
3618800
3618900
3619000
3619100
3619200
3619300
3619400
3619500
3619600
3619700
3619800
3619900
3620000

```

Figure 43. Subroutine DQICU Listing (continued)

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS:

| | | | | | | | |
|-----|-------|-----|-----|------|-----|-----|-----|
| DEC | OC1 | DEC | OC1 | DEC | OC1 | DEC | OC1 |
| 831 | 01477 | 14 | 337 | 3445 | | | |

STORAGE NOT USED BY PROGRAM

| | | | | | | | |
|------|-------|------|-------|-------|-------|------|-------|
| DEC | OC1 | DEC | OC1 | DEC | OC1 | DEC | OC1 |
| ANMP | 21942 | ARCA | 21793 | AREAK | 15140 | CL | 22154 |
| C2 | 21945 | CS | 21795 | CL | 15140 | C | 22154 |
| DT | 22102 | DX | 13246 | DF | 13179 | FA | 13185 |
| EM | 14449 | EM | 14449 | EM | 14449 | EM | 14449 |
| FX | 15493 | KC | 20716 | NO | 21194 | KO | 15492 |
| GP | 20942 | LD | 16129 | LI | 16121 | LP | 16123 |
| MO | 15168 | MOL | 32117 | NO | 21194 | NSM | 22119 |
| NH | 12183 | ND | 15494 | NO | 22102 | NH | 15184 |
| NH | 12183 | NMS | 16418 | NO | 21093 | NO | 21101 |
| PAF | 16151 | PP | 22061 | NO | 15182 | NVA | 15181 |
| SP | 14444 | QA | 16154 | NO | 15182 | NVA | 15181 |
| VA | 21094 | TD | 22000 | NO | 21184 | TSID | 22101 |
| YI | 13368 | Y | 14769 | NO | 20987 | X | 14889 |

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON STATEMENTS, OR EQUIVALENCE STATEMENTS

| | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|
| DEC | OC1 | DEC | OC1 | DEC | OC1 | DEC | OC1 |
| C5 | 830 | OC | 829 | DXL | 842 | DKP | 827 |
| DYL | 826 | DP | 825 | OZL | 824 | DIP | 823 |
| J | 817 | K | 816 | L | 815 | JM | 814 |
| JP | 816 | KN | 815 | K | 814 | K | 813 |
| M | 814 | NZ | 813 | PI | 812 | TC | 811 |

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

Figure 4A. Subroutine DOICU Core Storage Map

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| | | | | | |
|-------|-----------|-------|-----------|-------|-----------|
| 15300 | 54 00427 | 15600 | 59 00461 | 15655 | 60 00465 |
| 15600 | 51 00471 | 15700 | 60 00465 | 16000 | 61 00469 |
| 16000 | 48 00475 | 20000 | 78 00476 | 21000 | 79 00483 |
| 21300 | 82 00670 | 24000 | 95 01023 | 27000 | 95 01034 |
| 28000 | 97 01041 | 29000 | 98 01044 | 30000 | 100 01050 |
| 29000 | 104 01048 | 31000 | 111 01050 | 3232 | 115 01263 |
| 2932 | 104 01213 | 3232 | 116 01235 | | |

Figure 44. Subroutine DOICU Core Storage Map
(continued)


```

110 YMIN=PI2,K,MC)
120 M=K-K,NDI=YMAXI200,200,175
175 YMAX=PI2,K,NDI
180 K=K
200 CONTINUE
210 N1=21*MM
220 I1=1
230 DO 230 I=1,2
240 IF(I1)245,260,230
250 IF(N1)245,260,230
260 IF(N1)245,260,230
270 IF(N1)245,260,230
280 IF(N1)245,260,230
290 IF(N1)245,260,230
300 CONTINUE
310 INSTRUCTIONS COMPUTE THE POINTS OF INTERSECTION OF EACH
320 HORIZONTAL GRID LINE AND THE LINE SEGMENTS FORMING THE SURF BOUNDARY
330 COMPUTE THE VERTICAL INCREMENT
340 DP=(YMAX-YMIN)/FLOAT(N1)
350 COMPUTE THE HORIZONTAL GRID LINES
3604000
3640000
3680000
3720000
3760000
3800000
3840000
3880000
3920000
3960000
4000000
4040000
4080000
4120000
4160000
4200000
4240000
4280000
4320000
4360000
4400000
4440000
4480000
4520000
4560000
4600000
4640000
4680000
4720000
4760000
4800000
4840000
4880000
4920000
4960000
5000000
5040000
5080000
5120000
5160000
5200000
5240000
5280000
5320000
5360000
5400000
5440000
5480000
5520000
5560000
5600000
5640000
5680000
5720000
5760000
5800000
5840000
5880000
5920000
5960000
6000000
6040000
6080000
6120000
6160000
6200000
6240000
6280000
6320000
6360000
6400000
6440000
6480000
6520000
6560000
6600000
6640000
6680000
6720000
6760000
6800000
6840000
6880000
6920000
6960000
7000000
7040000
7080000
7120000
7160000
7200000
7240000
7280000
7320000
7360000
7400000
7440000
7480000
7520000
7560000
7600000
7640000
7680000
7720000
7760000
7800000
7840000
7880000
7920000
7960000
8000000
8040000
8080000
8120000
8160000
8200000
8240000
8280000
8320000
8360000
8400000
8440000
8480000
8520000
8560000
8600000
8640000
8680000
8720000
8760000
8800000
8840000
8880000
8920000
8960000
9000000
9040000
9080000
9120000
9160000
9200000
9240000
9280000
9320000
9360000
9400000
9440000
9480000
9520000
9560000
9600000
9640000
9680000
9720000
9760000
9800000
9840000
9880000
9920000
9960000
10000000

```

Figure 45. Subroutine MAP Listing (continued)

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73384 MAP (CONFAC II) ANALYSIS AND PROGRAMMING BY K.A.TOUSS-MAASID-11/1/63

```

IF (K=NLJ80) J001700
680 NEXT HAPPING LINE AND NEXT BOUNDARY LINE SEGMENT
690 CONTINUE
700 NEXT HAPPING LINE AND NEXT BOUNDARY LINE SEGMENT
800 NEXT HAPPING LINE AND NEXT BOUNDARY LINE SEGMENT
AR=O
C COMPUTE THE MAPPING AREA
      AND *X11*
      DXL=X11K-21-X111
      AR=AR+DXL/WHI
      MAP=MAP+DXL*(X111-21)/2.10DY
810
RETURN
END1110.0.0.0.1.0.1.0.1.0.0.0.0

```

- 36413600
- 36413700
- 36413800
- 36413900
- 36414000
- 36414100
- 36414200
- 36414300
- 36414400
- 36414500
- 36414600
- 36414700
- 36414800
- 36414900

Figure 45. Subroutine MAP Listing (continued)


```

985 PHII=PHI1+3.1415927
GO TO 990
C. COMPUTE THE COSINE OF VECTORS TO POINTS DEFINING LYSZ SEGMENT
990 F53=SQRT(F1*F2**2)
C COMPUTE THE COSINE OF ANGLE BETWEEN THE CIRCULAR SECTOR AND X-Y PLANE
C I=COS(F53)/F53
C I=COS(F53)/F53
C COMPUTE THE DOT PRODUCT SAME VECTORS
C I=COS(F53)/F53
C COMPUTE THE ANGLE BETWEEN VECTORS IN RADIAN
980 ANG=C3.1415927
985 PHII=PHI1+3.1415927
GO TO 990
%0 CONTINUE
C. A NEG. AREA RESULTS WHEN THE ORDER OF COMPUTATION REVERSES THE BACKSIDE OF SURFACE
C. RECOMPUTE SURFACE AREA WITH REVERSED ORDER OF POINTS INDUCED FROM THE
C SURFACE WHICH SHOULD BE BUT IS NOT QUITE PLANNAR
903 I1=PHI1+3.1415927
904 F11=I1+3.1415927
%95 GO TO 986
%96 I=INDI974.984*971
500 I=C-231274.520*988
520 F11=PHI1/6+2031853
C FOR THE PRINTED ANGLE ERROR IS REACHED, USE THE MAP BOUNDARY VALUE
975 I1=PHI1/972.973*986
976 I1=PHI1/972.973*986
C MAKE YEAR ZERO VALUES ZERO
904 I1=PHI1/972.973*986

```

Figure 47. Subroutine FACTOR Identifying (continued)

72365 FACTORCONFACTANALYSIS AND PROGRAMMING BY K.A.L.TOUPS,INAA:SD,11/17/63 11/07/73 PAGE 4

```

974 CONTINUE
C0 ID 987
C MOVE CURSOR TO THE POSITION OF THE POINT RELATIVE TO SURFACE Z1 TO
C THE RIGHT AND INCREMENT AND CONTINUE
975 DO 975 J=1,ML
976 CONTINUE
977 CONTINUE (J-J)-DXIK)
C INTEGRATE THE FUNCTION FH ALONG THE HORIZONTAL GRIC
980 DO 990 I=2,NMI
981 FV(I)=FV(I)+F(H(I)+FH(MHML)/2,1)*DXIK)
1000 CONTINUE
C INTEGRATE THE FUNCTION FV ALONG THE VERTICAL. DIVIDE BY 2 TO CONVERT
C FH TO AREA BY PT TO CONVERT MGD TO EQUATION FACTOR, AND BY
C THE MAPPING AREA TO YIELD THE FORM FACTOR.
1050 F=0.000 R=2.0*W1
C F=AREA*FIF-(FV1)+FV(NML)/2,1)*DY/AMAP /6.2831853
C REFLECT IF SURFACE 1 IS SHADDED, THE FACTOR MUST BE REDUCED TO
C HALF.
IF (I1) F=F/2.0
IF (I1) F=AREA(I)/AREA(J)
1060 F=F*AREA(I)/AREA(J)
C COMPUTE THE PRODUCT OF X AREA PRODUCT
1500 FAP=F*AGEN(J)
2000 RETURN
END(1,0,0,0,0,1,0,0,0,1,0,0,0,0)

```

Figure 47. Subroutine FACTOR Listing
(continued)

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

| | | | |
|-----------------|-------------------|------------------|------------------|
| DEC 459 00715 | DEC 10037 34935 | DEC 0CT | DEC 0CT |
| ANG 15169 35501 | AREA 21097 51113 | DEC 0CT | DEC 0CT |
| AOZ 22102 53176 | D2 15264 35498 | AREA 21011 51023 | C3 24029 53116 |
| OT 16119 31387 | DT 15179 35513 | DT 15179 35513 | DC 17214 35272 |
| PH 18498 34971 | FH 15011 35243 | F 15180 35514 | FC 11-450 35146 |
| HP 20942 50716 | KC 20976 50763 | HD 22139 53212 | FP 15-992 36204 |
| MDA 22100 53124 | MSDL 15187 35477 | MSMS 15023 35257 | MCLS 12178 35512 |
| MSD 15183 35517 | NOC 22132 53140 | NOL 21157 51245 | NOV 22114 53142 |
| NP 15491 34203 | NMS 10478 30002 | NMX 21692 52175 | NP 21024 47250 |
| NR 21269 51927 | NMC 21213 51335 | NSID 22101 53125 | MSL 22217 61201 |
| RA 16454 40166 | OTILE 22297 71455 | NV 35162 75516 | NVL 12181 35215 |
| SP 16443 40075 | RA 21009 51021 | RY 23998 51006 | SL 21693 52275 |
| Y1 15548 34010 | TDA 22100 53124 | TUN 22138 53142 | MSID 22101 53125 |
| | YB 18749 34601 | ZS 23987 50773 | AP 14869 35051 |

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS

| | | | |
|-----------------|-----------------|---------------|---------------|
| DEC 459 00715 | DEC 10037 34935 | DEC 0CT | DEC 0CT |
| ANG 15169 35501 | C5C 427 00711 | DEC 0CT | DEC 0CT |
| AOZ 22102 53176 | FK 449 00701 | FCS 456 00710 | F31 455 00707 |
| OT 16119 31387 | PK 449 00701 | HL 446 00700 | J1 431 00705 |
| PH 18498 34971 | | | |
| HP 20942 50716 | | | |
| MDA 22100 53124 | | | |
| MSD 15183 35517 | | | |
| NP 15491 34203 | | | |
| NR 21269 51927 | | | |
| RA 16454 40166 | | | |
| SP 16443 40075 | | | |
| Y1 15548 34010 | | | |

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

| | | | |
|----------------|-----------------|----------------|------------------|
| DEC 459 00715 | DEC 10037 34935 | DEC 0CT | DEC 0CT |
| 11 434 00642 | 21 416 00640 | DEC 0CT | DEC 0CT |
| C1G5 443 00672 | C1G6 443 00673 | C31 421 00445 | C1G 61 420 00654 |
| C1D1 444 00676 | C1C0 447 00577 | C1G7 444 00674 | C1C0 443 00675 |
| | | D1104 76 00116 | D1113 314 00472 |

Figure 48. Subroutine FACTOR Core Storage Map

7295 FACTORCONFAC IJANALYSIS AND PROGRAMMING BY K.A.TOUPS, MAISTO, 11/7/63

| | | | | | | | | | | | |
|-------|-----|-------|-------|-----|-------|-------|-----|-------|-------|-----|-------|
| D1210 | 287 | 00137 | D1210 | 357 | 00514 | D1211 | 500 | 00526 | 0121C | 350 | 00520 |
| D1315 | 313 | 00471 | D131A | 359 | 00523 | D1400 | 312 | 00210 | 0141D | 35 | 00524 |
| D1417 | 200 | 00620 | D1400 | 321 | 00227 | D1113 | 312 | 00620 | E1C | 187 | 00275 |
| E1204 | 231 | 00373 | E1210 | 286 | 00436 | E140N | 246 | 00370 | E1110 | 286 | 00826 |

LOCATIONS OF NAMES IN TRANSFER VECTOR

| | | | | | | | | | | | | |
|---|-----|-----|-----|---|-------|------|-----|-----|---|-------|-----|-----|
| A | TAN | DEC | OCT | 1 | 00001 | 30RT | DEC | OCT | 0 | 00000 | DEC | OCT |
|---|-----|-----|-----|---|-------|------|-----|-----|---|-------|-----|-----|

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

A TAN SORT

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND SOCIAL LOCATIONS

| | | | | | | | | |
|------|-----|-------|------|-----|-------|------|-----|-------|
| EFN | IFN | LOC | EFN | IFN | LOC | EFN | IFN | LOC |
| 840 | 12 | 00052 | 865 | 19 | 00132 | 870 | 20 | 00134 |
| 934 | 34 | 00266 | 917 | 35 | 00174 | 930 | 37 | 00207 |
| 950 | 40 | 00313 | 940 | 44 | 00317 | 965 | 46 | 00342 |
| 968 | 55 | 00419 | 931 | 51 | 00405 | 904 | 52 | 00431 |
| 984 | 59 | 00440 | 973 | 60 | 00452 | 944 | 55 | 00463 |
| 992 | 66 | 00511 | 975 | 67 | 00515 | 987 | 68 | 00525 |
| 1000 | 72 | 00536 | 1000 | 74 | 00536 | 1050 | 74 | 00576 |
| 1500 | 78 | 00631 | 2000 | 78 | 00636 | | | |

Figure 4.6. Subroutine FACTOR Core Storage Map (continued)

72360 SIFACCOMFAC IIIANALYSIS AND PROGRAMMING BY N.A.L.TOUSS-NMAASIO:11/11/83

```

OR I1700 K41-4
C PICKUP CONNECTING POINT K1 TO POINT J IN SURFACE IJ
C IF R1 J5 ZENUG AND DATA IN THIS SPOT= CONTINUE
C UPDATE IJ TO I1700,I1700,I1700,I1600
I1600 K2-K2+1
C UPDATE NO OF CONNECTIONS COMPLET
C UPD CONNECTING POINT NO TO TOTAL OF POINTS BEGINNING COMPOSITE SURFACE
C WITH MEM COMPOSITE SURFACE POINT NUMBER N.
I1700 P4RZ-NP=NO*PIR(J,IJ)
C LOAD TOTAL NO OF POINTS CONNECTING TO NEW POINT NO N.
M161=42
I5000 M161=42
C SET CONNECTIONS PROCESSING FLAG TO NONZERO(ONLY ONE ENTRY RECD)
KK=1
C REAR FLAG TO DETERMINE SILHOUETTE FROM LINE SEGMENTS PROJECTED ON Z=130613-00
C PLANE AND COMPUTE WINDING POINT FACTOR FROM THIS SILHOUETTE.
I2100 UO=877 MH=1,MHL
I2150 IF(FH(MH))GO TO I2150-I2150
I2200 D5C=K+2*5P25
D5=SQRT(D5C)
FH(MH)=1
FH(MH)=1/D5UOD)
I2300 IF(MH*112200,984,12390
IF(MH*112200,984,12390
IF(MH*112200,984,12390
I2350 BETA=SURTFAS/MZ//ALPHA)
FH(MH)=A-TAN(BETA)-PI+A TAN(BETA+D/(3+1.1*INH))-ALPHA+Beta/D5Q
I2400 FH(MH)=FH(MH)+F1+3.1459265
GO TO 266
C GRAB NEXT SET OF SLOPES, ANGLES AND Y-INTERCEPTS
I2600 NUS=LC ITC. SENSE LIGHT, 0
C PICKUP NO OF POINTS CONNECTING TO POINT I.
NP=MNE(I)

```

Figure 49. Subroutine SIFAC Listing (continued)

```

DO 400 J=1,NP
C PICKUP 3RD POINT CONNECTING TO I.
VALJ=VALI
C THE SLOPE OF LINE SEGMENT FROM I TO J IS THE SAME AS J TO I. IF THE
C CONNECTING POINT IS NUMERICALLY LESS THAN POINT, THE SLOPE AND
C SLOPE SIGN ARE REVERSED. THIS IS NOT NECESSARY FOR THIS PROGRAM.
C IF NP IS GREATER THAN I, GO TO COMPUTE LINE SEGMENT PARAMETERS.
IF I NP123=400,400
36612700
36612800
36612900
36613000
36613100
36613200
36613300
36613400
36613500
36613600
36613700
36613800
36613900
36614000
36614100
36614200
36614300
36614400
36614500
36614600
36614700
36614800
36614900
36615000
36615100
36615200
36615300
36615400
36615500
36615600
36615700
36615800
36615900
36616000
36616100
36616200
36616300
36616400
36616500
36616600
36616700
36616800
36616900
36617000
36617100
36617200
36617300
36617400
36617500
36617600
36617700
36617800
36617900
36618000
36618100
36618200
36618300
36618400
36618500
36618600
36618700
36618800
36618900
36619000
36619100
36619200
36619300
36619400
36619500
36619600
36619700
36619800
36619900
36620000

```

C IF NOT CLASS B SURFACE, THE FOLLOWING LINE ELEMENTS ARE NOT NEEDED

Figure 49. Subroutine SIFAC Listing (continued)


```

110 MLE=NPP
115 IF(SENSE LIGHT 2)
116 SENSE LIGHT 2
117 ME-3
140 UP=N0MLP
141 IF(MLE=NPP)160,180,180
160 IF(SENSE LIGHT 2)170,190
170 JSE LIGHT 3
175 IF(M-1)190,175,190
176 G=MO(SENSE LIGHT 2)
180 ME=MK1
181 JIMX=NLP
182 G=MO(SENSE LIGHT 2)
190 IF(SENSE LIGHT 3)195,835
195 G=MO(SENSE LIGHT 2)
649 VIL(JR,NPP)=1.
VIL(JR,NPP)=MIN(KIL)
VIL(JR,NPP)=MIN(KIL)
VIL(JR,NPP)=MIN(KIL)
C M=NO. OF POINTS DEFINING SILHOUETTE
C X1= X-VALUE OF HEAD OF DEPARTURE VECTOR
C X2= X-VALUE OF BASE OF DEPARTURE VECTOR
600 SERO=
X1=MI1,LE30
602 SERO=
X1=MI1,LE30
C INITIALIZE COUNT OF VECTORS TO BE CONSIDERED IN FINAL SELECTION OF
C SILHOUETTE PATH.
603 IF(CSILH01,MHI1404,652,662
*0% XH=7777777.

```

Figure 49. Subroutine SILFAC Listing (continue)

```

YM=2M
PRINT 5000,NS(NT,M),NL,NPP,SLD,NP(LJ,NPP),SL(LJ,NPP),YL(LJ,NPP),VL(
LJ,NPP),X(LNPP),Y(LNPP),Z(LNPP),X1,3,42
5000 1/12M NP(LJ,NPP) IS 1/12M SL(LJ,NPP)+ELN, 1/12M YL(LJ,NPP)+ELN, 1/12M Z(LJ,NPP)+ELN
4N VAL(LJ,NPP)+ELN, 1/52M(NP(LJ)+ELN, 1/52M(Y(LJ,NPP)+ELN, 1/52M(Z(LJ,NPP)+ELN, 1/52M(X(LNPP)+ELN)
C ENTER LOGS TO DETERMINE WHICH VECTORS TOUCH THE REFERENCE (6 DEPARTURE
C VECTOR LJA,NPP)
462 DO 604, I=1,M
604  IF (ABS(VL(I,NPP)-REF)) .GT. 1E-6
C SELECT VECTOR LJ, J=
643 L9 804 J=1,60P
644  IF (ABS(VL(I,NPP)-REF)) .GT. 1E-6
651 X(67177777)
XC=4A
YE=4A
ZF=4A
C SELECT HEAD END OF TEST VECTORS(I,J)
654  SENSE LIGHT 0
655  IF (ABS(VL(I,NPP)-REF)) .GT. 1E-6
C ONCE DETERMINED WITH REF VECTOR
656  DO SL(LJ,NPP)+SL(I,J)
C IF CO-ORDINATE NEAR ZERO, TEST VECTOR(I,J) AND REFERENCE VECTOR(LJ,NPP)
C EXTENDING BEYOND THE REF VECTOR TO THE OPPOSITE DIRECTION AND
665  IF (ABS(X(I,J)-REF)) .GT. 1E-6
C EXCLUDE ALL VECTORS HAVING SAME DIRECTION AS REF VECTOR
668  IF (ABS(Y(LJ,NPP)-REF)) .GT. 1E-6
669  IF (ABS(Z(LJ,NPP)-REF)) .GT. 1E-6
671  T(LJ,NPP)+E=5*VL(LJ,NPP)
672  IF (ABS(VL(LJ,NPP)-REF)) .GT. 1E-6
C QUANTITIES OF P UNITS ARE THE SAME AS I UNITLIST QUANTITIES (50EG VECTOR)
36627200
36627300
36627400
36627500
36627600
36627700
36627800
36627900
36628000
36628100
36628200
36628300
36628400
36628500
36628600
36628700
36628800
36628900
36629000
36629100
36629200
36629300
36629400
36629500
36629600
36629700
36629800
36629900
36630000
36630100
36630200
36630300
36630400
36630500
36630600
36630700
36630800
36630900
36631000

```

Figure 49. Subroutine S1LFAC Listing (continued)

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```

7366 SILFACONFAC II ANALYSIS AND PROGRAMMING BY R.A. TOUPS-NMAAS10/11/7/63 11/20/74 PAGE 13
C IF THE PROJECTED AREA IS NOT ZERO, PROCEED TO COMPUTE THE PROJECTED
C AREA FUNCTION OF THE CIRCULAR SECTOR FORMED BY THE TRIANGLE AND UNIT
C SPHERE
      F=ESS2190-980-950
C COMPUTE THE CROSS PRODUCT OF VECTORS TO POINTS DEFINING LINE SEGMENT
950 F53=SORF1(YJ3-VIK3)+ZIK3+XIK3+24F2+42
C COMPUTE THE SCALAR PRODUCT BETWEEN THE CIRCULAR SECTOR AND X-Y PLANE
C 1X-COMPONENT OF X-PRODUCT
      G=S*F2/F53
C COMPUTE THE SCALAR PRODUCT BETWEEN SAME VECTORS
      L=COMP(XJ3-VIK3)*YJ3-VIK3
C COMPUTE THE ANGLE BETWEEN VECTOR IN ARIZANS
      ANG=180-90+970
960 GO TO 970
965 FHEMP=FHEMHI+1.5707963*CSG
970 CONTINUE
      FHEM=FHEMHI+1A (YANF53/FCS1+ANG)*CSG
C IF THE POINT IS VERY SMALL, SET TO 0 (PH IS DOUBLE THIS AREA)
983 FHEM=0.
C A FLAGGED POINT WAS REQUESTED, COMPUTE THE POINT FACTOR
984 IF (MOD(POINT,1))=0 THEN
985 IF (M=231500+500+984
986 IF (M=231500+500+984
987 IF (M=231500+500+984
988 IF (M=231500+500+984
C POINT THE ORIGIN/NAME POSITION OF THE POINT RELATIVE TO SURFACE 21 TO
C THE SURFACE ORIGIN/NAME POSITION AND CONTINUE
989 DO 915 GOTO 915
990 XE=JX(21)-DX(1,2)
991 YE=JY(21)-DY(1,2)
992 Z=JZ(21)-DZ(1,2)
993 PH=PH(21)
994 CO=CO(21)
995 FHEM=0.1015+1000*LOIS
996 FHEM=32655.389+939
1015 IF (M=32655.389+939

```

Figure 49. Subroutine SILFAC Listing (continued)

STORAGE NOT USED BY PROGRAM

| | | | |
|------|-------|-------|-------|
| DEC | QCT | DEC | QCT |
| 3725 | 07215 | 14613 | 34425 |

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMPOH STATEMENTS

| | | | | | | | | |
|------|-------|-------|------|-------|-------|-----|-------|-------|
| AMAC | DLG | QCT | DEC | QCT | DEC | QCT | | |
| C | 21795 | 32443 | AREA | 21795 | 32443 | CL | 16140 | 37414 |
| DI | 22102 | 53126 | DR | 12746 | 35616 | DT | 12179 | 35813 |
| DU | 15180 | 35314 | FW | 14955 | 35146 | INC | 14649 | 34871 |
| FD | 22156 | 52412 | GP | 12602 | 36204 | KK | 12493 | 36205 |
| MSNL | 15183 | 35287 | NGLS | 15178 | 35512 | NDA | 22100 | 53126 |
| MDA | 22102 | 53126 | NON | 22114 | 53142 | NUN | 15168 | 35800 |
| MVA | 15282 | 35548 | MHJ | 15184 | 35520 | NHL | 15183 | 35817 |
| MY | 22098 | 51006 | NVL | 15181 | 35513 | NSM | 21269 | 51425 |
| TCM | 22114 | 53142 | NSIL | 22117 | 61201 | PAF | 16151 | 37425 |
| XK | 15280 | 36282 | NSID | 22101 | 53125 | SP | 14445 | 40076 |
| YS | 20789 | 36782 | X | 14689 | 35051 | VA | 22094 | 53116 |
| | | | | | | YK | 15368 | 36010 |

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

| | | | | | |
|------|-------|-------|------|-------|-------|
| DEC | QCT | DEC | QCT | | |
| 3455 | 02627 | MN | 3724 | 07214 | |
| MW | 3259 | 02623 | NY | 3159 | 08127 |
| XW | 3259 | 02623 | YI | 3159 | 08125 |

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS

| | | | | | |
|-------|------|-------|------|------|-------|
| DEC | QCT | DEC | QCT | | |
| ALPHA | 3355 | 04463 | ANG | 2385 | 04462 |
| BETA | 2353 | 04461 | BETA | 2353 | 04461 |
| CD | 4352 | 04460 | CD | 4352 | 04460 |
| DE | 2348 | 04459 | DE | 2348 | 04459 |
| DF | 2348 | 04459 | DF | 2348 | 04459 |
| EG | 2348 | 04459 | EG | 2348 | 04459 |
| FI | 2348 | 04459 | FI | 2348 | 04459 |
| FL | 2348 | 04459 | FL | 2348 | 04459 |
| GM | 2348 | 04459 | GM | 2348 | 04459 |
| GN | 2348 | 04459 | GN | 2348 | 04459 |
| GO | 2348 | 04459 | GO | 2348 | 04459 |
| GP | 2348 | 04459 | GP | 2348 | 04459 |
| GQ | 2348 | 04459 | GQ | 2348 | 04459 |
| GR | 2348 | 04459 | GR | 2348 | 04459 |
| GS | 2348 | 04459 | GS | 2348 | 04459 |
| GT | 2348 | 04459 | GT | 2348 | 04459 |
| HU | 2348 | 04459 | HU | 2348 | 04459 |
| IV | 2348 | 04459 | IV | 2348 | 04459 |
| JV | 2348 | 04459 | JV | 2348 | 04459 |
| KV | 2348 | 04459 | KV | 2348 | 04459 |
| LV | 2348 | 04459 | LV | 2348 | 04459 |
| MV | 2348 | 04459 | MV | 2348 | 04459 |
| NV | 2348 | 04459 | NV | 2348 | 04459 |
| OV | 2348 | 04459 | OV | 2348 | 04459 |
| PV | 2348 | 04459 | PV | 2348 | 04459 |
| QV | 2348 | 04459 | QV | 2348 | 04459 |
| RV | 2348 | 04459 | RV | 2348 | 04459 |
| SV | 2348 | 04459 | SV | 2348 | 04459 |
| TV | 2348 | 04459 | TV | 2348 | 04459 |
| UV | 2348 | 04459 | UV | 2348 | 04459 |
| VV | 2348 | 04459 | VV | 2348 | 04459 |
| WV | 2348 | 04459 | WV | 2348 | 04459 |
| XV | 2348 | 04459 | XV | 2348 | 04459 |
| YV | 2348 | 04459 | YV | 2348 | 04459 |
| ZV | 2348 | 04459 | ZV | 2348 | 04459 |

Figure 50. Subroutine SILFAC Core Storage Map

| | | | | | | | |
|------|------------|-----|------------|-----|------------|------|------------|
| FU | 4383 04447 | F52 | 3342 04440 | F53 | 2341 04445 | ID | 2340 04444 |
| GR | 2335 04437 | J | 2334 04436 | JX | 2333 04435 | KZ | 2332 04434 |
| KK | 2331 04433 | K | 2330 04432 | L | 2329 04431 | LI | 2328 04430 |
| LL | 2327 04429 | LL | 2326 04428 | MM | 2325 04427 | MM | 2324 04426 |
| MLP | 2319 04417 | MM | 2318 04416 | NLS | 2317 04415 | NOP | 2316 04414 |
| MP | 2313 04413 | NP | 2312 04412 | NPX | 2311 04411 | PSM | 2310 04410 |
| MP | 2311 04411 | PL | 2310 04410 | SLR | 2309 04409 | TOL | 2308 04408 |
| PK | 2307 04405 | PSO | 2306 04402 | TDL | 2301 04375 | TOL | 2300 04374 |
| TL2 | 2303 04377 | TOL | 2302 04376 | VAM | 2299 04368 | XL | 2298 04367 |
| TL2 | 2299 04373 | UK | 2298 04366 | XB | 2293 04345 | XI | 2292 04344 |
| XD | 2291 04363 | XE | 2290 04362 | XF | 2289 04361 | XI | 2288 04360 |
| XMIN | 2287 04357 | YM | 2286 04356 | YFM | 2281 04337 | YSP | 2280 04336 |
| YMC | 2279 04347 | YMN | 2278 04346 | YN | 2283 04332 | YSP2 | 2282 04330 |

SYMBOLS AND LOCATIONS PER SOURCE PROGRAM FORMAT STATEMENTS

| | | | | | | | |
|-------|------------|-------|------------|-------|------------|-----|-----|
| 911UP | 1999 04086 | EFN | LOC | EFN | LOC | EFN | LOC |
| | | 81458 | 5000 04266 | 81451 | 5010 04216 | | |

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

| | | | | | | | |
|-------|------------|-------|------------|-------|------------|-------|------------|
| 11 | 2231 04267 | DEC | 0CT | 31 | 2058 04024 | 61 | 2057 04021 |
| A11C2 | 2055 03643 | A11C3 | 1868 03600 | A1104 | 1981 03615 | A1105 | 1994 03712 |
| A11C7 | 2005 04277 | A11C8 | 2000 04274 | A1106 | 2007 04275 | A1107 | 2008 04276 |
| C115 | 2239 04277 | C116 | 2240 04300 | C117 | 2241 04301 | C118 | 2242 04302 |
| C109 | 2243 04303 | C11A | 2244 04304 | C11B | 2245 04305 | C11C | 2246 04306 |
| C10A | 2251 04311 | C11E | 2252 04314 | C11F | 2253 04315 | C11G | 2254 04316 |
| C10L | 2255 04317 | C11M | 2256 04320 | C1100 | 2257 04321 | C1101 | 2258 04322 |
| C1102 | 2259 04322 | C1107 | 2260 04330 | C1108 | 2261 04331 | C1109 | 2262 04332 |
| 71108 | 2267 04333 | C1160 | 2268 04334 | C11G1 | 2269 04335 | C11C2 | 2270 04336 |
| 7101 | 2271 04337 | C1202 | 2272 04340 | C1203 | 2273 04341 | C1204 | 2274 04342 |
| C1205 | 2275 04343 | C1206 | 2276 04344 | C1207 | 2277 04345 | C1208 | 2278 04346 |

Figure 50. Subroutine SILEFAC Core Storage Map (continued)

| | | | | | | | |
|-------|------------|-------|------------|-------|------------|-------|------------|
| D11C3 | 303 00457 | D1114 | 351 00537 | D113E | 712 01310 | D1121 | 738 01342 |
| D112K | 768 01400 | D1129 | -01 01441 | D11AK | 1208 02270 | D1158 | 1441 02641 |
| D1129 | 1453 04053 | D113M | 1203 03021 | D113C | 1383 03057 | D1166 | 1751 03127 |
| D1130 | 1453 04053 | D113N | 1203 03021 | D113D | 1383 03057 | D1167 | 1751 03127 |
| D12CL | 249 00441 | D121C | 462 00716 | D1111 | 505 00771 | D111M | 533 01025 |
| D121P | 543 01037 | D1223 | 661 01131 | D1214 | 609 01141 | D1-25 | 618 01132 |
| D121Q | 543 01037 | D1224 | 661 01131 | D1215 | 609 01141 | D121R | 1078 01096 |
| D123V | 107 01111 | D1245 | 1116 01134 | D124K | 1210 02071 | D124M | 1782 03366 |
| D1262 | 1691 01233 | D1266 | 1761 03341 | D1269 | 1746 03346 | D-280 | 1782 03366 |
| D131M | 1818 01705 | D125V | 1807 03350 | D1274 | 1921 01613 | D1-05 | 302 00456 |
| D1368 | 1768 01340 | D1369 | 1765 03345 | D136H | 1837 03455 | D1-0U | 1889 03541 |
| D1375 | 1945 03031 | D1376 | 1949 03035 | D140E | 130 02022 | D140C | 172 00234 |
| D142J | 747 01353 | D142T | 644 01314 | D1431 | 907 01015 | D-433 | 915 71145 |
| D144K | 1332 02467 | D145F | 1485 02715 | D1451 | 1560 03030 | D1-3P | 1616 01120 |
| D145L | 1556 02572 | D145K | 1630 01136 | D146J | 1815 03427 | D1310 | 324 00504 |
| D164P | 286 00414 | D162A | 668 01140 | D162J | 746 01352 | D162T | 843 01513 |
| D1633 | 732 01844 | D165P | 1615 01117 | D166V | 1695 01547 | D1705 | 301 00455 |
| D1772 | 1444 03630 | D1776 | 1948 01634 | D177C | 118 00360 | D178M | 422 00343 |
| E1M | 467 00413 | E1R | 294 00446 | E115 | 356 00344 | E1K | 478 00746 |
| E1S | 926 01077 | E1S1 | 92 01202 | E116 | 645 01205 | E1L | 772 01694 |
| E135 | 926 01077 | E13A | 92 01202 | E116 | 645 01205 | E1L | 772 01694 |
| E15P | 607 03107 | E16A | 1769 03351 | E1100 | 124 00174 | E14L | 121- 02216 |

LOCATIONS OF NAMES IN TRANSFER VECTOR

| A TAN | CNT | DEC | DEC | DEC | DEC | DEC | DEC |
|-------|---|---------|---------|---------|---------|---------|---------|
| TIMEY | 6 00002 | 6 00004 | 6 00004 | 6 00004 | 5 00003 | 5 00003 | 1 00001 |
| A TAN | COUNTY | DUMP | DUMP | DUMP | DUMP | DUMP | CAPT |
| | (FILL) | (FILL) | (FILL) | (FILL) | (FILL) | (FILL) | |
| | ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY | | | | | | |
| A TAN | COUNTY | DUMP | 3LCT | TIMEY | (FILL) | (FILL) | (SPN) |

Figure 50. Subroutine SIFAC Core Storage Map (continued)

11/09/83 11/09/83

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| | | | | | | | |
|------|-----------|------|-----------|------|-----------|------|-----------|
| 456 | 318 02614 | 4506 | 321 02637 | 835 | 321 02642 | 860 | 324 02645 |
| 496 | 319 02710 | 800 | 329 02702 | 870 | 331 02705 | 880 | 332 02707 |
| 896 | 333 02710 | 905 | 334 02716 | 910 | 334 03016 | 920 | 340 03022 |
| 940 | 341 03021 | 945 | 342 03016 | 4506 | 344 03121 | 657 | 349 03124 |
| 985 | 349 03127 | 996 | 355 03144 | 1660 | 356 03150 | 677 | 358 03167 |
| 198 | 359 03174 | 950 | 366 03234 | 960 | 370 03300 | 965 | 376 03307 |
| 976 | 374 03310 | 980 | 360 03350 | 540 | 381 03382 | 961 | 382 03367 |
| 974 | 369 03405 | 987 | 385 03413 | 987 | 385 03413 | 985 | 389 03420 |
| 996 | 387 03423 | 1015 | 400 03437 | 1017 | 402 03463 | 1000 | 403 03551 |
| 1200 | 405 03561 | 1060 | 408 03465 | 1560 | 409 03614 | 2000 | 414 03643 |
| 2300 | 415 03637 | | | | | | |

Figure 50. Subroutine SILFAC Core Storage Map
(continued)

POST PROCESSOR ASSEMBLY DATA
13 IS THE FIRST LOCATION NOT USED BY THIS PROGRAM

REFERENCES TO DEFINED SYMBOLS

| | | |
|-----|------|----|
| 10 | M1 | 2 |
| 11 | M2 | 4 |
| 12 | M3 | 6 |
| 13 | MIN | 10 |
| 14 | MOUT | 11 |
| 15 | M11 | 13 |
| 16 | MOUT | 11 |
| 17 | M11 | 13 |
| 18 | ISCH | 2 |
| 19 | ISCH | 2 |
| 20 | ISPM | 4 |
| 21 | ISPM | 4 |
| 22 | ISPM | 4 |
| 23 | ISPM | 4 |
| 24 | ISPM | 4 |
| 25 | ISPM | 4 |
| 26 | ISPM | 4 |
| 27 | ISPM | 4 |
| 28 | ISPM | 4 |
| 29 | ISPM | 4 |
| 30 | ISPM | 4 |
| 31 | ISPM | 4 |
| 32 | ISPM | 4 |
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| 36 | ISPM | 4 |
| 37 | ISPM | 4 |
| 38 | ISPM | 4 |
| 39 | ISPM | 4 |
| 40 | ISPM | 4 |
| 41 | ISPM | 4 |
| 42 | ISPM | 4 |
| 43 | ISPM | 4 |
| 44 | ISPM | 4 |
| 45 | ISPM | 4 |
| 46 | ISPM | 4 |
| 47 | ISPM | 4 |
| 48 | ISPM | 4 |
| 49 | ISPM | 4 |
| 50 | ISPM | 4 |
| 51 | ISPM | 4 |
| 52 | ISPM | 4 |
| 53 | ISPM | 4 |
| 54 | ISPM | 4 |
| 55 | ISPM | 4 |
| 56 | ISPM | 4 |
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| 58 | ISPM | 4 |
| 59 | ISPM | 4 |
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| 175 | ISPM | 4 |
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| 190 | ISPM | 4 |
| 191 | ISPM | 4 |
| 192 | ISPM | 4 |
| 193 | ISPM | 4 |
| 194 | ISPM | 4 |
| 195 | ISPM | 4 |
| 196 | ISPM | 4 |
| 197 | ISPM | 4 |
| 198 | ISPM | 4 |
| 199 | ISPM | 4 |
| 200 | ISPM | 4 |

NO ERROR IN ABOVE ASSEMBLY.

Figure 51. FAP Input-Output Compatibility Subroutine Listing (Continued)

APPENDIX C
COORDINATE TRANSFORMATION

PRIMARY TRANSFORMATION

As indicated in Section II, the surface coordinate transformation technique employed by the program does not require transformation parameters such as direction cosines, Euler angles and translation terms to be entered as input data to the program for transformation purposes. Instead, the x, y and z coordinates of three points, not in a line, are given from the new origin, or to the new position of the surface. These data are then used to derive the rotational and translation terms required to transform the remaining surface data to the new origin or surface position.

The classical equations for transformation of rectangular coordinates in space are employed for both primary and auxiliary transformation. The new x, y and z coordinates in terms of the old coordinates are:

$$x = x' \cos \alpha_1 + y' \cos \alpha_2 + z' \cos \alpha_3 + H \quad (1)$$

$$y = x' \cos \beta_1 + y' \cos \beta_2 + z' \cos \beta_3 + L \quad (2)$$

$$z = x' \cos \gamma_1 + y' \cos \gamma_2 + z' \cos \gamma_3 + K \quad (3)$$

Note that there are 9 unknown direction cosines and 3 translation terms, or a total of 12 unknowns. It is clear that the coordinates of four points from the new origin are required if these equations are to be used directly to determine the unknown parameters.

It can be shown, however, that the coordinates of three points (not in a line) are sufficient and necessary to fix the position of a surface in any rectangular coordinate system. It appears, therefore, that another point must be made available for solution of the above equations, or another technique developed which directly requires only three points. Investigation of the latter yielded a complex, difficult to program, solution. On the other hand, solution of the classical equations is straightforward, but requires the extra point (not in the plane of the other three). Rather than require the user to supply the extra point in data, it was decided to generate the point as a unit normal vector above the second point given in transformation data. This extra point must, of course, be generated in both old and new coordinate systems.

Figure 53 depicts a primary transformation of Surface A from the old (primed) to the new (unprimed) coordinate system. Note that the primary transformation shown affects only one surface, whereas both surfaces are involved in the auxiliary transformation, which will be discussed in more

Fig. 53. Coordinate Transformation

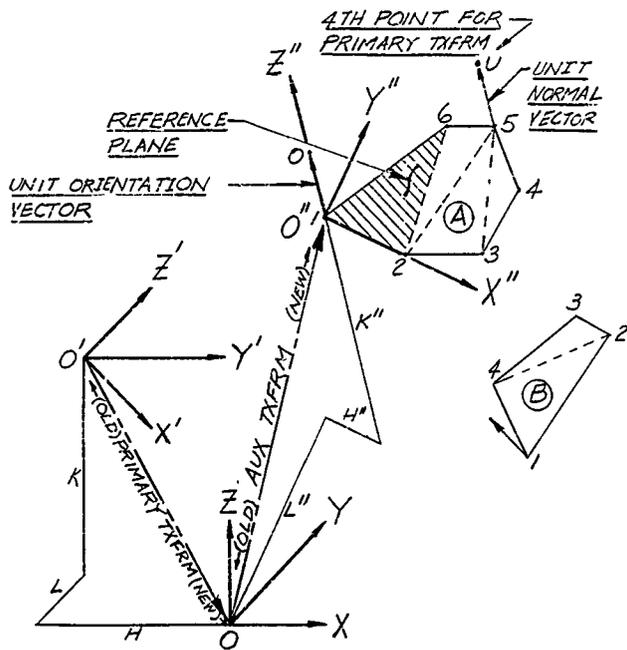


Figure 53. Coordinate Transformation

detail later in this Appendix. The angles (α , β and γ) shown in Equations 1, 2 and 3 are related in the following manner with the primed and unprimed coordinate axes shown in Figure 53:

$$\alpha_1 = \angle O'X'OX, \alpha_2 = \angle O'Y'OX, \alpha_3 = \angle O'Z'OX$$

$$\beta_1 = \angle O'X'OY, \beta_2 = \angle O'Y'OY, \beta_3 = \angle O'Z'OY$$

$$\gamma_1 = \angle O'X'OZ, \gamma_2 = \angle O'Y'OZ, \gamma_3 = \angle O'Z'OZ$$

Given the coordinates of points 2, 5 and 6 in Surface A, and the generated point U, from both the old and new coordinate systems, we may write four independent equations similar to Equation 1. Using Equation 2, the resulting set of equations in x is:

$$x_2 = x_2' \cos \alpha_1 + y_2' \cos \alpha_2 + z_2' \cos \alpha_3 + H \quad (4)$$

$$x_5 = x_5' \cos \alpha_1 + y_5' \cos \alpha_2 + z_5' \cos \alpha_3 + H \quad (5)$$

$$x_6 = x_6' \cos \alpha_1 + y_6' \cos \alpha_2 + z_6' \cos \alpha_3 + H \quad (6)$$

$$x_U = x_U' \cos \alpha_1 + y_U' \cos \alpha_2 + z_U' \cos \alpha_3 + H \quad (7)$$

We may similarly write two more sets of equations in y and z similar to Equations 2 and 3, for a total of twelve independent equations. Each set of four simultaneous equations is solved by Cramer's Rule (Reference 2) for the unknown direction cosines relating the old y' and z' axes to the new x, y and z axes.

For example, using the set developed above for Equation 1 (Equations 4, 5, 6 and 7), the coefficient determinant D is

$$D = \begin{vmatrix} x_2' & y_2' & z_2' & 1 \\ x_5' & y_5' & z_5' & 1 \\ x_6' & y_6' & z_6' & 1 \\ x_U' & y_U' & z_U' & 1 \end{vmatrix} \quad (8)$$

By Cramer's Rule, we successively replace the elements in each column of the set with the respective element on the left of each equation in the set. For example, the solution for $\cos \alpha_2$ is:

$$\cos \alpha_2 = \frac{\begin{vmatrix} x_2' & x_2 & z_2' & 1 \\ x_5' & x_5 & z_5' & 1 \\ x_6' & x_6 & z_6' & 1 \\ x_U' & x_U & z_U' & 1 \end{vmatrix}}{D} \quad (9)$$

and similarly,

$$\cos \alpha_3 = \frac{\begin{vmatrix} x_2' & y_2' & x_2 & 1 \\ x_5' & y_5' & x_5 & 1 \\ x_6' & y_6' & x_6 & 1 \\ x_U' & y_U' & x_U & 1 \end{vmatrix}}{D} \quad (10)$$

The above process is repeated for the solution of $\cos \beta_2$, $\cos \beta_3$, $\cos \gamma_2$, and $\cos \gamma_3$, using the sets developed for y and z . The coefficient determinant is the same for all sets, because the coefficients of the unknowns in all sets are identical.

To increase computational efficiency, repeated factors in the expanded determinants are computed only once for each set. Also, considerable economy results in computing the unknown direction cosines $\cos \alpha_1$, $\cos \beta_1$, $\cos \gamma_1$, as the cross product of the corresponding direction cosines of the other (y and z) axes:

$$\cos \alpha_1 = \cos \beta_2 \cos \gamma_3 - \cos \gamma_2 \cos \beta_3 \quad (11)$$

$$\cos \beta_1 = \cos \gamma_2 \cos \alpha_3 - \cos \alpha_2 \cos \gamma_3 \quad (12)$$

$$\cos \gamma_1 = \cos \alpha_2 \cos \beta_3 - \cos \beta_2 \cos \alpha_3 \quad (13)$$

The translation components H , L and K are computed by substituting the coordinates of the point below point U in the surface to be transformed into Equations 1, 2 and 3, along with the known values of direction cosines. For the Surface A shown in Figure 53, using point 5,

$$H = x_5 - x_5' \cos \alpha_1 - y_5' \cos \alpha_2 - z_5' \cos \alpha_3 \quad (14)$$

$$L = y_5 - x_5' \cos \beta_1 - y_5' \cos \beta_2 - z_5' \cos \beta_3 \quad (15)$$

$$K = z_5 - x_5' \cos \gamma_1 - y_5' \cos \gamma_2 - z_5' \cos \gamma_3 \quad (16)$$

The program now transforms all point coordinates in Surface A from the old to the new system by direct substitution in Equations 1, 2 and 3.

The method outlined above will always perform the transformation desired, providing the three points selected are (1) sufficiently separated in space, (2) accurately computed, and (3) do not form a straight line in space. Because the fourth point U is always computed outside the plane of the other three, the coefficient determinant D can never be 0. Hence, by Cramer's Rule, a unique solution must always exist.

AUXILIARY TRANSFORMATION

An auxiliary transformation transforms the coordinates of both surfaces into the reference plane of a specified surface--the "Control" surface. In Figure 53, Surface A is the control surface; the auxiliary transformation depicted transforms both Surface A and B from the unprimed (old) system to the double-primed (new) system. In general, the origin O'' in the control surface is always point 1 in the control surface coordinate array. It may not always be the first point entered in input surface data; if a bisection of the surface occurs, and the original point 1 is not seen by the other surface (assumed planar), then a new point 1 will be computed. The new point will be used as the origin O'' . The same processing occurs for internally generated surfaces. Only surfaces classed as plane surfaces may be control surfaces, i.e., Classes 1, 3, 4 and planar 6. For example, if both Surface A and B in Figure 53 are plane and bisect each other, two auxiliary transformations would occur to facilitate surface reconstruction. Actually, if Surface A were entered as Surface 1, the first auxiliary transformation to occur would be to point 1 in Surface B, rather than Surface A. This would not occur, however, if Surface A were not bisected by Surface B. In any case, the last transformation always is to point 1 in Surface 1, so that mapping and factor computation may proceed forthwith.

The processing of an auxiliary transformation differs from the primary transformation because unknowns may be more readily computed from available data. Equations 1, 2 and 3 are rewritten for the auxiliary old and new coordinate systems,

$$x'' = x \cos \alpha_1 + y \cos \alpha_2 + z \cos \alpha_3 + H'' \quad (17)$$

$$y'' = x \cos \beta_1 + y \cos \beta_2 + z \cos \beta_3 + L'' \quad (18)$$

$$z'' = x \cos \gamma_1 + y \cos \gamma_2 + z \cos \gamma_3 + K'' \quad (19)$$

The angles are defined as follows, referring to Figure 53:

$$\alpha_1 = \angle OXO''X'', \alpha_2 = \angle OYO''X'', \alpha_3 = \angle ZOZO''X''$$

$$\beta_1 = \angle OXO''Y'', \beta_2 = \angle OYO''Y'', \beta_3 = \angle ZOZO''Y''$$

$$\gamma_1 = \angle OXO''Z'', \gamma_2 = \angle OYO''Z'', \gamma_3 = \angle ZOZO''Z''$$

Because the O^*X^* axis in the new system is directed along the line segment formed by the first and second point in the control surface, the direction cosines related to that axis are readily computed.

The length of line $\overline{12}$ in Surface A is

$$LS_{12} = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2},$$

and the direction cosines relating the new O^*X^* axis to the old OX , OY and OZ axes are:

$$\cos \alpha_1 = (x_2 - x_1)/LS_{12} \quad (20)$$

$$\cos \alpha_2 = (y_2 - y_1)/LS_{12} \quad (21)$$

$$\cos \alpha_3 = (z_2 - z_1)/LS_{12} \quad (22)$$

Because the new O^*Z^* axis is directed along the surface unit orientation vector (point O above Surface A) the cosines relating that axis to the old OX , OY and OZ axes are

$$\cos \gamma_1 = x_0 - x_1 \quad (23)$$

$$\cos \gamma_2 = y_0 - y_1 \quad (24)$$

$$\cos \gamma_3 = z_0 - z_1 \quad (25)$$

The remaining direction cosines are computed by cross products of the X^* and Z^* axis unit base vectors (direction cosines).

$$\cos \beta_1 = \cos \gamma_2 \cos \alpha_3 - \cos \alpha_2 \cos \gamma_3 \quad (26)$$

$$\cos \beta_2 = \cos \alpha_1 \cos \gamma_3 - \cos \gamma_1 \cos \alpha_3 \quad (27)$$

$$\cos \beta_3 = \cos \gamma_1 \cos \alpha_2 - \cos \alpha_1 \cos \gamma_2 \quad (28)$$

The unknown translation terms are determined from Equations 17, 18 and 19 for point 1 in Surface A ($x_1^i = 0$, $y_1^i = 0$, $z_1^i = 0$).

$$H^i = -x_1 \cos \alpha_1 - y_1 \cos \alpha_2 - z_1 \cos \alpha_3 \quad (29)$$

$$L^i = -x_1 \cos \beta_1 - y_1 \cos \beta_2 - z_1 \cos \beta_3 \quad (30)$$

$$K^i = -x_1 \cos \gamma_1 - y_1 \cos \gamma_2 - z_1 \cos \gamma_3 \quad (31)$$

The program now transforms all coordinates in Surface A and Surface B to the new system by using Equations 17, 18 and 19.

APPENDIX D

COMPUTATION OF SURFACE AREA OF INTERNALLY GENERATED SURFACES

In Figure 54, View J-J shows a view of the surface of a right elliptical cone between the two arbitrary cross-sections indicated in the isometric sketch of the cone. Because the program internal surface generator uses the elliptical cross-section as the basic generating element, elemental surface areas such as $ABCD$ in Figure 54 are trapezoids having, in general, unequal nonparallel sides. Also, because each elemental surface is developed by equal elliptical ~~parametric~~ angles, one need compute the area of only one elemental surface for each pair of cross-sections (providing, of course, the cross-sections are similar).

The plane area of trapezoid $ABCD$ is

$$A_T = \frac{1}{2} h (L_1 + L_2). \quad (1)$$

L_1 and L_2 are readily computed from the X , Y coordinates of points A , B , C and D :

$$L_1 = \sqrt{(X_C - X_A)^2 + (Y_C - Y_A)^2} \quad (2)$$

$$L_2 = \sqrt{(X_D - X_B)^2 + (Y_D - Y_B)^2} \quad (3)$$

The trapezoid height h is computed indirectly from the projected area A_p of the trapezoid on the XY plane in the following manner:

$$h = \sqrt{h_p^2 + Z^2} \quad (4)$$

where h_p is the projected length of trapezoid height h , and Z is the distance between cross-sections.

The projected area of $ABCD$ is:

$$A_p = \frac{1}{2} h_p (L_1 + L_2). \quad (5)$$

Solving for h_p in Equation 5:

$$h_p = \frac{2 A_p}{(L_1 + L_2)} \quad (6)$$

The area A_p is computed from the trapezoid (X, Y) coordinates in the following manner:

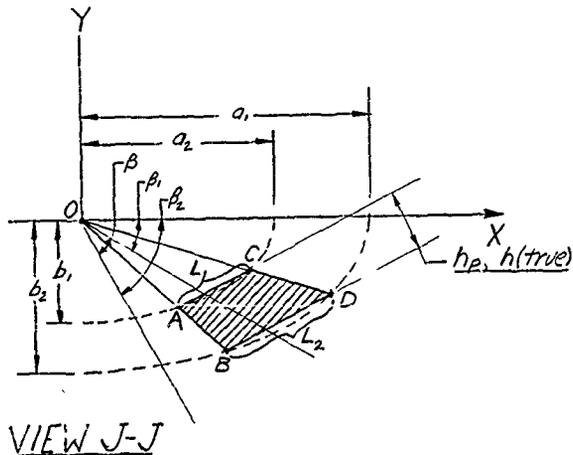
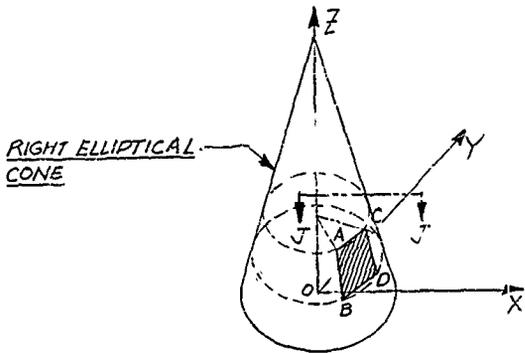


Figure 54. Surface Area Geometry of Internally Generated Polyhedra

Noting triangles BOD and AOC

$$A_p = \text{Area } \triangle BOD - \text{Area } \triangle AOC \quad (7)$$

It is desirable for computational efficiency to compute A_p using known parameters. In this case, $\sin \beta$ is known and is used. The parametric equations of the ellipse are:

$$x = a \cos \theta \quad (8)$$

$$y = b \sin \theta \quad (9)$$

where a is the semi-major axis, b is the semi-minor axis and θ is the parametric angle. In Figure 54, angle β_1 defines points A and B and angle β_2 defines points C and D. Angle $\beta = \beta_2 - \beta_1$.

The area of triangle AOC can be computed by vector cross products,

$$A_{AOC} = \frac{1}{2} (X_A Y_C - X_C Y_A) \quad (10)$$

From Equations 8 and 9 for the parametric angles β_1 and β_2 defining points A and C,

$$X_A = a_1 \cos \beta_1, Y_A = b_1 \sin \beta_1 \quad (11)$$

$$X_C = a_1 \cos \beta_2, Y_C = b_1 \sin \beta_2 \quad (12)$$

Substituting Equations 11 and 12 in Equation 10,

$$A_{AOC} = \frac{1}{2} a_1 b_1 (\cos \beta_1 \sin \beta_2 - \cos \beta_2 \sin \beta_1)$$

$$A_{AOC} = \frac{1}{2} a_1 b_1 \sin (\beta_2 - \beta_1)$$

$$A_{AOC} = \frac{1}{2} a_1 b_1 \sin \beta \quad (13)$$

A similar derivation is developed to obtain the area of triangle BOD.

$$A_{BOD} = \frac{1}{2} a_2 b_2 \sin \beta \quad (14)$$

Substituting Equations 13 and 14 in Equation 7,

$$A_p = \frac{1}{2} \sin \beta (a_2 b_2 - a_1 b_1) \quad (15)$$

Substituting Equation 15 into Equation 6,

$$h_p = \frac{2 \left[\frac{1}{2} \sin \beta (a_2 b_2 - a_1 b_1) \right]}{I_1 + I_2} \quad (16)$$

Substituting Equation 16 into Equation 4,

$$h = \sqrt{\left[\frac{\sin \beta (a_2 b_2 - a_1 b_1)}{l_1 + l_2} \right]^2 + z^2} \quad (17)$$

Finally, substituting Equation 17 into Equation 1,

$$A_T = \frac{l_1 + l_2}{2} \sqrt{\left[\frac{\sin \beta (a_2 b_2 - a_1 b_1)}{l_1 + l_2} \right]^2 + z^2}$$

Rearranging terms,

$$A_T = \frac{1}{2} \sqrt{[\sin \beta (a_2 b_2 - a_1 b_1)]^2 + [z (l_1 + l_2)]^2} \quad (18)$$

The total surface area is computed by repeated evaluation of Equation 18 for the particular surface generated.

APPENDIX E

DERIVATION OF CONFIGURATION FACTOR TO A SPHERE

The analytic solution of the configuration factor to a sphere depends upon the position of the sphere relative to the plane of Surface 1. This is clearly demonstrated geometrically by using the Nusselt unit sphere projection as shown in Figure 55. Three unique solutions are apparent from the five different sphere positions; Ia and IIIa represent "Limit" values in each case. The unit sphere projections (crosshatched areas) shown in the lower part of Figure 55 correspond respectively to sphere positions (not to scale) depicted in the upper half. Case I results when the sphere is above (Ia) and/or touching (Ib) the plane of Surface 1. The locus on the Nusselt hemisphere base is an ellipse, and varies from a circle (when the sphere is vertically over the point O) to the single tangency position shown in Ib. When the sphere goes below the plane of Surface 1, the Case II locus appears, and is formed by the ellipse boundary on the left and the unit circle boundary on the right.

The locus projected on the unit sphere surface is a circle, in every case. The radius, b, of the circle becomes the semi-major axis of the projected ellipse. By similar triangles,

$$\frac{b}{1} = \frac{R}{D}$$

$$b = \frac{R}{D} \quad (1)$$

where D = distance from center of sphere to origin of unit sphere and R is the sphere radius. The semi-minor axis, a, of the ellipse is the projection on the unit circle of b; again by similar triangles,

$$\frac{z}{D} = \frac{a}{b}$$

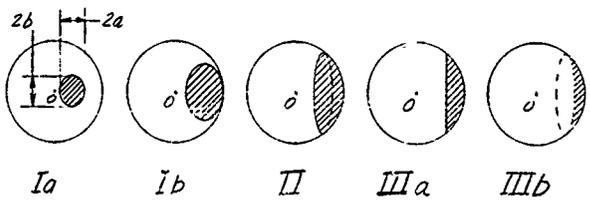
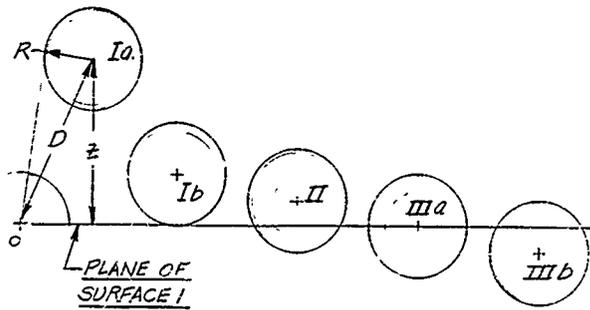
or

$$a = b \frac{z}{D} = \frac{Rz}{D^2} \quad (2)$$

The area of the ellipse is

$$A = \pi ab = \pi \frac{R^2 z}{D^3} \quad (3)$$

The configuration factor for Case I is the area of the ellipse divided by the area of the unit radius circle,



NUSSELT UNIT SPHERE PROJECTIONS
(NOT TO ANY SCALE)

Figure 55. Areas Involved in Configuration Factor to Spheres

$$e_I = \frac{\pi R^2 Z}{\pi D^3}$$

$$e_I = \frac{R^2 Z}{D^3}, \quad Z > R \quad (L)$$

The computation of Case III proceeds as follows. Referring to Figure 56, a detailed drawing of the upper half of the Case III locus, the area to be determined is Area ACB.

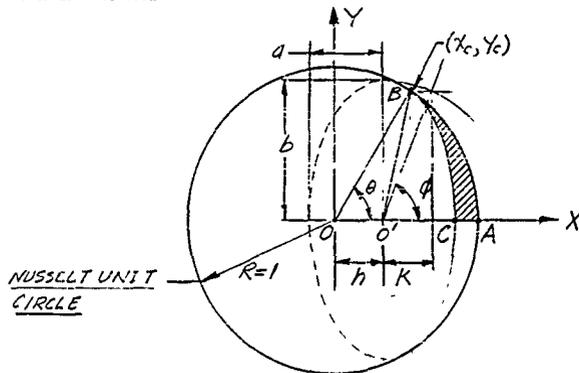


Figure 56. Case IIIb Detail Geometry

By inspection,

$$A_{ACB} = A_{AOB} - A_{O'OB} - A_{CO'B} \quad (5)$$

Area AOB is a sector of the unit circle, $R = 1$,

$$A_{AOB} = \frac{1}{2} R^2 \theta = \frac{1}{2} \theta \quad (6)$$

Given h , the distance between centers O and O' , and Y_C , the value of y at the tangency point between the ellipse and the circle. The area of the triangle $O'O'B$ is

$$A_{O'OB} = \frac{1}{2} h Y_C \quad (7)$$

The area CO'B is an elliptical sector defined by the parametric angle ϕ at (x_c, y_c) the point of tangency,

$$A_{CO'B} = \frac{ab}{2} \phi \quad (8)$$

Inserting Equations 6, 7 and 8 into Equation 5,

$$A_{ACB} = \frac{1}{2} (\theta - by_c - ab\phi) \quad (9)$$

The unknowns b , h , y_c and ϕ must be evaluated in terms of \bar{N} , Z and D . The tangency point x_c, y_c is determined as follows. The equation of the ellipse when translated a distance h in the x direction from the origin O is

$$\frac{(x-h)^2}{a^2} + \frac{y^2}{b^2} = 1 \quad (10)$$

The equation of the unit circle is

$$x^2 + y^2 = 1 \quad (11)$$

At the intersection point the slopes are equal. Taking the first derivative of Equation 10,

$$\frac{2}{a^2} (x-h) dx + \frac{2y}{b^2} dy = 0$$

Rearranging,

$$\frac{dy}{dx} = \frac{b^2}{2y} \left[\frac{2}{a^2} (h-x) \right] - \frac{b^2}{a^2} \frac{(h-x)}{y} \quad (12)$$

The slope at any point x, y on the circle is:

$$\frac{dy}{dx} = -\frac{x}{y} \quad (13)$$

Equating Equations 12 and 13,

$$\frac{b^2}{a^2} \frac{(h-x)}{y} = -\frac{x}{y}$$

Solving for h , at $x = x_c$ and $y = y_c$,

$$h = x_c \frac{(y_c^2 - a^2)}{b^2} \quad (14)$$

Substituting Equation 14 into Equation 10,

$$\left[\frac{x_c - x_c \frac{(b^2 - a^2)}{b^2}}{a^2} \right]^2 + \frac{y_c^2}{b^2} = 1$$

Reducing and rearranging terms, and solving simultaneously with Equation 11:

$$\left(\frac{a}{b}\right)^2 x_c^2 + y_c^2 = b^2 \quad (15)$$

$$x_c^2 + y_c^2 = 1$$

Subtracting Equation 11 from Equation 15,

$$x_c^2 \left[\left(\frac{a}{b}\right)^2 - 1 \right] = b^2 - 1$$

Solving for x_c ,

$$x_c^2 = \frac{b^2 - 1}{\left(\frac{a}{b}\right)^2 - 1} \quad (16)$$

$$x_c = b \sqrt{\frac{1 - b^2}{b^2 - a^2}} \quad (17)$$

Solving for y_c in Equation 11,

$$y_c = \sqrt{1 - x_c^2} \quad (18)$$

Substituting Equation 1 and 2 into Equation 17,

$$x_c = \sqrt{\frac{R^2 - D^2}{Z^2 - D^2}} \quad (19)$$

Substituting Equation 1, 2 and 16 into Equation 18,

$$y_c = \sqrt{\frac{Z^2 - R^2}{Z^2 - D^2}} \quad (20)$$

The angle ϕ may be defined as

$$\phi = \tan^{-1} \frac{y_c}{x_c} = \tan^{-1} \frac{y_c}{\sqrt{b^2 - y_c^2}} \quad (21)$$

Substituting Equation 1 and 20 into Equation 21,

$$\phi = \tan^{-1} \left[\frac{D}{|Z|} \cdot \sqrt{\frac{Z^2 - R^2}{R^2 - D^2}} \right] \quad (22)$$

The angle θ may be defined as

$$\theta = \tan^{-1} \frac{y_c}{r_c} \quad (23)$$

Substituting Equations 19 and 20 into Equation 23,

$$\theta = \tan^{-1} \sqrt{\frac{Z^2 - R^2}{R^2 - D^2}} \quad (24)$$

Substituting Equations 1, 2 and 19 into Equation 14,

$$h = \frac{D^2 - Z^2}{D^2} \sqrt{\frac{R^2 - D^2}{Z^2 - D^2}} \quad (25)$$

The parameter hy_c in Equation 9 is evaluated by multiplying Equations 20 and 25,

$$\begin{aligned} hy_c &= \left[\frac{D^2 - Z^2}{D^2} \sqrt{\frac{R^2 - D^2}{Z^2 - D^2}} \right] \frac{Z^2 - R^2}{Z^2 - D^2} \\ hy_c &= \frac{\sqrt{D^2 - R^2} \cdot \sqrt{R^2 - Z^2}}{D^2} \\ hy_c &= \left(\frac{D^2 - R^2}{D^2} \right) \sqrt{\frac{R^2 - Z^2}{D^2 - R^2}} \quad (26) \end{aligned}$$

Let $\alpha = D^2 - R^2$ (27)

and $\beta = \sqrt{\frac{R^2 - Z^2}{\alpha}}$ (28)

Substituting Equations 27 and 28 into Equations 22, 24 and 26, respectively,

$$\phi = \tan^{-1} \left[\frac{D}{2R} \beta \right] \quad (29)$$

$$\theta = \tan^{-1} \beta \quad (30)$$

and $hy_c = \frac{\alpha \beta}{D^2}$ (31)

Finally, substitute Equations 29, 30 and 31 into 9; the actual area projected on the hemisphere base is twice Area ACB and is divided by the base area to yield the configuration factor.

$$c_{III} = \frac{1}{\pi} \left[(\tan^{-1} \beta) - \frac{R^2 Z}{D^3} \left(\tan^{-1} \frac{\beta D}{|Z|} \right) \right] \quad (2)$$

where

$$\alpha = D^2 - R^2$$

$$\beta = \sqrt{\frac{R^2 - Z^2}{\alpha}}, \quad Z \leq 0 \text{ and } Z^2 \leq R^2$$

By inspection of Figure 55, the projected area for Case II is the sum of the ellipse evaluated by the Case I formula and the crescent shaped area determined by the Case III formula,

$$c_{II} = c_I + c_{III}, \quad 0 < Z < R \quad (3)$$

In summary, referring to Figure 55,

$$c_I = \frac{R^2 Z}{D^3}, \quad Z \geq R$$

$$c_{III} = \frac{1}{\pi} \left[(\tan^{-1} \beta) - \frac{R^2 Z}{D^3} \left(\tan^{-1} \frac{\beta D}{|Z|} \right) - \frac{\beta}{Z} \right]$$

where

$$\alpha = D^2 - R^2, \quad \beta = \sqrt{\frac{R^2 - Z^2}{\alpha}},$$

$$Z \leq 0, \quad Z^2 \leq R^2$$

$$c_{II} = c_I + c_{III}, \quad 0 < Z < R$$